

# DRAINAGE ANALYSIS

FOR  
Definitive Subdivision  
Donovan Estates

LOCATED IN  
FRANKLIN, MASSACHUSETTS

PREPARED FOR  
Donovan Family Realty Trust  
47 Partridge Street  
Franklin, MA 02038

PREPARED BY  
UNITED CONSULTANTS, INC.  
850 FRANKLIN STREET, SUITE 11D  
WRENTHAM, MA. 02093

DATE: September 3, 2025  
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*Carlos A. Quintal*  
2/17/26

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## APPENDIX A

## I. DESCRIPTION

This report is offered in support of the stormwater management system designed for the “Definitive Subdivision – Donovan Estates” in Franklin, Massachusetts. The site currently consists of three lots with a total area of approximately 12 acres. One existing house is located on the site with out buildings and a pool. There are existing houses and vacant land abutting the site. The site has a wetland system which includes bordering vegetated wetlands, a river and a flood plain.

The project included the construction of a roadway with a water main underground utilities and a stormwater system.

The primary goals of the stormwater system are to collect and treat the stormwater runoff generated from the proposed roadway, driveways, and houses. The stormwater will be directed to an infiltration pond.

Infiltration Pond 1 is open infiltration area located on Lot P.

Both the pre-development and post-development conditions flowing to the bordering vegetated wetlands are summarized in Appendix B.

## II. Purpose

The purpose of this report is to examine the hydrological and hydraulic aspects of the proposed “Definitive Subdivision – Donovan Estates”. This report was developed for review by the Town of Franklin Planning Board and Conservation Commission to obtain the necessary permits to allow the project to proceed.

This report considers the overall hydrological impact of proposed additional development upon the local watersheds with specific emphasis directed toward the adjacent and immediate downstream areas. The hydrology and criteria are consistent with the Town of Franklin Planning Board, Franklin Conservation Commission and Mass DEP Storm Water Management Policies.

## III. Pre-Development Conditions

The site currently consists of three lots with a total area of approximately 12 acres. One existing house is located on the site with out buildings and a pool. There are existing houses and vacant land abutting the site. The site has a wetland system which includes bordering vegetated wetlands, a river and a flood plain. The project included the construction of a roadway with a water main underground utilities and a stormwater system.

The upland soils for the site were taken from the soil survey of Norfolk and Suffolk counties. The soils are mapped as -Charlton Hollis Rock-Outcrop Complex (HSG-C) and Woodbridge Fine Sandy Loam (HSG-B) Note: Refer to the subdivision plan for the location and soil types. Soil testing was conducted on the site to determine soil types and permeability rates. See the soil logs and permeability test results located in Appendix F. Permeability test was completed on site and the results can be found in Appendix F.

Utilizing a Hydrocad computer model the pre-development and post development conditions were calculated. This included an analysis of the watershed utilizing a Hydrologic soil group B or C. A comparison of the pre-development vs. post development rate and volume of runoff can be found in Appendix B.

#### IV. Post Development Conditions

The project included the construction of a roadway with a water main underground utilities and a stormwater system.

The roadway stormwater runoff will be captured in deep sump hooded catch basin and then directed to a sediment forebay and then to an open infiltration pond. The proposed infiltration system will promote groundwater re-charge as required by the Town of Franklin Stormwater Regulations. Municipal utility connections are also proposed for the project. The proposal is to service the houses with town water and sewer. The project includes the construction of a proposed roadway.

TSS removal will be accomplished by a treatment train with deep sump hooded catch basin, sediment forebay and an infiltration pond. Additionally, the entrance portion of the roadway will have a sediment forebay and two water quality swales. Utilizing the same computer model as the existing conditions we have modeled the changes in surfaces and ground cover and have calculated the post development conditions.

All calculations for the above have been included in this report. Pre-development calculations are in Appendix C. Post-development calculations are located in Appendix D.

#### V. Conclusion

Stormwater from the proposed roadway will be captured by the catch basins type water quality units and a sediment forebay for TSS removal which will then be directed to the underground infiltration pond. Additionally, the entrance portion of the roadway will have a sediment forebay and two water quality swales.

The comparison in Appendix B summarizes the rate and volumes of runoff at the bordering vegetated wetland boundary in both the pre-development and post-development conditions.

#### VI. Stormwater Management Standards

Refer to Checklist for Stormwater Report in Appendix H

#### **Town of Franklin Stormwater Management Bylaw – Chapter 153 – Bylaw Amendment 21-867**

Impervious Coverage Entire Site site =

1" x 61,111 sq. ft. impervious = 5,093 cubic feet (Required)

Storage in Pond 1 below the outlet invert (171.0) = 14,338 cubic feet (Provided) See Stage-Area-Storage for Pond 1 this Appendix.

#### **LID Measures**

- Existing Vegetation Removal within the buffer zone has been reduced to the extent practicable and mitigation plantings have been proposed.

#### **Standard 1: No New Untreated Discharges**

No new untreated discharges are proposed.

A stormwater system has been provided or is proposed which will provide the required TSS removal which includes the installation of deep sump hooded catch basins, sediment forebay and an infiltration basin as well as a sediment forebay and water quality swales.

**Standard 2: Peak Rate Attenuation**

The drainage system has been designed to match or reduce the rate of storm-water runoff from the site when comparing the pre-development conditions to the post development conditions. See Appendix B of this report for a summary of the design storms.

**Standard 3: Recharge**

- Soil testing has been completed. See Appendix F of this report for permeability test results and soil testing information. Additionally, soil testing results can be found on the plan sheets.
- Drawdown within 72 hours  
Pond 1 - Storage Volume below outlet = 14,338 cubic feet  
Time =  $(14,338) / (0.39''/\text{hr} \times 1' / 12'' \times 8,348 \text{ sf.}) = 52.85 \text{ hours} < 72 \text{ hours}$   
See Stage-Area-Storage table for Pond 1 this Appendix.

**Standard 4: Water Quality**

- The owner will be responsible for compliance with standard four requirements.
- Refer to the Operation and Maintenance Plan and the Storm-water Facilities Plan for the Inspection and Maintenance Schedule and the Operation and Maintenance Schedule.
- See Appendix E for the Manufactures TSS removal rate. The site is not located within a zone II. The Infiltration Pond has been designed with an infiltration rate of 0.39 inches per hour. This led to a Water Quality volume of 1/2" WQV.

The proposed project will include a stormwater system which includes the installation of deep sump hooded catch basins, sediment forebay and an infiltration basin as well as a sediment forebay and water quality swales.

Water Quality Volumes for Pond 1 Note: Due to Town of Franklin Stormwater Management Bylaw a WQV of 1" is being used.

Storage in Pond 1 below the outlet invert (171.0) = 14,338 cubic feet (Provided)

**Standard 5: Land uses with higher potential pollutant loads**

None proposed.

**Standard 6: Critical Areas**

N/A

**Standard 7: Re-developments and Other Projects**

N/A

**Standard 8: Construction Period Pollution Prevention and Erosion Sedimentation Control**

- Refer to Site Plans for the Inspection and Maintenance Schedule and the Operation and Maintenance Schedule.
- The project will be covered by an NPDES Construction General Permit.

**Standard 9: Operation and Maintenance Plan**

- Refer to Site Plans for the Inspection and Maintenance Schedule and the Operation and Maintenance Schedule.

- The owner will be responsible for the storm-water management system, implementation of the operation and maintenance, the maintenance costs, and completion of the maintenance logs.

**Standard 10: Prohibition of Illicit Discharges**

- Owner to be responsible for compliance with avoiding illicit discharges.
- The site will be connected to the town sewer system.

## Stage-Area-Storage for Pond 1P: POND 1

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
169.50	8,348	0	170.02	9,173	4,555
169.51	8,364	84	170.03	9,190	4,647
169.52	8,380	167	170.04	9,206	4,739
169.53	8,396	251	170.05	9,223	4,831
169.54	8,411	335	170.06	9,239	4,923
169.55	8,427	419	170.07	9,256	5,016
169.56	8,443	504	170.08	9,272	5,108
169.57	8,459	588	170.09	9,289	5,201
169.58	8,475	673	170.10	9,305	5,294
169.59	8,491	758	170.11	9,322	5,387
169.60	8,506	843	170.12	9,338	5,481
169.61	8,522	928	170.13	9,355	5,574
169.62	8,538	1,013	170.14	9,371	5,668
169.63	8,554	1,099	170.15	9,388	5,762
169.64	8,570	1,184	170.16	9,404	5,856
169.65	8,586	1,270	170.17	9,421	5,950
169.66	8,601	1,356	170.18	9,437	6,044
169.67	8,617	1,442	170.19	9,454	6,138
169.68	8,633	1,528	170.20	9,470	6,233
169.69	8,649	1,615	170.21	9,487	6,328
169.70	8,665	1,701	170.22	9,503	6,423
169.71	8,681	1,788	170.23	9,520	6,518
169.72	8,696	1,875	170.24	9,536	6,613
169.73	8,712	1,962	170.25	9,553	6,709
169.74	8,728	2,049	170.26	9,569	6,804
169.75	8,744	2,137	170.27	9,586	6,900
169.76	8,760	2,224	170.28	9,602	6,996
169.77	8,776	2,312	170.29	9,619	7,092
169.78	8,792	2,400	170.30	9,635	7,188
169.79	8,807	2,488	170.31	9,652	7,285
169.80	8,823	2,576	170.32	9,668	7,381
169.81	8,839	2,664	170.33	9,685	7,478
169.82	8,855	2,752	170.34	9,701	7,575
169.83	8,871	2,841	170.35	9,718	7,672
169.84	8,887	2,930	170.36	9,734	7,769
169.85	8,902	3,019	170.37	9,751	7,867
169.86	8,918	3,108	170.38	9,767	7,964
169.87	8,934	3,197	170.39	9,784	8,062
169.88	8,950	3,287	170.40	9,800	8,160
169.89	8,966	3,376	170.41	9,817	8,258
169.90	8,982	3,466	170.42	9,833	8,356
169.91	8,997	3,556	170.43	9,850	8,455
169.92	9,013	3,646	170.44	9,866	8,553
169.93	9,029	3,736	170.45	9,883	8,652
169.94	9,045	3,826	170.46	9,899	8,751
169.95	9,061	3,917	170.47	9,916	8,850
169.96	9,077	4,008	170.48	9,932	8,949
169.97	9,092	4,099	170.49	9,949	9,049
169.98	9,108	4,190	170.50	9,966	9,148
169.99	9,124	4,281	170.51	9,982	9,248
170.00	9,140	4,372	170.52	9,999	9,348
170.01	9,157	4,463	170.53	10,015	9,448

## Stage-Area-Storage for Pond 1P: POND 1 (continued)

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
170.54	10,032	9,548	171.06	10,890	14,988
170.55	10,048	9,649	171.07	10,907	15,097
170.56	10,065	9,749	171.08	10,923	15,206
170.57	10,081	9,850	171.09	10,940	15,315
170.58	10,098	9,951	171.10	10,956	15,425
170.59	10,114	10,052	171.11	10,973	15,534
170.60	10,131	10,153	171.12	10,989	15,644
170.61	10,147	10,255	171.13	11,006	15,754
170.62	10,164	10,356	171.14	11,022	15,864
170.63	10,180	10,458	171.15	11,039	15,975
170.64	10,197	10,560	171.16	11,055	16,085
170.65	10,213	10,662	171.17	11,072	16,196
170.66	10,230	10,764	171.18	11,088	16,307
170.67	10,246	10,866	171.19	11,105	16,418
170.68	10,263	10,969	171.20	11,121	16,529
170.69	10,279	11,072	171.21	11,138	16,640
170.70	10,296	11,174	171.22	11,154	16,751
170.71	10,312	11,278	171.23	11,171	16,863
170.72	10,329	11,381	171.24	11,187	16,975
170.73	10,345	11,484	171.25	11,204	17,087
170.74	10,362	11,588	171.26	11,220	17,199
170.75	10,378	11,691	171.27	11,237	17,311
170.76	10,395	11,795	171.28	11,253	17,424
170.77	10,411	11,899	171.29	11,270	17,536
170.78	10,428	12,003	171.30	11,286	17,649
170.79	10,444	12,108	171.31	11,303	17,762
170.80	10,461	12,212	171.32	11,319	17,875
170.81	10,477	12,317	171.33	11,336	17,988
170.82	10,494	12,422	171.34	11,352	18,102
170.83	10,510	12,527	171.35	11,369	18,215
170.84	10,527	12,632	171.36	11,385	18,329
170.85	10,543	12,737	171.37	11,402	18,443
170.86	10,560	12,843	171.38	11,418	18,557
170.87	10,576	12,949	171.39	11,435	18,672
170.88	10,593	13,054	171.40	11,451	18,786
170.89	10,609	13,160	171.41	11,468	18,901
170.90	10,626	13,267	171.42	11,484	19,015
170.91	10,642	13,373	171.43	11,501	19,130
170.92	10,659	13,480	171.44	11,517	19,245
170.93	10,675	13,586	171.45	11,534	19,361
170.94	10,692	13,693	171.46	11,550	19,476
170.95	10,708	13,800	171.47	11,567	19,592
170.96	10,725	13,907	171.48	11,583	19,707
170.97	10,741	14,015	171.49	11,600	19,823
170.98	10,758	14,122	171.50	11,617	19,939
170.99	10,774	14,230	171.51	11,633	20,056
171.00	10,791	14,338	171.52	11,650	20,172
171.01	10,808	14,445	171.53	11,666	20,289
171.02	10,824	14,554	171.54	11,683	20,405
171.03	10,841	14,662	171.55	11,699	20,522
171.04	10,857	14,770	171.56	11,716	20,639
171.05	10,874	14,879	171.57	11,732	20,757

**Stage-Area-Storage for Pond 1P: POND 1 (continued)**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
171.58	11,749	20,874	172.10	12,617	27,207
171.59	11,765	20,992	172.11	12,634	27,333
171.60	11,782	21,109	172.12	12,652	27,460
171.61	11,798	21,227	172.13	12,669	27,586
171.62	11,815	21,345	172.14	12,687	27,713
171.63	11,831	21,463	172.15	12,704	27,840
171.64	11,848	21,582	172.16	12,722	27,967
171.65	11,864	21,700	172.17	12,739	28,094
171.66	11,881	21,819	172.18	12,757	28,222
171.67	11,897	21,938	172.19	12,774	28,350
171.68	11,914	22,057	172.20	12,791	28,477
171.69	11,930	22,176	172.21	12,809	28,605
171.70	11,947	22,296	172.22	12,826	28,734
171.71	11,963	22,415	172.23	12,844	28,862
171.72	11,980	22,535	172.24	12,861	28,990
171.73	11,996	22,655	172.25	12,879	29,119
171.74	12,013	22,775	172.26	12,896	29,248
171.75	12,029	22,895	172.27	12,914	29,377
171.76	12,046	23,015	172.28	12,931	29,506
171.77	12,062	23,136	172.29	12,949	29,636
171.78	12,079	23,257	172.30	12,966	29,765
171.79	12,095	23,378	172.31	12,984	29,895
171.80	12,112	23,499	172.32	13,001	30,025
171.81	12,128	23,620	172.33	13,019	30,155
171.82	12,145	23,741	172.34	13,036	30,285
171.83	12,161	23,863	172.35	13,054	30,416
171.84	12,178	23,984	172.36	13,071	30,546
171.85	12,194	24,106	172.37	13,089	30,677
171.86	12,211	24,228	172.38	13,106	30,808
171.87	12,227	24,350	172.39	13,123	30,939
171.88	12,244	24,473	172.40	13,141	31,071
171.89	12,260	24,595	172.41	13,158	31,202
171.90	12,277	24,718	172.42	13,176	31,334
171.91	12,293	24,841	172.43	13,193	31,466
171.92	12,310	24,964	172.44	13,211	31,598
171.93	12,326	25,087	172.45	13,228	31,730
171.94	12,343	25,210	172.46	13,246	31,862
171.95	12,359	25,334	172.47	13,263	31,995
171.96	12,376	25,458	172.48	13,281	32,127
171.97	12,392	25,581	172.49	13,298	32,260
171.98	12,409	25,705	172.50	13,316	32,393
171.99	12,425	25,830	172.51	13,333	32,527
172.00	12,442	25,954	172.52	13,351	32,660
172.01	12,459	26,079	172.53	13,368	32,794
172.02	12,477	26,203	172.54	13,386	32,927
172.03	12,494	26,328	172.55	13,403	33,061
172.04	12,512	26,453	172.56	13,421	33,196
172.05	12,529	26,578	172.57	13,438	33,330
172.06	12,547	26,704	172.58	13,455	33,464
172.07	12,564	26,829	172.59	13,473	33,599
172.08	12,582	26,955	172.60	13,490	33,734
172.09	12,599	27,081	172.61	13,508	33,869

**Stage-Area-Storage for Pond 1P: POND 1 (continued)**

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
172.62	13,525	34,004	173.14	14,434	41,273
172.63	13,543	34,139	173.15	14,451	41,418
172.64	13,560	34,275	173.16	14,469	41,562
172.65	13,578	34,410	173.17	14,486	41,707
172.66	13,595	34,546	173.18	14,504	41,852
172.67	13,613	34,682	173.19	14,521	41,997
172.68	13,630	34,819	173.20	14,539	42,142
172.69	13,648	34,955	173.21	14,556	42,288
172.70	13,665	35,091	173.22	14,574	42,434
172.71	13,683	35,228	173.23	14,591	42,579
172.72	13,700	35,365	173.24	14,609	42,725
172.73	13,718	35,502	173.25	14,626	42,872
172.74	13,735	35,639	173.26	14,644	43,018
172.75	13,753	35,777	173.27	14,661	43,164
172.76	13,770	35,915	173.28	14,679	43,311
172.77	13,787	36,052	173.29	14,696	43,458
172.78	13,805	36,190	173.30	14,714	43,605
172.79	13,822	36,328	173.31	14,731	43,752
172.80	13,840	36,467	173.32	14,748	43,900
172.81	13,857	36,605	173.33	14,766	44,047
172.82	13,875	36,744	173.34	14,783	44,195
172.83	13,892	36,883	173.35	14,801	44,343
172.84	13,910	37,022	173.36	14,818	44,491
172.85	13,927	37,161	173.37	14,836	44,639
172.86	13,945	37,300	173.38	14,853	44,788
172.87	13,962	37,440	173.39	14,871	44,936
172.88	13,980	37,580	173.40	14,888	45,085
172.89	13,997	37,719	173.41	14,906	45,234
172.90	14,015	37,859	173.42	14,923	45,383
172.91	14,032	38,000	173.43	14,941	45,533
172.92	14,050	38,140	173.44	14,958	45,682
172.93	14,067	38,281	173.45	14,976	45,832
172.94	14,084	38,421	173.46	14,993	45,982
172.95	14,102	38,562	173.47	15,011	46,132
172.96	14,119	38,703	173.48	15,028	46,282
172.97	14,137	38,845	173.49	15,046	46,432
172.98	14,154	38,986	173.50	<b>15,063</b>	<b>46,583</b>
172.99	14,172	39,128			
173.00	14,189	39,270			
173.01	14,207	39,412			
173.02	14,224	39,554			
173.03	14,242	39,696			
173.04	14,259	39,839			
173.05	14,277	39,981			
173.06	14,294	40,124			
173.07	14,312	40,267			
173.08	14,329	40,410			
173.09	14,347	40,554			
173.10	14,364	40,697			
173.11	14,382	40,841			
173.12	14,399	40,985			
173.13	14,416	41,129			

## APPENDIX B

## Pre-Development vs. Post Development Rate and Volume of Runoff

This analysis was prepared to show the summary of the pre-development and post development rate and volume of runoff as required by the Town of Franklin Storm-water Requirements.

The pre-development watershed area 1S has a discharge to the on-site wetland. Post-development Link 1L was provided to combine the outlet from Pond 1 and the wet swale with the undeveloped area which discharge to the on-site wetland. A comparison of the rate and volume for pre-development area 1S and post-development Link 1L (To Wetlands) is provided below:

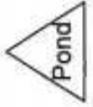
2-year storm event (CFS)			2 year storm event (A.F.)		
Pre		Post	Pre		Post
1S	vs	1L	1S	vs	1L
5.23		4.15	0.729		0.568
10 year storm event (CFS)			10 year storm event (A.F.)		
Pre		Post	Pre		Post
1S	vs	1L	1S	vs	1L
17.14		12.98	1.995		1.851
100 year storm event (CFS)			100 year storm event (A.F.)		
Pre		Post	Pre		Post
1S	vs	1L	1S	vs	1L
41.08		33.52	4.544		4.521

The rate of runoff and volume of runoff for the 2 year, 10 year and 100 year storm events have been matched or reduced.

## APPENDIX C



1S



Drainage Diagram for UC1340-PRE

Prepared by United Consultants, Inc.

HydroCAD® 8.00 s/n 001535 © 2006 HydroCAD Software Solutions LLC

**Area Listing (all nodes)**

<u>Area (acres)</u>	<u>CN</u>	<u>Description (subcats)</u>
1.766	55	Woods, Good, HSG B (1S)
8.386	61	>75% Grass cover, Good, HSG B (1S)
0.494	70	Woods, Good, HSG C (1S)
2.412	74	>75% Grass cover, Good, HSG C (1S)
0.609	98	Paved parking & roofs (1S)
<hr/>		
13.667		

## **2 YR PRE-DEVELOPMENT**

**Subcatchment 1S: 1S**

Runoff = 5.23 cfs @ 12.38 hrs, Volume= 0.729 af, Depth= 0.64"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 2YR-NOAA Rainfall=3.37"

Area (sf)	CN	Description
26,517	98	Paved parking & roofs
365,308	61	>75% Grass cover, Good, HSG B
105,060	74	>75% Grass cover, Good, HSG C
76,931	55	Woods, Good, HSG B
21,529	70	Woods, Good, HSG C
595,345	64	Weighted Average
568,828		Pervious Area
26,517		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
13.3	42	0.0110	0.05		<b>Sheet Flow,</b> Woods: Light underbrush n= 0.400 P2= 3.37"
2.4	127	0.0310	0.88		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
1.6	172	0.0650	1.78		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.1	13	0.0220	3.01		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
4.8	301	0.0220	1.04		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
22.2	655	Total			

## 10 YR PRE-DEVELOPMENT

**Subcatchment 1S: 1S**

Runoff = 17.14 cfs @ 12.33 hrs, Volume= 1.995 af, Depth= 1.75"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 10YR-NOAA Rainfall=5.26"

Area (sf)	CN	Description
26,517	98	Paved parking & roofs
365,308	61	>75% Grass cover, Good, HSG B
105,060	74	>75% Grass cover, Good, HSG C
76,931	55	Woods, Good, HSG B
21,529	70	Woods, Good, HSG C
595,345	64	Weighted Average
568,828		Pervious Area
26,517		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
13.3	42	0.0110	0.05		<b>Sheet Flow,</b> Woods: Light underbrush n= 0.400 P2= 3.37"
2.4	127	0.0310	0.88		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
1.6	172	0.0650	1.78		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.1	13	0.0220	3.01		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
4.8	301	0.0220	1.04		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
22.2	655	Total			

## **100 YR PRE-DEVELOPMENT**

**Subcatchment 1S: 1S**

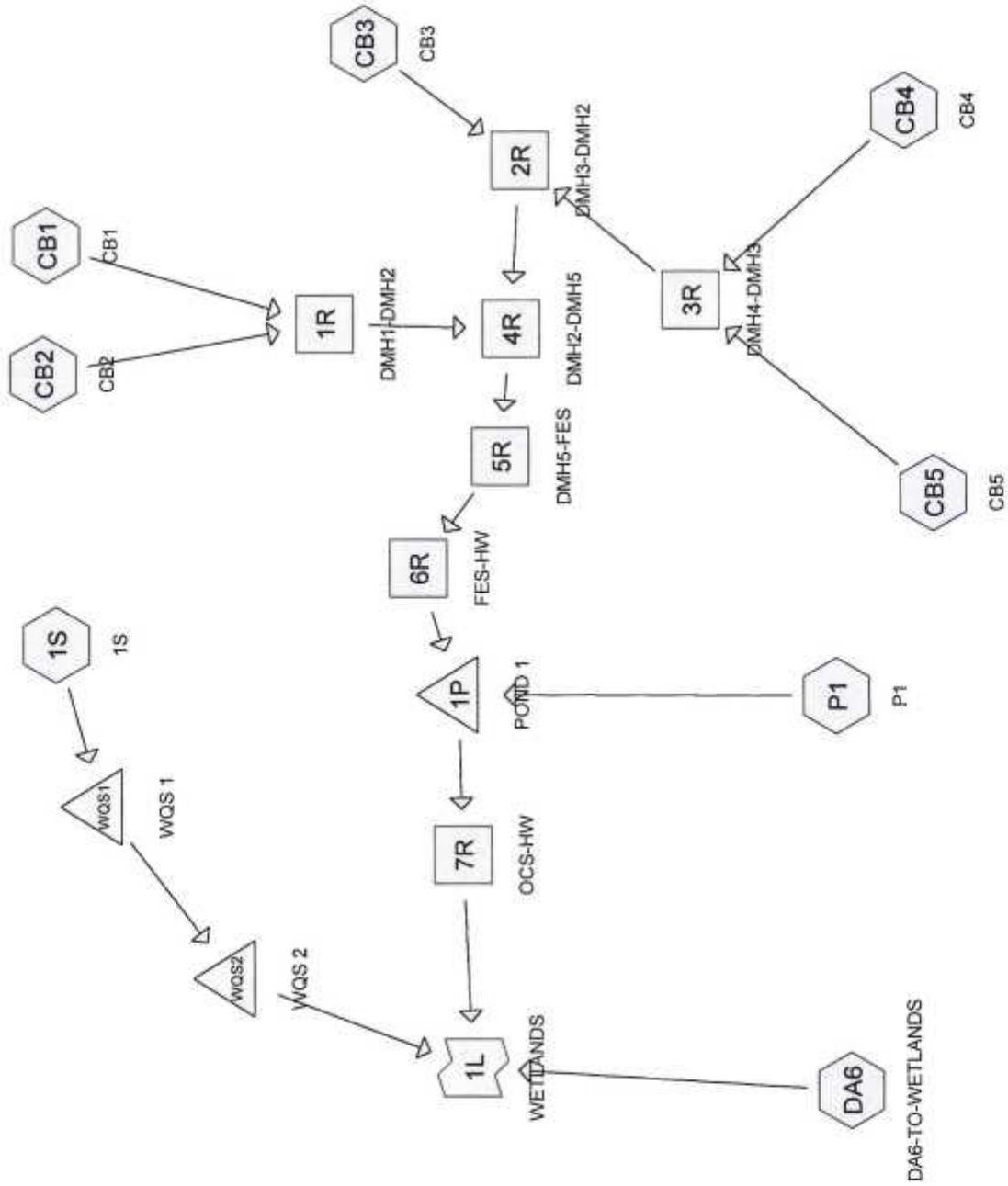
Runoff = 41.08 cfs @ 12.31 hrs, Volume= 4.544 af, Depth= 3.99"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100YR-NOAA Rainfall=8.26"

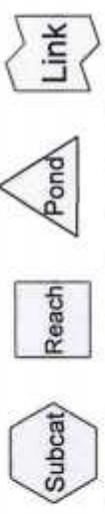
Area (sf)	CN	Description
26,517	98	Paved parking & roofs
365,308	61	>75% Grass cover, Good, HSG B
105,060	74	>75% Grass cover, Good, HSG C
76,931	55	Woods, Good, HSG B
21,529	70	Woods, Good, HSG C
595,345	64	Weighted Average
568,828		Pervious Area
26,517		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
13.3	42	0.0110	0.05		<b>Sheet Flow,</b> Woods: Light underbrush n= 0.400 P2= 3.37"
2.4	127	0.0310	0.88		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
1.6	172	0.0650	1.78		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.1	13	0.0220	3.01		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
4.8	301	0.0220	1.04		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
22.2	655	Total			

## APPENDIX D



**Drainage Diagram for UC1340-POST**  
 Prepared by United Consultants, Inc.  
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**Area Listing (all nodes)**

<u>Area (acres)</u>	<u>CN</u>	<u>Description (subcats)</u>
1.140	55	Woods, Good, HSG B (CB1,CB3,DA6)
7.943	61	>75% Grass cover, Good, HSG B (1S,CB1,CB2,CB3,CB4,CB5,DA6,P1)
0.494	70	Woods, Good, HSG C (DA6)
2.386	74	>75% Grass cover, Good, HSG C (CB5,DA6,P1)
0.305	98	POND (P1)
1.403	98	Paved parking & roofs (1S,CB1,CB2,CB3,CB4,CB5,DA6,P1)
<hr/>		
13.671		

## 2 YR POST-DEVELOPMENT

**Subcatchment 1S: 1S**

Runoff = 0.70 cfs @ 12.10 hrs, Volume= 0.054 af, Depth= 0.98"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 2YR-NOAA Rainfall=3.37"

Area (sf)	CN	Description
8,143	98	Paved parking & roofs
20,718	61	>75% Grass cover, Good, HSG B
28,861	71	Weighted Average
20,718		Pervious Area
8,143		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.8	50	0.0280	0.17		<b>Sheet Flow,</b> Grass: Short n= 0.150 P2= 3.37"
0.2	15	0.0280	1.17		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.3	28	0.0910	1.51		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
0.2	16	0.1250	1.77		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
0.0	5	0.1250	2.47		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.0	5	0.0200	2.87		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	5	0.0200	0.99		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.4	89	0.0300	3.52		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	32	0.0460	4.35		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
6.1	245	Total			

**Subcatchment CB1: CB1**

Runoff = 0.13 cfs @ 12.39 hrs, Volume= 0.022 af, Depth= 0.44"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 2YR-NOAA Rainfall=3.37"

Area (sf)	CN	Description
1,788	98	Paved parking & roofs
3,957	61	>75% Grass cover, Good, HSG B
20,562	55	Woods, Good, HSG B
26,307	59	Weighted Average
24,519		Pervious Area
1,788		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
12.0	50	0.0200	0.07		<b>Sheet Flow,</b> Woods: Light underbrush n= 0.400 P2= 3.37"
2.5	109	0.0210	0.72		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
2.8	160	0.0375	0.97		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
0.8	62	0.0678	1.30		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
0.1	12	0.1667	2.04		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
0.1	7	0.0200	0.99		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.0	5	0.0200	2.87		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	5	0.0200	0.99		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.5	86	0.0200	2.87		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	21	0.0100	4.91	3.86	<b>Circular Channel (pipe),</b> Diam= 12.0" Area= 0.8 sf Perim= 3.1' r= 0.25' n= 0.012 Concrete pipe, finished
19.0	517	Total			

**Subcatchment CB2: CB2**

Runoff = 0.22 cfs @ 12.13 hrs, Volume= 0.018 af, Depth= 1.15"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
Type III 24-hr 2YR-NOAA Rainfall=3.37"

Area (sf)	CN	Description
2,838	98	Paved parking & roofs
5,427	61	>75% Grass cover, Good, HSG B
8,265	74	Weighted Average
5,427		Pervious Area
2,838		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.2	50	0.0100	0.12		<b>Sheet Flow,</b> Grass: Short n= 0.150 P2= 3.37"
1.3	53	0.0100	0.70		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.1	10	0.0200	2.87		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.0	11	0.0190	6.77	5.32	<b>Circular Channel (pipe),</b> Diam= 12.0" Area= 0.8 sf Perim= 3.1' r= 0.25' n= 0.012 Concrete pipe, finished
8.6	124	Total			

**Subcatchment CB3: CB3**

Runoff = 0.50 cfs @ 12.22 hrs, Volume= 0.056 af, Depth= 0.73"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
Type III 24-hr 2YR-NOAA Rainfall=3.37"

Area (sf)	CN	Description
6,010	98	Paved parking & roofs
28,667	61	>75% Grass cover, Good, HSG B
5,036	55	Woods, Good, HSG B
39,713	66	Weighted Average
33,703		Pervious Area
6,010		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.3	50	0.0380	0.09		<b>Sheet Flow,</b> Woods: Light underbrush n= 0.400 P2= 3.37"
1.2	77	0.0227	1.05		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
1.1	92	0.0435	1.46		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
1.1	66	0.0200	0.99		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.1	27	0.1850	3.01		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.3	25	0.0400	1.40		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.4	22	0.0220	1.04		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.0	5	0.0200	2.87		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	5	0.0200	0.99		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.2	24	0.0100	2.03		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	21	0.0100	4.91	3.86	<b>Circular Channel (pipe),</b> Diam= 12.0" Area= 0.8 sf Perim= 3.1' r= 0.25' n= 0.012 Concrete pipe, finished
13.9	414	Total			

**Subcatchment CB4: CB4**

Runoff = 1.27 cfs @ 12.10 hrs, Volume= 0.096 af, Depth= 1.04"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
Type III 24-hr 2YR-NOAA Rainfall=3.37"

Area (sf)	CN	Description
14,187	98	Paved parking & roofs
34,440	61	>75% Grass cover, Good, HSG B
48,627	72	Weighted Average
34,440		Pervious Area
14,187		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.0	50	0.0440	0.21		<b>Sheet Flow,</b> Grass: Short n= 0.150 P2= 3.37"
0.5	64	0.0781	1.96		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.6	63	0.0645	1.78		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.5	46	0.0500	1.57		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.0	5	0.0200	2.87		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	5	0.0100	0.70		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.2	25	0.0100	2.03		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	21	0.0100	5.70	7.00	<b>Circular Channel (pipe),</b> Diam= 15.0" Area= 1.2 sf Perim= 3.9' r= 0.31' n= 0.012 Concrete pipe, finished
6.0	279	Total			

**Subcatchment CB5: CB5**

Runoff = 0.80 cfs @ 12.09 hrs, Volume= 0.057 af, Depth= 1.68"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
Type III 24-hr 2YR-NOAA Rainfall=3.37"

Area (sf)	CN	Description
9,299	98	Paved parking & roofs
6,735	61	>75% Grass cover, Good, HSG B
1,715	74	>75% Grass cover, Good, HSG C
17,749	82	Weighted Average
8,450		Pervious Area
9,299		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.9	5	0.0200	0.10		<b>Sheet Flow,</b> Grass: Short n= 0.150 P2= 3.37"
0.1	5	0.0200	0.78		<b>Sheet Flow,</b> Smooth surfaces n= 0.011 P2= 3.37"
0.9	5	0.0200	0.10		<b>Sheet Flow,</b> Grass: Short n= 0.150 P2= 3.37"
1.2	201	0.0200	2.87		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
2.9					<b>Direct Entry, MIN TC</b>
0.0	12	0.0100	4.91	3.86	<b>Circular Channel (pipe),</b> Diam= 12.0" Area= 0.8 sf Perim= 3.1' r= 0.25' n= 0.012 Concrete pipe, finished
6.0	228	Total			

**Subcatchment DA6: DA6-TO-WETLANDS**

Runoff = 4.15 cfs @ 12.33 hrs, Volume= 0.525 af, Depth= 0.73"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
Type III 24-hr 2YR-NOAA Rainfall=3.37"

Area (sf)	CN	Description
13,120	98	Paved parking & roofs
215,109	61	>75% Grass cover, Good, HSG B
102,048	74	>75% Grass cover, Good, HSG C
24,053	55	Woods, Good, HSG B
21,529	70	Woods, Good, HSG C
375,859	66	Weighted Average
362,739		Pervious Area
13,120		Impervious Area

**UC1340-POST**

Type III 24-hr 2YR-NOAA Rainfall=3.37"

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	13	0.0340	0.07		<b>Sheet Flow,</b> Woods: Light underbrush n= 0.400 P2= 3.37"
3.5	37	0.0340	0.18		<b>Sheet Flow,</b> Grass: Short n= 0.150 P2= 3.37"
1.8	101	0.0180	0.94		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.8	61	0.0330	1.27		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
4.3	357	0.0400	1.40		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
5.6	225	0.0090	0.66		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.2	17	0.0400	1.40		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.5	32	0.0400	1.00		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
20.0	843	Total			

**Subcatchment P1: P1**

Runoff = 1.58 cfs @ 12.09 hrs, Volume= 0.116 af, Depth= 1.21"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
Type III 24-hr 2YR-NOAA Rainfall=3.37"

Area (sf)	CN	Description
5,726	98	Paved parking & roofs
30,929	61	>75% Grass cover, Good, HSG B
155	74	>75% Grass cover, Good, HSG C
13,301	98	POND
50,111	75	Weighted Average
31,084		Pervious Area
19,027		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.7	50	0.0300	0.18		<b>Sheet Flow,</b> Grass: Short n= 0.150 P2= 3.37"
0.2	16	0.0300	1.21		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.4	40	0.0500	1.57		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.7	58	0.0340	1.29		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
6.0	164	Total			

**Reach 1R: DMH1-DMH2**

Inflow Area = 0.794 ac, Inflow Depth = 0.61" for 2YR-NOAA event  
Inflow = 0.26 cfs @ 12.16 hrs, Volume= 0.040 af  
Outflow = 0.26 cfs @ 12.23 hrs, Volume= 0.040 af, Atten= 1%, Lag= 3.7 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
Max. Velocity= 2.28 fps, Min. Travel Time= 1.8 min  
Avg. Velocity = 1.08 fps, Avg. Travel Time= 3.8 min

Peak Storage= 28 cf @ 12.20 hrs, Average Depth at Peak Storage= 0.19'  
Bank-Full Depth= 1.25', Capacity at Bank-Full= 5.43 cfs

15.0" Diameter Pipe, n= 0.012 Concrete pipe, finished  
Length= 246.0' Slope= 0.0060 '/  
Inlet Invert= 173.97', Outlet Invert= 172.49'



**Reach 2R: DMH3-DMH2**

Inflow Area = 2.435 ac, Inflow Depth = 1.03" for 2YR-NOAA event  
Inflow = 2.38 cfs @ 12.11 hrs, Volume= 0.209 af  
Outflow = 2.38 cfs @ 12.11 hrs, Volume= 0.209 af, Atten= 0%, Lag= 0.1 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
Max. Velocity= 4.95 fps, Min. Travel Time= 0.1 min  
Avg. Velocity = 1.86 fps, Avg. Travel Time= 0.1 min

Peak Storage= 8 cf @ 12.11 hrs, Average Depth at Peak Storage= 0.42'  
Bank-Full Depth= 2.00', Capacity at Bank-Full= 24.51 cfs

24.0" Diameter Pipe, n= 0.012 Concrete pipe, finished  
Length= 16.0' Slope= 0.0100 '/  
Inlet Invert= 172.00', Outlet Invert= 171.84'



**Reach 3R: DMH4-DMH3**

Inflow Area = 1.524 ac, Inflow Depth = 1.21" for 2YR-NOAA event  
 Inflow = 2.07 cfs @ 12.09 hrs, Volume= 0.153 af  
 Outflow = 2.06 cfs @ 12.10 hrs, Volume= 0.153 af, Atten= 0%, Lag= 0.4 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 4.89 fps, Min. Travel Time= 0.2 min  
 Avg. Velocity = 1.77 fps, Avg. Travel Time= 0.6 min

Peak Storage= 25 cf @ 12.10 hrs, Average Depth at Peak Storage= 0.43'  
 Bank-Full Depth= 1.50', Capacity at Bank-Full= 11.38 cfs

18.0" Diameter Pipe, n= 0.012 Concrete pipe, finished  
 Length= 60.0' Slope= 0.0100 '/  
 Inlet Invert= 173.10', Outlet Invert= 172.50'



**Reach 4R: DMH2-DMH5**

Inflow Area = 3.229 ac, Inflow Depth = 0.93" for 2YR-NOAA event  
 Inflow = 2.55 cfs @ 12.12 hrs, Volume= 0.249 af  
 Outflow = 2.55 cfs @ 12.12 hrs, Volume= 0.249 af, Atten= 0%, Lag= 0.3 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 4.65 fps, Min. Travel Time= 0.2 min  
 Avg. Velocity = 1.77 fps, Avg. Travel Time= 0.5 min

Peak Storage= 29 cf @ 12.12 hrs, Average Depth at Peak Storage= 0.46'  
 Bank-Full Depth= 2.00', Capacity at Bank-Full= 21.82 cfs

24.0" Diameter Pipe, n= 0.012  
 Length= 53.0' Slope= 0.0079 '/  
 Inlet Invert= 171.74', Outlet Invert= 171.32'



**Reach 5R: DMH5-FES**

Inflow Area = 3.229 ac, Inflow Depth = 0.93" for 2YR-NOAA event  
 Inflow = 2.55 cfs @ 12.12 hrs, Volume= 0.249 af  
 Outflow = 2.54 cfs @ 12.13 hrs, Volume= 0.249 af, Atten= 0%, Lag= 0.5 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 4.67 fps, Min. Travel Time= 0.3 min  
 Avg. Velocity = 1.78 fps, Avg. Travel Time= 0.7 min

Peak Storage= 42 cf @ 12.13 hrs, Average Depth at Peak Storage= 0.46'  
 Bank-Full Depth= 2.00', Capacity at Bank-Full= 21.99 cfs

24.0" Diameter Pipe, n= 0.012  
 Length= 77.0' Slope= 0.0081 '/  
 Inlet Invert= 171.22', Outlet Invert= 170.60'



**Reach 6R: FES-HW**

Inflow Area = 3.229 ac, Inflow Depth = 0.93" for 2YR-NOAA event  
 Inflow = 2.54 cfs @ 12.13 hrs, Volume= 0.249 af  
 Outflow = 2.54 cfs @ 12.14 hrs, Volume= 0.249 af, Atten= 0%, Lag= 0.3 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 4.65 fps, Min. Travel Time= 0.2 min  
 Avg. Velocity = 1.77 fps, Avg. Travel Time= 0.5 min

Peak Storage= 27 cf @ 12.13 hrs, Average Depth at Peak Storage= 0.46'  
 Bank-Full Depth= 2.00', Capacity at Bank-Full= 21.86 cfs

24.0" Diameter Pipe, n= 0.012  
 Length= 49.0' Slope= 0.0080 '/  
 Inlet Invert= 171.19', Outlet Invert= 170.80'



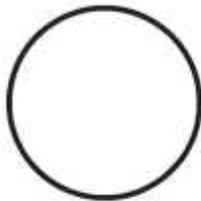
**Reach 7R: OCS-HW**

Inflow Area = 4.380 ac, Inflow Depth = 0.00" for 2YR-NOAA event  
 Inflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af  
 Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 0.00 fps, Min. Travel Time= 0.0 min  
 Avg. Velocity = 0.00 fps, Avg. Travel Time= 0.0 min

Peak Storage= 0 cf @ 0.00 hrs, Average Depth at Peak Storage= 0.00'  
 Bank-Full Depth= 1.50', Capacity at Bank-Full= 16.09 cfs

18.0" Diameter Pipe, n= 0.012 Concrete pipe, finished  
 Length= 28.0' Slope= 0.0200 1/  
 Inlet Invert= 169.50', Outlet Invert= 168.94'



**Pond 1P: POND 1**

Inflow Area = 4.380 ac, Inflow Depth = 1.00" for 2YR-NOAA event  
 Inflow = 4.01 cfs @ 12.12 hrs, Volume= 0.365 af  
 Outflow = 0.09 cfs @ 22.54 hrs, Volume= 0.365 af, Atten= 98%, Lag= 625.2 min  
 Discarded = 0.09 cfs @ 22.54 hrs, Volume= 0.365 af  
 Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Peak Elev= 170.75' @ 22.54 hrs Surf.Area= 10,382 sf Storage= 11,717 cf

Plug-Flow detention time= 1,297.6 min calculated for 0.365 af (100% of inflow)  
 Center-of-Mass det. time= 1,297.7 min ( 2,165.3 - 867.5 )

Volume	Invert	Avail.Storage	Storage Description
#1	169.50'	46,583 cf	<b>Custom Stage Data (Prismatic)</b> Listed below (Recalc)
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
169.50	8,348	0	0
170.00	9,140	4,372	4,372
172.00	12,442	21,582	25,954
173.50	15,063	20,629	46,583

**UC1340-POST**

Type III 24-hr 2YR-NOAA Rainfall=3.37"

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Device	Routing	Invert	Outlet Devices
#1	Primary	169.50'	<b>18.0" x 28.0' long Culvert</b> RCP, square edge headwall, Ke= 0.500 Outlet Invert= 168.94' S= 0.0200 ' Cc= 0.900 n= 0.012 Concrete pipe, finished
#2	Device 1	171.00'	<b>3.0" Vert. Orifice/Grate X 2.00</b> C= 0.600
#3	Device 1	171.10'	<b>3.0" Vert. Orifice/Grate</b> C= 0.600
#4	Device 1	171.50'	<b>12.0" Vert. Orifice/Grate</b> C= 0.600
#5	Device 1	172.35'	<b>4.00' x 4.00' Horiz. Orifice/Grate</b> Limited to weir flow C= 0.600
#6	Discarded	0.00'	<b>0.390 in/hr Exfiltration over Surface area</b>

**Discarded OutFlow** Max=0.09 cfs @ 22.54 hrs HW=170.75' (Free Discharge)

↳ **6=Exfiltration** (Exfiltration Controls 0.09 cfs)

**Primary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=169.50' (Free Discharge)

- ↳ **1=Culvert** ( Controls 0.00 cfs)
  - ↳ **2=Orifice/Grate** ( Controls 0.00 cfs)
  - ↳ **3=Orifice/Grate** ( Controls 0.00 cfs)
  - ↳ **4=Orifice/Grate** ( Controls 0.00 cfs)
  - ↳ **5=Orifice/Grate** ( Controls 0.00 cfs)

**Pond WQS1: WQS 1**

Inflow Area = 0.663 ac, Inflow Depth = 0.98" for 2YR-NOAA event  
 Inflow = 0.70 cfs @ 12.10 hrs, Volume= 0.054 af  
 Outflow = 0.27 cfs @ 12.43 hrs, Volume= 0.050 af, Atten= 62%, Lag= 19.9 min  
 Primary = 0.27 cfs @ 12.43 hrs, Volume= 0.050 af

Routing by Stor-Ind method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Peak Elev= 169.68' @ 12.43 hrs Surf.Area= 856 sf Storage= 669 cf

Plug-Flow detention time= 142.4 min calculated for 0.049 af (91% of inflow)  
 Center-of-Mass det. time= 99.6 min ( 968.3 - 868.7 )

Volume	Invert	Avail.Storage	Storage Description
#1	168.50'	2,110 cf	<b>Custom Stage Data (Prismatic)</b> Listed below (Recalc)
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
168.50	276	0	0
170.00	1,013	967	967
171.00	1,273	1,143	2,110

Device	Routing	Invert	Outlet Devices
#1	Primary	170.00'	<b>13.5' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#2	Primary	169.00'	<b>30.0 deg Sharp-Crested Vee/Trap Weir</b> C= 2.61

**Primary OutFlow** Max=0.27 cfs @ 12.43 hrs HW=169.68' (Free Discharge)

- ↳ **1=Broad-Crested Rectangular Weir** ( Controls 0.00 cfs)
- ↳ **2=Sharp-Crested Vee/Trap Weir** (Weir Controls 0.27 cfs @ 2.15 fps)

**Pond WQS2: WQS 2**

Inflow Area = 0.663 ac, Inflow Depth > 0.90" for 2YR-NOAA event  
 Inflow = 0.27 cfs @ 12.43 hrs, Volume= 0.050 af  
 Outflow = 0.09 cfs @ 13.60 hrs, Volume= 0.042 af, Atten= 67%, Lag= 70.4 min  
 Primary = 0.09 cfs @ 13.60 hrs, Volume= 0.042 af

Routing by Stor-Ind method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Peak Elev= 168.94' @ 13.60 hrs Surf.Area= 938 sf Storage= 662 cf

Plug-Flow detention time= 271.2 min calculated for 0.042 af (85% of inflow)  
 Center-of-Mass det. time= 174.4 min ( 1,142.7 - 968.3 )

Volume	Invert	Avail.Storage	Storage Description
#1	168.00'	1,936 cf	<b>Custom Stage Data (Prismatic)</b> Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
168.00	473	0	0
169.50	1,216	1,267	1,267
170.00	1,461	669	1,936

Device	Routing	Invert	Outlet Devices
#1	Primary	169.50'	<b>16.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#2	Primary	168.50'	<b>30.0 deg Sharp-Crested Vee/Trap Weir</b> C= 2.61

**Primary OutFlow** Max=0.09 cfs @ 13.60 hrs HW=168.94' (Free Discharge)

- 1=Broad-Crested Rectangular Weir ( Controls 0.00 cfs)
- 2=Sharp-Crested Vee/Trap Weir (Weir Controls 0.09 cfs @ 1.73 fps)

**Link 1L: WETLANDS**

Inflow Area = 13.671 ac, Inflow Depth = 0.50" for 2YR-NOAA event  
 Inflow = 4.15 cfs @ 12.33 hrs, Volume= 0.568 af  
 Primary = 4.15 cfs @ 12.33 hrs, Volume= 0.568 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs

## **10 YR POST-DEVELOPMENT**

**Subcatchment 1S: 1S**

Runoff = 1.77 cfs @ 12.09 hrs, Volume= 0.128 af, Depth= 2.31"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
Type III 24-hr 10YR-NOAA Rainfall=5.26"

Area (sf)	CN	Description
8,143	98	Paved parking & roofs
20,718	61	>75% Grass cover, Good, HSG B
28,861	71	Weighted Average
20,718		Pervious Area
8,143		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.8	50	0.0280	0.17		<b>Sheet Flow,</b> Grass: Short n= 0.150 P2= 3.37"
0.2	15	0.0280	1.17		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.3	28	0.0910	1.51		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
0.2	16	0.1250	1.77		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
0.0	5	0.1250	2.47		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.0	5	0.0200	2.87		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	5	0.0200	0.99		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.4	89	0.0300	3.52		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	32	0.0460	4.35		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
6.1	245	Total			

**Subcatchment CB1: CB1**

Runoff = 0.60 cfs @ 12.30 hrs, Volume= 0.070 af, Depth= 1.38"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
Type III 24-hr 10YR-NOAA Rainfall=5.26"

Area (sf)	CN	Description
1,788	98	Paved parking & roofs
3,957	61	>75% Grass cover, Good, HSG B
20,562	55	Woods, Good, HSG B
26,307	59	Weighted Average
24,519		Pervious Area
1,788		Impervious Area

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Type III 24-hr 10YR-NOAA Rainfall=5.26"

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
12.0	50	0.0200	0.07		<b>Sheet Flow,</b> Woods: Light underbrush n= 0.400 P2= 3.37"
2.5	109	0.0210	0.72		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
2.8	160	0.0375	0.97		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
0.8	62	0.0678	1.30		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
0.1	12	0.1667	2.04		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
0.1	7	0.0200	0.99		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.0	5	0.0200	2.87		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	5	0.0200	0.99		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.5	86	0.0200	2.87		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	21	0.0100	4.91	3.86	<b>Circular Channel (pipe),</b> Diam= 12.0" Area= 0.8 sf Perim= 3.1' r= 0.25' n= 0.012 Concrete pipe, finished
19.0	517	Total			

**Subcatchment CB2: CB2**

Runoff = 0.52 cfs @ 12.12 hrs, Volume= 0.041 af, Depth= 2.57"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
Type III 24-hr 10YR-NOAA Rainfall=5.26"

Area (sf)	CN	Description
2,838	98	Paved parking & roofs
5,427	61	>75% Grass cover, Good, HSG B
8,265	74	Weighted Average
5,427		Pervious Area
2,838		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.2	50	0.0100	0.12		<b>Sheet Flow,</b> Grass: Short n= 0.150 P2= 3.37"
1.3	53	0.0100	0.70		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.1	10	0.0200	2.87		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.0	11	0.0190	6.77	5.32	<b>Circular Channel (pipe),</b> Diam= 12.0" Area= 0.8 sf Perim= 3.1' r= 0.25' n= 0.012 Concrete pipe, finished
8.6	124	Total			

**Subcatchment CB3: CB3**

Runoff = 1.52 cfs @ 12.20 hrs, Volume= 0.145 af, Depth= 1.91"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 10YR-NOAA Rainfall=5.26"

Area (sf)	CN	Description
6,010	98	Paved parking & roofs
28,667	61	>75% Grass cover, Good, HSG B
5,036	55	Woods, Good, HSG B
39,713	66	Weighted Average
33,703		Pervious Area
6,010		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.3	50	0.0380	0.09		<b>Sheet Flow,</b> Woods: Light underbrush n= 0.400 P2= 3.37"
1.2	77	0.0227	1.05		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
1.1	92	0.0435	1.46		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
1.1	66	0.0200	0.99		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.1	27	0.1850	3.01		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.3	25	0.0400	1.40		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.4	22	0.0220	1.04		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.0	5	0.0200	2.87		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	5	0.0200	0.99		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.2	24	0.0100	2.03		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	21	0.0100	4.91	3.86	<b>Circular Channel (pipe),</b> Diam= 12.0" Area= 0.8 sf Perim= 3.1' r= 0.25' n= 0.012 Concrete pipe, finished
13.9	414	Total			

**Subcatchment CB4: CB4**

Runoff = 3.12 cfs @ 12.09 hrs, Volume= 0.223 af, Depth= 2.40"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 10YR-NOAA Rainfall=5.26"

Area (sf)	CN	Description
14,187	98	Paved parking & roofs
34,440	61	>75% Grass cover, Good, HSG B
48,627	72	Weighted Average
34,440		Pervious Area
14,187		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.0	50	0.0440	0.21		<b>Sheet Flow,</b> Grass: Short n= 0.150 P2= 3.37"
0.5	64	0.0781	1.96		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.6	63	0.0645	1.78		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.5	46	0.0500	1.57		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.0	5	0.0200	2.87		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	5	0.0100	0.70		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.2	25	0.0100	2.03		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	21	0.0100	5.70	7.00	<b>Circular Channel (pipe),</b> Diam= 15.0" Area= 1.2 sf Perim= 3.9' r= 0.31' n= 0.012 Concrete pipe, finished
6.0	279	Total			

**Subcatchment CB5: CB5**

Runoff = 1.58 cfs @ 12.09 hrs, Volume= 0.112 af, Depth= 3.31"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
Type III 24-hr 10YR-NOAA Rainfall=5.26"

Area (sf)	CN	Description
9,299	98	Paved parking & roofs
6,735	61	>75% Grass cover, Good, HSG B
1,715	74	>75% Grass cover, Good, HSG C
17,749	82	Weighted Average
8,450		Pervious Area
9,299		Impervious Area

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Type III 24-hr 10YR-NOAA Rainfall=5.26"

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.9	5	0.0200	0.10		<b>Sheet Flow,</b> Grass: Short n= 0.150 P2= 3.37"
0.1	5	0.0200	0.78		<b>Sheet Flow,</b> Smooth surfaces n= 0.011 P2= 3.37"
0.9	5	0.0200	0.10		<b>Sheet Flow,</b> Grass: Short n= 0.150 P2= 3.37"
1.2	201	0.0200	2.87		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
2.9					<b>Direct Entry, MIN TC</b>
0.0	12	0.0100	4.91	3.86	<b>Circular Channel (pipe),</b> Diam= 12.0" Area= 0.8 sf Perim= 3.1' r= 0.25' n= 0.012 Concrete pipe, finished
6.0	228	Total			

**Subcatchment DA6: DA6-TO-WETLANDS**

Runoff = 12.51 cfs @ 12.29 hrs, Volume= 1.371 af, Depth= 1.91"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
Type III 24-hr 10YR-NOAA Rainfall=5.26"

Area (sf)	CN	Description
13,120	98	Paved parking & roofs
215,109	61	>75% Grass cover, Good, HSG B
102,048	74	>75% Grass cover, Good, HSG C
24,053	55	Woods, Good, HSG B
21,529	70	Woods, Good, HSG C
375,859	66	Weighted Average
362,739		Pervious Area
13,120		Impervious Area

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Type III 24-hr 10YR-NOAA Rainfall=5.26"

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	13	0.0340	0.07		<b>Sheet Flow,</b> Woods: Light underbrush n= 0.400 P2= 3.37"
3.5	37	0.0340	0.18		<b>Sheet Flow,</b> Grass: Short n= 0.150 P2= 3.37"
1.8	101	0.0180	0.94		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.8	61	0.0330	1.27		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
4.3	357	0.0400	1.40		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
5.6	225	0.0090	0.66		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.2	17	0.0400	1.40		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.5	32	0.0400	1.00		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
20.0	843	Total			

**Subcatchment P1: P1**

Runoff = 3.59 cfs @ 12.09 hrs, Volume= 0.255 af, Depth= 2.66"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
Type III 24-hr 10YR-NOAA Rainfall=5.26"

Area (sf)	CN	Description
5,726	98	Paved parking & roofs
30,929	61	>75% Grass cover, Good, HSG B
155	74	>75% Grass cover, Good, HSG C
13,301	98	POND
50,111	75	Weighted Average
31,084		Pervious Area
19,027		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.7	50	0.0300	0.18		<b>Sheet Flow,</b> Grass: Short n= 0.150 P2= 3.37"
0.2	16	0.0300	1.21		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.4	40	0.0500	1.57		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.7	58	0.0340	1.29		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
6.0	164	Total			

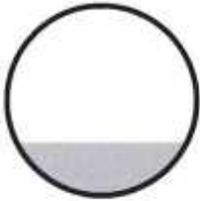
**Reach 1R: DMH1-DMH2**

Inflow Area = 0.794 ac, Inflow Depth = 1.67" for 10YR-NOAA event  
 Inflow = 0.93 cfs @ 12.20 hrs, Volume= 0.110 af  
 Outflow = 0.93 cfs @ 12.24 hrs, Volume= 0.110 af, Atten= 0%, Lag= 2.5 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 3.30 fps, Min. Travel Time= 1.2 min  
 Avg. Velocity = 1.34 fps, Avg. Travel Time= 3.1 min

Peak Storage= 69 cf @ 12.22 hrs, Average Depth at Peak Storage= 0.35'  
 Bank-Full Depth= 1.25', Capacity at Bank-Full= 5.43 cfs

15.0" Diameter Pipe, n= 0.012 Concrete pipe, finished  
 Length= 246.0' Slope= 0.0060 '/  
 Inlet Invert= 173.97', Outlet Invert= 172.49'



**Reach 2R: DMH3-DMH2**

Inflow Area = 2.435 ac, Inflow Depth = 2.37" for 10YR-NOAA event  
 Inflow = 5.78 cfs @ 12.10 hrs, Volume= 0.481 af  
 Outflow = 5.77 cfs @ 12.11 hrs, Volume= 0.481 af, Atten= 0%, Lag= 0.1 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 6.38 fps, Min. Travel Time= 0.0 min  
 Avg. Velocity = 2.22 fps, Avg. Travel Time= 0.1 min

Peak Storage= 14 cf @ 12.11 hrs, Average Depth at Peak Storage= 0.66'  
 Bank-Full Depth= 2.00', Capacity at Bank-Full= 24.51 cfs

24.0" Diameter Pipe, n= 0.012 Concrete pipe, finished  
 Length= 16.0' Slope= 0.0100 '/  
 Inlet Invert= 172.00', Outlet Invert= 171.84'



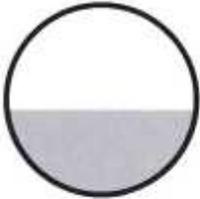
**Reach 3R: DMH4-DMH3**

Inflow Area = 1.524 ac, Inflow Depth = 2.64" for 10YR-NOAA event  
Inflow = 4.70 cfs @ 12.09 hrs, Volume= 0.336 af  
Outflow = 4.69 cfs @ 12.09 hrs, Volume= 0.336 af, Atten= 0%, Lag= 0.3 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
Max. Velocity= 6.13 fps, Min. Travel Time= 0.2 min  
Avg. Velocity = 2.10 fps, Avg. Travel Time= 0.5 min

Peak Storage= 46 cf @ 12.09 hrs, Average Depth at Peak Storage= 0.67'  
Bank-Full Depth= 1.50', Capacity at Bank-Full= 11.38 cfs

18.0" Diameter Pipe, n= 0.012 Concrete pipe, finished  
Length= 60.0' Slope= 0.0100 '/  
Inlet Invert= 173.10', Outlet Invert= 172.50'



**Reach 4R: DMH2-DMH5**

Inflow Area = 3.229 ac, Inflow Depth = 2.20" for 10YR-NOAA event  
Inflow = 6.45 cfs @ 12.11 hrs, Volume= 0.591 af  
Outflow = 6.44 cfs @ 12.12 hrs, Volume= 0.591 af, Atten= 0%, Lag= 0.3 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
Max. Velocity= 6.04 fps, Min. Travel Time= 0.1 min  
Avg. Velocity = 2.13 fps, Avg. Travel Time= 0.4 min

Peak Storage= 56 cf @ 12.12 hrs, Average Depth at Peak Storage= 0.74'  
Bank-Full Depth= 2.00', Capacity at Bank-Full= 21.82 cfs

24.0" Diameter Pipe, n= 0.012  
Length= 53.0' Slope= 0.0079 '/  
Inlet Invert= 171.74', Outlet Invert= 171.32'



**Reach 5R: DMH5-FES**

Inflow Area = 3.229 ac, Inflow Depth = 2.20" for 10YR-NOAA event  
 Inflow = 6.44 cfs @ 12.12 hrs, Volume= 0.591 af  
 Outflow = 6.43 cfs @ 12.12 hrs, Volume= 0.591 af, Atten= 0%, Lag= 0.4 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 6.08 fps, Min. Travel Time= 0.2 min  
 Avg. Velocity = 2.14 fps, Avg. Travel Time= 0.6 min

Peak Storage= 82 cf @ 12.12 hrs, Average Depth at Peak Storage= 0.74'  
 Bank-Full Depth= 2.00', Capacity at Bank-Full= 21.99 cfs

24.0" Diameter Pipe, n= 0.012  
 Length= 77.0' Slope= 0.0081 1/  
 Inlet Invert= 171.22', Outlet Invert= 170.60'



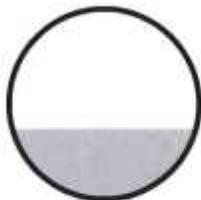
**Reach 6R: FES-HW**

Inflow Area = 3.229 ac, Inflow Depth = 2.20" for 10YR-NOAA event  
 Inflow = 6.43 cfs @ 12.12 hrs, Volume= 0.591 af  
 Outflow = 6.42 cfs @ 12.13 hrs, Volume= 0.591 af, Atten= 0%, Lag= 0.2 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 6.05 fps, Min. Travel Time= 0.1 min  
 Avg. Velocity = 2.13 fps, Avg. Travel Time= 0.4 min

Peak Storage= 52 cf @ 12.13 hrs, Average Depth at Peak Storage= 0.74'  
 Bank-Full Depth= 2.00', Capacity at Bank-Full= 21.86 cfs

24.0" Diameter Pipe, n= 0.012  
 Length= 49.0' Slope= 0.0080 1/  
 Inlet Invert= 171.19', Outlet Invert= 170.80'



**Reach 7R: OCS-HW**

Inflow Area = 4.380 ac, Inflow Depth = 1.00" for 10YR-NOAA event  
 Inflow = 0.56 cfs @ 14.88 hrs, Volume= 0.364 af  
 Outflow = 0.56 cfs @ 14.89 hrs, Volume= 0.364 af, Atten= 0%, Lag= 0.2 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 4.27 fps, Min. Travel Time= 0.1 min  
 Avg. Velocity = 3.14 fps, Avg. Travel Time= 0.1 min

Peak Storage= 4 cf @ 14.88 hrs, Average Depth at Peak Storage= 0.19'  
 Bank-Full Depth= 1.50', Capacity at Bank-Full= 16.09 cfs

18.0" Diameter Pipe, n= 0.012 Concrete pipe, finished  
 Length= 28.0' Slope= 0.0200 '/  
 Inlet Invert= 169.50', Outlet Invert= 168.94'



**Pond 1P: POND 1**

Inflow Area = 4.380 ac, Inflow Depth = 2.32" for 10YR-NOAA event  
 Inflow = 9.80 cfs @ 12.11 hrs, Volume= 0.846 af  
 Outflow = 0.67 cfs @ 14.88 hrs, Volume= 0.846 af, Atten= 93%, Lag= 166.3 min  
 Discarded = 0.11 cfs @ 14.88 hrs, Volume= 0.482 af  
 Primary = 0.56 cfs @ 14.88 hrs, Volume= 0.364 af

Routing by Stor-Ind method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Peak Elev= 171.63' @ 14.88 hrs Surf.Area= 11,834 sf Storage= 21,487 cf

Plug-Flow detention time= 996.5 min calculated for 0.846 af (100% of inflow)  
 Center-of-Mass det. time= 996.5 min ( 1,840.0 - 843.5 )

Volume	Invert	Avail.Storage	Storage Description
#1	169.50'	46,583 cf	<b>Custom Stage Data (Prismatic)</b> Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
169.50	8,348	0	0
170.00	9,140	4,372	4,372
172.00	12,442	21,582	25,954
173.50	15,063	20,629	46,583

Device	Routing	Invert	Outlet Devices
#1	Primary	169.50'	<b>18.0" x 28.0' long Culvert</b> RCP, square edge headwall, Ke= 0.500 Outlet Invert= 168.94' S= 0.0200 '/ Cc= 0.900 n= 0.012 Concrete pipe, finished
#2	Device 1	171.00'	<b>3.0" Vert. Orifice/Grate X 2.00</b> C= 0.600
#3	Device 1	171.10'	<b>3.0" Vert. Orifice/Grate</b> C= 0.600
#4	Device 1	171.50'	<b>12.0" Vert. Orifice/Grate</b> C= 0.600
#5	Device 1	172.35'	<b>4.00' x 4.00' Horiz. Orifice/Grate</b> Limited to weir flow C= 0.600
#6	Discarded	0.00'	<b>0.390 in/hr Exfiltration over Surface area</b>

**Discarded OutFlow** Max=0.11 cfs @ 14.88 hrs HW=171.63' (Free Discharge)

↳ **6=Exfiltration** (Exfiltration Controls 0.11 cfs)

**Primary OutFlow** Max=0.56 cfs @ 14.88 hrs HW=171.63' (Free Discharge)

↳ **1=Culvert** (Passes 0.56 cfs of 10.00 cfs potential flow)

↳ **2=Orifice/Grate** (Orifice Controls 0.34 cfs @ 3.43 fps)

↳ **3=Orifice/Grate** (Orifice Controls 0.15 cfs @ 3.07 fps)

↳ **4=Orifice/Grate** (Orifice Controls 0.08 cfs @ 1.24 fps)

↳ **5=Orifice/Grate** ( Controls 0.00 cfs)

**Pond WQS1: WQS 1**

Inflow Area = 0.663 ac, Inflow Depth = 2.31" for 10YR-NOAA event

Inflow = 1.77 cfs @ 12.09 hrs, Volume= 0.128 af

Outflow = 1.63 cfs @ 12.13 hrs, Volume= 0.123 af, Atten= 8%, Lag= 2.1 min

Primary = 1.63 cfs @ 12.13 hrs, Volume= 0.123 af

Routing by Stor-Ind method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs

Peak Elev= 170.08' @ 12.13 hrs Surf.Area= 1,033 sf Storage= 1,045 cf

Plug-Flow detention time= 74.6 min calculated for 0.123 af (96% of inflow)

Center-of-Mass det. time= 54.1 min ( 896.6 - 842.5 )

Volume	Invert	Avail.Storage	Storage Description
#1	168.50'	2,110 cf	<b>Custom Stage Data (Prismatic)</b> Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
168.50	276	0	0
170.00	1,013	967	967
171.00	1,273	1,143	2,110

Device	Routing	Invert	Outlet Devices
#1	Primary	170.00'	<b>13.5' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#2	Primary	169.00'	<b>30.0 deg Sharp-Crested Vee/Trap Weir</b> C= 2.61

**Primary OutFlow** Max=1.63 cfs @ 12.13 hrs HW=170.08' (Free Discharge)

↳ **1=Broad-Crested Rectangular Weir** (Weir Controls 0.79 cfs @ 0.77 fps)

↳ **2=Sharp-Crested Vee/Trap Weir** (Weir Controls 0.84 cfs @ 2.71 fps)

**Pond WQS2: WQS 2**

Inflow Area = 0.663 ac, Inflow Depth = 2.23" for 10YR-NOAA event  
 Inflow = 1.63 cfs @ 12.13 hrs, Volume= 0.123 af  
 Outflow = 0.62 cfs @ 12.50 hrs, Volume= 0.116 af, Atten= 62%, Lag= 22.6 min  
 Primary = 0.62 cfs @ 12.50 hrs, Volume= 0.116 af

Routing by Stor-Ind method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Peak Elev= 169.46' @ 12.50 hrs Surf.Area= 1,194 sf Storage= 1,213 cf

Plug-Flow detention time= 123.8 min calculated for 0.116 af (94% of inflow)  
 Center-of-Mass det. time= 80.7 min ( 977.4 - 896.6 )

Volume	Invert	Avail.Storage	Storage Description
#1	168.00'	1,936 cf	<b>Custom Stage Data (Prismatic)</b> Listed below (Recalc)
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
168.00	473	0	0
169.50	1,216	1,267	1,267
170.00	1,461	669	1,936

Device	Routing	Invert	Outlet Devices
#1	Primary	169.50'	<b>16.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#2	Primary	168.50'	<b>30.0 deg Sharp-Crested Vee/Trap Weir</b> C= 2.61

**Primary OutFlow** Max=0.62 cfs @ 12.50 hrs HW=169.46' (Free Discharge)

- └1=Broad-Crested Rectangular Weir ( Controls 0.00 cfs)
- └2=Sharp-Crested Vee/Trap Weir (Weir Controls 0.62 cfs @ 2.55 fps)

**Link 1L: WETLANDS**

Inflow Area = 13.671 ac, Inflow Depth = 1.63" for 10YR-NOAA event  
 Inflow = 12.98 cfs @ 12.29 hrs, Volume= 1.851 af  
 Primary = 12.98 cfs @ 12.29 hrs, Volume= 1.851 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs

## 100 YR POST-DEVELOPMENT

**Subcatchment 1S: 1S**

Runoff = 3.72 cfs @ 12.09 hrs, Volume= 0.265 af, Depth= 4.81"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
Type III 24-hr 100YR-NOAA Rainfall=8.26"

Area (sf)	CN	Description
8,143	98	Paved parking & roofs
20,718	61	>75% Grass cover, Good, HSG B
28,861	71	Weighted Average
20,718		Pervious Area
8,143		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.8	50	0.0280	0.17		<b>Sheet Flow,</b> Grass: Short n= 0.150 P2= 3.37"
0.2	15	0.0280	1.17		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.3	28	0.0910	1.51		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
0.2	16	0.1250	1.77		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
0.0	5	0.1250	2.47		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.0	5	0.0200	2.87		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	5	0.0200	0.99		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.4	89	0.0300	3.52		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	32	0.0460	4.35		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
6.1	245	Total			

**Subcatchment CB1: CB1**

Runoff = 1.63 cfs @ 12.27 hrs, Volume= 0.172 af, Depth= 3.42"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
Type III 24-hr 100YR-NOAA Rainfall=8.26"

Area (sf)	CN	Description
1,788	98	Paved parking & roofs
3,957	61	>75% Grass cover, Good, HSG B
20,562	55	Woods, Good, HSG B
26,307	59	Weighted Average
24,519		Pervious Area
1,788		Impervious Area

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Type III 24-hr 100YR-NOAA Rainfall=8.26"

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
12.0	50	0.0200	0.07		<b>Sheet Flow,</b> Woods: Light underbrush n= 0.400 P2= 3.37"
2.5	109	0.0210	0.72		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
2.8	160	0.0375	0.97		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
0.8	62	0.0678	1.30		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
0.1	12	0.1667	2.04		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
0.1	7	0.0200	0.99		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.0	5	0.0200	2.87		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	5	0.0200	0.99		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.5	86	0.0200	2.87		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	21	0.0100	4.91	3.86	<b>Circular Channel (pipe),</b> Diam= 12.0" Area= 0.8 sf Perim= 3.1' r= 0.25' n= 0.012 Concrete pipe, finished
19.0	517	Total			

**Subcatchment CB2: CB2**

Runoff = 1.05 cfs @ 12.12 hrs, Volume= 0.082 af, Depth= 5.16"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
Type III 24-hr 100YR-NOAA Rainfall=8.26"

Area (sf)	CN	Description
2,838	98	Paved parking & roofs
5,427	61	>75% Grass cover, Good, HSG B
8,265	74	Weighted Average
5,427		Pervious Area
2,838		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.2	50	0.0100	0.12		<b>Sheet Flow,</b> Grass: Short n= 0.150 P2= 3.37"
1.3	53	0.0100	0.70		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.1	10	0.0200	2.87		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.0	11	0.0190	6.77	5.32	<b>Circular Channel (pipe),</b> Diam= 12.0" Area= 0.8 sf Perim= 3.1' r= 0.25' n= 0.012 Concrete pipe, finished
8.6	124	Total			

**Subcatchment CB3: CB3**

Runoff = 3.51 cfs @ 12.19 hrs, Volume= 0.321 af, Depth= 4.22"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100YR-NOAA Rainfall=8.26"

Area (sf)	CN	Description
6,010	98	Paved parking & roofs
28,667	61	>75% Grass cover, Good, HSG B
5,036	55	Woods, Good, HSG B
39,713	66	Weighted Average
33,703		Pervious Area
6,010		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
9.3	50	0.0380	0.09		<b>Sheet Flow,</b> Woods: Light underbrush n= 0.400 P2= 3.37"
1.2	77	0.0227	1.05		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
1.1	92	0.0435	1.46		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
1.1	66	0.0200	0.99		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.1	27	0.1850	3.01		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.3	25	0.0400	1.40		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.4	22	0.0220	1.04		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.0	5	0.0200	2.87		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	5	0.0200	0.99		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.2	24	0.0100	2.03		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	21	0.0100	4.91	3.86	<b>Circular Channel (pipe),</b> Diam= 12.0" Area= 0.8 sf Perim= 3.1' r= 0.25' n= 0.012 Concrete pipe, finished
13.9	414	Total			

**Subcatchment CB4: CB4**

Runoff = 6.44 cfs @ 12.09 hrs, Volume= 0.458 af, Depth= 4.92"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Type III 24-hr 100YR-NOAA Rainfall=8.26"

Area (sf)	CN	Description
14,187	98	Paved parking & roofs
34,440	61	>75% Grass cover, Good, HSG B
48,627	72	Weighted Average
34,440		Pervious Area
14,187		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.0	50	0.0440	0.21		<b>Sheet Flow,</b> Grass: Short n= 0.150 P2= 3.37"
0.5	64	0.0781	1.96		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.6	63	0.0645	1.78		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.5	46	0.0500	1.57		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.0	5	0.0200	2.87		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	5	0.0100	0.70		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.2	25	0.0100	2.03		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
0.1	21	0.0100	5.70	7.00	<b>Circular Channel (pipe),</b> Diam= 15.0" Area= 1.2 sf Perim= 3.9' r= 0.31' n= 0.012 Concrete pipe, finished
6.0	279	Total			

**Subcatchment CB5: CB5**

Runoff = 2.85 cfs @ 12.09 hrs, Volume= 0.207 af, Depth= 6.11"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
Type III 24-hr 100YR-NOAA Rainfall=8.26"

Area (sf)	CN	Description
9,299	98	Paved parking & roofs
6,735	61	>75% Grass cover, Good, HSG B
1,715	74	>75% Grass cover, Good, HSG C
17,749	82	Weighted Average
8,450		Pervious Area
9,299		Impervious Area

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Type III 24-hr 100YR-NOAA Rainfall=8.26"

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.9	5	0.0200	0.10		<b>Sheet Flow,</b> Grass: Short n= 0.150 P2= 3.37"
0.1	5	0.0200	0.78		<b>Sheet Flow,</b> Smooth surfaces n= 0.011 P2= 3.37"
0.9	5	0.0200	0.10		<b>Sheet Flow,</b> Grass: Short n= 0.150 P2= 3.37"
1.2	201	0.0200	2.87		<b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps
2.9					<b>Direct Entry, MIN TC</b>
0.0	12	0.0100	4.91	3.86	<b>Circular Channel (pipe),</b> Diam= 12.0" Area= 0.8 sf Perim= 3.1' r= 0.25' n= 0.012 Concrete pipe, finished
6.0	228	Total			

**Subcatchment DA6: DA6-TO-WETLANDS**

Runoff = 28.72 cfs @ 12.28 hrs, Volume= 3.036 af, Depth= 4.22"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
Type III 24-hr 100YR-NOAA Rainfall=8.26"

Area (sf)	CN	Description
13,120	98	Paved parking & roofs
215,109	61	>75% Grass cover, Good, HSG B
102,048	74	>75% Grass cover, Good, HSG C
24,053	55	Woods, Good, HSG B
21,529	70	Woods, Good, HSG C
375,859	66	Weighted Average
362,739		Pervious Area
13,120		Impervious Area

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Type III 24-hr 100YR-NOAA Rainfall=8.26"

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.3	13	0.0340	0.07		<b>Sheet Flow,</b> Woods: Light underbrush n= 0.400 P2= 3.37"
3.5	37	0.0340	0.18		<b>Sheet Flow,</b> Grass: Short n= 0.150 P2= 3.37"
1.8	101	0.0180	0.94		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.8	61	0.0330	1.27		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
4.3	357	0.0400	1.40		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
5.6	225	0.0090	0.66		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.2	17	0.0400	1.40		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.5	32	0.0400	1.00		<b>Shallow Concentrated Flow,</b> Woodland Kv= 5.0 fps
20.0	843	Total			

**Subcatchment P1: P1**

Runoff = 7.08 cfs @ 12.09 hrs, Volume= 0.506 af, Depth= 5.28"

Runoff by SCS TR-20 method, UH=SCS, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
Type III 24-hr 100YR-NOAA Rainfall=8.26"

Area (sf)	CN	Description
5,726	98	Paved parking & roofs
30,929	61	>75% Grass cover, Good, HSG B
155	74	>75% Grass cover, Good, HSG C
13,301	98	POND
50,111	75	Weighted Average
31,084		Pervious Area
19,027		Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.7	50	0.0300	0.18		<b>Sheet Flow,</b> Grass: Short n= 0.150 P2= 3.37"
0.2	16	0.0300	1.21		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.4	40	0.0500	1.57		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
0.7	58	0.0340	1.29		<b>Shallow Concentrated Flow,</b> Short Grass Pasture Kv= 7.0 fps
6.0	164	Total			

**Reach 1R: DMH1-DMH2**

Inflow Area = 0.794 ac, Inflow Depth = 3.83" for 100YR-NOAA event  
 Inflow = 2.30 cfs @ 12.22 hrs, Volume= 0.253 af  
 Outflow = 2.30 cfs @ 12.24 hrs, Volume= 0.253 af, Atten= 0%, Lag= 1.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 4.24 fps, Min. Travel Time= 1.0 min  
 Avg. Velocity = 1.60 fps, Avg. Travel Time= 2.6 min

Peak Storage= 133 cf @ 12.22 hrs, Average Depth at Peak Storage= 0.57'  
 Bank-Full Depth= 1.25', Capacity at Bank-Full= 5.43 cfs

15.0" Diameter Pipe, n= 0.012 Concrete pipe, finished  
 Length= 246.0' Slope= 0.0060 1/  
 Inlet Invert= 173.97', Outlet Invert= 172.49'

**Reach 2R: DMH3-DMH2**

Inflow Area = 2.435 ac, Inflow Depth = 4.86" for 100YR-NOAA event  
 Inflow = 11.88 cfs @ 12.10 hrs, Volume= 0.986 af  
 Outflow = 11.88 cfs @ 12.10 hrs, Volume= 0.986 af, Atten= 0%, Lag= 0.1 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 7.74 fps, Min. Travel Time= 0.0 min  
 Avg. Velocity = 2.61 fps, Avg. Travel Time= 0.1 min

Peak Storage= 25 cf @ 12.10 hrs, Average Depth at Peak Storage= 0.98'  
 Bank-Full Depth= 2.00', Capacity at Bank-Full= 24.51 cfs

24.0" Diameter Pipe, n= 0.012 Concrete pipe, finished  
 Length= 16.0' Slope= 0.0100 1/  
 Inlet Invert= 172.00', Outlet Invert= 171.84'



**Reach 3R: DMH4-DMH3**

Inflow Area = 1.524 ac, Inflow Depth = 5.24" for 100YR-NOAA event  
 Inflow = 9.28 cfs @ 12.09 hrs, Volume= 0.665 af  
 Outflow = 9.27 cfs @ 12.09 hrs, Volume= 0.665 af, Atten= 0%, Lag= 0.3 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 7.18 fps, Min. Travel Time= 0.1 min  
 Avg. Velocity = 2.45 fps, Avg. Travel Time= 0.4 min

Peak Storage= 78 cf @ 12.09 hrs, Average Depth at Peak Storage= 1.03'  
 Bank-Full Depth= 1.50', Capacity at Bank-Full= 11.38 cfs

18.0" Diameter Pipe, n= 0.012 Concrete pipe, finished  
 Length= 60.0' Slope= 0.0100 '/'  
 Inlet Invert= 173.10', Outlet Invert= 172.50'



**Reach 4R: DMH2-DMH5**

Inflow Area = 3.229 ac, Inflow Depth = 4.61" for 100YR-NOAA event  
 Inflow = 13.63 cfs @ 12.11 hrs, Volume= 1.240 af  
 Outflow = 13.62 cfs @ 12.11 hrs, Volume= 1.240 af, Atten= 0%, Lag= 0.2 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 7.33 fps, Min. Travel Time= 0.1 min  
 Avg. Velocity = 2.51 fps, Avg. Travel Time= 0.4 min

Peak Storage= 99 cf @ 12.11 hrs, Average Depth at Peak Storage= 1.15'  
 Bank-Full Depth= 2.00', Capacity at Bank-Full= 21.82 cfs

24.0" Diameter Pipe, n= 0.012  
 Length= 53.0' Slope= 0.0079 '/'  
 Inlet Invert= 171.74', Outlet Invert= 171.32'



**Reach 5R: DMH5-FES**

Inflow Area = 3.229 ac, Inflow Depth = 4.61" for 100YR-NOAA event  
 Inflow = 13.62 cfs @ 12.11 hrs, Volume= 1.240 af  
 Outflow = 13.61 cfs @ 12.12 hrs, Volume= 1.240 af, Atten= 0%, Lag= 0.3 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 7.37 fps, Min. Travel Time= 0.2 min  
 Avg. Velocity = 2.52 fps, Avg. Travel Time= 0.5 min

Peak Storage= 142 cf @ 12.12 hrs, Average Depth at Peak Storage= 1.14'  
 Bank-Full Depth= 2.00', Capacity at Bank-Full= 21.99 cfs

24.0" Diameter Pipe, n= 0.012  
 Length= 77.0' Slope= 0.0081 '/  
 Inlet Invert= 171.22', Outlet Invert= 170.60'



**Reach 6R: FES-HW**

Inflow Area = 3.229 ac, Inflow Depth = 4.61" for 100YR-NOAA event  
 Inflow = 13.61 cfs @ 12.12 hrs, Volume= 1.240 af  
 Outflow = 13.60 cfs @ 12.12 hrs, Volume= 1.240 af, Atten= 0%, Lag= 0.2 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 7.34 fps, Min. Travel Time= 0.1 min  
 Avg. Velocity = 2.51 fps, Avg. Travel Time= 0.3 min

Peak Storage= 91 cf @ 12.12 hrs, Average Depth at Peak Storage= 1.14'  
 Bank-Full Depth= 2.00', Capacity at Bank-Full= 21.86 cfs

24.0" Diameter Pipe, n= 0.012  
 Length= 49.0' Slope= 0.0080 '/  
 Inlet Invert= 171.19', Outlet Invert= 170.80'



**Reach 7R: OCS-HW**

Inflow Area = 4.380 ac, Inflow Depth = 3.37" for 100YR-NOAA event  
 Inflow = 7.68 cfs @ 12.48 hrs, Volume= 1.232 af  
 Outflow = 7.68 cfs @ 12.48 hrs, Volume= 1.232 af, Atten= 0%, Lag= 0.1 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Max. Velocity= 9.00 fps, Min. Travel Time= 0.1 min  
 Avg. Velocity = 3.98 fps, Avg. Travel Time= 0.1 min

Peak Storage= 24 cf @ 12.48 hrs, Average Depth at Peak Storage= 0.73'  
 Bank-Full Depth= 1.50', Capacity at Bank-Full= 16.09 cfs

18.0" Diameter Pipe, n= 0.012 Concrete pipe, finished  
 Length= 28.0' Slope= 0.0200 '/'  
 Inlet Invert= 169.50', Outlet Invert= 168.94'



**Pond 1P: POND 1**

Inflow Area = 4.380 ac, Inflow Depth = 4.78" for 100YR-NOAA event  
 Inflow = 20.30 cfs @ 12.11 hrs, Volume= 1.745 af  
 Outflow = 7.80 cfs @ 12.48 hrs, Volume= 1.745 af, Atten= 62%, Lag= 22.2 min  
 Discarded = 0.12 cfs @ 12.48 hrs, Volume= 0.514 af  
 Primary = 7.68 cfs @ 12.48 hrs, Volume= 1.232 af

Routing by Stor-Ind method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Peak Elev= 172.53' @ 12.48 hrs Surf.Area= 13,372 sf Storage= 32,825 cf

Plug-Flow detention time= 553.2 min calculated for 1.745 af (100% of inflow)  
 Center-of-Mass det. time= 553.4 min ( 1,377.0 - 823.6 )

Volume	Invert	Avail.Storage	Storage Description
#1	169.50'	46,583 cf	<b>Custom Stage Data (Prismatic)</b> Listed below (Recalc)
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
169.50	8,348	0	0
170.00	9,140	4,372	4,372
172.00	12,442	21,582	25,954
173.50	15,063	20,629	46,583

Device	Routing	Invert	Outlet Devices
#1	Primary	169.50'	<b>18.0" x 28.0' long Culvert</b> RCP, square edge headwall, Ke= 0.500 Outlet Invert= 168.94' S= 0.0200 ' Cc= 0.900 n= 0.012 Concrete pipe, finished
#2	Device 1	171.00'	<b>3.0" Vert. Orifice/Grate X 2.00</b> C= 0.600
#3	Device 1	171.10'	<b>3.0" Vert. Orifice/Grate</b> C= 0.600
#4	Device 1	171.50'	<b>12.0" Vert. Orifice/Grate</b> C= 0.600
#5	Device 1	172.35'	<b>4.00' x 4.00' Horiz. Orifice/Grate</b> Limited to weir flow C= 0.600
#6	Discarded	0.00'	<b>0.390 in/hr Exfiltration over Surface area</b>

**Discarded OutFlow** Max=0.12 cfs @ 12.48 hrs HW=172.53' (Free Discharge)

↳ **6=Exfiltration** (Exfiltration Controls 0.12 cfs)

**Primary OutFlow** Max=7.66 cfs @ 12.48 hrs HW=172.53' (Free Discharge)

- ↳ **1=Culvert** (Passes 7.66 cfs of 12.85 cfs potential flow)
- ↳ **2=Orifice/Grate** (Orifice Controls 0.56 cfs @ 5.71 fps)
- ↳ **3=Orifice/Grate** (Orifice Controls 0.27 cfs @ 5.51 fps)
- ↳ **4=Orifice/Grate** (Orifice Controls 2.76 cfs @ 3.51 fps)
- ↳ **5=Orifice/Grate** (Weir Controls 4.07 cfs @ 1.40 fps)

### Pond WQS1: WQS 1

Inflow Area = 0.663 ac, Inflow Depth = 4.81" for 100YR-NOAA event  
 Inflow = 3.72 cfs @ 12.09 hrs, Volume= 0.265 af  
 Outflow = 3.68 cfs @ 12.10 hrs, Volume= 0.261 af, Atten= 1%, Lag= 0.7 min  
 Primary = 3.68 cfs @ 12.10 hrs, Volume= 0.261 af

Routing by Stor-Ind method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Peak Elev= 170.17' @ 12.10 hrs Surf.Area= 1,057 sf Storage= 1,142 cf

Plug-Flow detention time= 45.5 min calculated for 0.261 af (98% of inflow)  
 Center-of-Mass det. time= 34.9 min ( 856.3 - 821.4 )

Volume	Invert	Avail.Storage	Storage Description
#1	168.50'	2,110 cf	<b>Custom Stage Data (Prismatic)</b> Listed below (Recalc)
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
168.50	276	0	0
170.00	1,013	967	967
171.00	1,273	1,143	2,110

Device	Routing	Invert	Outlet Devices
#1	Primary	170.00'	<b>13.5' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#2	Primary	169.00'	<b>30.0 deg Sharp-Crested Vee/Trap Weir</b> C= 2.61

**Primary OutFlow** Max=3.67 cfs @ 12.10 hrs HW=170.17' (Free Discharge)

- ↳ **1=Broad-Crested Rectangular Weir** (Weir Controls 2.64 cfs @ 1.15 fps)
- ↳ **2=Sharp-Crested Vee/Trap Weir** (Weir Controls 1.03 cfs @ 2.82 fps)

**Pond WQS2: WQS 2**

Inflow Area = 0.663 ac, Inflow Depth = 4.72" for 100YR-NOAA event  
 Inflow = 3.68 cfs @ 12.10 hrs, Volume= 0.261 af  
 Outflow = 3.64 cfs @ 12.11 hrs, Volume= 0.253 af, Atten= 1%, Lag= 0.8 min  
 Primary = 3.64 cfs @ 12.11 hrs, Volume= 0.253 af

Routing by Stor-Ind method, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs  
 Peak Elev= 169.65' @ 12.11 hrs Surf.Area= 1,290 sf Storage= 1,456 cf

Plug-Flow detention time= 68.2 min calculated for 0.253 af (97% of inflow)  
 Center-of-Mass det. time= 46.3 min ( 902.6 - 856.3 )

Volume	Invert	Avail.Storage	Storage Description
#1	168.00'	1,936 cf	<b>Custom Stage Data (Prismatic)</b> Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
168.00	473	0	0
169.50	1,216	1,267	1,267
170.00	1,461	669	1,936

Device	Routing	Invert	Outlet Devices
#1	Primary	169.50'	<b>16.0' long x 0.5' breadth Broad-Crested Rectangular Weir</b> Head (feet) 0.20 0.40 0.60 0.80 1.00 Coef. (English) 2.80 2.92 3.08 3.30 3.32
#2	Primary	168.50'	<b>30.0 deg Sharp-Crested Vee/Trap Weir</b> C= 2.61

**Primary OutFlow** Max=3.63 cfs @ 12.11 hrs HW=169.65' (Free Discharge)  
 1=Broad-Crested Rectangular Weir (Weir Controls 2.63 cfs @ 1.09 fps)  
 2=Sharp-Crested Vee/Trap Weir (Weir Controls 0.99 cfs @ 2.80 fps)

**Link 1L: WETLANDS**

Inflow Area = 13.671 ac, Inflow Depth = 3.97" for 100YR-NOAA event  
 Inflow = 33.52 cfs @ 12.35 hrs, Volume= 4.521 af  
 Primary = 33.52 cfs @ 12.35 hrs, Volume= 4.521 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-96.00 hrs, dt= 0.01 hrs

## **APPENDIX E**

## De Minimus Storm-water Discharge Calculation

### Impervious Areas

To Deep Sump Hooded Catch Basins, Sediment Forebay and Pond 1 – 34,122 sq. ft.

To Sediment Forebay and Water Quality Swales – 8,143 sq. ft.

### TSS Removal

To Ponds 1 - 85%

To Sediment Forebay and Water Quality Swales 78%

Pond 1 –  $34,122 \times .85 = 29,004$

To Sediment Forebay and Water Quality Swales –  $8,143 \times .78 = 6,352$

$29,004 + 6,352 = 35,356$

$34,122 + 8,143 = 42,265$

35,356

$42,268 = 83.6\%$  which is greater than 80%

*Pre-treatment - To Pond 1*

v

**INSTRUCTIONS:**

1. In BMP Column, click on Blue Cell to Activate Drop Down Menu
2. Select BMP from Drop Down Menu
3. After BMP is selected, TSS Removal and other Columns are automatically completed.

Version 1, Automated: Mar. 4, 2008

Location:

BMP <sup>1</sup>	C TSS Removal Rate <sup>1</sup>	D Starting TSS Load*	E Amount Removed (C*D)	F Remaining Load (D-E)
Sediment Forebay	0.25	1.00	0.25	0.75
	0.00	0.75	0.00	0.75
	0.00	0.75	0.00	0.75
	0.00	0.75	0.00	0.75
	0.00	0.75	0.00	0.75

Separate Form Needs to be Completed for Each Outlet or BMP Train

**Total TSS Removal =**

Project:   
 Prepared By:   
 Date:

\*Equals remaining load from previous BMP (E) which enters the BMP

Non-automated TSS Calculation Sheet must be used if Proprietary BMP Proposed  
 1. From MassDEP Stormwater Handbook Vol. 1

**INSTRUCTIONS:**

1. In BMP Column, click on Blue Cell to Activate Drop Down Menu
2. Select BMP from Drop Down Menu
3. After BMP is selected, TSS Removal and other Columns are automatically completed.

Version 1, Automated: Mar. 4, 2008

Location:

B	C	D	E	F
BMP <sup>1</sup>	TSS Removal Rate <sup>1</sup>	Starting TSS Load*	Amount Removed (C*D)	Remaining Load (D-E)
Deep Sump and Hooded Catch Basin	0.25	1.00	0.25	0.75
Infiltration Basin	0.80	0.75	0.60	0.15
	0.00	0.15	0.00	0.15
	0.00	0.15	0.00	0.15
	0.00	0.15	0.00	0.15

Separate Form Needs to be Completed for Each Outlet or BMP Train

**Total TSS Removal =**

Project:   
 Prepared By:   
 Date:

\*Equals remaining load from previous BMP (E) which enters the BMP

**INSTRUCTIONS:**

1. In BMP Column, click on Blue Cell to Activate Drop Down Menu
2. Select BMP from Drop Down Menu
3. After BMP is selected, TSS Removal and other Columns are automatically completed.

Version 1, Automated: Mar. 4, 2008

Location:

B	C	D	E	F
BMP <sup>1</sup>	TSS Removal Rate <sup>1</sup>	Starting TSS Load*	Amount Removed (C*D)	Remaining Load (D-E)
Sediment Forebay	0.25	1.00	0.25	0.75
Water Quality Swale - Wet	0.70	0.75	0.53	0.23
	0.00	0.23	0.00	0.23
	0.00	0.23	0.00	0.23
	0.00	0.23	0.00	0.23

**Total TSS Removal =**  **Separate Form Needs to be Completed for Each Outlet or BMP Train**

Project:   
 Prepared By:   
 Date:

\*Equals remaining load from previous BMP (E) which enters the BMP

## APPENDIX F



### Guelph Permeameter Data Sheet

Investigator: CARLOS ROSALTA Date: 6/23/25  
 Location: 47 BRIDGEMAN ST Test Id: PT.# 2  
 Depth of hole: 30" Radius: 3cm (standard calcs assume 3 cm radius)  
 Reservoirs used during test (check one): Combined:  Inner only:   
 Reservoir constant used: 35.22

Water level in well = 5 cm				
Time <i>t</i> (min)	<i>Dt</i> (min)	Water level in reservoir <i>h</i> (cm)	<i>Dh</i> (cm)	Rate of change <i>Dh/Dt</i>
0		18		
3:40	3.67	20	2	0.55
13:37	9.88	25	5	0.51
25:00	11.38	30	5	0.44
36:09	11.15	35	5	0.45
47:09	11.0	40	5	0.46
59:26	12.28	46	6	0.49
1:08:10	8.57	50	4	0.47
10:09	10.02	55	5	0.50
14:51		60	5	
29:36	14.65	65	5	0.34

Steady rate for 3 consecutive readings (**R<sub>1</sub>**): 0.48

Water level in well = 10 cm				
Time <i>t</i> (min)	<i>Dt</i> (min)	Water level in reservoir <i>r</i> <i>h</i> (cm)	<i>Dh</i> (cm)	Rate of change <i>Dh/Dt</i>
0		15		
9:22	9.37	20	5	0.53
15:02	5.40	25	5	0.93
20:41	5.65	30	5	0.89
26:22	5.85	35	5	0.86
32:03	5.68	40	5	0.88
37:34	5.52	45	5	0.91
42:55	5.35	50	5	0.94
48:32	5.62	55	5	0.89
53:54	5.37	60	5	0.93
59:11	5.28	65	5	0.94
1:04:40	5.48	70	5	0.91
1:12:28	7.78	75	5	0.64*

Steady rate for 3 consecutive readings (**R<sub>2</sub>**): 0.91

Comments:

$$K_{sat} = 0.0129 \text{ in/min} = 0.27 \text{ in/hr}$$

GP FIELD DATA SHEET

SECTION 1: SITE INFORMATION

Date 6/23/25 Investigator CARLOS COUINTEL

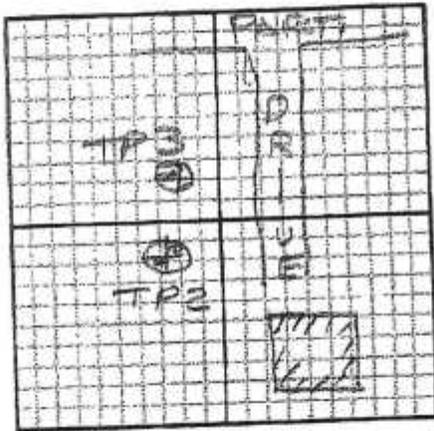
Site Location 47 PENNINGTON ST, FRAWKLIN

Dominant Soil Type(s) CHARLTON HOLLIS PEARL DUTCH

Site Map:

Soil Profile Description (horizon depth, texture, structure, color, etc.):

TP# 2



Depth	Description
12" A	FSL
30" B	FSL
C	Gravelly SL
102"	

Presence of special soil conditions (mottling, water table depth, hardpan, induration, compacted layers, etc.):

Water @ 60"  
Mottles @ 52" (7.54 G/A)

Comments and Notes (topography, slope, vegetation, etc.):





### Guelph Permeameter Data Sheet

Investigator: CARLOS QUINTANA Date: 6/23/25

Location: 47 PARTRIDGE ST Test Id: PT #3

Depth of hole: 33" Radius: 3 cm (standard calcs assume 3 cm radius)

Reservoirs used during test (check one): Combined:  Inner only:

Reservoir constant used: 35.22

Water level in well = 5 cm					Water level in well = 10 cm				
Time <i>t</i> (min)	<i>Dt</i> (min)	Water level in reservoir <i>h</i> (cm)	<i>Dh</i> (cm)	Rate of change <i>Dh/Dt</i>	Time <i>t</i> (min)	<i>Dt</i> (min)	Water level in reservoir <i>h</i> (cm)	<i>Dh</i> (cm)	Rate of change <i>Dh/Dt</i>
0		18			0		18		
1:16	1.27	20	2	1.58	0:24	0.40	20	2	5.00
3:02	1.93	25	5	2.59	2:01	1.62	25	5	3.09
5:19	2.28	30	5	2.19	3:38	1.62	30	5	3.09
7:35	2.27	35	5	2.21	5:17	1.65	35	5	3.03
9:51	2.27	40	5	2.21	6:59	1.70	40	5	2.94
12:17	2.43	45	5	2.06	8:45	1.77	45	5	2.83
12:32	2.33	50	5	2.14	10:23	1.63	50	5	3.06
1:40	2.43	55	5	2.06	11:55	1.37	55	5	3.66
4:12	2.53	60	5	1.97	13:35	1.67	60	5	3.00
6:25	2.22	65	5	2.26	15:19	1.73	65	5	2.89
8:55	2.50	70	5	2.00	16:58	1.65	70	5	3.03
11:20	2.42	75	5	2.07	18:49	1.85	75	5	2.70
Steady rate for 3 consecutive readings ( <b>R<sub>1</sub></b> ): <u>2.16</u>					Steady rate for 3 consecutive readings ( <b>R<sub>2</sub></b> ): <u>3.03</u>				

Comments:

$$K_{SAT} = 0.0496 \text{ in/min} = 2.98 \text{ in/hr}$$

GP FIELD DATA SHEET

SECTION 1: SITE INFORMATION

Date 6/23/25 Investigator CARLOS QUINTAL

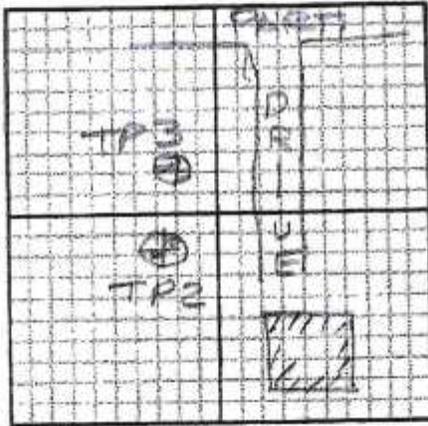
Site Location 47 PARTRIDGE ST, FRANKLIN

Dominant Soil Type(s) CHARLTON HOLLIS ROCK OUTCROP

Site Map:

Soil Profile Description (horizon depth, texture, structure, color, etc.):

TP#3



Depth	Description
6"	A FSL
24"	B FSL
	GENERALLY SL
108"	

Presence of special soil conditions (mottling, water table depth, hardpan, induration, compacted layers, etc.):

moisture @ 52"  
water @ 60"

Comments and Notes (topography, slope, vegetation, etc.):









# Guelph Permeameter Calculations

## Head #1

Reservoir Type (enter "1" for Combined and "2" for lower reservoir)  
 Enter water head height ("H1" in cm): 1  
 Enter the Reservoir Radius ("R" in cm): 3

Enter the soil texture-structure category (enter one of the below numbers): 3

1. Combined, structureless, clayey or silty materials with a fine (FB) top and level or low (L) texture or matrix structure, etc.
2. Soil which are both fine textured (clayey or silty) and structureless, may also include some fine sands.
3. Most structureless soils (fine silts through loams) also include unconsolidated medium and fine sands. The category must frequently apply to agricultural soils.
4. Coarse and gravelly sands may also include some highly structured soils with large angular materials (grasses, mushrooms, etc.)

Steady State Rate of Water Level Change ("Q" in cm/hr): 0.0009

$\phi^* = 0.12 \text{ cm}^2/\text{s}$   
 $C = 0.00316$   
 $Q = 0.00306$   
 $K_p = 0.07024 \text{ cm/hr}$   
 $K_p = 0.07024 \text{ cm/hr}$   
 $K_p = 0.07024 \text{ cm/hr}$   
 $K_p = 0.07024 \text{ cm/hr}$

## Head #2

Reservoir Type (enter "1" for Combined and "2" for lower reservoir)  
 Enter water head height ("H2" in cm): 10  
 Enter the Reservoir Radius ("R" in cm): 3

Enter the soil texture-structure category (enter one of the below numbers): 2

1. Combined, structureless, clayey or silty materials with a fine (FB) top and level or low (L) texture or matrix structure, etc.
7. Soil which are both fine textured (clayey or silty) and structureless, may also include some fine sands.
3. Most structureless soils (fine silts through loams) also include unconsolidated medium and fine sands. The category must frequently apply to agricultural soils.
4. Coarse and gravelly sands may also include some highly structured soils with large angular materials (grasses, mushrooms, etc.)

Steady State Rate of Water Level Change ("Q" in cm/hr): 0.0009

$\phi^* = 0.12 \text{ cm}^2/\text{s}$   
 $C = 0.00704$   
 $Q = 0.00108$   
 $K_p = 0.00204 \text{ cm/hr}$   
 $K_p = 0.00204 \text{ cm/hr}$   
 $K_p = 0.00204 \text{ cm/hr}$   
 $K_p = 0.00204 \text{ cm/hr}$

## Average

$K_p = 0.00204 \text{ cm/hr}$   
 $K_p = 0.00204 \text{ cm/hr}$   
 $K_p = 0.00204 \text{ cm/hr}$   
 $K_p = 0.00204 \text{ cm/hr}$

$\phi^* = 0.00204 \text{ cm}^2/\text{s}$

## Two Head Method

Reservoir Type (enter "1" for Combined and "2" for lower reservoir): 1  
 Enter the first water head height ("H1" in cm): 1  
 Enter the second water head height ("H2" in cm): 50

Enter the Reservoir Radius ("R" in cm): 3

Enter the soil texture-structure category (enter one of the below numbers): 1

1. Combined, structureless, clayey or silty materials with a fine (FB) top and level or low (L) texture or matrix structure, etc.
- Soil which are both fine textured (clayey or silty) and structureless, may also include some fine sands.
- Most structureless soils (fine silts through loams) also include unconsolidated medium and fine sands. The category must frequently apply to agricultural soils.
- Coarse and gravelly sands may also include some highly structured soils with large angular materials (grasses, mushrooms, etc.)

Steady State Rate of Water Level Change ("Q") in cm/hr: 0.0009  
 Steady State Rate of Water Level Change ("Q") in cm/hr: 0.0009  
 $\phi^* = 0.12 \text{ cm}^2/\text{s}$

$K_p = 0.0009 \text{ cm/hr}$   
 $K_p = 0.0009 \text{ cm/hr}$

Calculations based on the average head (Q) where H1 is the first water head height (cm), H2 is the second water head height (cm), R is a reservoir radius (cm), C is permeability (cm/hr), Kp is permeability (cm/hr), Q is the average water level change (cm/hr), and phi\* is the average head change (cm/hr).

Soil Texture-Structure Category	Q (cm/hr)	Q (cm/hr)	Q (cm/hr)
Combined, structureless, clayey or silty materials with a fine (FB) top and level or low (L) texture or matrix structure, etc.	0.01	0.01	0.01
Soils which are both fine textured (clayey or silty) and structureless, may also include some fine sands.	0.01	0.01	0.01
Most structureless soils (fine silts through loams) also include unconsolidated medium and fine sands. The category must frequently apply to agricultural soils.	0.01	0.01	0.01
Coarse and gravelly sands may also include some highly structured soils with large angular materials (grasses, mushrooms, etc.)	0.01	0.01	0.01

Calculations based on the combined and two-head methods. Where K is steady-state rate of flow at water level height H1, Kp is soil saturated hydraulic conductivity (cm/hr), R is soil radius (cm), H1 is the first water head height (cm), H2 is the second water head height (cm), C is permeability (cm/hr), Q is the average water level change (cm/hr), and phi\* is the average head change (cm/hr).

Soil Texture-Structure Category	Q (cm/hr)	Q (cm/hr)	Q (cm/hr)
Combined, structureless, clayey or silty materials with a fine (FB) top and level or low (L) texture or matrix structure, etc.	0.01	0.01	0.01
Soils which are both fine textured (clayey or silty) and structureless, may also include some fine sands.	0.01	0.01	0.01
Most structureless soils (fine silts through loams) also include unconsolidated medium and fine sands. The category must frequently apply to agricultural soils.	0.01	0.01	0.01
Coarse and gravelly sands may also include some highly structured soils with large angular materials (grasses, mushrooms, etc.)	0.01	0.01	0.01

P.T.S

### Guelph Permeameter Data Sheet

Investigator: CARLOS QUINITAL Date: 12/18/25

Location: 47 BRIDGEMAN Test Id: PT 5

Depth of hole: 30' Radius: 3 CM (standard caics assume 3 cm radius)

Reservoirs used during test (check one): Combined:  Inner only:

Reservoir constant used: 35,22

PT 5

Water level in well = 5 cm				
Time <i>t</i> (min)	<i>Dt</i> (min)	Water level in reservoir <i>h</i> (cm)	<i>Dh</i> (cm)	Rate of change <i>Dh/Dt</i>
0		17		
3:25	3.42	20	3	0.88
9:53	6.47	25	5	0.77
16:15	6.37	30	5	0.78
22:10	5.92	35	5	0.85
28:18	6.13	40	5	0.82
34:31	6.22	45	5	0.80
40:20	5.82	50	5	0.86
46:17	5.95	55	5	0.84
51:58	5.68	60	5	0.88
58:00	6.03	65	5	0.83

Steady rate for 3 consecutive readings (**R<sub>1</sub>**): 0.84

Water level in well = 10 cm				
Time <i>t</i> (min)	<i>Dt</i> (min)	Water level in reservoir <i>h</i> (cm)	<i>Dh</i> (cm)	Rate of change <i>Dh/Dt</i>
0		14		
4:14	4.23	21	7	1.65
6:52	2.63	25	4	1.52
10:06	3.23	30	5	1.55
13:12	3.10	35	5	1.61
16:26	3.23	40	5	1.55
19:39	3.22	45	5	1.55
22:55	3.27	50	5	1.53
26:07	3.20	55	5	1.56
29:13	3.10	60	5	1.61
32:18	3.08	65	5	1.62

Steady rate for 3 consecutive readings (**R<sub>2</sub>**): 1.57

Comments:

$$K_{SAT} = 0.0224 \text{ in/min} = 1.34 \text{ in/hr}$$

GP FIELD DATA SHEET

SECTION 1: SITE INFORMATION

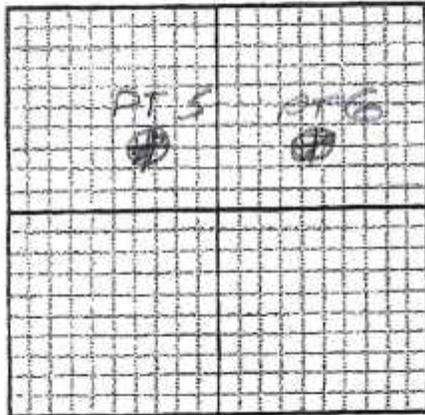
Date 12/18/25 Investigator CARLOS A. RUIZ

Site Location 47 PARTRIDGE ST - FRANKLIN

Dominant Soil Type(s) WOODBRIDGE FINE SANDY LOAM

Site Map:

Soil Profile Description (horizon depth, texture, structure, color, etc.):



Depth	Description
12" A	SL
18" B	SL
60" C	PSL

Presence of special soil conditions (mottling, water table depth, hardpan, induration, compacted layers, etc.):

\_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

\_\_\_\_\_

Comments and Notes (topography, slope, vegetation, etc.):

\_\_\_\_\_

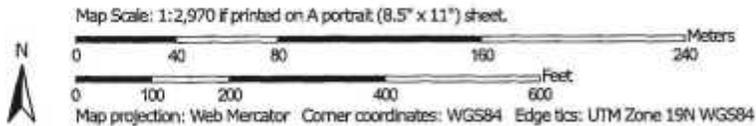
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Soil Map—Norfolk and Suffolk Counties, Massachusetts  
(47 Partridge Street Franklin)



## MAP LEGEND

 Area of Interest (AOI)	 Spoil Area
 Soils	 Stony Spot
 Soil Map Unit Polygons	 Very Stony Spot
 Soil Map Unit Lines	 Wet Spot
 Soil Map Unit Points	 Other
 Special Point Features	 Special Line Features
 Blowout	 Water Features
 Borrow Pit	 Streams and Canals
 Clay Spot	 Transportation
 Closed Depression	 RAILS
 Gravel Pit	 Interstate Highways
 Gravelly Spot	 US Routes
 Landfill	 Major Roads
 Lava Flow	 Local Roads
 Marsh or swamp	 Background
 Mine or Quarry	 Aerial Photography
 Miscellaneous Water	
 Perennial Water	
 Rock Outcrop	
 Saline Spot	
 Sandy Spot	
 Severely Eroded Spot	
 Sinkhole	
 Slide or Slip	
 Sodic Spot	

## MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:25,000.

**Warning:** Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service  
Web Soil Survey URL:  
Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Norfolk and Suffolk Counties, Massachusetts  
Survey Area Data: Version 20, Aug 27, 2024

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: May 22, 2022—Jun 5, 2022

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
5	Saco silt loam, frequently ponded, 0 to 1 percent slopes, frequently flooded	11.1	26.8%
103C	Charlton-Hollis-Rock outcrop complex, 8 to 15 percent slopes	3.9	9.4%
260B	Sudbury fine sandy loam, 2 to 8 percent slopes	2.7	6.5%
307C	Paxton fine sandy loam, 8 to 15 percent slopes, extremely stony	1.3	3.1%
310B	Woodbridge fine sandy loam, 3 to 8 percent slopes	19.0	45.9%
626B	Merrimac-Urban land complex, 0 to 8 percent slopes	3.4	8.3%
<b>Totals for Area of Interest</b>		<b>41.5</b>	<b>100.0%</b>

## Norfolk and Suffolk Counties, Massachusetts

### 310B—Woodbridge fine sandy loam, 3 to 8 percent slopes

#### Map Unit Setting

National map unit symbol: 2t2ql  
Elevation: 0 to 1,470 feet  
Mean annual precipitation: 36 to 71 inches  
Mean annual air temperature: 39 to 55 degrees F  
Frost-free period: 140 to 240 days  
Farmland classification: All areas are prime farmland

#### Map Unit Composition

Woodbridge, fine sandy loam, and similar soils: 82 percent  
Minor components: 18 percent  
Estimates are based on observations, descriptions, and transects of  
the mapunit.

#### Description of Woodbridge, Fine Sandy Loam

##### Setting

Landform: Ground moraines, drumlins, hills  
Landform position (two-dimensional): Summit, backslope, footslope  
Landform position (three-dimensional): Side slope  
Down-slope shape: Concave  
Across-slope shape: Linear  
Parent material: Coarse-loamy lodgment till derived from gneiss,  
granite, and/or schist

##### Typical profile

Ap - 0 to 7 inches: fine sandy loam  
Bw1 - 7 to 18 inches: fine sandy loam  
Bw2 - 18 to 30 inches: fine sandy loam  
Cd - 30 to 65 inches: gravelly fine sandy loam

##### Properties and qualities

Slope: 3 to 8 percent  
Depth to restrictive feature: 20 to 39 inches to densic material  
Drainage class: Moderately well drained  
Runoff class: Medium  
Capacity of the most limiting layer to transmit water (Ksat): Very low  
to moderately low (0.00 to 0.14 in/hr)  
Depth to water table: About 18 to 30 inches  
Frequency of flooding: None  
Frequency of ponding: None  
Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)  
Available water supply, 0 to 60 inches: Low (about 3.6 inches)

##### Interpretive groups

Land capability classification (irrigated): None specified  
Land capability classification (nonirrigated): 2w  
Hydrologic Soil Group: C/D

*Ecological site:* F144AY037MA - Moist Dense Till Uplands  
*Hydric soil rating:* No

### Minor Components

#### Paxton

*Percent of map unit:* 10 percent  
*Landform:* Drumlins, ground moraines, hills  
*Landform position (two-dimensional):* Summit, shoulder, backslope  
*Landform position (three-dimensional):* Nose slope, side slope,  
crest  
*Down-slope shape:* Convex, linear  
*Across-slope shape:* Convex  
*Hydric soil rating:* No

#### Ridgebury

*Percent of map unit:* 8 percent  
*Landform:* Depressions, ground moraines, hills, drainageways  
*Landform position (two-dimensional):* Toeslope, backslope,  
footslope  
*Landform position (three-dimensional):* Base slope, head slope, dip  
*Down-slope shape:* Concave  
*Across-slope shape:* Concave  
*Hydric soil rating:* Yes

## Data Source Information

Soil Survey Area: Norfolk and Suffolk Counties, Massachusetts  
Survey Area Data: Version 20, Aug 27, 2024

## Norfolk and Suffolk Counties, Massachusetts

### 103C—Charlton-Hollis-Rock outcrop complex, 8 to 15 percent slopes

#### Map Unit Setting

National map unit symbol: 2wzp1  
Elevation: 0 to 1,390 feet  
Mean annual precipitation: 36 to 71 inches  
Mean annual air temperature: 39 to 55 degrees F  
Frost-free period: 140 to 240 days  
Farmland classification: Not prime farmland

#### Map Unit Composition

Charlton, extremely stony, and similar soils: 50 percent  
Hollis, extremely stony, and similar soils: 20 percent  
Rock outcrop: 10 percent  
Minor components: 20 percent  
Estimates are based on observations, descriptions, and transects of the mapunit.

#### Description of Charlton, Extremely Stony

##### Setting

Landform: Ridges, hills  
Landform position (two-dimensional): Backslope  
Landform position (three-dimensional): Side slope  
Down-slope shape: Convex, linear  
Across-slope shape: Convex  
Parent material: Coarse-loamy melt-out till derived from granite, gneiss, and/or schist

##### Typical profile

Oe - 0 to 2 inches: moderately decomposed plant material  
A - 2 to 4 inches: fine sandy loam  
Bw - 4 to 27 inches: gravelly fine sandy loam  
C - 27 to 65 inches: gravelly fine sandy loam

##### Properties and qualities

Slope: 8 to 15 percent  
Surface area covered with cobbles, stones or boulders: 9.0 percent  
Depth to restrictive feature: More than 80 inches  
Drainage class: Well drained  
Runoff class: Low  
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high (0.14 to 14.17 in/hr)  
Depth to water table: More than 80 inches  
Frequency of flooding: None  
Frequency of ponding: None  
Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)  
Available water supply, 0 to 60 inches: Moderate (about 8.7 inches)

### Interpretive groups

*Land capability classification (irrigated):* None specified  
*Land capability classification (nonirrigated):* 7s  
*Hydrologic Soil Group:* B  
*Ecological site:* F144AY034CT - Well Drained Till Uplands  
*Hydric soil rating:* No

### Description of Hollis, Extremely Stony

#### Setting

*Landform:* Ridges, hills  
*Landform position (two-dimensional):* Summit, shoulder, backslope  
*Landform position (three-dimensional):* Nose slope, side slope, crest  
*Down-slope shape:* Convex  
*Across-slope shape:* Linear, convex  
*Parent material:* Coarse-loamy melt-out till derived from granite, gneiss, and/or schist

#### Typical profile

*O<sub>i</sub> - 0 to 2 inches:* slightly decomposed plant material  
*A - 2 to 7 inches:* gravelly fine sandy loam  
*B<sub>w</sub> - 7 to 16 inches:* gravelly fine sandy loam  
*2R - 16 to 26 inches:* bedrock

#### Properties and qualities

*Slope:* 8 to 15 percent  
*Surface area covered with cobbles, stones or boulders:* 9.0 percent  
*Depth to restrictive feature:* 8 to 23 inches to lithic bedrock  
*Drainage class:* Somewhat excessively drained  
*Runoff class:* Very high  
*Capacity of the most limiting layer to transmit water (K<sub>sat</sub>):* Very low (0.00 to 0.00 in/hr)  
*Depth to water table:* More than 80 inches  
*Frequency of flooding:* None  
*Frequency of ponding:* None  
*Maximum salinity:* Nonsaline (0.0 to 1.9 mmhos/cm)  
*Available water supply, 0 to 60 inches:* Very low (about 2.7 inches)

### Interpretive groups

*Land capability classification (irrigated):* None specified  
*Land capability classification (nonirrigated):* 7s  
*Hydrologic Soil Group:* D  
*Ecological site:* F144AY033MA - Shallow Dry Till Uplands  
*Hydric soil rating:* No

### Description of Rock Outcrop

#### Setting

*Landform:* Ridges, hills  
*Parent material:* Igneous and metamorphic rock

#### Typical profile

*R - 0 to 79 inches:* bedrock

### Properties and qualities

*Slope:* 8 to 15 percent

*Depth to restrictive feature:* 0 inches to lithic bedrock

*Runoff class:* Very high

*Capacity of the most limiting layer to transmit water (Ksat):* Very low  
(0.00 to 0.00 in/hr)

*Available water supply, 0 to 60 inches:* Very low (about 0.0 inches)

### Interpretive groups

*Land capability classification (irrigated):* None specified

*Land capability classification (nonirrigated):* 8

*Hydrologic Soil Group:* D

*Hydric soil rating:* No

### Minor Components

#### Woodbridge, extremely stony

*Percent of map unit:* 8 percent

*Landform:* Ground moraines, hills, drumlins

*Landform position (two-dimensional):* Backslope, footslope

*Landform position (three-dimensional):* Side slope

*Down-slope shape:* Convex

*Across-slope shape:* Linear

*Hydric soil rating:* No

#### Canton, extremely stony

*Percent of map unit:* 5 percent

*Landform:* Moraines, hills, ridges

*Landform position (two-dimensional):* Backslope

*Landform position (three-dimensional):* Side slope

*Down-slope shape:* Convex, linear

*Across-slope shape:* Convex

*Hydric soil rating:* No

#### Chatfield, extremely stony

*Percent of map unit:* 5 percent

*Landform:* Ridges, hills

*Landform position (two-dimensional):* Summit, shoulder, backslope

*Landform position (three-dimensional):* Nose slope, side slope,  
crest

*Down-slope shape:* Convex

*Across-slope shape:* Linear, convex

*Hydric soil rating:* No

#### Ridgebury, extremely stony

*Percent of map unit:* 2 percent

*Landform:* Hills, drainageways, drumlins, depressions, ground  
moraines

*Landform position (two-dimensional):* Footslope, toeslope

*Landform position (three-dimensional):* Head slope, base slope

*Down-slope shape:* Concave

*Across-slope shape:* Concave

*Hydric soil rating: Yes*

## **Data Source Information**

Soil Survey Area: Norfolk and Suffolk Counties, Massachusetts  
Survey Area Data: Version 20, Aug 27, 2024

## APPENDIX G

## **CHECKLIST FOR DESIGNERS**

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**GOALS and NEEDS Addressed:**

1. Create a visually appealing community
2. Stabilize and increase property values
3. Encourage low impact development
4. Preserve the Town's historic and cultural heritage
5. Protect Franklin's natural environment, including habitat, water resources, and ecosystem services

**FRANKLIN POLICY:**  
 Subdivision plans and site plans for all forms of development shall adhere to the principles of environmental and aesthetic compatibility and energy-efficient design.

<b>BEST DEVELOPMENT PRACTICES</b>	<b>Incorporated into Project?</b>
The site plan should be designed to address the following to the maximum extent practicable	
Unique natural features have been preserved <i>(the development program should either avoid altering or showcase significant natural features)</i>	N/A
Native vegetation planted in disturbed areas as needed to enhance or restore habitat	✓
Historic and cultural resources have been preserved <i>(the development program should either avoid altering or showcase significant historic and cultural features)</i>	N/A
Clearing, grading, and building placement consider view sheds	✓
Cut and fill have been minimized	✓
Buildings blend into the natural topography	✓
Buildings are oriented to the sun and wind for maximum energy efficiency <i>Vegetated protection from northwest (winter) winds is provided Deciduous species planted or retained close to the East, South and West building edges</i>	✓
Conforms to §185-31 of the Town of Franklin Zoning Code and/or Chapter 300 of the Town of Franklin Subdivision Regulations	✓ With waiver request

## GOALS and NEEDS addressed:

1. Protect local and regional wetlands and water bodies;
2. Maximize groundwater recharge to retain a viable local groundwater supply; and
3. Minimize pollutants in stormwater runoff.

**FRANKLIN POLICY:** In addition to MassDEP's Stormwater Management Standards, all new development projects in Franklin must meet the following performance measures. All redevelopment projects shall meet the standards and if they fail to meet the standards, shall retrofit or expand existing stormwater management systems to improve existing conditions.

1. Post-development peak discharge rates and volumes from the site shall not exceed pre-development peak discharge rates and volumes from the site.
2. All drainage facilities proposed shall utilize best management practices as outlined in the Massachusetts Stormwater Management Standards.
3. All sites will have an Operation and Maintenance plan to insure future compliance.

Additionally, new development projects must:

1. Retain the volume of runoff equivalent to, or greater than, one (1.0) inch multiplied by the total post-construction impervious surface area on the site AND/OR
2. Remove 90% of the average annual load of Total Suspended Solids (TSS) generated from the total post-construction impervious area on the site AND 60% of the average annual load of Total Phosphorus (TP) generated from the total post-construction impervious surface area on the site.

And redevelopment projects must:

1. Retain the volume of runoff equivalent to, or greater than, 0.80 inch multiplied by the total post-construction impervious surface area on the site AND/OR
2. Remove 80% of the average annual post-construction load of Total Suspended Solids (TSS) generated from the total post-construction impervious area on the site AND 50% of the average annual load of Total Phosphorus (TP) generated from the total post-construction impervious surface area on the site.

BEST DEVELOPMENT PRACTICES	Incorporated into Project?
The site plan should be designed to address the following to the maximum extent practicable	
<b>Vegetated swales</b> <i>(recommended to convey runoff from roadways &amp; parking lots)</i>	✓
<b>Vegetated filter strips</b> <i>(recommended to filter and infiltrate runoff from roadways, parking lots, and driveways; use along roadsides and parking lots)</i>	
<b>Constructed wetlands</b> <i>(preferred method for stormwater retention &amp; pollutant removal)</i>	
<b>Bioretention cells</b> <i>(rain gardens)</i> <i>(recommended on residential lots and parking lot islands)</i>	
<b>Pervious paving surfaces</b> <i>(recommended in overflow parking and low-traffic areas)</i>	
<b>Sediment Forebays</b> <i>(use in combination with other BDP)</i>	✓
<b>Roof gardens</b> <i>(encouraged on flat or gently sloped commercial and industrial rooftops)</i>	
<b>Retention/Detention basins</b> <i>(may be used in series with other practices to provide pre-treatment)</i>	✓
<b>Recharge Systems</b> <i>(suitable for all areas of development)</i>	✓
<b>Drain pipe/catch basin systems</b> <i>(as required to collect runoff when other systems are not practical)</i>	✓
<b>If utilizing drain pipe and/or catch basin systems, have you documented that other systems are infeasible?</b>	✓ <i>preliminary subdivision</i>

# Erosion & Sedimentation Control

Checklist for Designers

## GOALS and NEEDS addressed:

1. Minimize clearing and regrading
2. Prevent erosion and sedimentation

### FRANKLIN POLICIES:

- a) Any proposed project on a previously undeveloped site shall accommodate the development program in a way that minimizes clearing and re-grading, especially in areas of steep slopes, erosion-prone soils, or sensitive vegetation. For redevelopment projects, the site plan shall concentrate development in previously-disturbed areas to the extent possible.
- b) As a condition of approval, every proposed project shall submit and adhere to an erosion control plan that addresses soil stabilization, sediment retention, perimeter protection, construction scheduling, and traffic area stabilization and dust control.
- c) If the proposed project is in an area under conservation jurisdiction, the project will require permitting deemed appropriate by the Conservation Commission.

BEST DEVELOPMENT PRACTICES	Incorporated into Project?
The site plan should be designed to address the following to the maximum extent practicable:	
Clearing and re-grading have been minimized	✓
Plan identifies sensitive areas to be protected and areas that are suitable for development	✓
Conservation Permits have been obtained <i>(when applicable)</i>	Applying For
<p>The erosion and sedimentation control plan addresses:</p> <ul style="list-style-type: none"> <li>• Soil stabilization               <ul style="list-style-type: none"> <li>○ <i>(cover or stabilize erodible surfaces not in immediate use)</i></li> </ul> </li> <li>• Sediment retention               <ul style="list-style-type: none"> <li>○ <i>(runoff interceptors and sediment traps/ponds)</i></li> </ul> </li> <li>• Perimeter protection               <ul style="list-style-type: none"> <li>○ <i>(vegetated buffers, compost socks or straw wattles at limit of work)</i></li> </ul> </li> <li>• Construction scheduling               <ul style="list-style-type: none"> <li>○ <i>(minimize disturbed area at any given time)</i></li> </ul> </li> <li>• Traffic area stabilization               <ul style="list-style-type: none"> <li>○ <i>(crushed rock or similar at construction vehicle entrance and parking areas)</i></li> </ul> </li> <li>• Dust control               <ul style="list-style-type: none"> <li>○ <i>(plan for stabilizing dry, dust-prone surfaces when necessary)</i></li> </ul> </li> <li>• Vegetation               <ul style="list-style-type: none"> <li>○ <i>(preserve existing vegetation and/or identify areas to be revegetated including proposed planting species, quantity and planting specifications)</i></li> </ul> </li> </ul>	✓

## GOALS and NEEDS addressed:

1. Stabilize water use at a sustainable level;
2. Create landscapes that minimize habitat destruction and maximize habitat value;
3. Encourage the development of landscapes that provide environmental quality and visual relief through the planting of native or naturalized species

### FRANKLIN POLICIES:

- a) Site plans and landscape plans for all proposed projects shall take appropriate steps, as outlined in the Guidebook, to minimize water use for irrigation and to allow for natural recharge of groundwater. Landscape plans shall follow the guidelines in the Guidebook for selecting species that are most appropriate to the site conditions.
- b) Native and habitat-creating species shall be used in all landscape plans to the maximum extent possible while still meeting the site's landscaping needs. Invasive species may not be planted in Franklin under any condition. Refer to the Massachusetts Prohibited Plant list for more information.
- c) Actively promote the Town of Franklin's Water Conservation Measures.

### BEST DEVELOPMENT PRACTICES

Incorporated into Project?

The site plan must address all of the following principles.

Retain and Recharge water on site ( <i>install bio-retention cells, vegetated filter strips and minimize lawn areas where feasible</i> )	✓
Preserve natural vegetation to the maximum extent practicable	✓
Irrigation system is water efficient ( <i>if an in-ground irrigation system is proposed, it is a water efficient system with timers and automatic sensors to prevent overwatering</i> )	
Preserve soil permeability ( <i>minimize disturbing existing landscapes. Prepare new planting beds in accordance to the Planting Bed Guidelines on p. 13, and install 1-2" of shredded pine bark mulch on new planting areas</i> )	✓
Minimize the use of turf grass ( <i>when applicable, reduce the size of the lawn area; instead, plant a bio-retention cell, use alternative, drought tolerant groundcover</i> )	✓
Specify variety of native and naturalized species ( <i>species from the plant list have been incorporated into the landscape design, and no invasive species are used. Refer to the Plant Species Section and the Massachusetts Prohibited Plant List</i> )	✓
Species are appropriate to the soil, site, and microclimate conditions ( <i>select appropriate species from the plant list in this guidebook</i> )	✓

## APPENDIX H



# Checklist for Stormwater Report

## A. Introduction

**Important:** When filling out forms on the computer, use only the tab key to move your cursor - do not use the return key.



A Stormwater Report must be submitted with the Notice of Intent permit application to document compliance with the Stormwater Management Standards. The following checklist is NOT a substitute for the Stormwater Report (which should provide more substantive and detailed information) but is offered here as a tool to help the applicant organize their Stormwater Management documentation for their Report and for the reviewer to assess this information in a consistent format. As noted in the Checklist, the Stormwater Report must contain the engineering computations and supporting information set forth in Volume 3 of the [Massachusetts Stormwater Handbook](#). The Stormwater Report must be prepared and certified by a Registered Professional Engineer (RPE) licensed in the Commonwealth.

The Stormwater Report must include:

- The Stormwater Checklist completed and stamped by a Registered Professional Engineer (see page 2) that certifies that the Stormwater Report contains all required submittals.<sup>1</sup> This Checklist is to be used as the cover for the completed Stormwater Report.
- Applicant/Project Name
- Project Address
- Name of Firm and Registered Professional Engineer that prepared the Report
- Long-Term Pollution Prevention Plan required by Standards 4-6
- Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan required by Standard 8<sup>2</sup>
- Operation and Maintenance Plan required by Standard 9

In addition to all plans and supporting information, the Stormwater Report must include a brief narrative describing stormwater management practices, including environmentally sensitive site design and LID techniques, along with a diagram depicting runoff through the proposed BMP treatment train. Plans are required to show existing and proposed conditions, identify all wetland resource areas, NRCS soil types, critical areas, Land Uses with Higher Potential Pollutant Loads (LUHPPL), and any areas on the site where infiltration rate is greater than 2.4 inches per hour. The Plans shall identify the drainage areas for both existing and proposed conditions at a scale that enables verification of supporting calculations.

As noted in the Checklist, the Stormwater Management Report shall document compliance with each of the Stormwater Management Standards as provided in the Massachusetts Stormwater Handbook. The soils evaluation and calculations shall be done using the methodologies set forth in Volume 3 of the Massachusetts Stormwater Handbook.

To ensure that the Stormwater Report is complete, applicants are required to fill in the Stormwater Report Checklist by checking the box to indicate that the specified information has been included in the Stormwater Report. If any of the information specified in the checklist has not been submitted, the applicant must provide an explanation. The completed Stormwater Report Checklist and Certification must be submitted with the Stormwater Report.

<sup>1</sup> The Stormwater Report may also include the Illicit Discharge Compliance Statement required by Standard 10. If not included in the Stormwater Report, the Illicit Discharge Compliance Statement must be submitted prior to the discharge of stormwater runoff to the post-construction best management practices.

<sup>2</sup> For some complex projects, it may not be possible to include the Construction Period Erosion and Sedimentation Control Plan in the Stormwater Report. In that event, the issuing authority has the discretion to issue an Order of Conditions that approves the project and includes a condition requiring the proponent to submit the Construction Period Erosion and Sedimentation Control Plan before commencing any land disturbance activity on the site.



# Checklist for Stormwater Report

## B. Stormwater Checklist and Certification

The following checklist is intended to serve as a guide for applicants as to the elements that ordinarily need to be addressed in a complete Stormwater Report. The checklist is also intended to provide conservation commissions and other reviewing authorities with a summary of the components necessary for a comprehensive Stormwater Report that addresses the ten Stormwater Standards.

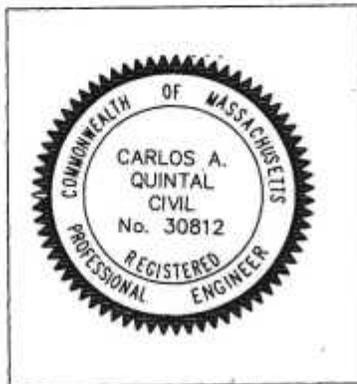
*Note:* Because stormwater requirements vary from project to project, it is possible that a complete Stormwater Report may not include information on some of the subjects specified in the Checklist. If it is determined that a specific item does not apply to the project under review, please note that the item is not applicable (N.A.) and provide the reasons for that determination.

A complete checklist must include the Certification set forth below signed by the Registered Professional Engineer who prepared the Stormwater Report.

### Registered Professional Engineer's Certification

I have reviewed the Stormwater Report, including the soil evaluation, computations, Long-term Pollution Prevention Plan, the Construction Period Erosion and Sedimentation Control Plan (if included), the Long-term Post-Construction Operation and Maintenance Plan, the Illicit Discharge Compliance Statement (if included) and the plans showing the stormwater management system, and have determined that they have been prepared in accordance with the requirements of the Stormwater Management Standards as further elaborated by the Massachusetts Stormwater Handbook. I have also determined that the information presented in the Stormwater Checklist is accurate and that the information presented in the Stormwater Report accurately reflects conditions at the site as of the date of this permit application.

Registered Professional Engineer Block and Signature



*Carlos A. Quintal* 1/20/26  
Signature and Date

## Checklist

**Project Type:** Is the application for new development, redevelopment, or a mix of new and redevelopment?

- New development  
 Redevelopment  
 Mix of New Development and Redevelopment



# Checklist for Stormwater Report

---

## Checklist (continued)

**LID Measures:** Stormwater Standards require LID measures to be considered. Document what environmentally sensitive design and LID Techniques were considered during the planning and design of the project:

- No disturbance to any Wetland Resource Areas
- Site Design Practices (e.g. clustered development, reduced frontage setbacks)
- Reduced Impervious Area (Redevelopment Only)
- Minimizing disturbance to existing trees and shrubs
- LID Site Design Credit Requested:
  - Credit 1
  - Credit 2
  - Credit 3
- Use of "country drainage" versus curb and gutter conveyance and pipe
- Bioretention Cells (includes Rain Gardens)
- Constructed Stormwater Wetlands (includes Gravel Wetlands designs)
- Treebox Filter
- Water Quality Swale
- Grass Channel
- Green Roof
- Other (describe): \_\_\_\_\_

### Standard 1: No New Untreated Discharges

- No new untreated discharges
- Outlets have been designed so there is no erosion or scour to wetlands and waters of the Commonwealth
- Supporting calculations specified in Volume 3 of the Massachusetts Stormwater Handbook included.



# Checklist for Stormwater Report

## Checklist (continued)

### Standard 2: Peak Rate Attenuation

- Standard 2 waiver requested because the project is located in land subject to coastal storm flowage and stormwater discharge is to a wetland subject to coastal flooding.
- Evaluation provided to determine whether off-site flooding increases during the 100-year 24-hour storm.
- Calculations provided to show that post-development peak discharge rates do not exceed pre-development rates for the 2-year and 10-year 24-hour storms. If evaluation shows that off-site flooding increases during the 100-year 24-hour storm, calculations are also provided to show that post-development peak discharge rates do not exceed pre-development rates for the 100-year 24-hour storm.

### Standard 3: Recharge

- Soil Analysis provided.
- Required Recharge Volume calculation provided.
- Required Recharge volume reduced through use of the LID site Design Credits.
- Sizing the infiltration, BMPs is based on the following method: Check the method used.
  - Static
  - Simple Dynamic
  - Dynamic Field<sup>1</sup>
- Runoff from all impervious areas at the site discharging to the infiltration BMP.
- Runoff from all impervious areas at the site is *not* discharging to the infiltration BMP and calculations are provided showing that the drainage area contributing runoff to the infiltration BMPs is sufficient to generate the required recharge volume.
- Recharge BMPs have been sized to infiltrate the Required Recharge Volume.
- Recharge BMPs have been sized to infiltrate the Required Recharge Volume *only* to the maximum extent practicable for the following reason:
  - Site is comprised solely of C and D soils and/or bedrock at the land surface
  - M.G.L. c. 21E sites pursuant to 310 CMR 40.0000
  - Solid Waste Landfill pursuant to 310 CMR 19.000
  - Project is otherwise subject to Stormwater Management Standards only to the maximum extent practicable.
- Calculations showing that the infiltration BMPs will drain in 72 hours are provided.
- Property includes a M.G.L. c. 21E site or a solid waste landfill and a mounding analysis is included.

<sup>1</sup> 80% TSS removal is required prior to discharge to infiltration BMP if Dynamic Field method is used.



# Checklist for Stormwater Report

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## Checklist (continued)

### Standard 3: Recharge (continued)

- The infiltration BMP is used to attenuate peak flows during storms greater than or equal to the 10-year 24-hour storm and separation to seasonal high groundwater is less than 4 feet and a mounding analysis is provided.
- Documentation is provided showing that infiltration BMPs do not adversely impact nearby wetland resource areas.

### Standard 4: Water Quality

The Long-Term Pollution Prevention Plan typically includes the following:

- Good housekeeping practices;
  - Provisions for storing materials and waste products inside or under cover;
  - Vehicle washing controls;
  - Requirements for routine inspections and maintenance of stormwater BMPs;
  - Spill prevention and response plans;
  - Provisions for maintenance of lawns, gardens, and other landscaped areas;
  - Requirements for storage and use of fertilizers, herbicides, and pesticides;
  - Pet waste management provisions;
  - Provisions for operation and management of septic systems;
  - Provisions for solid waste management;
  - Snow disposal and plowing plans relative to Wetland Resource Areas;
  - Winter Road Salt and/or Sand Use and Storage restrictions;
  - Street sweeping schedules;
  - Provisions for prevention of illicit discharges to the stormwater management system;
  - Documentation that Stormwater BMPs are designed to provide for shutdown and containment in the event of a spill or discharges to or near critical areas or from LUHPPL;
  - Training for staff or personnel involved with implementing Long-Term Pollution Prevention Plan;
  - List of Emergency contacts for implementing Long-Term Pollution Prevention Plan.
- A Long-Term Pollution Prevention Plan is attached to Stormwater Report and is included as an attachment to the Wetlands Notice of Intent.
  - Treatment BMPs subject to the 44% TSS removal pretreatment requirement and the one inch rule for calculating the water quality volume are included, and discharge:
    - is within the Zone II or Interim Wellhead Protection Area
    - is near or to other critical areas
    - is within soils with a rapid infiltration rate (greater than 2.4 inches per hour)
    - involves runoff from land uses with higher potential pollutant loads.
  - The Required Water Quality Volume is reduced through use of the LID site Design Credits.
  - Calculations documenting that the treatment train meets the 80% TSS removal requirement and, if applicable, the 44% TSS removal pretreatment requirement, are provided.



# Checklist for Stormwater Report

## Checklist (continued)

### Standard 4: Water Quality (continued)

- The BMP is sized (and calculations provided) based on:
  - The ½" or 1" Water Quality Volume or
  - The equivalent flow rate associated with the Water Quality Volume and documentation is provided showing that the BMP treats the required water quality volume.
- The applicant proposes to use proprietary BMPs, and documentation supporting use of proprietary BMP and proposed TSS removal rate is provided. This documentation may be in the form of the propriety BMP checklist found in Volume 2, Chapter 4 of the Massachusetts Stormwater Handbook and submitting copies of the TARP Report, STEP Report, and/or other third party studies verifying performance of the proprietary BMPs.
- A TMDL exists that indicates a need to reduce pollutants other than TSS and documentation showing that the BMPs selected are consistent with the TMDL is provided.

### Standard 5: Land Uses With Higher Potential Pollutant Loads (LUHPPLs)

- The NPDES Multi-Sector General Permit covers the land use and the Stormwater Pollution Prevention Plan (SWPPP) has been included with the Stormwater Report.
- The NPDES Multi-Sector General Permit covers the land use and the SWPPP will be submitted *prior to* the discharge of stormwater to the post-construction stormwater BMPs.
- The NPDES Multi-Sector General Permit does *not* cover the land use.
- LUHPPLs are located at the site and industry specific source control and pollution prevention measures have been proposed to reduce or eliminate the exposure of LUHPPLs to rain, snow, snow melt and runoff, and been included in the long term Pollution Prevention Plan.
- All exposure has been eliminated.
- All exposure has *not* been eliminated and all BMPs selected are on MassDEP LUHPPL list.
- The LUHPPL has the potential to generate runoff with moderate to higher concentrations of oil and grease (e.g. all parking lots with >1000 vehicle trips per day) and the treatment train includes an oil grit separator, a filtering bioretention area, a sand filter or equivalent.

### Standard 6: Critical Areas

- The discharge is near or to a critical area and the treatment train includes only BMPs that MassDEP has approved for stormwater discharges to or near that particular class of critical area.
- Critical areas and BMPs are identified in the Stormwater Report.



# Checklist for Stormwater Report

## Checklist (continued)

### Standard 7: Redevelopments and Other Projects Subject to the Standards only to the maximum extent practicable

- The project is subject to the Stormwater Management Standards only to the maximum Extent Practicable as a:
- Limited Project
  - Small Residential Projects: 5-9 single family houses or 5-9 units in a multi-family development provided there is no discharge that may potentially affect a critical area.
  - Small Residential Projects: 2-4 single family houses or 2-4 units in a multi-family development with a discharge to a critical area
  - Marina and/or boatyard provided the hull painting, service and maintenance areas are protected from exposure to rain, snow, snow melt and runoff
  - Bike Path and/or Foot Path
  - Redevelopment Project
  - Redevelopment portion of mix of new and redevelopment.
- Certain standards are not fully met (Standard No. 1, 8, 9, and 10 must always be fully met) and an explanation of why these standards are not met is contained in the Stormwater Report.
- The project involves redevelopment and a description of all measures that have been taken to improve existing conditions is provided in the Stormwater Report. The redevelopment checklist found in Volume 2 Chapter 3 of the Massachusetts Stormwater Handbook may be used to document that the proposed stormwater management system (a) complies with Standards 2, 3 and the pretreatment and structural BMP requirements of Standards 4-6 to the maximum extent practicable and (b) improves existing conditions.

### Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control

A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan must include the following information:

- Narrative;
  - Construction Period Operation and Maintenance Plan;
  - Names of Persons or Entity Responsible for Plan Compliance;
  - Construction Period Pollution Prevention Measures;
  - Erosion and Sedimentation Control Plan Drawings;
  - Detail drawings and specifications for erosion control BMPs, including sizing calculations;
  - Vegetation Planning;
  - Site Development Plan;
  - Construction Sequencing Plan;
  - Sequencing of Erosion and Sedimentation Controls;
  - Operation and Maintenance of Erosion and Sedimentation Controls;
  - Inspection Schedule;
  - Maintenance Schedule;
  - Inspection and Maintenance Log Form.
- A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan containing the information set forth above has been included in the Stormwater Report.



# Checklist for Stormwater Report

## Checklist (continued)

### Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control (continued)

- The project is highly complex and information is included in the Stormwater Report that explains why it is not possible to submit the Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan with the application. A Construction Period Pollution Prevention and Erosion and Sedimentation Control has **not** been included in the Stormwater Report but will be submitted **before** land disturbance begins.
- The project is **not** covered by a NPDES Construction General Permit.
- The project is covered by a NPDES Construction General Permit and a copy of the SWPPP is in the Stormwater Report.
- The project is covered by a NPDES Construction General Permit but no SWPPP been submitted. The SWPPP will be submitted BEFORE land disturbance begins.

### Standard 9: Operation and Maintenance Plan

- The Post Construction Operation and Maintenance Plan is included in the Stormwater Report and includes the following information:
  - Name of the stormwater management system owners;
  - Party responsible for operation and maintenance;
  - Schedule for implementation of routine and non-routine maintenance tasks;
  - Plan showing the location of all stormwater BMPs maintenance access areas;
  - Description and delineation of public safety features;
  - Estimated operation and maintenance budget; and
  - Operation and Maintenance Log Form.
- The responsible party is **not** the owner of the parcel where the BMP is located and the Stormwater Report includes the following submissions:
  - A copy of the legal instrument (deed, homeowner's association, utility trust or other legal entity) that establishes the terms of and legal responsibility for the operation and maintenance of the project site stormwater BMPs;
  - A plan and easement deed that allows site access for the legal entity to operate and maintain BMP functions.

### Standard 10: Prohibition of Illicit Discharges

- The Long-Term Pollution Prevention Plan includes measures to prevent illicit discharges;
- An Illicit Discharge Compliance Statement is attached;
- NO Illicit Discharge Compliance Statement is attached but will be submitted **prior to** the discharge of any stormwater to post-construction BMPs.

## APPENDIX I

# **Operation and Maintenance Plan**

FOR  
Definitive Subdivision  
**Donovan Estates**

LOCATED IN  
FRANKLIN, MASSACHUSETTS

PREPARED FOR  
Donovan Family Realty Trust  
47 Partridge Street  
Franklin, MA 02038

PREPARED BY  
UNITED CONSULTANTS, INC.  
850 FRANKLIN STREET, SUITE 11D  
WRENTHAM, MA. 02093

DATE: September 3, 2025  
Revised: January 16, 2026

## **Operation and Maintenance Plan**

### **Good House Keeping Measures**

1. The roadway and driveway will receive the minimum amount of sand and salt. Snow will be stored at the roadway edges in windrows consistent with Town of Franklin Snow plowing of roadways.
2. The site landscaping will consist of turf lawn, mulch with trees, shrubs, and existing wooded areas. Minimal amounts of fertilizers, herbicides and pesticides will be applied.
3. The site will be stabilized with landscaped areas with mulch and native seed mixes. This will improve the existing site coverage.

### **Long Term Pollution Prevention Plan**

The owner shall employ good housekeeping measures, which include removing trash and debris from the site, keeping trash in receptacles and complying with the long-term operation and maintenance plan. The owner does not plan to store materials or waste products on the site. The owner will have routine inspections and maintenance completed for the Storm-water BMP's. See the Operation and Maintenance Plan Stormwater Facilities Plan for details and schedule. Typical hazardous materials for single family residences are anticipated. All hazardous materials shall be stored within the houses. The owner's shall apply the minimum amounts of fertilizers, herbicides and pesticides. The houses will be serviced by Town water and sewer. Town trash receptacles are expected to provide refuse storage and will be emptied and disposed of offsite. The owner will designate an emergency contact person prior to commencing construction. Snow will be stored at the roadway edges in windrows consistent with Town of Franklin Snow plowing of roadways. The owner will apply the minimum amount of sand and salt necessary. The roadway will be swept by the Town of Franklin DPW based on their street sweeping program. Sand piles will not be stored on site.

### **Operation and Maintenance Plan Reference**

An operation and maintenance schedule for the construction period and the post-development period has been provided on the Operation and Maintenance Plan Stormwater Facilities Plan. Refer to the O&M plan (Sheet 5) for the location of the proposed grading and drainage easement.

During the construction period and after completion the future Owner shall be responsible for the operation and maintenance of the site and the drainage system. Upon completion of the construction work the Town of Franklin shall be responsible for the maintenance of the drainage facilities. The yearly estimated operation and maintenance budget is \$2,500.

### **During Construction:**

The owner will provide documentation which will be submitted to the Franklin DPW confirming when maintenance has been satisfactorily completed.

The maintenance in the maintenance agreement may be amended to achieve the purpose of the bylaws by mutual agreement of the Director of the DPW and the responsible parties.



# Yearly Inspection and Maintenance Log

## Page 1

### Lot 2 Forge Parkway Franklin, Massachusetts

#### Road Sweeping and Curb Inspection – Per Town of Franklin Street Sweeping and Inspection Plan

Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_

Roadway sweeping should be completed by a mechanical or vacuum sweeper.

Notes:

#### Deep Sump Hooded Catch Basins - Per Town of Franklin Catch Basin Cleaning and Inspection Plan

Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_

Cleaning Performed

Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_

Notes:

#### Sediment Forebay– Per Town of Franklin Drainage Facility Inspection Plan

Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_

Cleaning Performed:

Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_

Infiltration Pond – Per Town of Franklin Drainage Facility Inspection Plan

Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_

Cleaning Performed:

Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_

Sediment Forebay and Water Quality Swales – Per Town of Franklin Drainage Facility Inspection Plan

Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_

Cleaning Performed:

Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_

Notes:

Landscape Area Inspection – 4 times per year

Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_

Work Performed Repairs completed:

Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_  
Date: \_\_\_\_\_ Performed By: \_\_\_\_\_

Inspect the area with grass for bare spots and erosion. Repair eroded areas with loam and seed to provide adequate coverage. Inspect landscaped areas for erosion and weeds. Fix erosion and apply additional mulch or landscape stone as necessary.

Inspect and clean pretreatment BMP's every six months and after every major storm event (2 year return frequency). Check the inlet and outlet pipes to determine if they are clogged. Remove accumulated sediment, trash, debris, leaves, lawn clippings from mowing. Inspect the infiltration area after the first several rainfall events, after all major storms, and on regularly scheduled dates every six months.

Inspect the infiltration area 24 hours to several days after a rain event, to look for ponded water at the surface of the trench. If water is present it may be that the infiltration area is clogged. If so then rehabilitation of the bottom of the trench shall be completed including removing all accumulated sediment, scarifying and till the bottom area, remove and replace the stone media.

## APPENDIX J

## In Compliance with DEP Storm-water Management Standard 10

### Definitive Subdivision "**Donovan Estates**"

No Illicit discharges to the storm-water management system, including wastewater discharges and discharges of storm-water contaminated by contact with process wastes, raw materials, toxic pollutants, hazardous substances, oil, or grease are proposed and shall not be allowed.

The site map located in Appendix J shall be part of this Illicit Discharge Compliance Statement.

During Construction the future owner will be the responsible party.

---

Name	Title
------	-------

Note: Once ownership of an approved Subdivisions is secured this document shall be signed and submitted with SWPPP and the Town of Franklin Stormwater Permit.

## APPENDIX K

# Rip Rap Sizing Calculations

Into Sediment Forebay at Wet Swale

## Rip Rap Calculator

I want to find the... ...

average rock diameter ( $D_{50}$ )

rip rap volume

both  $D_{50}$  and rip rap volume

### ^ Rip rap specifications

Water velocity ( $v$ ) <sup>i</sup> ...

4.35 ft/s ∨

Isbash constant ( $C$ ) ...

Highly turbulent (0.86)

Low turbulence (1.2)

Gravitational acceleration ( $g$ ) ...

32.17 ft/s<sup>2</sup> ∨

Specific gravity ( $s$ ) <sup>i</sup> ...

2.75

Average rock diameter ( $D_{50}$ ) ...

2.727 in ∨

# Rip Rap Sizing Calculations

Into Sediment Forebay at Pond 1

## Rip Rap Calculator

I want to find the... ...

average rock diameter ( $D_{50}$ )

rip rap volume

both  $D_{50}$  and rip rap volume

### ^ Rip rap specifications

Water velocity ( $V$ ) <sup>i</sup> ...

5.56 ft/s ∨

Isbash constant ( $C$ ) ...

Highly turbulent (0.86)

Low turbulence (1.2)

Gravitational acceleration ( $g$ ) ...

32.17 ft/s<sup>2</sup> ∨

Specific gravity ( $S$ ) <sup>i</sup> ...

2.75

Average rock diameter ( $D_{50}$ ) ...

4.455 in ∨



Share result

Reload calculator

Clear all changes

Did we solve your problem today?

Yes

No

# Rip Rap Sizing Calculations

Into Pond 1

## Rip Rap Calculator

I want to find the...

...

average rock diameter ( $D_{50}$ )

rip rap volume

both  $D_{50}$  and rip rap volume

### ^ Rip rap specifications

Water velocity ( $V$ ) <sup>i</sup>

...

5.59

ft/s  $\nabla$

Isbash constant ( $C$ )

...

Highly turbulent (0.86)

Low turbulence (1.2)

Gravitational acceleration ( $g$ )

...

32.17

ft/s<sup>2</sup>  $\nabla$

Specific gravity ( $S$ ) <sup>i</sup>

...

2.75

Average rock diameter ( $D_{50}$ )

...

4.503

in  $\nabla$

# Rip Rap Sizing Calculations

Out of Pond 1

## Rip Rap Calculator

I want to find the... ...

average rock diameter ( $D_{50}$ )

rip rap volume

both  $D_{50}$  and rip rap volume

### ^ Rip rap specifications

Water velocity ( $V$ ) <sup>i</sup> ...

8.63 ft/s ∨

Isbash constant ( $C$ ) ...

Highly turbulent (0.86)

Low turbulence (1.2)

Gravitational acceleration ( $g$ ) ...

32.17 ft/s<sup>2</sup> ∨

Specific gravity ( $s$ ) <sup>i</sup> ...

2.75

Average rock diameter ( $D_{50}$ ) ...

10.732 in ∨



Share result

Reload calculator

Clear all changes

Did we solve your problem today?

Yes

No

## **APPENDIX L**