

STORMWATER REPORT FOR 15 LIBERTY WAY FRANKLIN, MA



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LDG Project No.: 2081.00



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### HYDROLOGIC SUMMARY

### METHODOLOGY

The HydroCAD computer program (Hydro CAD) was used to model the existing and proposed hydrology of the site and design a stormwater management system. HydroCAD generates flood hydrographs dependent upon the type of land use, vegetation, soil types, land slope, watershed areas and rainfall data. HydroCAD also takes into account the antecedent moisture condition of the soil. The peak rate of runoff and volume of runoff are projected for the input storm frequency events (design storms).

Rainfall data was obtained from the Northeast Regional Climate Center and are based on Extreme Precipitation Events for the 2-, 10-, 25- and 100-year return periods for Franklin, Massachusetts. A 24-hour type III rainfall distribution was used in the HydroCAD analysis as prescribed for New England by the Northeast Regional Climate Center. A copy of the precipitation table is included herein.

### **PRE-DEVELOPMENT CONDITIONS**

The existing site property is located at 15 Liberty Way between Constitution Boulevard and Rachael Circle. The existing property is developed and contains an approximately 95,000 square foot warehouse, paved driveway, and paved parking areas for cars and for trailer trucks. For the purposes of hydrological calculations, the proposed development consists of approximately 105,320 square feet located at the rear of the existing warehouse as shown on the site plans.

The existing topography of the site generally slopes from east to west and directs runoff to an existing stormwater basin located onsite. The southeastern corner of the site slopes south directing runoff to the existing paved driveway and parking area to the site east of the existing warehouse. The land cover is mostly wooded area and also includes pavement from the rear portion of the existing driveway and some grass areas.

Test pits were dug on-site in the areas of the proposed infiltration basin to verify the groundwater elevation. Groundwater depth in the area of the infiltration basin varies between approximately 2.5-feet to 3-feet below the surface. The soil logs of the test pits are attached.

The on-site soils as classified by the Soil Survey for Norfolk County Massachusetts are:

312B - Woodbridge fine sandy loam; 0 to 8 percent slopes; Hydrologic Soil Group (HSG) C/D

See the attached SCS soils documentation herein for additional soil details

### POST-DEVELOPMENT CONDITIONS

The Applicant is proposing construct a new paved area to provide additional driveway and trailer parking area at the rear of the site. The project will also include the installation of a new stormwater management system and associated grading for this development.



A new fully compliant stormwater management system has been designed to mitigate the impacts of the proposed site redevelopment. Runoff from the impervious areas will be directed to new catch basins and trench drains which will convey runoff to a subsurface infiltration basin. The subsurface infiltration basin will provide water quality treatment as well as attenuate peak rates of runoff and provide groundwater recharge.

A fully compliant stormwater management system for the entire site addressing compliance with the 10 MADEP Stormwater Standards will be part of the site redevelopment. Site improvements have been made to the maximum extent practicable in accordance with MADEP Stormwater Regulations.

### **STANDARD 1: Untreated Discharges**

Stormwater Management Standard 1 requires that, "No new stormwater conveyances (e.g. outfalls) may discharge untreated stormwater directly to or cause erosion in wetlands or waters of the Commonwealth".

This standard is met by the proposed redevelopment not creating any new non-treated stormwater discharges and improving an existing residential site with no existing stormwater management system. All surface runoff from proposed impervious areas, with the exception of a redeveloped portion of the existing driveway, is collected in deep sump catch basins and trench drains and directed to a Stormceptor treatment unit prior to discharging to a subsurface infiltration basin. Overflow from the subsurface infiltration basin discharges from an outlet control structure to the existing detention basin through a 15" HPDE pipe. All discharges are designed to be placed in areas which mimic existing drainage flow patterns.

**Redevelopment:** The project has been designed to fully comply with Massachusetts Stormwater Regulations for Standard 1.

Full compliance with Standard 1 is required for new outfalls.

- What BMPs are proposed to ensure that all new discharges associated with the discharge are adequately treated? Proprietary Treatment Units, Subsurface infiltration basin
- What BMPs are proposed to ensure that no new discharges cause erosion in wetlands or waters of the Commonwealth? rip rap outlets are proposed in the existing stormwater basin designed to prevent erosion.
- Will the proposed discharge comply with all applicable requirements of the Massachusetts Clean Waters Act and the regulations promulgated thereunder at 314 CMR 3.00, 314 CMR 4.00 and 314 CMR 5.00? yes

Existing outfalls shall be brought into compliance with Standard 1 to the maximum extent practicable.

- Are there any existing discharges associated with the redevelopment project for which new treatment could be provided? No existing outfalls
- If so, the proponent shall specify the stormwater BMP retrofit measures that have been considered to ensure that the discharges are adequately treated and indicate the reasons for adopting or rejecting those measures. (See Section entitled "Retrofit of Existing BMPs".) N/A
- What BMPs have been considered to prevent erosion from existing stormwater discharges? N/A



### **STANDARD 2: Peak Rate Control and Flood Prevention**

Stormwater Management Standard 2 requires that, "Stormwater management systems must be designed so that post-development peak discharge rates do not exceed pre-development peak discharge rates. This Standard may be waived for land subject to coastal storm flowage."

This standard is met by the proposed development mitigating the post-development peak discharge rates at the designated control points for all design storm events. This is accomplished by directing stormwater flow to a subsurface infiltration basin. Below is a description of the design points used in the hydrologic analysis and a summary of pre- and post- development discharge rates. The proposed development will reduce the peak rate of runoff at all the design points and provide ample groundwater recharge.

**Redevelopment:** The project has been designed to fully comply with Massachusetts Stormwater Regulations for Standard 2.

Compliance to the Maximum Extent Practicable:

- Does the redevelopment design meet Standard 2, comparing post-development to predevelopment conditions? Yes
- If not, the applicant shall document an analysis of alternative approaches for meeting the Standard. (See Menu of Strategies to Reduce Runoff and Peak Flows and/or Increase Recharge Menu included at the end of this chapter.) N/A

Improvement of existing conditions:

- Does the project reduce the volume and/or rate of runoff to less than current estimated conditions? Has the applicant considered all the alternatives for reducing the volume and/or rate of runoff from the site? (See Menu.) Yes
- Is the project located within a watershed subject to damage by flooding during the 2-year or 10year 24-hour storm event? If so, does the project design provide for attenuation of the 2-year and 10-year 24-hour storm event to less than current estimated conditions? Have measures been implemented to reduce the volume of runoff from the site resulting from the 2 year or 10 year 24 hour storm event? (See Menu.) N/A
- Is the project located adjacent to a water body or watercourse subject to adverse impacts from flooding during the 100-year 24-hour storm event? If so, are portions of the site available to increase flood storage adjacent to existing Bordering Land Subject to Flooding (BLSF)? N/A
- Have measures been implemented to attenuate peak rates of discharge during the 100-year 24hour storm event to less than the peak rates under current estimated conditions? Have measures been implemented to reduce the volume of runoff from the site resulting from the 100-year 24hour storm event? (See Menu.) Yes



### SUMMARY OF PEAK STORMWATER RUNOFF (CFS)

Three design points were utilized to analyze the runoff characteristics of the site. Design Point 1 (DP-1) is the existing rip rap detention basin. The existing basin is the ultimate design point and no further analysis is included in the stormwater model, however it is assumed to provide infiltration and overflow to the wetlands on site. The existing basin currently collects runoff from surrounding areas on the site and discharges through an outlet without any issues. The proposed flow from the developed portion of the site is less than existing flow from the same area and therefore no adverse impacts are expected. As part of this project the owner is proposing to inspect and clean up any areas of the basin as needed. Design Point 2 (DP-2) is the existing paved driveway and parking area to the east of the existing warehouse. Design Point 3 (DP-3) is the northwestern corner of the property. The pre- and post- development peak discharge rates for all analyzed design storms is summarized in the following table:

		Design Point -	- DP-1		
Year Pre-Development		elopment	Post-De	Development	
Storm	Flow	Volume	Flow	Volume (Acre-Ft.)	
2-yr	1.49 cfs	0.144	1.31 cfs	0.292	
10-yr	4.53 cfs	0.399	4.15 cfs	0.636	
25-yr	6.49 cfs	0.566	5.78 cfs	0.846	
100-yr	9.57 cfs	0.833	8.73 cfs	1.169	
		Design Point -	- DP-2		
Year	Pre-Development		Post-Development		
Storm	Flow	Volume	Flow	Volume	
2-yr	0.41 cfs	0.036	0.41 cfs	0.032	
10-yr	0.94 cfs	0.081	0.70 cfs	0.062	
25-yr	1.26 cfs	0.109	0.86 cfs	0.085	
100-yr	1.73 cfs	0.151	1.11 cfs	0.121	
		Design Point	– DP-3		
Year	Pre-Development		Post-Development		
Storm	Flow	Volume	Flow	Volume	
2-yr	0.05 cfs	0.004	0.03 cfs	0.002	
10-yr	0.13 cfs	0.010	0.08 cfs	0.006	
25-yr	0.19 cfs	0.014	0.10 cfs	0.008	
100-yr	0.27 cfs	0.020	0.14 cfs	0.011	

The net peak discharge for DP-1 is controlled by the subsurface infiltration basin and does not increase flows off site for any of the evaluated design storms. There is a slight increase in volumes for the evaluated storms however based on the size of the total contributing area on abutting properties, the increase is negligible and there will be no adverse impacts to the wetlands. The net peak discharges for both DP-2 and DP-3 are un-controlled and flow off-site overland as occurs in existing conditions. Based on the proposed grading and the locations of new catch basins and trench drains, there is a reduction in total area contributing to both DP-2 and DP-3 and the proposed development does not increase flows or volumes to these design points for any of the evaluated design storms from existing conditions.



### **STANDARD 3: Recharge to Groundwater**

Stormwater Management Standard 3 requires that, "Loss of annual recharge to groundwater shall be eliminated or minimized through the use of infiltration measures, including environmentally sensitive site design, low impact development techniques, best management practices, and good operation and maintenance. At a minimum, the annual recharge from the post-development site shall approximate the annual recharge from the pre-development conditions based on soil type. This Standard is met when the stormwater management system is designed to infiltrate the required recharge volume as determined in accordance with the Massachusetts Stormwater Handbook."

### **GROUND WATER RECHARGE**

The proposed project will result in an increase in impervious area to a total of approximately 80,078 square feet. The on-site soils of the areas contributing to the proposed subsurface infiltration system as classified by the Soil Survey for Norfolk County Massachusetts are 312B – Woodbridge fine sandy loam 0 to 8 percent slopes with a hydrologic soil group classification of HSG C/D. On-site soil textures are sandy loam based on test pits performed by Level Design Group, LLC. Groundwater recharge will be provided by a proposed subsurface infiltration system. A curtain drain is proposed around the system to lower the groundwater in order to provide the minimum 2-feet of separation.

The on-site soils as classified by the Soil Survey for Plymouth County Massachusetts as Hydrologic Soil Group (HSG) C. The required infiltration for HSG C soil is 0.25 inches of runoff times the total impervious area.

The total post-development impervious area created is 80,078±sf. entirely located within soils with an HSA rating of C.

Water used to satisfy the recharge to groundwater standard is from proposed pavement area. The Simple Dynamic Method of Recharge Volume was utilized to calculate recharged groundwater.

Simple Dynamic Method Calculations for all proposed infiltration practices:

Required Recharge Volume:

**Massachusetts Stormwater Handbook**: Rv = (F) x (New Impervious Area)

F = 0.25 (HSG C)Impervious Area = 80,078 SF  $Rv = (0.25) \times (80,078 \text{ SF}) \times (1 \text{ ft./12 in.})$ = 1,669 CF

Recharge Volume Provided:

<u>SSI-1</u> Lowest Outlet Invert = 322.55 (6" orifice) Volume at El. 322.55 = 1,801 CF  $\rightarrow$  HydroCAD Report



1,801 CF > 1,669 CF

The recharge volume requirement 1,669 CF is exceeded with a total volume of 1,801 CF of storage provided below the lowest outlet of the infiltration systems.

Drawdown Calculations

 $Time_{drawdown} = Rv / (K) x (Bottom Area)$ 

Rv = Required recharge volume

K = Saturated Conductivity Rate

Bottom Area = Bottom area of recharge structure

 $\frac{\text{SSI-1}}{\text{Bottom Area}} = 7,434 \text{ SF}$ K = 0.27 in./hr. Time<sub>drawdown</sub> = 1,801 CF / (0.27 in./hr.) x (7,434 SF) x (1 ft./12 in.) = 10.77 hours

**Redevelopment:** The project has been designed comply with Massachusetts Stormwater Regulations for Standard 3 to the Maximum Extent Practicable.

Compliance to the Maximum Extent Practicable:

- Does the redevelopment design meet Standard 3, comparing post-development to predevelopment conditions? No
- If not, the applicant shall document an analysis of alternative approaches for meeting the Standard? See Alternatives Analysis above.
- What soil types are present on the site? Is the site is comprised solely of C and D soils and bedrock at the land surface? Solely of C and D soils
- Does the project include sites where recharge is proposed at or adjacent to an area classified as contaminated, sites where contamination has been capped in place, sites that have an Activity and Use Limitation (AUL) that precludes inducing runoff to the groundwater, pursuant to MGL Chapter 21E and the Massachusetts Contingency Plan 310 CMR 40.0000; sites that are the location of a solid waste landfill as defined in 310 CMR 19.000; or sites where groundwater from the recharge location flows directly toward a solid waste landfill or 21E site?<sup>1</sup> N/A
- Is the stormwater runoff from a land use with a higher potential pollutant load? N/A
- Is the discharge to the ground located within the Zone II or Interim Wellhead Protection Area of a public water supply? No
- Does the site have an infiltration rate greater than 2.4 inches per hour? No

Improvements to Existing Conditions:

• Does the project increase the required recharge volume over existing (developed) conditions? If so, can the project be redesigned to reduce the required recharge volume by decreasing impervious surfaces (make building higher, put parking under the building, narrower roads, sidewalks on only one side of street, etc.) or using low impact development techniques such as porous pavement?

<sup>&</sup>lt;sup>1</sup> A mounding analysis is needed if a site falls within this category. See Volume 3.



The site increases the recharge volume requirement. Porous pavement was considered as an alternative to provide infiltration but is not practical based on it being primarily utilized by trailer trucks.

- Is the project located within a basin or sub-basin that has been categorized as under high or medium stress by the Massachusetts Water Resources Commission, or where there is other evidence that there are rivers and streams experiencing low flow problems? If so, have measures been considered to replace the natural recharge lost as a result of the prior development? (See Menu.) N/A
- Has the applicant evaluated measures for reducing site runoff? (See Menu.) Yes, See Alternatives Analysis above.

### STANDARD 4: 80% TSS Removal

Stormwater Management Standard 4 requires that, "Stormwater management systems must be designed to remove 80% of the average annual post-construction of Total Suspended Solids (TSS). This standard is met when:

- a. Suitable practices for source control and pollution prevention are identified in a long-term pollution prevention plan and thereafter are implemented and maintained;
- b. Stormwater BMPs are sized to capture the required water quality volume determined in accordance with the Massachusetts Stormwater Handbook and;
- c. Pretreatment is provided in accordance with the Massachusetts Stormwater Handbook"

To achieve the required 80% TSS removal, new stormwater BMP's will be installed. A subsurface infiltration basin is proposed which will collect runoff from all impervious areas within Drainage Area Pla and provide the maximum level or stormwater treatment practicable. A proprietary stormwater treatment unit is proposed which provides treatment prior to discharge to the subsurface infiltration basin. MADEP TSS Removal Sheets are included herein which show 80% TSS removal by the proprietary stormwater treatment unit and the subsurface infiltration basin meeting the requirements for total treatment.

### Water Quality Calculations:

### CDS Stormwater Treatment Unit Sizing

Water quality treatment is provided by using CDS treatment units. The CDS Units are sized using the *Massachusetts Department of Environmental Protection Wetlands Program – Standard Method to Convert Required Water Quality Volume to a Discharge Rate for Sizing Flow Based Manufactured Proprietary Stormwater Treatment Practices.* 

The water quality flow calculations are detailed below:

### Flow to DHM-2/CDS

- $Q_{1,0}=(qu)(A)(WQV)$
- qu=774 csm/in for a Tc of 0.1 hours (taken from Figure 2 of the Massachusetts Department of Environmental Protection Wetlands program - Standard Method to Convert Required Water Quality Volume to a Discharge Rate
- A=1.633 Acres



WQV=1.0 inches

 $Q_{1.0} = (774 \text{ csm/in}) (1.633 \text{ acres}) (0.0015625 \text{ sq. mi} I \text{ acre}) (1.0 \text{ inch})$ 

### Q1.0 = 1.97 cfs < CDS Model 2020-5 Inlet Unit with a Treatment Capacity = 2.20 cfs

### Flow to CB-3/STC-450i

 $Q_{1.0}=(qu)(A)(WQV)$ 

qu=774 csm/in for a Tc of 0.1 hours (taken from Figure 2 of the Massachusetts Department of Environmental Protection Wetlands program - Standard Method to Convert Required Water Quality Volume to a Discharge Rate

A=0.071 Acres WQV=1.0 inches

 $Q_{1,0} = (774 \text{ csm/in}) (0.071 \text{ acres}) (0.0015625 \text{ sq. mi } I \text{ acre}) (1.0 \text{ inch})$ 

### Q1.0 = 0.09 cfs < STC-450i with a Treatment Capacity =0.40 cfs

**Redevelopment:** The project has been designed to fully comply with Massachusetts Stormwater Regulations for Standard 4.

Full compliance for any component that is not a redevelopment Full compliance with the long-term pollution plan requirement for new developments and redevelopments.

- Has the proponent developed a long-term pollution plan that fully meets the requirements of Standard 4? A Long Term Pollution Prevention Plan is provided
- Does the pollution prevention plan include the following source control measures?
  - Street sweeping yes
  - Proper management of snow, salt, sand and other deicing chemicals yes
  - o Proper management of fertilizers, herbicides and pesticides yes
  - Stabilization of existing eroding surfaces yes

Compliance to the Maximum Extent Practicable for the other requirements:

- Does the redevelopment design provide for treatment of all runoff from existing (as well as new) impervious areas to achieve 80% TSS removal? If 80% TSS removal is not achieved, has the stormwater management system been designed to remove TSS to the maximum extent practicable? 80% TSS removal achieved
- Have the proposed stormwater BMPs been properly sized to capture the prescribed runoff volume? Yes
  - One inch rule applies for discharge
    - within a Zone II or Interim Wellhead Protection Area, N/A
    - near or to another critical area, N/A
    - from a land use with a higher potential pollutant load N/A



- to the ground where the infiltration rate is greater than 2.4 inches per hour N/A
- · Has adequate pretreatment been proposed?
  - o 44% TSS Removal Pretreatment Requirement applies if:
    - Stormwater runoff is from a land use with a higher potential pollutant load
    - Stormwater is discharged Yes, 44% TSS removal achieved (Zone II and rapid infiltration)
      - To the ground within the Zone II or Interim Wellhead Protection Area of a Public Water Supply N/A
      - To the ground with an infiltration rate greater than 2.4 inches per hour
         N/A
      - Near or to an Outstanding Resource Water, Special Resource Water, Cold-Water Fishery, Shellfish Growing Area, or Bathing Beach. -N/A

• If the stormwater BMPs do not meet all the requirements set forth above, the applicant shall document an analysis of alternative approaches for meeting the these requirements. (See Section on Retrofitting Existing BMPs (the "Retrofit Section"). N/A

Improvements to Existing Conditions:

- Have measures been provided to achieve at least partial compliance with the TSS removal standard? Fully complies
- Have any of the best management practices in the Retrofit Section been considered? N/A
- Have any of the following pollution prevention measures been considered? Operation & Maintenance and Long Term Pollution Prevention Plans have been prepared for the site in accordance with Massachusetts Stormwater regulations and are included in the Stormwater Report.
  - Reduction or elimination of winter sanding, where safe and prudent to do so
  - Tighter controls over the application of fertilizers, herbicides, and pesticides
  - Landscaping that reduces the need for fertilizer, herbicides and pesticides
  - High frequency sweeping of paved surfaces using vacuum sweepers
  - o Improved catch basin cleaning
  - Waterfowl control programs

Are there any discharges (new or existing) to impaired waters? If so, see TMDL section. N/A

### **STANDARD 5: Higher Potential Pollutant Loads**

Stormwater Management Standard 5 requires that, "For land uses with higher potential pollutant loads, source control and pollution prevention shall be implemented in accordance with the Massachusetts Stormwater Handbook to eliminate or reduce the discharge of stormwater runoff from such land uses to the maximum extent practicable. If through source control and/or pollution prevention, all land uses with higher potential pollutant loads cannot be completely protected from exposure to rain, snow, snow melt and stormwater runoff, the proponent shall use the specific stormwater BMPs determined by the Department to be suitable for such use as provided in the Massachusetts Stormwater Handbook. Stormwater discharges from land uses with higher potential pollutant loads shall also comply with the requirements of the Massachusetts Clean Waters Act, M.G.L. c. 2,§26-53, and the regulations promulgated thereunder at 314 CMF 3.00, 314 CMR 4.00 and 314 CMR 5.00."



The proposed use in not considered a use that would generate Higher Potential Pollutant Loads.

**Redevelopment:** The project use is not considered a use that would generate Higher Potential Pollutant Loads.

### **STANDARD 6: Critical Areas**

Stormwater Management Standard 6 requires that Stormwater discharge to a Zone II Interim Wellhead Protection Area of a public water supply and stormwater discharges near any other critical area require the use of specific source control and pollution prevention measures and the specific stormwater best management practices determined by the Department to be suitable for managing discharges to such area, as provided in the Massachusetts Stormwater Handbook. A discharge near a critical area, if there is a strong likelihood of a significant impact occurring to said area, taking into account site-specific factors. Stormwater discharges to Outstanding Resource Waters or Special Resource Waters shall be set back from the receiving water and receive the highest and best practical method of treatment. A "stormwater discharge," as defined in 314 CMR 3.04(2)(a)1. or (b), to an Outstanding Resource Waters or Special Resource Waters shall comply with 314 CMF 3.00 and 314 CMR 4.00. Stormwater discharges to a Zone I or Zone A area prohibited unless essential to the operation of the public water supply."

The development site is not located within a Critical Area as defined by the Massachusetts Stormwater Handbook.

**Redevelopment:** The project is not located in a critical area as defined by the Massachusetts Stormwater Regulations for Standard 6.

# STANDARD 7: Redevelopment and Other Projects Subject to the Standards only to the Maximum Extent Practicable

The definition of a Redevelopment Project under the definition provided in the MADEP Stormwater Handbook for Standard 7 is listed below:

"Development rehabilitation, expansion and phased projected on previously developed sites, provided that redevelopment results in no next increase in impervious area."

The proposed development is not considered a Redevelopment Project and fully complies with the requirements of the MADEP Stormwater Management Standards.

### STANDARD 8: Erosion and Sediment Control

Stormwater Management Standard 8 requires that, "A plan to control construction-related impacts, including erosion sedimentation and other pollutant sources during construction and land disturbance activities (construction period erosion, sedimentation, and pollution prevention plan), must be developed and implemented."



This standard is met through the type and style of construction. The existing driveway will, to the extent possible, remain intact until the proposed driveway is to be graded and paved. This will provide a pad for wheel cleaning prior to the vehicle exit on Washington Street. The site is self-contained with abutting properties draining overland to the rear of the subject property. Thereby there will be no additional erosion from this property to abutting properties. With careful construction the project will limit erosion potential through the development itself and no additional structural measures, passive or active, are proposed. A Construction Period Pollution and Erosion & Sedimentation Control Plan has also been prepared and is included as part of the Stormwater Report.

**Redevelopment:** The project has been designed to fully comply with Massachusetts Stormwater Regulations for Standard 8.

All redevelopment projects shall fully comply with Standard 8.

Has the proponent submitted a construction period erosion, sedimentation and pollution
prevention plan that meets the requirements of Standard 8?
 A draft Stormwater Pollution Prevention Plan is included with the stormwater report and will be
finalized prior to the start of construction.

### **STANDARD 9: Operation and Maintenance**

Stormwater Management Standard 9 requires that, "A long-term operation and maintenance plan must be developed and implemented to ensure that stormwater management systems function as designed".

This standard is fully met with development and implementation of an Operation and Maintenance Plan is included in Stormwater Management Report.

**Redevelopment:** The project has been designed to fully comply with Massachusetts Stormwater Regulations for Standard 9.

All redevelopment projects shall fully comply with Standard 9.

 Has the proponent submitted a long-term Operation and Maintenance plan that meets the requirements of Standard 9?
 O&M included in Stormwater Report

### **STANDARD 10: Illicit Discharges**

Stormwater Management Standard 10 requires that, "All illicit discharges to the stormwater management system are prohibited".

This standard is fully met with development and implementation of a Long-Term Pollution Prevention which is included in the Stormwater Management Report. An Illicit Discharge statement has been prepared and is included herein.

**Redevelopment:** The project has been designed to fully comply with Massachusetts Stormwater Regulations for Standard 10.



All redevelopment projects shall fully comply with Standard 10.

- Are there any known or suspected illicit discharges to the stormwater management system at the redevelopment project site? No
- Has an illicit connection detection program been implemented using visual screening, dye or smoke testing? No
- Have an Illicit Discharge Compliance Statement and associated site map been submitted verifying that there are no illicit discharges to the stormwater management system at the site? Yes

Improvements to Existing Conditions:

• Once all illicit discharges are removed, has the proponent implemented any measures to prevent additional illicit discharges? N/A

### CONCLUSION

The proposed redevelopment of this parcel will be a significant improvement to the area and to the resource area on and adjacent to the site. The proposed 2081 redevelopment meets or exceeds the current MADEP Stormwater Management Standards and Guidelines and provides a stormwater management system that will maintain water quality while attenuating peak rates of runoff at the control points. This was achieved by using pretreatment BMPs and directing the stormwater runoff to a subsurface infiltration basin which attenuates peak flows, provides groundwater recharge, and provides a high level of TSS removal. An Operation and Maintenance Plan for post-construction maintenance of the Stormwater Management System has been developed and is included with this report.



## **MADEP Stormwater Report Checklist**



### Massachusetts Department of Environmental Protection Bureau of Resource Protection - Wetlands Program Checklist for Stormwater Report

### A. Introduction

Important: When filling out forms on the computer, use only the tab key to move your cursor - do not use the return key



A Stormwater Report must be submitted with the Notice of Intent permit application to document compliance with the Stormwater Management Standards. The following checklist is NOT a substitute for the Stormwater Report (which should provide more substantive and detailed information) but is offered here as a tool to help the applicant organize their Stormwater Management documentation for their Report and for the reviewer to assess this information in a consistent format. As noted in the Checklist, the Stormwater Report must contain the engineering computations and supporting information set forth in Volume 3 of the Massachusetts Stormwater Handbook. The Stormwater Report must be prepared and certified by a Registered Professional Engineer (RPE) licensed in the Commonwealth.

The Stormwater Report must include:

- The Stormwater Checklist completed and stamped by a Registered Professional Engineer (see page 2) that certifies that the Stormwater Report contains all required submittals.<sup>1</sup> This Checklist is to be used as the cover for the completed Stormwater Report.
- Applicant/Project Name
- Project Address
- Name of Firm and Registered Professional Engineer that prepared the Report
- Long-Term Pollution Prevention Plan required by Standards 4-6
- Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan required by Standard 8<sup>2</sup>
- Operation and Maintenance Plan required by Standard 9

In addition to all plans and supporting information, the Stormwater Report must include a brief narrative describing stormwater management practices, including environmentally sensitive site design and LID techniques, along with a diagram depicting runoff through the proposed BMP treatment train. Plans are required to show existing and proposed conditions, identify all wetland resource areas, NRCS soil types, critical areas, Land Uses with Higher Potential Pollutant Loads (LUHPPL), and any areas on the site where infiltration rate is greater than 2.4 inches per hour. The Plans shall identify the drainage areas for both existing and proposed conditions at a scale that enables verification of supporting calculations.

As noted in the Checklist, the Stormwater Management Report shall document compliance with each of the Stormwater Management Standards as provided in the Massachusetts Stormwater Handbook. The soils evaluation and calculations shall be done using the methodologies set forth in Volume 3 of the Massachusetts Stormwater Handbook.

To ensure that the Stormwater Report is complete, applicants are required to fill in the Stormwater Report Checklist by checking the box to indicate that the specified information has been included in the Stormwater Report. If any of the information specified in the checklist has not been submitted, the applicant must provide an explanation. The completed Stormwater Report Checklist and Certification must be submitted with the Stormwater Report.

<sup>&</sup>lt;sup>1</sup> The Stormwater Report may also include the Illicit Discharge Compliance Statement required by Standard 10. If not included in the Stormwater Report, the Illicit Discharge Compliance Statement must be submitted prior to the discharge of stormwater runoff to the post-construction best management practices.

<sup>&</sup>lt;sup>2</sup> For some complex projects, it may not be possible to include the Construction Period Erosion and Sedimentation Control Plan in the Stormwater Report. In that event, the issuing authority has the discretion to issue an Order of Conditions that approves the project and includes a condition requiring the proponent to submit the Construction Period Erosion and Sedimentation Control Plan before commencing any land disturbance activity on the site.



### Massachusetts Department of Environmental Protection Bureau of Resource Protection - Wetlands Program Checklist for Stormwater Report

### **B. Stormwater Checklist and Certification**

The following checklist is intended to serve as a guide for applicants as to the elements that ordinarily need to be addressed in a complete Stormwater Report. The checklist is also intended to provide conservation commissions and other reviewing authorities with a summary of the components necessary for a comprehensive Stormwater Report that addresses the ten Stormwater Standards.

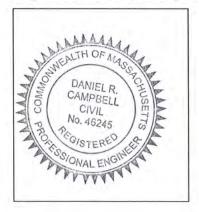
*Note:* Because stormwater requirements vary from project to project, it is possible that a complete Stormwater Report may not include information on some of the subjects specified in the Checklist. If it is determined that a specific item does not apply to the project under review, please note that the item is not applicable (N.A.) and provide the reasons for that determination.

A complete checklist must include the Certification set forth below signed by the Registered Professional Engineer who prepared the Stormwater Report.

### **Registered Professional Engineer's Certification**

I have reviewed the Stormwater Report, including the soil evaluation, computations, Long-term Pollution Prevention Plan, the Construction Period Erosion and Sedimentation Control Plan (if included), the Long-term Post-Construction Operation and Maintenance Plan, the Illicit Discharge Compliance Statement (if included) and the plans showing the stormwater management system, and have determined that they have been prepared in accordance with the requirements of the Stormwater Management Standards as further elaborated by the Massachusetts Stormwater Handbook. I have also determined that the information presented in the Stormwater Checklist is accurate and that the information presented in the Stormwater Report accurately reflects conditions at the site as of the date of this permit application.

Registered Professional Engineer Block and Signature



10/16/23 Signature and Date

Checklist

**Project Type:** Is the application for new development, redevelopment, or a mix of new and redevelopment?

New development

Redevelopment

Mix of New Development and Redevelopment



### Checklist (continued)

LID Measures: Stormwater Standards require LID measures to be considered. Document what environmentally sensitive design and LID Techniques were considered during the planning and design of the project:

$\square$	No disturbance to any Wetland Resource Areas
	Site Design Practices (e.g. clustered development, reduced frontage setbacks)
	Reduced Impervious Area (Redevelopment Only)
	Minimizing disturbance to existing trees and shrubs
	LID Site Design Credit Requested:
	Credit 1
	Credit 2
	Credit 3
	Use of "country drainage" versus curb and gutter conveyance and pipe
	Bioretention Cells (includes Rain Gardens)
	Constructed Stormwater Wetlands (includes Gravel Wetlands designs)
	Treebox Filter
	Water Quality Swale
	Grass Channel
	Green Roof
	Other (describe):
•	

#### Standard 1: No New Untreated Discharges

No new untreated discharges

- Outlets have been designed so there is no erosion or scour to wetlands and waters of the Commonwealth
- Supporting calculations specified in Volume 3 of the Massachusetts Stormwater Handbook included.



### Checklist (continued)

#### Standard 2: Peak Rate Attenuation

- Standard 2 waiver requested because the project is located in land subject to coastal storm flowage and stormwater discharge is to a wetland subject to coastal flooding.
- Evaluation provided to determine whether off-site flooding increases during the 100-year 24-hour storm.

Calculations provided to show that post-development peak discharge rates do not exceed predevelopment rates for the 2-year and 10-year 24-hour storms. If evaluation shows that off-site flooding increases during the 100-year 24-hour storm, calculations are also provided to show that post-development peak discharge rates do not exceed pre-development rates for the 100-year 24hour storm.

#### Standard 3: Recharge

Soil Analysis provided.

- Required Recharge Volume calculation provided.
- Required Recharge volume reduced through use of the LID site Design Credits.
- Sizing the infiltration, BMPs is based on the following method: Check the method used.

Static	Simple Dynamic
--------	----------------

Dynamic Field<sup>1</sup>

- Runoff from all impervious areas at the site discharging to the infiltration BMP.
- Runoff from all impervious areas at the site is *not* discharging to the infiltration BMP and calculations are provided showing that the drainage area contributing runoff to the infiltration BMPs is sufficient to generate the required recharge volume.

Recharge BMPs have been sized to infiltrate the Required Recharge Volume.

$\boxtimes$	Recharge BMPs have been sized to infiltrate the Required Recharge Volume only to the maximum
	extent practicable for the following reason:

- $\boxtimes$  Site is comprised solely of C and D soils and/or bedrock at the land surface
- M.G.L. c. 21E sites pursuant to 310 CMR 40.0000
- Solid Waste Landfill pursuant to 310 CMR 19.000
- Project is otherwise subject to Stormwater Management Standards only to the maximum extent practicable.
- Calculations showing that the infiltration BMPs will drain in 72 hours are provided.

	Property includes	a M.G.L. c. 21E site c	r a solid waste landfil	I and a mounding a	nalysis is included.
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<sup>&</sup>lt;sup>1</sup> 80% TSS removal is required prior to discharge to infiltration BMP if Dynamic Field method is used.



### Checklist (continued)

### Standard 3: Recharge (continued)

The infiltration BMP is used to attenuate peak flows during storms greater than or equal to the 10year 24-hour storm and separation to seasonal high groundwater is less than 4 feet and a mounding analysis is provided.

Documentation is provided showing that infiltration BMPs do not adversely impact nearby wetland resource areas.

#### **Standard 4: Water Quality**

The Long-Term Pollution Prevention Plan typically includes the following:

- Good housekeeping practices;
- Provisions for storing materials and waste products inside or under cover;
- Vehicle washing controls;
- Requirements for routine inspections and maintenance of stormwater BMPs;
- Spill prevention and response plans;
- Provisions for maintenance of lawns, gardens, and other landscaped areas;
- Requirements for storage and use of fertilizers, herbicides, and pesticides;
- Pet waste management provisions;
- Provisions for operation and management of septic systems;
- Provisions for solid waste management;
- Snow disposal and plowing plans relative to Wetland Resource Areas;
- Winter Road Salt and/or Sand Use and Storage restrictions;
- Street sweeping schedules;
- Provisions for prevention of illicit discharges to the stormwater management system;
- Documentation that Stormwater BMPs are designed to provide for shutdown and containment in the event of a spill or discharges to or near critical areas or from LUHPPL;
- Training for staff or personnel involved with implementing Long-Term Pollution Prevention Plan;
- List of Emergency contacts for implementing Long-Term Pollution Prevention Plan.
- A Long-Term Pollution Prevention Plan is attached to Stormwater Report and is included as an attachment to the Wetlands Notice of Intent.
- Treatment BMPs subject to the 44% TSS removal pretreatment requirement and the one inch rule for calculating the water quality volume are included, and discharge:
  - is within the Zone II or Interim Wellhead Protection Area
  - is near or to other critical areas
  - is within soils with a rapid infiltration rate (greater than 2.4 inches per hour)
  - involves runoff from land uses with higher potential pollutant loads.
- The Required Water Quality Volume is reduced through use of the LID site Design Credits.
- Calculations documenting that the treatment train meets the 80% TSS removal requirement and, if applicable, the 44% TSS removal pretreatment requirement, are provided.



Checklist	(continued)
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### Standard 4: Water Quality (continued)

- The BMP is sized (and calculations provided) based on:
  - ☐ The ½" or 1" Water Quality Volume or
  - The equivalent flow rate associated with the Water Quality Volume and documentation is provided showing that the BMP treats the required water quality volume.
- The applicant proposes to use proprietary BMPs, and documentation supporting use of proprietary BMP and proposed TSS removal rate is provided. This documentation may be in the form of the propriety BMP checklist found in Volume 2, Chapter 4 of the Massachusetts Stormwater Handbook and submitting copies of the TARP Report, STEP Report, and/or other third party studies verifying performance of the proprietary BMPs.
- A TMDL exists that indicates a need to reduce pollutants other than TSS and documentation showing that the BMPs selected are consistent with the TMDL is provided.

#### Standard 5: Land Uses With Higher Potential Pollutant Loads (LUHPPLs)

- The NPDES Multi-Sector General Permit covers the land use and the Stormwater Pollution Prevention Plan (SWPPP) has been included with the Stormwater Report.
- The NPDES Multi-Sector General Permit covers the land use and the SWPPP will be submitted **prior to** the discharge of stormwater to the post-construction stormwater BMPs.
- The NPDES Multi-Sector General Permit does *not* cover the land use.
- LUHPPLs are located at the site and industry specific source control and pollution prevention measures have been proposed to reduce or eliminate the exposure of LUHPPLs to rain, snow, snow melt and runoff, and been included in the long term Pollution Prevention Plan.
- All exposure has been eliminated.
- All exposure has *not* been eliminated and all BMPs selected are on MassDEP LUHPPL list.
- The LUHPPL has the potential to generate runoff with moderate to higher concentrations of oil and grease (e.g. all parking lots with >1000 vehicle trips per day) and the treatment train includes an oil grit separator, a filtering bioretention area, a sand filter or equivalent.

#### **Standard 6: Critical Areas**

- The discharge is near or to a critical area and the treatment train includes only BMPs that MassDEP has approved for stormwater discharges to or near that particular class of critical area.
- Critical areas and BMPs are identified in the Stormwater Report.



### Checklist (continued)

# Standard 7: Redevelopments and Other Projects Subject to the Standards only to the maximum extent practicable

The project is subject to the Stormwater Management Standards only to the maximum Extent Practicable as a:

Limited	Project
---------	---------

- Small Residential Projects: 5-9 single family houses or 5-9 units in a multi-family development provided there is no discharge that may potentially affect a critical area.
- Small Residential Projects: 2-4 single family houses or 2-4 units in a multi-family development with a discharge to a critical area
- Marina and/or boatyard provided the hull painting, service and maintenance areas are protected from exposure to rain, snow, snow melt and runoff
- Bike Path and/or Foot Path
- Redevelopment Project
- Redevelopment portion of mix of new and redevelopment.
- Certain standards are not fully met (Standard No. 1, 8, 9, and 10 must always be fully met) and an explanation of why these standards are not met is contained in the Stormwater Report.

☐ The project involves redevelopment and a description of all measures that have been taken to improve existing conditions is provided in the Stormwater Report. The redevelopment checklist found in Volume 2 Chapter 3 of the Massachusetts Stormwater Handbook may be used to document that the proposed stormwater management system (a) complies with Standards 2, 3 and the pretreatment and structural BMP requirements of Standards 4-6 to the maximum extent practicable and (b) improves existing conditions.

### Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control

A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan must include the following information:

- Narrative;
- Construction Period Operation and Maintenance Plan;
- Names of Persons or Entity Responsible for Plan Compliance;
- Construction Period Pollution Prevention Measures;
- Erosion and Sedimentation Control Plan Drawings;
- Detail drawings and specifications for erosion control BMPs, including sizing calculations;
- Vegetation Planning;
- Site Development Plan;
- Construction Sequencing Plan;
- Sequencing of Erosion and Sedimentation Controls;
- Operation and Maintenance of Erosion and Sedimentation Controls;
- Inspection Schedule;
- Maintenance Schedule;
- Inspection and Maintenance Log Form.

A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan containing the information set forth above has been included in the Stormwater Report.



### Checklist (continued)

# **Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control** (continued)

- ☐ The project is highly complex and information is included in the Stormwater Report that explains why it is not possible to submit the Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan with the application. A Construction Period Pollution Prevention and Erosion and Sedimentation Control has *not* been included in the Stormwater Report but will be submitted *before* land disturbance begins.
- The project is *not* covered by a NPDES Construction General Permit.
- The project is covered by a NPDES Construction General Permit and a copy of the SWPPP is in the Stormwater Report.
- The project is covered by a NPDES Construction General Permit but no SWPPP been submitted. The SWPPP will be submitted BEFORE land disturbance begins.

#### **Standard 9: Operation and Maintenance Plan**

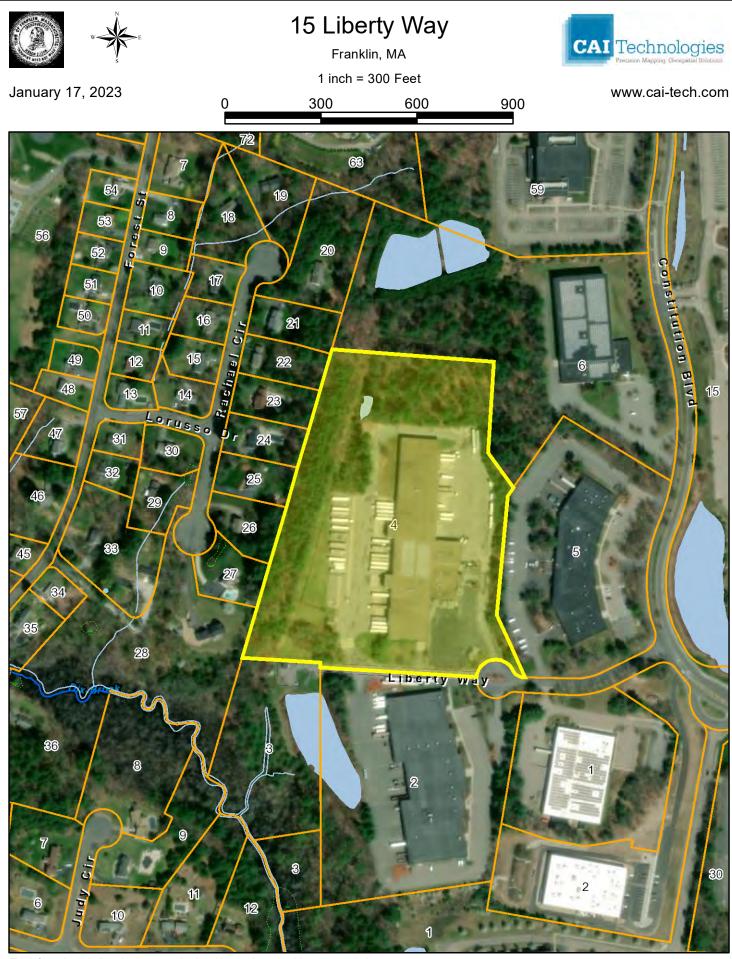
- The Post Construction Operation and Maintenance Plan is included in the Stormwater Report and includes the following information:
  - Name of the stormwater management system owners;
  - Party responsible for operation and maintenance;
  - Schedule for implementation of routine and non-routine maintenance tasks;
  - Plan showing the location of all stormwater BMPs maintenance access areas;
  - Description and delineation of public safety features;
  - Estimated operation and maintenance budget; and
  - Operation and Maintenance Log Form.
- The responsible party is *not* the owner of the parcel where the BMP is located and the Stormwater Report includes the following submissions:
  - A copy of the legal instrument (deed, homeowner's association, utility trust or other legal entity) that establishes the terms of and legal responsibility for the operation and maintenance of the project site stormwater BMPs;
  - A plan and easement deed that allows site access for the legal entity to operate and maintain BMP functions.

#### Standard 10: Prohibition of Illicit Discharges

- The Long-Term Pollution Prevention Plan includes measures to prevent illicit discharges;
- An Illicit Discharge Compliance Statement is attached;
- NO Illicit Discharge Compliance Statement is attached but will be submitted *prior to* the discharge of any stormwater to post-construction BMPs.



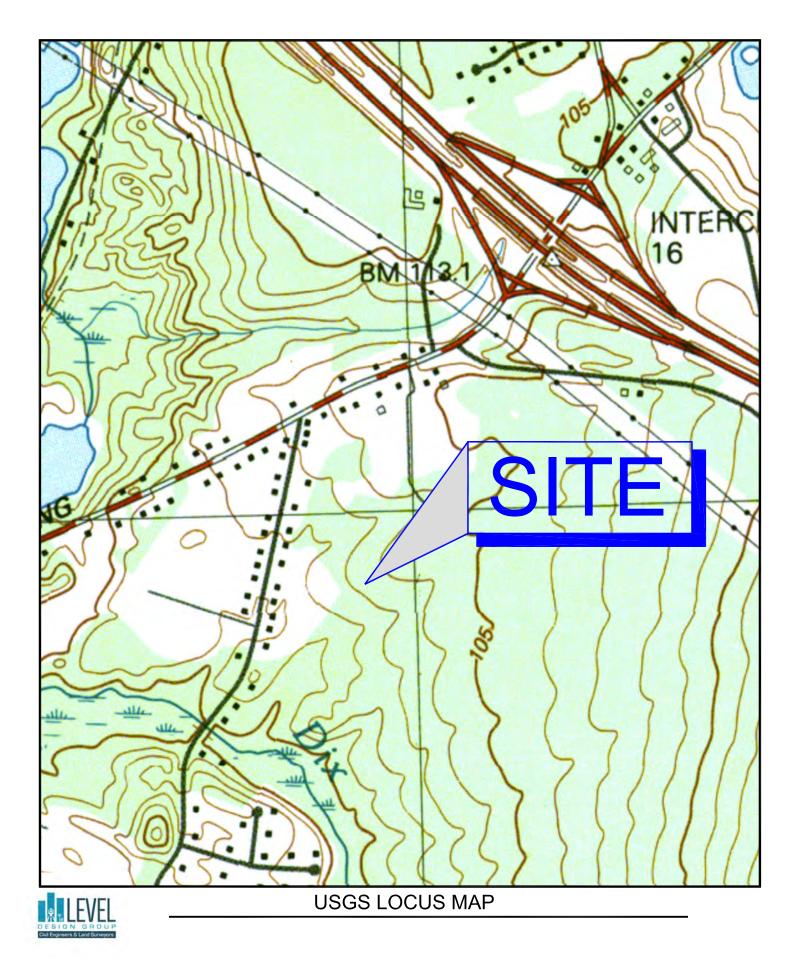
# Aerial Photograph (MAGIS)



This information is believed to be correct but is subject to change and is not warrantied.



## **USGS Topographic Map (MAGIS)**



CIVIL ENGINEERS AND LAND SURVEYORS 249 SOUTH STREET, UNIT 1 PLAINVILLE, MA 02762 508.695.2221 (F) 508.695.2219 WWW.LEVELDG.COM

### 15 LIBERTY WAY FRANKLIN, MA



## **On-Site Soils Documentation**

Project No:	2081.00	Soil Evaluator	Adam Hunt E.I.T.	SE# 12794
Project:	15 Liberty Way Franklin	Тетр	48F Rain	
Date of Testing	11/16/22			

Test Hole No.:	TH-1	Ground Elevation at Hole = 334.70
Time:	10:15 AM	Groundwater Elevation = 331.78

Depth (inches)	Horizon	Color	Texture	Redox Depth	Redox Color	Comments
0-10	А	10YR 2/2	SL			
10-24	В	10YR 5/6	SL			
24-108	C1	2.5Y 6/3	SL	35"		Very Compact
Weeping Observe	ed		none			
Standing Water C	bserved	none				
Redox Observed				35"		

Test Hole No.:	TH-2	Ground Elevation at Hole = 331.05
Time:	11:00 AM	Groundwater Elevation = 328.38

Depth (inches)	Horizon	Color	Texture	Redox Depth	Redox Color	Comments
0-12	А	10YR 2/2	SL			
12-24	В	10YR 5/6	SL			
24-120	C1	2.5Y 6/3	SL	32"		Very Compact
Weeping Observe	ed					
Standing Water C	bserved	none		none		
Redox Observed			32"			]

 Test Hole No.:
 TH-3

 Time:
 11:45 AM

Ground Elevation at Hole = 328.50 Groundwater Elevation = 326.00

Depth (inches)	Horizon	Color	Texture	Redox Depth	Redox Color	Comments
0-12	А	10YR 2/2	SL			
12-28	В	10YR 5/6	SL			
28-72	C1	2.5Y 6/3	SL	30"		Very Compact
Weeping Observe	Weeping Observed none					
Standing Water Observed		none				
Redox Observed		30"				]

Project No:	2081.00	Soil Evaluator	Adam Hunt E.I.T.	SE# 12794
Project:	15 Liberty Way Franklin	Temp	68F Sunny	
Date of Testing	10/4/23			

Test Hole No.:	TH-4	Ground Elevation at Hole = 325.65
Time:	9:45 AM	Groundwater Elevation = 323.32

Depth (inches)	Horizon	Color	Texture	Redox Depth	Redox Color	Comments
0-10	А	10YR 2/2	SL			
10-20	В	10YR 5/6	SL			
20-100	C1	2.5Y 6/3	SL	28"		Very Compact
Weeping Observe	Weeping Observed					
Standing Water Observed						
Redox Observed				28"		

Test Hole No.:	TH-5	Ground Elevation at Hole = 326.45
Time:	10:30 AM	Groundwater Elevation = 323.03

Depth (inches)	Horizon	Color	Texture	Redox Depth	<b>Redox Color</b>	Comments
0-12	А	10YR 2/2	SL			
12-18	В	10YR 5/6	SL			
18-76	C1	2.5Y 6/3	SL	41"		Very Compact
Weeping Observe	Weeping Observed 41"					
Standing Water C	bserved	69"				
Redox Observed				41"		

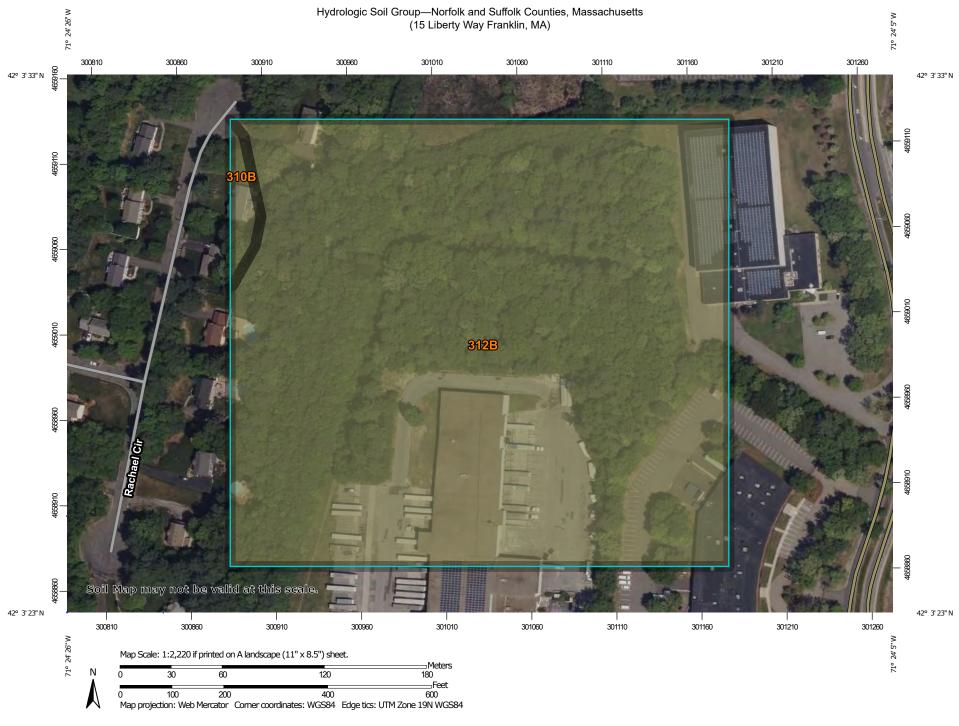
Test Hole No.: TH-6 Time: 11:15 AM

Ground Elevation at Hole = 325.70 Groundwater Elevation = 323.45

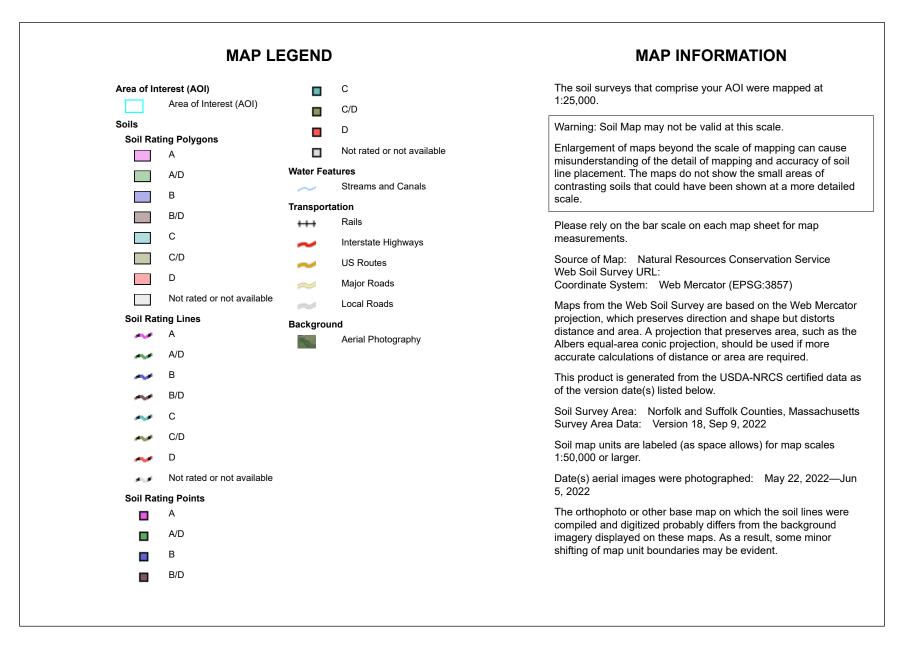
Depth (inches)	Horizon	Color	Texture	Redox Depth	Redox Color	Comments
0-12	А	10YR 2/2	SL			
12-24	В	10YR 5/6	SL			
24-84	C1	2.5Y 6/3	SL	27"		Very Compact
Weeping Observe	ed			36"		
Standing Water C	bserved			82"		
Redox Observed				27"		

Test Hole No.: TH-7 Time: 12:00 AM Ground Elevation at Hole = 324.90 Groundwater Elevation = 322.65

Depth (inches)	Horizon	Color	Texture	Redox Depth	Redox Color	Comments
0-10	А	10YR 2/2	SL			
10-20	В	10YR 5/6	SL			
20-90	C1	2.5Y 6/3	SL	27"		Very Compact
Weeping Observed				50"		
Standing Water Observed						
Redox Observed				27"		



USDA Natural Resources Conservation Service Web Soil Survey National Cooperative Soil Survey



### Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
310B	Woodbridge fine sandy loam, 3 to 8 percent slopes	C/D	0.3	1.5%
312B	Woodbridge fine sandy loam, 0 to 8 percent slopes, extremely stony	C/D	18.8	98.5%
Totals for Area of Interest			19.0	100.0%

### Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

### **Rating Options**

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher





# **Stormwater Treatment Unit Information**

### STORM WATER TREATMENT DEVICE

### 1.0 GENERAL

- 1.1 This item shall govern the furnishing and installation of the CDS<sup>®</sup> by Contech Engineered Solutions LLC, complete and operable as shown and as specified herein, in accordance with the requirements of the plans and contract documents.
- 1.2 The Contractor shall furnish all labor, equipment and materials necessary to install the storm water treatment device(s) (SWTD) and appurtenances specified in the Drawings and these specifications.
- 1.3 The manufacturer of the SWTD shall be one that is regularly engaged in the engineering design and production of systems deployed for the treatment of storm water runoff for at least five (5) years and which have a history of successful production, acceptable to the Engineer. In accordance with the Drawings, the SWTD(s) shall be a CDS<sup>®</sup> device manufactured by:

Contech Engineered Solutions LLC 9025 Centre Pointe Drive West Chester, OH, 45069 Tel: 1 800 338 1122

### 1.4 Related Sections

- 1.4.1 Section 02240: Dewatering
- 1.4.2 Section 02260: Excavation Support and Protection
- 1.4.3 Section 02315: Excavation and Fill
- 1.4.4 Section 02340: Soil Stabilization
- 1.5 All components shall be subject to inspection by the engineer at the place of manufacture and/or installation. All components are subject to being rejected or identified for repair if the quality of materials and manufacturing do not comply with the requirements of this specification. Components which have been identified as defective may be subject for repair where final acceptance of the component is contingent on the discretion of the Engineer.
- 1.6 The manufacturer shall guarantee the SWTD components against all manufacturer originated defects in materials or workmanship for a period of twelve (12) months from the date the components are delivered to the owner for installation. The manufacturer shall upon its determination repair, correct or replace any manufacturer originated defects advised in writing to the manufacturer within the referenced warranty period. The use of SWTD components shall be limited to the application for which it was specifically designed.
- 1.7 The SWTD manufacturer shall submit to the Engineer of Record a "Manufacturer's Performance Certification" certifying that each SWTD is capable of achieving the specified removal efficiencies listed in these specifications. The certification shall be supported by independent third-party research

1.8 No product substitutions shall be accepted unless submitted 10 days prior to project bid date, or as directed by the Engineer of Record. Submissions for substitutions require review and approval by the Engineer of Record, for hydraulic performance, impact to project designs, equivalent treatment performance, and any required project plan and report (hydrology/hydraulic, water quality, stormwater pollution) modifications that would be required by the approving jurisdictions/agencies. Contractor to coordinate with the Engineer of Record any applicable modifications to the project estimates of cost, bonding amount determinations, plan check fees for changes to approved documents, and/or any other regulatory requirements resulting from the product substitution.

### 2.0 MATERIALS

- 2.1 Housing unit of stormwater treatment device shall be constructed of pre-cast or cast-in-place concrete, no exceptions. Precast concrete components shall conform to applicable sections of ASTM C 478, ASTM C 857 and ASTM C 858 and the following:
  - 2.1.1 Concrete shall achieve a minimum 28-day compressive strength of 4,000 pounds per square-inch (psi);
  - 2.1.2 Unless otherwise noted, the precast concrete sections shall be designed to withstand lateral earth and AASHTO H-20 traffic loads;
  - 2.1.3 Cement shall be Type III Portland Cement conforming to ASTM C 150;
  - 2.1.4 Aggregates shall conform to ASTM C 33;
  - 2.1.5 Reinforcing steel shall be deformed billet-steel bars, welded steel wire or deformed welded steel wire conforming to ASTM A 615, A 185, or A 497.
  - 2.1.6 Joints shall be sealed with preformed joint sealing compound conforming to ASTM C 990.
  - 2.1.7 Shipping of components shall not be initiated until a minimum compressive strength of 4,000 psi is attained or five (5) calendar days after fabrication has expired, whichever occurs first.
- 2.2 Internal Components and appurtenances shall conform to the following:
  - 2.2.1 Screen and support structure shall be manufactured of Type 316 and 316L stainless steel conforming to ASTM F 1267-01;
  - 2.2.2 Hardware shall be manufactured of Type 316 stainless steel conforming to ASTM A 320;
  - 2.2.3 Fiberglass components shall conform to the ASTM D-4097
  - 2.2.4 Access system(s) conform to the following:
  - 2.2.5 Manhole castings shall be designed to withstand AASHTO H-20 loadings and manufactured of cast-iron conforming to ASTM A 48 Class 30.

### 3.0 PERFORMANCE

- 3.1 The SWTD shall be sized to either achieve an 80 percent average annual reduction in the total suspended solid load or treat a flow rate designated by the jurisdiction in which the project is located. Both methods should be sized using a particle size distribution having a mean particle size (d<sub>50</sub>) of 125 microns unless otherwise stated.
- 3.2 The SWTD shall be capable of capturing and retaining 100 percent of pollutants greater than or equal to 2.4 millimeters (mm) regardless of the pollutant's specific gravity (i.e.: floatable and neutrally buoyant materials) for flows up to the device's rated-treatment capacity. The SWTD shall be designed to retain all previously captured pollutants addressed by this

subsection under all flow conditions. The SWTD shall be capable of capturing and retaining total petroleum hydrocarbons. The SWTD shall be capable of achieving a removal efficiency of 92 and 78 percent when the device is operating at 25 and 50 percent of its rated-treatment capacity. These removal efficiencies shall be based on independent third-party research for influent oil concentrations representative of storm water runoff ( $20 \pm 5 \text{ mg/L}$ ). The SWTD shall be greater than 99 percent effective in controlling dry-weather accidental oil spills.

- 3.3 The SWTD shall be designed with a sump chamber for the storage of captured sediments and other negatively buoyant pollutants in between maintenance cycles. The minimum storage capacity provided by the sump chamber shall be in accordance with the volume listed in Table 1. The boundaries of the sump chamber shall be limited to that which do not degrade the SWTD's treatment efficiency as captured pollutants accumulate. The sump chamber shall be separate from the treatment processing portion(s) of the SWTD to minimize the probability of fine particle re-suspension. In order to not restrict the Owner's ability to maintain the SWTD, the minimum dimension providing access from the ground surface to the sump chamber shall be 16 inches in diameter.
- 3.4 The SWTD shall be designed to capture and retain Total Petroleum Hydrocarbons generated by wet-weather flow and dry-weather gross spills and have a capacity listed in Table 1 of the required unit.
- 3.5 The SWTD shall convey the flow from the peak storm event of the drainage network, in accordance with required hydraulic upstream conditions as defined by the Engineer. If a substitute SWTD is proposed, supporting documentation shall be submitted that demonstrates equal or better upstream hydraulic conditions compared to that specified herein. This documentation shall be signed and sealed by a Professional Engineer registered in the State of the work. All costs associated with preparing and certifying this documentation shall be born solely by the Contractor.
- 3.6 The SWTD shall have completed field tested following TARP Tier II protocol requirements

### 4.0 EXECUTION

- 4.1 The contractor shall exercise care in the storage and handling of the SWTD components prior to and during installation. Any repair or replacement costs associated with events occurring after delivery is accepted and unloading has commenced shall be borne by the contractor.
- 4.2 The SWTD shall be installed in accordance with the manufacturer's recommendations and related sections of the contract documents. The manufacturer shall provide the contractor installation instructions and offer on-site guidance during the important stages of the installation as identified by the manufacturer at no additional expense. A minimum of 72 hours notice shall be provided to the manufacturer prior to their performance of the services included under this subsection.
- 4.3 The contractor shall fill all voids associated with lifting provisions provided by the manufacturer. These voids shall be filled with non-shrinking grout providing a finished surface consistent with adjacent surfaces. The contractor shall trim all protruding lifting provisions flush with the adjacent concrete surface in a manner, which leaves no sharp points or edges.

4.4 The contractor shall removal all loose material and pooling water from the SWTD prior to the transfer of operational responsibility to the Owner.

Storage Capacities						
CDS Model	Minimum Sump Storage Capacity (yd <sup>3</sup> )/(m <sup>3</sup> )	Minimum Oil Storage Capacity (gal)/(L)				
CDS2015-4	0.9(0.7)	61(232)				
CDS2015-5	1.5(1.1)	83(313)				
CDS2020-5	1.5(1.1)	99(376)				
CDS2025-5	1.5(1.1)	116(439)				
CDS3020-6	2.1 (1.6)	184(696)				
CDS3025-6	2.1(1.6)	210(795)				
CDS3030-6	2.1 (1.6)	236(895)				
CDS3035-6	2.1 (1.6)	263(994)				
CDS3535-7	2.9(2.2)	377(1426)				
CDS4030-8	5.6(4.3)	426(1612)				
CDS4040-8	5.6 (4.3)	520(1970)				
CDS4045-8	5.6 (4.3)	568(2149)				
CDS5640-10	8.7(6.7)	758(2869)				
CDS5653-10	8.7(6.7)	965(3652)				
CDS5668-10	8.7(6.7)	1172(4435)				
CDS5678-10	8.7(6.7)	1309(4956)				
CDS7070-DV	3.6(2.8)	914 (3459)				
CDS10060-DV	5.0 (3.8)	792 (2997)				
CDS10080-DV	5.0 (3.8)	1057 (4000)				
CDS100100-DV	5.0 (3.8)	1320 (4996)				

TABLE 1 Storm Water Treatment Device Storage Capacities

END OF SECTION







# The experts you need to solve your stormwater challenges

Contech is the leader in stormwater solutions, helping engineers, contractors and owners with infrastructure and land development projects throughout North America.

With our responsive team of stormwater experts, local regulatory expertise and flexible solutions, Contech is the trusted partner you can count on for stormwater management solutions.

# **Your Contech Team**









### STORMWATER CONSULTANT

It's my job to recommend the best solution to meet permitting requirements.

#### STORMWATER DESIGN ENGINEER

I work with consultants to design the best approved solution to meet your project's needs.

### **REGULATORY MANAGER**

I understand the local stormwater regulations and what solutions will be approved.

SALES ENGINEER

I make sure our solutions meet the needs of the contractor during construction.

### Contech is your partner in stormwater management solutions



# Removing Pollutants using Hydrodynamic Separation

HDS systems play a vital role in protecting our waterways by removing high levels of sediment, trash, debris, and hydrocarbons from stormwater runoff.

Frequently used as end-of-pipe solutions, they are also used to provide stormwater quality treatment in places where space is limited.

HDS systems capture and retain a variety of stormwater pollutants and are very easy to maintain. These two key benefits have resulted in new uses for HDS technologies, such as pretreating detention, Low Impact Development, and green infrastructure practices, as well as other land-based stormwater treatment systems. Utilize high-performance hydrodynamic separation to effectively remove finer sediment, oil and grease, and floating and sinking debris.







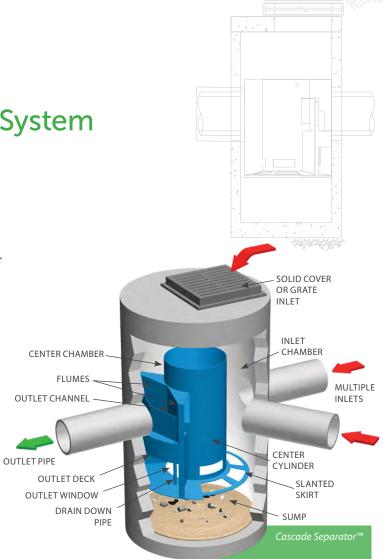


# The Cascade Separator® System

### Advanced Sediment Capture Technology ...

The Cascade Separator<sup>®</sup> is the newest innovation in stormwater treatment from Contech. The Cascade Separator was developed by Contech's stormwater experts using advanced modeling tools and Contech's industry leading stormwater laboratory.

This innovative hydrodynamic separator excels at sediment capture and retention while also removing hydrocarbons, trash, and debris from stormwater runoff. What makes the Cascade Separator unique is the use of opposing vortices that enhance particle settling and a unique skirt design that allows for sediment transport into the sump while reducing turbulence and resuspension of previously captured material. These two factors allow the Cascade Separator to treat high flow rates in a small footprint, resulting in an efficient and economical solution for any site.



FEATURE	BENEFIT
Unique skirt design & opposing vortices	Superior TSS removal; reduced system size and costs
Inlet area accepts wide range of inlet pipe angles	Design and installation flexibility
Accepts multiple inlet pipes*	Eliminates the need for separate junction structure
Grate inlet option*	Eliminates the need for a separate grate inlet structure
Internal bypass	Eliminates the need for a separate bypass structure
Clear access to sump and stored pollutants	Fast, easy maintenance

www.ContechES.com/cascade

Learn More:

### SELECT CASCADE APPROVALS

 New Jersey Department of Environmental Protection Certification (NJDEP)

#### CASCADE MAINTENANCE

Cascade provides unobstructed access to stored pollutants, making it easy to maintain using a vacuum truck, with no requirement to enter the unit.

\* NJDEP testing based on Cascade Separator with one inlet pipe and no grate inlet

### Setting new standards in Stormwater Treatment

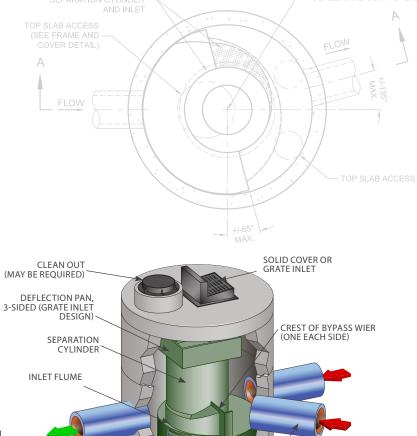
# The CDS® System

### Superior TSS and Trash Removal ...

The CDS is a hybrid technology that uses a combination of swirl concentration and indirect screening to separate and trap sediment, trash, debris, and hydrocarbons from stormwater runoff.

At the heart of the CDS system is a unique screening technology used to capture and retain sediment. The screen face is louvered so that it is smooth in the downstream direction. The effect created is called "Continuous Deflective Separation." The power of the incoming flow is harnessed to continually shear debris off the screen and to direct trash and sediment toward the center of the separation cylinder. This results in a screen that is self-cleaning and provides 100% removal of floatables and neutrally buoyant material debris 2.4 mm or larger, without blinding.

FEATURE	BENEFIT
Unique flow path and isolated storage sump	Excellent TSS capture and retention
Captures and retains 100% of floatables and neutrally buoyant debris 2.4 MM or larger	Superior trash removal
Self-cleaning screen	Ease of maintenance
Inline, offline, multiple inlet pipes, grate inlet, and drop inlet configurations available	Design flexibility
Internal bypass	Eliminates the need for additional structures
Clear access to sump and stored pollutants	Fast, easy maintenance



e and Learn More: www.ContechES.com/cds SELECT CDS APPROVALS • Washington Department of Ecology (GULD)

- Pretreatment
- New Jersey Department of Environmental
   Protection Certification (NJDEP)
- Canadian Environmental Technology
   Verification (ETV)
- MASTEP
- Connecticut DOT

The CDS system has been accepted and used extensively in all New England states for over 20 years with thousands of installations.



# The Vortechs® System

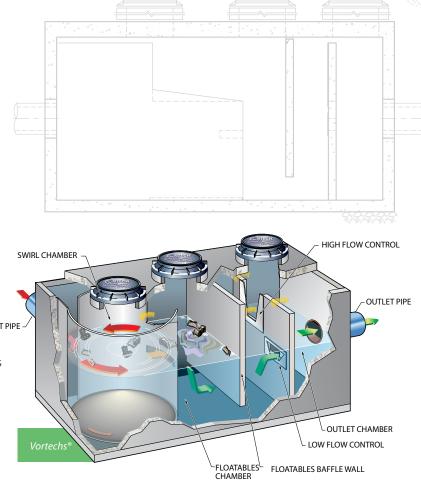
# Stormwater Treatment in a Shallow Footprint ....

Vortechs combines swirl concentration and flow controls into a single treatment unit that captures and retains trash, debris, sediment, and hydrocarbons from stormwater runoff.

The Vortechs system's large swirl chamber and flow controls work together to create a low energy environment, ideal for capturing and retaining particles down to 50 microns.

Vortechs is the ideal solution for sites with high groundwater, bedrock, utility conflicts, or sites with a large volume runoff.

The Vortechs System is approved by the Washington Department of Ecology (GULD) - Pretreatment.



Learn More: www.ContechES.com/vortechs

### SELECT VORTECHS APPROVALS

- Washington Department of Ecology (GULD) – Pretreatment
- MASTEP
- Connecticut DOT

FEATURE	BENEFIT
Large swirl chamber	Fine particle removal down to 50 microns
Shallow profile – Typical depth below pipe invert is only 3 feet.	Can be used on sites with high groundwater, bedrock, or utility conflicts
Unobstructed access to stored pollutants	Fast, easy maintenance

The Vortechs System was developed in New England and has been used extensively in the region for over 20 years.

### The ideal solution for sites with high groundwater

# Stormceptor® STC

Stormceptor STC is the recognized leader in stormwater treatment, offering a range of versatile treatment systems that effectively remove pollutants from stormwater and snowmelt runoff. Stormceptor is flexibly designed to protect waterways from hazardous material spills and stormwater pollution, including suspended sediment, free oils, and other pollutants that attach to particles, no matter how fierce the storm.

Stormceptor's scour prevention technology ensures pollutants are captured and contained during all rainfall events.

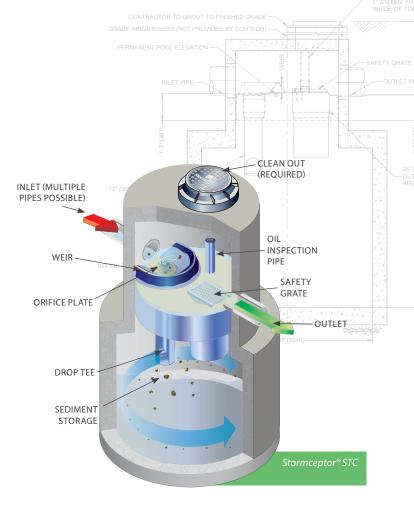
### **Ideal uses**

- Sediment (TSS) removal
- Spill control
- Debris and small floatables capture
- Pretreatment for filtration, detention/retention systems, ponds, wetlands, Low Impact Development (LID), green infrastructure, and water-sensitive urban design

### **Proven performance**

With more than 20 years of industry experience, Stormceptor has been performance tested and verified by some of the most stringent technology evaluation programs in North America.

- NJCAT
- Washington Ecology to Washington Department of Ecology (GULD) – Pretreatment
- EN858 Class 2



Learn More: www.ContechES.com/stormceptor

BENEFIT
Superior pollutant removal and retention
Eliminates the need for additional structures
Site flexibility
Design flexibility
Eliminates the need for a separate bypass structure

With over 40,000 units operating worldwide, Stormceptor performs and protects every day, in every storm.

# **Product Flow Rates**

CASCADE		
Model	Treatment Rate (cfs)	Sediment Capacity <sup>1</sup> (CF)
CS-3	1.02	11
CS-4	2.00	19
CS-5	3.50	29
CS-6	5.60	42
CS-8	12.00	75
CS-10	18.00	118

### CDS

Model	Treatment Rate <sup>2</sup> (cfs)	Sediment Capacity <sup>1</sup> (CF)
1515-3	1.00	14
2015-4	1.40	25
2015-5	1.40	39
2015-6	1.40	57
2020-5	2.20	39
2020-6	2.20	57
2025-5	3.20	39
2025-6	3.20	57
3020-6	3.90	57
3025-6	5.00	57
3030-6	5.70	57
3035-6	6.50	57
4030-8	7.50	151
4040-8	9.50	151

VORTECHS		
Model	Treatment Rate	Sediment Capacity <sup>3</sup>
Model	(cfs)	(CF)
1000	1.60	16
2000	2.80	32
3000	4.50	49
4000	6.00	65
5000	8.50	86
7000	11.00	108
9000	14.00	130
11000	17.5	151
16000	25	192

### STORMCEPTOR STC

Model	Treatment Rate (cfs)	Sediment Capacity <sup>1</sup> (CF)	
STC 450i	0.40	46	
STC 900	0.89	89	
STC 2400	1.58	205	
STC 4800	2.47	543	
STC 7200	3.56	839	
STC 11000	4.94	1086	
STC 16000	7.12	1677	

1 Additional sediment storage capacity available – Check with your local representative for information.

2 Treatment Capacity is based on laboratory testing using OK-110 (average D50 particle size of approximately 100 microns) and a 2400 micron screen.

3 Maintenance recommended when sediment depth has accumulated to within 12-18 inches of the dry weather water surface elevation.



STORMWATER SOLUTIONS



NOTHING IN THIS CATALOG SHOULD BE CONSTRUED AS A WARRANTY. APPLICATIONS SUGGESTED HEREIN ARE DESCRIBED ONLY TO HELP READERS MAKE THEIR OWN EVALUATIONS AND DECISIONS, AND ARE NEITHER GUARANTEES NOR WARRANTIES OF SUITABILITY FOR ANY APPLICATION. CONTECH MAKES NO WARRANTY WHATSOEVER, EXPRESS OR IMPLIED, RELATED TO THE APPLICATIONS, MATERIALS, COATINGS, OR PRODUCTS DISCUSSED HEREIN. ALL IMPLIED WARRANTIES OF MERCHANTABILITY AND ALL IMPLIED WARRANTIES OF FITNESS FOR ANY PARTICULAR PURPOSE ARE DISCLAIMED BY CONTECH. SEE CONTECH'S CONDITIONS OF SALE (AVAILABLE AT WWW.CONTECHES.COM/COS) FOR MORE INFORMATION.





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# **MADEP TSS Removal Calculation Sheets**

INSTRUCTIONS:

1. Sheet is nonautomated. Print sheet and complete using hand calculations. Column A and B: See MassDEP Structural BMP Table

- 2. The calculations must be completed using the Column Headings specified in Chart and Not the Excel Column Headings
- 3. To complete Chart Column D, multiple Column B value within Row x Column C value within Row

-

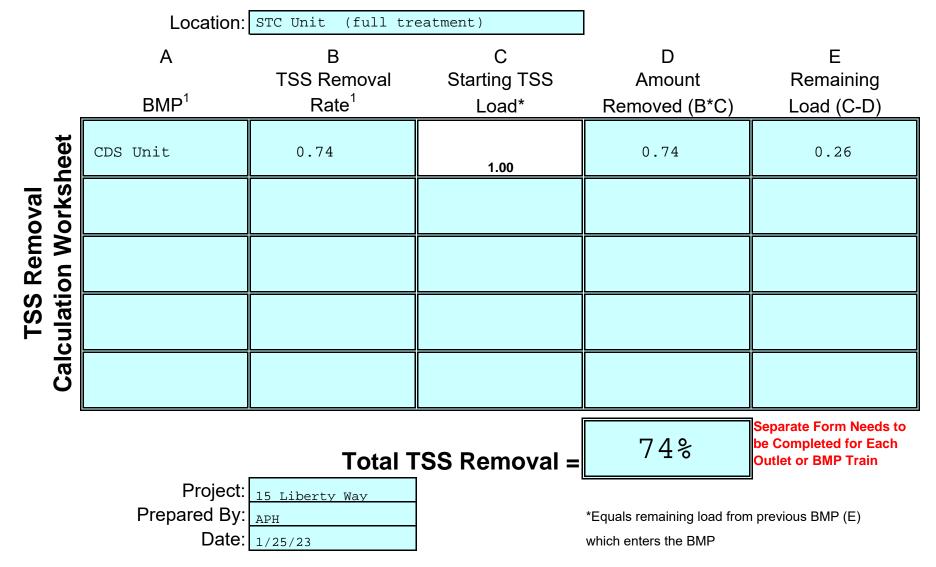
- 4. To complete Chart Column E value, subtract Column D value within Row from Column C within Row
- 5. Total TSS Removal = Sum All Values in Column D

	Location: CB#1 to SSI-1 (full treatment)				
	А	В	С	D	Е
	BMP <sup>1</sup>	TSS Removal Rate <sup>1</sup>	Starting TSS Load*	Amount Removed (B*C)	Remaining Load (C-D)
reet	Deep Sump & Hooded CBs	0.25	1.00	0.25	0.75
moval Worksheet	CDS Unit	0.74	0.75	0.55	0.20
<b>a</b>	SSI-1	0.80	0.20	0.16	0.04
TSS Re Calculation					
Calo					
			SS Removal =	96%	Separate Form Needs to be Completed for Each Outlet or BMP Train
	Project: <u>15 Liberty Way</u> Prepared By: <u>APH</u> Date: 10/17/23			*Equals remaining load from which enters the BMP	n previous BMP (E)

Non-automated TSS Calculation Sheet must be used if Proprietary BMP Proposed 1. From MassDEP Stormwater Handbook Vol. 1 INSTRUCTIONS:

1. Sheet is nonautomated. Print sheet and complete using hand calculations. Column A and B: See MassDEP Structural BMP Table

- 2. The calculations must be completed using the Column Headings specified in Chart and Not the Excel Column Headings
- 3. To complete Chart Column D, multiple Column B value within Row x Column C value within Row
- 4. To complete Chart Column E value, subtract Column D value within Row from Column C within Row
- 5. Total TSS Removal = Sum All Values in Column D



Non-automated TSS Calculation Sheet must be used if Proprietary BMP Proposed 1. From MassDEP Stormwater Handbook Vol. 1 INSTRUCTIONS:

1. Sheet is nonautomated. Print sheet and complete using hand calculations. Column A and B: See MassDEP Structural BMP Table

- 2. The calculations must be completed using the Column Headings specified in Chart and Not the Excel Column Headings
- 3. To complete Chart Column D, multiple Column B value within Row x Column C value within Row
- 4. To complete Chart Column E value, subtract Column D value within Row from Column C within Row
- 5. Total TSS Removal = Sum All Values in Column D

	Location: CB#1 to CDS 2020-5 (pretreatment)				
	А	В	С	D	E
	BMP <sup>1</sup>	TSS Removal Rate <sup>1</sup>	Starting TSS Load*	Amount Removed (B*C)	Remaining Load (C-D)
	Deep Sump &	Nate		Kellioved (B C)	
leet	Hooded CBs	0.25	1.00	0.25	0.75
moval Worksheet	CDS Unit	0.74	0.75	0.55	0.20
d) I					
TSS Re Calculation					
Calc					
l		Total T	80%	Separate Form Needs to be Completed for Each Outlet or BMP Train	
	Prepared By:	15 Liberty Way APH 10/17/23		*Equals remaining load from which enters the BMP	n previous BMP (E)

Non-automated TSS Calculation Sheet must be used if Proprietary BMP Proposed 1. From MassDEP Stormwater Handbook Vol. 1



## **Phosphorous Removal Calculations**



### PHOSPHORUS LOAD REDUCTION CALCUATION – STORMTECH SYTEM 1

Note - Phosphorus Load Reductions Calculations are based on MA MS4 General Permit (Effective July 1, 2018 with Modification Effective January 6, 2021) - ATTACHMENT 3 TO APPENDIX F - Methods to Calculate Phosphorus and Nitrogen Load Reductions for Structural Stormwater Best Management Practices

- 1) Phosphorous Load reduction target (P  $_{target}$ ) = 60%
- 2) Infiltration Basin. Information for the contributing impervious (IA) and pervious (PA) areas are summarized below:

Impervious Area Draining to SSI-Basin-1: <u>1.633 Ac. HSG C</u> Pervious Area Draining to SSI-Basin-1: <u>0.007 Ac. HSG C</u>

- **3)** Infiltration Rate = 0.27 in./hr.
- 4) BMP Volume (IA-in) = 0.25 in. (From Table 3-11 & Figure 3.8)
- 5) Pervious Area runoff depth = 0.01 (From Table 3-4) BMP Volume (PA-ft<sup>3</sup>) = (0.007 acre) x (0.01 in) x (3,630 ft<sup>3</sup>/acre-in) = 0.25 ft<sup>3</sup>

BMP Volume (IA&PA-ft<sup>3</sup>) =  $(0.25 \text{ ft}^3 + ((1.663 \text{ acre x } 0.25 \text{ in}) \text{ x } (3,630 \text{ ft}^3/\text{acre-in})) = 1,509.4 \text{ ft}^3$ 

The available storage volume ( $ft^3$ ) of the infiltration basin (BMP-Volume  $ft^3$ ) below the lowest proposed outlet is 1,801  $ft^3$  (taken from HydroCAD summary of node SSI-1)

1,801 ft<sup>3</sup> > 1,509.4 ft<sup>3</sup>



# **Groundwater Mounding Calculations**

Input Values

0.0808 0.100 5.40 58.770 31.625 3.000 10.000

11.298

1.298

Mounding, in in x direction, in

Ground-

water

feet

h(max)

Δh(max) Distance from

center of basin

### Bioretention Basin Mounding Analysis

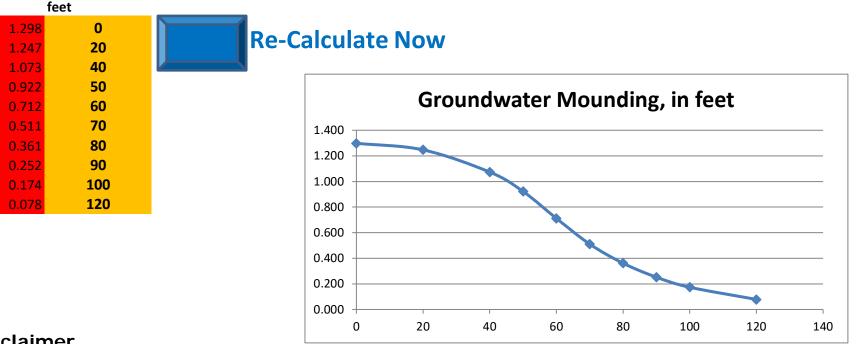
This spreadsheet will calculate the height of a groundwater mound beneath a stormwater infiltration basin. More information can be found in the U.S. Geological Survey Scientific Investigations Report 2010-5102 "Simulation of groundwater mounding beneath hypothetical stormwater infiltration basins".

The user must specify infiltration rate (R), specific yield (Sy), horizontal hydraulic conductivity (Kh), basin dimensions (x, y), duration of infiltration period (t), and the initial thickness of the saturated zone (hi(0), height of the water table if the bottom of the aquifer is the datum). For a square basin the half width equals the half length (x = y). For a rectangular basin, if the user wants the water-table changes perpendicular to the long side, specify x as the short dimension and y as the long dimension. Conversely, if the user wants the values perpendicular to the short dimension, x as the long dimension. All distances are from the center of the basin. Users can change the distances from the center of the basin at which water-table aquifer thickness are calculated.

Cells highlighted in yellow are values that can be changed by the user. Cells highlighted in red are output values based on user-specified inputs. The user MUST click the blue "Re-Calculate Now" button each time ANY of the user-specified inputs are changed otherwise necessary iterations to converge on the correct solution will not be done and values shown will be incorrect. Use consistent units for all input values (for example, feet and days)

	use consistent units (e.g. feet & days <b>or</b> inches & hours)	Conversion Table inch/hour fee	e et/day
R	Recharge (infiltration) rate (feet/day)	0.67	1.33
Sy	Specific yield, Sy (dimensionless, between 0 and 1)		
К	Horizontal hydraulic conductivity, Kh (feet/day)*	2.00	4.00 In the report accompanying this spreadsheet
х	1/2 length of basin (x direction, in feet)		(USGS SIR 2010-5102), vertical soil permeability
У	1/2 width of basin (y direction, in feet)	hours da	
t	duration of infiltration period (days)	36	1.50 hydraulic conductivity (ft/d).
hi(0)	initial thickness of saturated zone (feet)		

maximum thickness of saturated zone (beneath center of basin at end of infiltration period) maximum groundwater mounding (beneath center of basin at end of infiltration period)



### Disclaimer

This spreadsheet solving the Hantush (1967) equation for ground-water mounding beneath an infiltration basin is made available to the general public as a convenience for those wishing to replicate values documented in the USGS Scientific Investigations Report 2010-5102 "Groundwater mounding beneath hypothetical stormwater infiltration basins" or to calculate values based on user-specified site conditions. Any changes made to the spreadsheet (other than values identified as user-specified) after transmission from the USGS could have unintended, undesirable consequences. These consequences could include, but may not be limited to: erroneous output, numerical instabilities, and violations of underlying assumptions that are inherent in results presented in the accompanying USGS published report. The USGS assumes no responsibility for the consequences of any changes made to the spreadsheet. If changes are made to the spreadsheet, the user is responsible for documenting the changes and justifying the results and conclusions.

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#### Design Storm Depth / Infiltration Period R

**0.1** (1,801 cu ft vol. below outlet / 7,434 sq.ft syst. footprint) / 3 days

Κ Hydraulic conductivity (feet/day) 2.41 in/hr =

Specific yield (dimensionless constant) =

1/2 legth basin (feet) = Х

1/2 width basin (feet) = y

Sy

t Duration of infiltration period (days) = t

hi(o) Initial saturated thickness hi

0.1 **5.4** ft/day = 0.27 in/hr (24 hr/day \* 1 ft/12 in) = 4.82 ft/day \* 10 **58.77** ft. = 100/2 (conv. Vert Perm to Horz Perm)

**31.625** ft. = 40/2 **3** day = (MADEP req. time for basin to empy) **10** ft



# Illicit Discharge Statement

## **Illicit Discharge Statement**

Under the Massachusetts Wetlands Protection Act – Stormwater Management Standards

For

15 LIBERTY WAY

FRANKLIN, MA

All illicit discharges to the Stormwater Management System are prohibited. The Stormwater Management System is the system for conveying, treating, and infiltrating stormwater. Illicit discharges to Stormwater Management Systems are discharges that are not entirely comprised of stormwater, but do not include discharges from the following activities or facilities:

- Firefighting
- Water Line Flushing
- Potable Water Sources
- Landscape Irrigation
- Potable Water Sources
- Uncontaminated Groundwater
- Air-conditioning Condensation

- Dechlorinated Water from Swimming Pools
- Water used for street washing
- Water used for clean residential buildings without detergents
- Foundation Drains

The site will be operated and maintained in accordance with the Operation and Maintenance Plan dated January 17, 2023 prepared by Level Design Group, LLC.

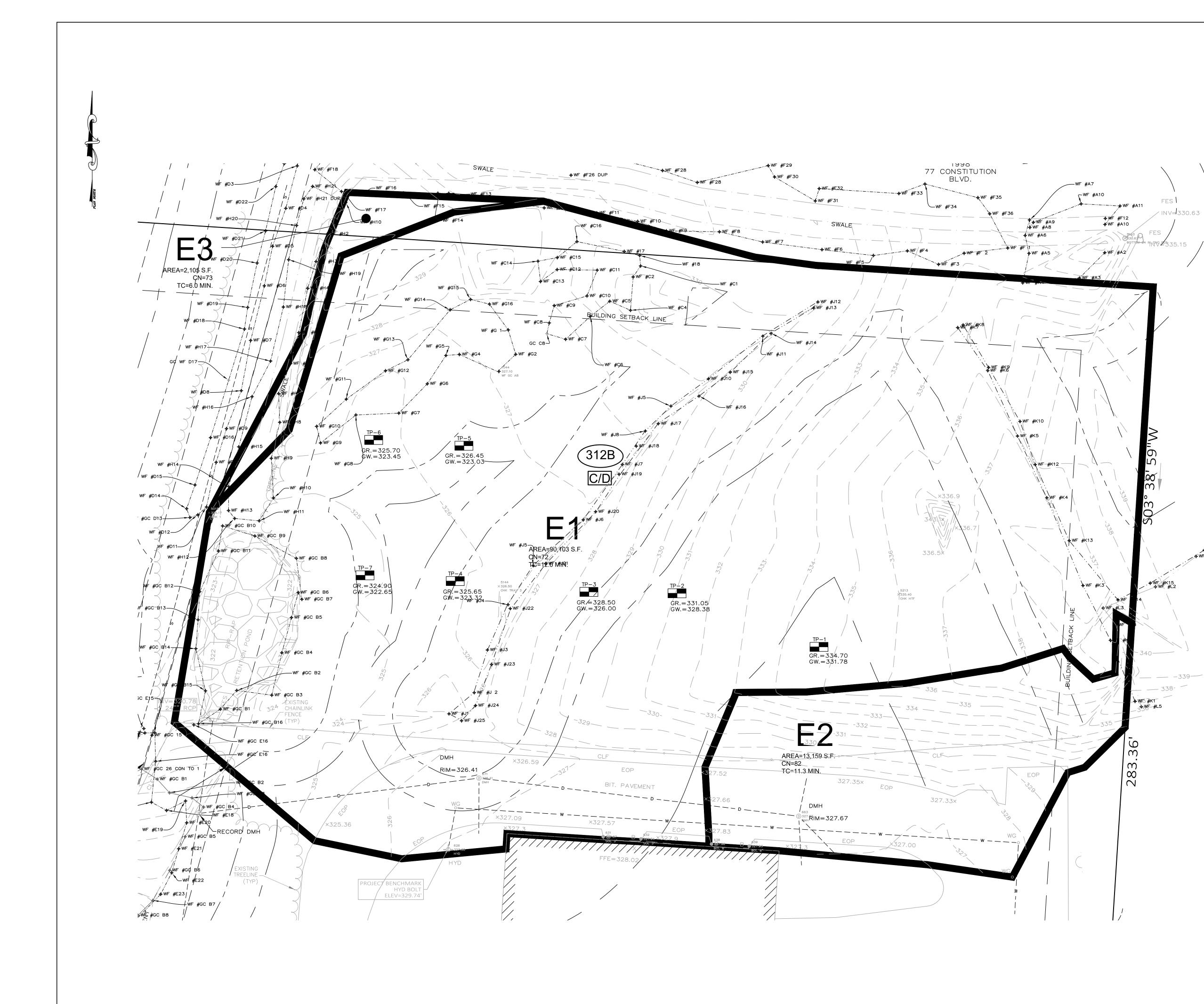
I, <u>Atlant: Disc 15 Liberty</u> (Applicant) do hereby agree to comply with requirements set forth within the Illicit Discharge Statement and will not knowingly discharge illicit materials to the stormwater management system once it is brought online **upon** completion of construction.

Signature:

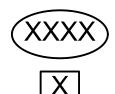
Date: 2/7/23



# Existing Drainage Plan & HydroCAD Diagram



# WATERSHED LEGEND



SOIL TYPE

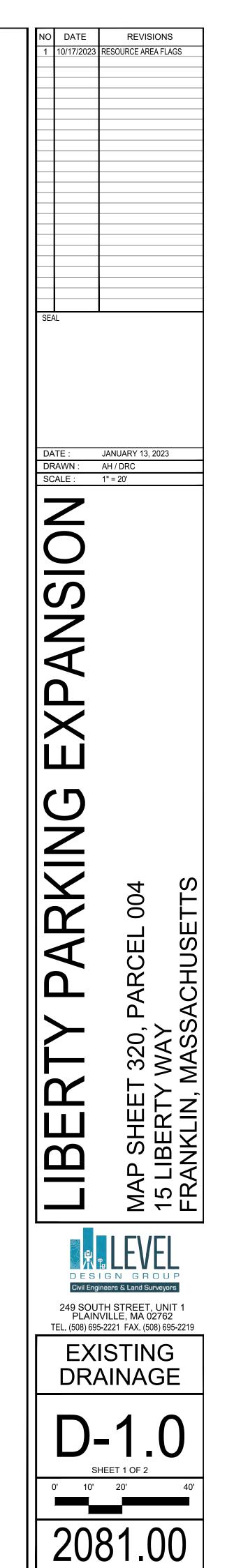


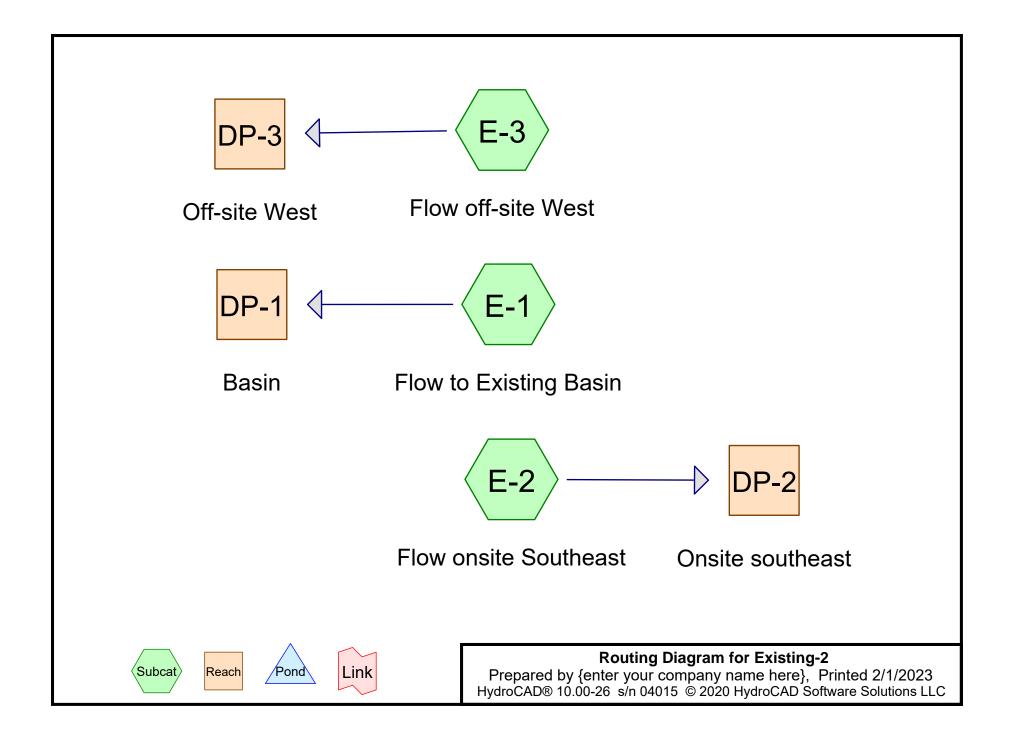
HYDROLOGIC SOIL GROUP

SOILS

(312B)

WOODBRIDGE FINE SANDY LOAM







# HydroCAD Analysis

# **Existing Conditions – 2 Year Storm**

249 SOUTH STREET UNIT 1 PLAINVILLE MA 02762 TEL508 695 2221 FAX508 695 2219 CONTACT@LEVELDG.COM LEVELDG.COM

### Area Listing (all nodes)

Area (sq-ft)	CN	Description (subcatchment-numbers)
9,896	79	50-75% Grass cover, Fair, HSG C (E-1, E-2, E-3)
10,479	98	Paved parking (E-1, E-2)
84,992	70	Woods, Good, HSG C (E-1, E-2, E-3)
105,367	74	TOTAL AREA

Existing-2 Prepared by {enter your company name here} HydroCAD® 10.00-26 s/n 04015 © 2020 HydroCAD Software Solutions LLC

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## Soil Listing (all nodes)

Area (sq-ft)	Soil Group	Subcatchment Numbers
0	HSG A	
0	HSG B	
94,888	HSG C	E-1, E-2, E-3
0	HSG D	
10,479	Other	E-1, E-2
105.367		TOTAL AREA

Existing-2
Prepared by {enter your company name here}
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			Grou	und Covers (	(all nodes)	1	
HSG-A	HSG-B	HSG-C	HSG-D	Other	Total	Ground	Subcatchment
(sq-ft)	(sq-ft)	(sq-ft)	(sq-ft)	(sq-ft)	(sq-ft)	Cover	Numbers
0 0	0 0	9,896 0	0 0	0 10,479	9,896 10,479	50-75% Grass cover, Fair Paved parking	E-1, E-2, E-3 E-1, E-2
0	0	84,992	0	0	84,992	,	E-1, E-2, E-3
0	0	94,888	0	10,479	105,367	TOTAL AREA	
cisting-2 epared by {enter	er your comp	any name he	re}			Type III	24-hr 2-Year Rainfall=3.05" Printed 2/12023
<u>/droCAD® 10.00-2</u>		T Ru	ime span=0.00 noff by SCS TF	-80.00 hrs, dt= R-20 method, l	UH=SCS, W		Page 4
bcatchment E-1	: Flow to Exis	sting Basin					Impervious Runoff Depth=0.84" CN=72 Runoff=1.49 cfs 6,292 cf
bcatchment E-2	2: Flow onsite	Southeast			Run Flow L	off Area=13,159 sf 38.16% ength=140' Tc=11.3 min (	Impervious Runoff Depth=1.42" CN=82 Runoff=0.42 cfs 1,555 cf
ubcatchment E-3	3: Flow off-site	e West			R	unoff Area=2,105 sf 0.00% Tc=6.0 min	Impervious Runoff Depth=0.89" CN=73 Runoff=0.05 cfs 156 cf
ach DP-1: Basir	n						Inflow=1.49 cfs 6,292 cf Outflow=1.49 cfs 6,292 cf
each DP-2: Onsit	te southeast						Inflow=0.42 cfs 1,555 cf Outflow=0.42 cfs 1,555 cf
ech DP-3: Off-si	ite West						Inflow=0.05 cfs 156 cf Outflow=0.05 cfs 156 cf
each DP-3: Off-si	ite West		Total Run	off Area = 105			

		R-20 me	thod, UH= nfall=3.05"		ume= 6,292 cf, Depth= 0.84" hted-CN, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs
А	Area (sf)	CN	Descriptior		
	5,457 76,777		Paved park Woods, Go		<u></u>
	7,869	79	50-75% Gr	ass cover,	Fair, HSG C
	90,103 84,646 5,457		Weighted A 93.94% Pe 6.06% Imp	rvious Area	
(min)	Length (feet)	(ft/ft	) (ft/sec)	Capacity (cfs)	
8.6 3.4	50 503	0.0530 0.0240			Sheet Flow, Sheet Flow Woods: Light underbrush n= 0.400 P2= 3.05" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
12.0	553	Total			
	ed by {en		r company 4015 © 202		
repare	ed by {en			0 HydroCAI	re} Printed 2/1/2023

### Summary for Subcatchment E-2: Flow onsite Southeast

Runoff 0.42 cfs @ 12.16 hrs, Volume= 1,555 cf, Depth= 1.42" =

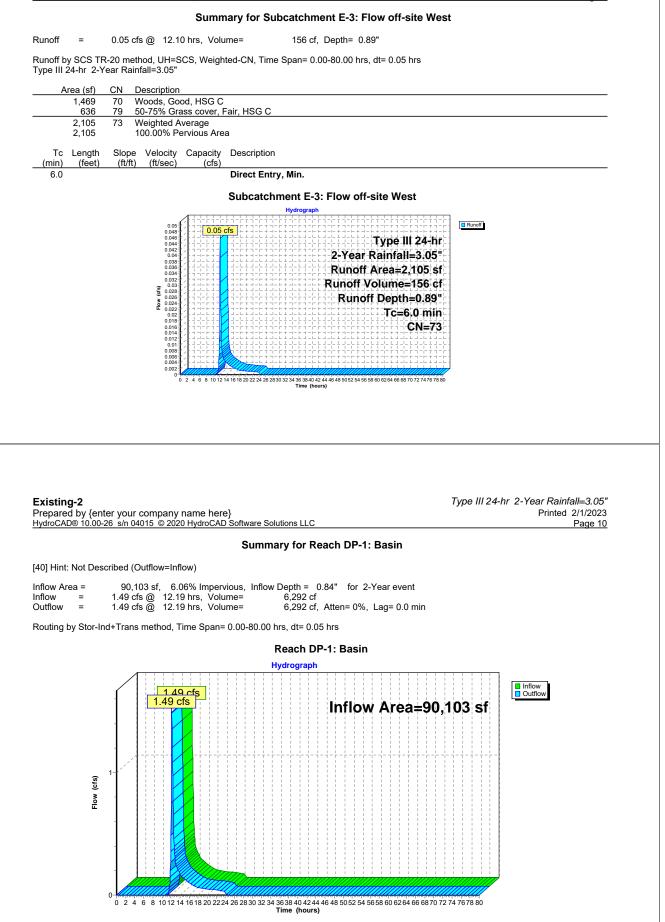
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.05"

		CN	Decemintien		
-	rea (sf)	-	Description		
*	5,022	98	Paved park	ing	
	6,746	70	Woods, Go	od, HSG C	
	1,391	79	50-75% Gra	ass cover, F	Fair, HSG C
	13.159	82	Weighted A	verage	
	8.137			vious Area	
	5,022			pervious Are	
	0,022		00.1070 111		
Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)		(cfs)	
11.0	50	0.0280	0.08		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.05"
0.1	45	0.1750	6.74		Shallow Concentrated Flow,
0.1	10	0.1100	0.71		Unpaved Kv= 16.1 fps
0.0	11	0.1640	6.52		Shallow Concentrated Flow,
0.0		0.1040	0.52		Unpaved Kv= 16.1 fps
0.2	24	0.0240	3.14		
0.2	34	0.0240	3.14		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
11 3	140	Total			

11.3 140 Total



Type III 24-hr 2-Year Rainfall=3.05" Prepared by {enter your company name here} HydroCAD® 10.00-26 s/n 04015 © 2020 HydroCAD Software Solutions LLC Printed 2/1/2023 Page 8 Subcatchment E-2: Flow onsite Southeast Hydrograph 0.46 Runoff 0.44 0.42 cfs 0.42 Type III 24-hr 0.4 0.38 2-Year Rainfall=3.05" 0.36 0.34 Runoff Area=13,159 sf 0.32 0.3 Runoff Volume=1,555 cf 0.28 () 0.26 0.24 Runoff Depth=1.42" 0.24 0.22 0.2 Flow Length=140' 0.2 0.18 Tc=11.3 min 0.16 0.14 CN=82 0.12 0.1 0.08 0.06 0.04 0.02 0 0 2 4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 34 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70 72 74 76 78 80 Time (hours)



#### Summary for Reach DP-2: Onsite southeast

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area	a =	13,159 sf, 38.16% Impervious, Inflow Depth = 1.42" for 2-Yea	r event
Inflow	=	0.42 cfs @ 12.16 hrs, Volume= 1,555 cf	
Outflow	=	0.42 cfs @ 12.16 hrs, Volume= 1,555 cf, Atten= 0%, Laç	g= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs Reach DP-2: Onsite southeast Hydrograph Inflow
Outflow 0.42 cfs 0.42 cfs 0.46 0.44 Inflow Area=13,159 sf 0.42 0.4 0.38 0.36 0.34 0.3 0.28 0.26 0.24 (cfs) Flow 0.22 0.18 0.16 0.14 0.12 0.1 0.06 0.04 0.02 0-0 2 4 6 8 1012 1416 18 2022 24 26 28 30 32 34 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70 72 74 76 78 80 Time (hours)

Existing-2

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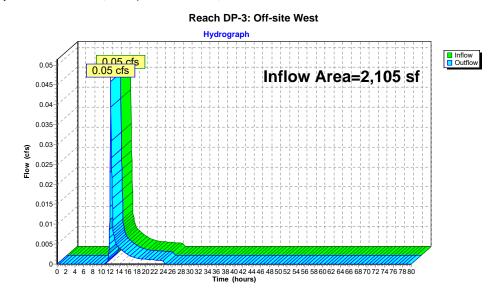
Type III 24-hr 2-Year Rainfall=3.05" Printed 2/1/2023 Page 12

### Summary for Reach DP-3: Off-site West

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area	a =	2,105 sf,	0.00% Impervious	, Inflow Depth = 0.89"	for 2-Year event
Inflow	=	0.05 cfs @	12.10 hrs, Volume=	156 cf	
Outflow	=	0.05 cfs @	12.10 hrs, Volume=	156 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs





# HydroCAD Analysis

# **Existing Conditions – 10 Year Storm**

249 SOUTH STREET UNIT 1 PLAINVILLE MA 02762 TEL508 695 2221 FAX508 695 2219 CONTACT@LEVELDG.COM LEVELDG.COM

### Area Listing (all nodes)

Area (sq-ft)	CN	Description (subcatchment-numbers)
9,896	79	50-75% Grass cover, Fair, HSG C (E-1, E-2, E-3)
10,479	98	Paved parking (E-1, E-2)
84,992	70	Woods, Good, HSG C (E-1, E-2, E-3)
105,367	74	TOTAL AREA

Existing-2 Prepared by {enter your company name here} HydroCAD® 10.00-26 s/n 04015 © 2020 HydroCAD Software Solutions LLC

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## Soil Listing (all nodes)

Area (sq-ft)	Soil Group	Subcatchment Numbers
0	HSG A	
0	HSG B	
94,888	HSG C	E-1, E-2, E-3
0	HSG D	
10,479	Other	E-1, E-2
105.367		TOTAL AREA

Existing-2	
Prepared by {enter	your company name here}
HydroCAD® 10.00-26	s/n 04015 © 2020 HydroCAD Software Solutions LLC

Printed 2/1/2023 Page 3

HSG-A HSG-E		Grou	nd Covers (a	all nodes)		
(sq-ft) (sq-ft)		HSG-D (sq-ft)	Other (sq-ft)	Total (sq-ft)	Ground Cover	Subcatchment Numbers
	0 9,896 0 0	0 0 0	0 10,479 0	9,896 10,479 84,992	50-75% Grass cover, Fair Paved parking Woods, Good	
0 0	0 94,888	0	10,479	105,367		
sting-2 pared by {enter your co					Type III 2	24-hr 10-Year Rainfall=5.15" Printed 2/1/2023 Page 4
100AD@ 10.00-20 3/11040	Tim	ne span=0.00-8 off by SCS TR-	30.00 hrs, dt= 20 method, L	H=SCS, W		raye 4
ocatchment E-1: Flow to	Existing Basin					Impervious Runoff Depth=2.31" N=72 Runoff=4.53 cfs 17,375 cf
bcatchment E-2: Flow or	nsite Southeast					Impervious Runoff Depth=3.21" CN=82 Runoff=0.95 cfs 3,524 cf
bcatchment E-3: Flow of	ff-site West			R		Impervious Runoff Depth=2.40" CN=73 Runoff=0.13 cfs 421 cf
						Inflow=4.53 cfs 17,375 cf Outflow=4.53 cfs 17,375 cf
nch DP-1: Basin						
ach DP-1: Basin ach DP-2: Onsite southe	east					Inflow=0.95 cfs 3,524 cf Outflow=0.95 cfs 3,524 cf

			hod, UH=S infall=5.15		tted-CN, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs
A	Area (sf)	CN	Description		
	5,457 76,777	70	Paved park Woods, Go	od, HSG C	
	7,869		50-75% Gra Neighted A		Fair, HSG C
	84,646 5,457	9	93.94% Per 6.06% Impe	vious Area	
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description
8.6 3.4		0.0530 0.0240			Sheet Flow, Sheet Flow Woods: Light underbrush n= 0.400 P2= 3.05" Shallow Concentrated Flow,
12.0	553	Total			Unpaved Kv= 16.1 fps
Existin	ed by {en	ter your	company	name here	<i>Type III 24-hr 10-Year Rainfall=</i> 5.15" e} Printed 2/1/2023
repare	ed by {en	ter your 26 s/n 0	company 4015 © 202	0 HydroCAE	e} Printed 2/1/2023 D Software Solutions LLC Page 6
repare	ed by {en	ter your 26 s/n 0	company 4015 © 202	0 HydroCAE	e} Printed 2/1/2023

### Summary for Subcatchment E-2: Flow onsite Southeast

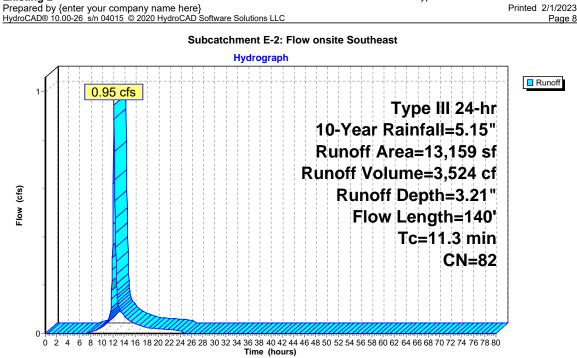
Runoff 0.95 cfs @ 12.16 hrs, Volume= 3,524 cf, Depth= 3.21" =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs Type III 24-hr 10-Year Rainfall=5.15"

	A	rea (sf)	CN	Description		
1		5,022	98	Paved park	ing	
		6,746	70	Woods. Go	od. HSG C	
		1,391	79	50-75% Gra	ass cover, F	Fair, HSG C
-		13,159	82	Weighted A	verage	· · ·
		8.137			vious Area	
		5,022		38.16% Im	pervious Are	ea
		,				
	Tc	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	11.0	50	0.0280	0.08		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 3.05"
	0.1	45	0.1750	6.74		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
	0.0	11	0.1640	6.52		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
	0.2	34	0.0240	3.14		Shallow Concentrated Flow,
_						Paved Kv= 20.3 fps
-	11.3	140	Total			



Type III 24-hr 10-Year Rainfall=5.15" Printed 2/1/2023 Page 8



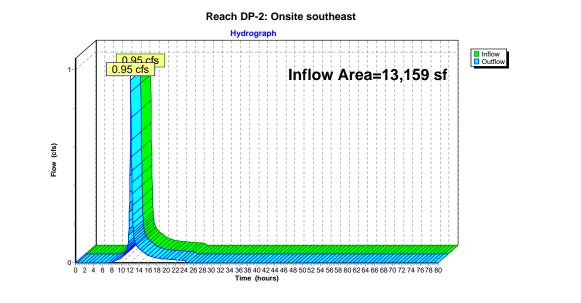
Dunoff by SCS T		-	0 hrs, Volum			, Depth=		- 0.05 k								
Runoff by SCS T Type III 24-hr 10				a-CN, Time	Span= 0.	00-80.00	J nrs, at	= 0.05 r	irs							
Area (sf) 1,469		Description	od, HSG C													
636	79	50-75% Gra	ass cover, Fa	ir, HSG C												
2,105 2,105	73	Neighted A	verage ervious Area													
Tc Length (min) (feet)		Velocity (ft/sec)	Capacity	Description												
<u>(min) (feet)</u> 6.0	(1011)	(10/360)	(cfs)	Direct Entr	y, Min.											
			5	Subcatch	ment E-3	B: Flow	off-sit	e Wes	st							
		0.14 0.13 0.12 0.11 0.09 0.08 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.01 0.06 0.06 0.06 0.06 0.01 0.06	2 4 6 8 1012141		13234 95 58 40 A	Run - Runc - Ru - Ru	ear Ra Ioff Ar Inoff I Inoff I	ea=2, ume= Depth= Tc=6	=5.1 105 421 =2.4 .0 m CN=7	hr 5" ¢f 0" 73	Runoff	I				
Existing-2										Тур	be /// 2	24-hr	10-Y		infall=5.1	
Prepared by {er	nter your )-26 s/n 0	company 4015 © 202	name here}	Software Solu						Тур	pe III 2	24-hr	10-Y		<i>infall=5.</i> ed 2/1/20 Page	23
Prepared by {ei HydroCAD® 10.00	)-26 s/n 0	4015 © 202	0 HydroCAD S	Software Solu	utions LLC	each D	P-1: B	asin		Тур	oe III 2	24-hr	10-Y		ed 2/1/20	23
Prepared by {er HydroCAD® 10.00 [40] Hint: Not De	<u>)-26 s/n 0</u> scribed ((	4015 © 202 Dutflow=Inf	0 HydroCAD S	Software Solu Summa	iry for R				ont	Тур	oe /// 2	24-hr	10-Y		ed 2/1/20	23
Prepared by {ei HydroCAD® 10.00 [40] Hint: Not De Inflow Area = Inflow =	<u>)-26 s/n 0</u> scribed (( 90,7 4.53 c	4 <u>015 © 202</u> Dutflow=Inf 03 sf, 6.0 fs @ 12.1	<u>0 HydroCAD s</u> low) 06% Impervic 7 hrs, Volun	Software Solu Summa Sus, Inflow	Depth = 17,375 cf	2.31" f	or 10-Y	ear eve		Тур	oe /// 2	24-hr	10-Y		ed 2/1/20	23
Prepared by {er HydroCAD® 10.00 [40] Hint: Not De Inflow Area = Inflow = Outflow =	<u>)-26 s/n 0</u> scribed (( 90, 4.53 c 4.53 c	4015 © 202 Dutflow=Inf 03 sf, 6.1 fs @ 12.1 fs @ 12.1	<u>0 HydroCAD s</u> low) 06% Impervid 7 hrs, Volum 7 hrs, Volum	Software Solu Summa bus, Inflow te=	Depth = 17,375 cf 17,375 cf	2.31" f , Atten=	or 10-Y	ear eve		Тур	e III 2	24-hr	10-Y		ed 2/1/20	23
Prepared by {ei HydroCAD® 10.00 [40] Hint: Not De Inflow Area = Inflow =	<u>)-26 s/n 0</u> scribed (( 90, 4.53 c 4.53 c	4015 © 202 Dutflow=Inf 03 sf, 6.1 fs @ 12.1 fs @ 12.1	<u>0 HydroCAD s</u> low) 06% Impervid 7 hrs, Volum 7 hrs, Volum	Software Solu Summa bus, Inflow le= le= .00-80.00 h	Depth = 17,375 cf 17,375 cf	2.31" f , Atten= !5 hrs	or 10-Y 0%, La	ear eve		Тур	e III 2	24-hr	10-Yi		ed 2/1/20	23
Prepared by {er HydroCAD® 10.00 [40] Hint: Not De Inflow Area = Inflow = Outflow =	<u>)-26 s/n 0</u> scribed (( 90, 4.53 c 4.53 c	4015 © 202 Dutflow=Inf 03 sf, 6.1 fs @ 12.1 fs @ 12.1	<u>0 HydroCAD s</u> low) 06% Impervid 7 hrs, Volum 7 hrs, Volum	Software Solu Summa bus, Inflow lee= .00-80.00 h	Depth = 17,375 cf 17,375 cf rs, dt= 0.0	2.31" f , Atten= <sup>15</sup> hrs <b>P-1: Ba</b>	or 10-Y 0%, La	ear eve		Τγε	De III 2		10-Y		ed 2/1/20	23
Prepared by {er HydroCAD® 10.00 [40] Hint: Not De Inflow Area = Inflow = Outflow =	5 5 5 6 5 6 6 6 7 7 7 7 7 7 7 7 7 7 7 7 7	4015 © 202 Dutflow=Inf 03 sf, 6.1 fs @ 12.1 fs @ 12.1	<u>0 HydroCAD 3</u> low) 06% Impervid 7 hrs, Volun 7 hrs, Volun 7 ime Span= 0	Software Solu Summa bus, Inflow lee= .00-80.00 h	Depth = 17,375 cf 17,375 cf rs, dt= 0.0 Reach D	2.31" f , Atten= 15 hrs <b>P-1: Ba</b>	or 10-Y 0%, La	ear eve				- L		Print	ed 2/1/20	23

#### Summary for Reach DP-2: Onsite southeast

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area	a =	13,159 sf,	38.16% Impervious,	Inflow Depth = 3.21"	for 10-Year event
Inflow	=	0.95 cfs @	12.16 hrs, Volume=	3,524 cf	
Outflow	=	0.95 cfs @	12.16 hrs, Volume=	3,524 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs



Existing-2

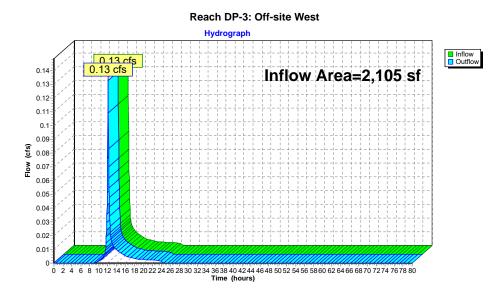
Prepared by {enter your company name here} HydroCAD® 10.00-26 s/n 04015 © 2020 HydroCAD Software Solutions LLC Type III 24-hr 10-Year Rainfall=5.15" Printed 2/1/2023 Page 12

### Summary for Reach DP-3: Off-site West

[40] Hint: Not Described (Outflow=Inflow)

Inflow Are	a =	2,105 sf,	0.00% Impervious,	Inflow Depth = 2.40"	for 10-Year event
Inflow	=	0.13 cfs @ 1	12.10 hrs, Volume=	421 cf	
Outflow	=	0.13 cfs @ 1	12.10 hrs, Volume=	421 cf, Atte	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs





# HydroCAD Analysis

# **Existing Conditions - 25 Year Storm**

### Area Listing (all nodes)

Area (sq-ft)	CN	Description (subcatchment-numbers)
9,896	79	50-75% Grass cover, Fair, HSG C (E-1, E-2, E-3)
10,479	98	Paved parking (E-1, E-2)
84,992	70	Woods, Good, HSG C (E-1, E-2, E-3)
105,367	74	TOTAL AREA

Existing-2 Prepared by {enter your company name here} HydroCAD® 10.00-26 s/n 04015 © 2020 HydroCAD Software Solutions LLC

Printed 2/1/2023 Page 2

## Soil Listing (all nodes)

Area (sq-ft)	Soil Group	Subcatchment Numbers
0	HSG A	
0	HSG B	
94,888	HSG C	E-1, E-2, E-3
0	HSG D	
10,479	Other	E-1, E-2
105.367		TOTAL AREA

Existing-2	
Prepared by {enter	your company name here}
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Printed 2/1/2023 Page 3

(sq-ft)         (sq-ft) <t< th=""><th>HSG-A HSG-B HSG-C</th><th>Groun HSG-D</th><th>d Covers (</th><th>Total</th><th>Ground</th><th>Subcatchment</th></t<>	HSG-A HSG-B HSG-C	Groun HSG-D	d Covers (	Total	Ground	Subcatchment
0       0       0       10.473       10.479       Paved parking       E-1, E-2         0       0       84.892       0       0       84.992       Woods, Good       E-1, E-2, E-3         0       0       94.888       0       10.479       195.367       TOTAL AREA						
0       0       84.992       0       0       84.992       Words, Good       E-1, E-2, E-3         0       0       94,888       0       10,479       105,367       TOTAL AREA	-					
isting-2 Type III 24-hr 25-Year Rainfall=6.3 pared by (enter your company name here) printed 21/1202 Page Time span=0.00-80.00 hrs, dt=0.05 hrs, 1601 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind rethod ScatchmentE-1: Flow to Existing Basin Runoff Degree 2010 and 100 method Runoff Degree 2010 and 100 method Runoff Degree 2010 and 100 method ScatchmentE-1: Flow to Existing Basin						
pared by {enter your company name here} printed 2/1/202 Page Time span=0.00-80.00 hrs, dt=0.05 hrs, 1601 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method reatchment E-1: Flow to Existing Basin Runoff Area=90,103 sf 6.06% Impervious Runoff Depth=3.20 Flow Length=553' Tc=12.0 min CN=72 Runoff=6.49 cfs 24,642	0 0 94,888	0	10,479	105,367	TOTAL AREA	
pared by {enter your company name here} printed 2/1/202 Page Time span=0.00-80.00 hrs, dt=0.05 hrs, 1601 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method reatchment E-1: Flow to Existing Basin Runoff Area=90,103 sf 6.06% Impervious Runoff Depth=3.20 Flow Length=553' Tc=12.0 min CN=72 Runoff=6.49 cfs 24,642						
Time span=0.00-80.00 hrs, dt=0.05 hrs, 1601 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method catchment E-1: Flow to Existing Basin Runoff Area=90,103 sf 6.06% Impervious Runoff Depth=3.2 Flow Length=553' Tc=12.0 min CN=72 Runoff=6.49 cfs 24,642	pared by {enter your company name here				Type III 2	Printed 2/1/2023
Flow Length=553' Tc=12.0 min CN=72 Runoff=6.49 cfs 24,642	Tim Runc	ne span=0.00-8 off by SCS TR-2	0.00 hrs, dt= 20 method, L	JH=SCS, W	eighted-CN	Page 4
Perstehment E. 2: Elow ancite Southaret Runoff Area=13,159 of 38,16% Impensious Runoff Denth=4.3	ocatchment E-1: Flow to Existing Basin					
Flow Length=140' Tc=11.3 min CN=82 Runoff=1.26 cfs 4,727	bcatchment E-2: Flow onsite Southeast					
bcatchment E-3: Flow off-site West Runoff Area=2,105 sf 0.00% Impervious Runoff Depth=3.3 Tc=6.0 min CN=73 Runoff=0.19 cfs 593	bcatchment E-3: Flow off-site West			R		
	ach DP-1: Basin					Inflow=6.49 cfs 24,642 cf Outflow=6.49 cfs 24,642 cf
	ach DP-2: Onsite southeast					Inflow=1.26 cfs 4,727 cf Outflow=1.26 cfs 4,727 cf
	ach DP-3: Off-site West					Inflow=0.19 cfs 593 cf Outflow=0.19 cfs 593 cf

	by SCS TI 24-hr 25		untall=6.35		
A	Area (sf) 5,457				
	76,777	70		od, HSG C	
	7,869 90,103	72	Weighted A	verage	Fair, HSG C
	84,646 5,457			rvious Area ervious Area	
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	
8.6		0.0530		(013)	Sheet Flow, Sheet Flow Woods: Light underbrush n= 0.400 P2= 3.05"
3.4	503	0.0240	2.49		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
12.0	553	Total			
Existir	ed by {en	ter your	company	name here	
Prepare	ed by {en	ter your -26 s/n 0	company 4015 © 202	0 HydroCAE	re} Printed 2/1/2023 AD Software Solutions LLC Page 6
Prepare	ed by {en	ter your -26 s/n 0	company 4015 © 202	0 HydroCAE	re} Printed 2/1/2023
Prepare HydroCA	ed by {en \D® 10.00	ter your 26 s/n 0	company 4015 © 202	0 HydroCAE	re} Printed 2/1/2023 AD Software Solutions LLC Page 6 Subcatchment E-1: Flow to Existing Basin Hydrograph
Prepare HydroCA	ed by {en	-26 s/n 0	company 4015 © 202	0 HydroCAE	re} Printed 2/1/2023 D Software Solutions LLC Page 6 Subcatchment E-1: Flow to Existing Basin Hydrograph Runoff
⊃repare HydroCA	ed by {en	-26 s/n 0	4015 © 202	0 HydroCAE	re} Printed 2/1/2023 Page 6 Subcatchment E-1: Flow to Existing Basin Hydrograph Runoff Runoff Runoff
⊃repare HydroCA	ed by {en \D® 10.00	-26 s/n 0	4015 © 202	0 HydroCAE	re} Printed 2/1/2023 D Software Solutions LLC Page 6 Subcatchment E-1: Flow to Existing Basin Hydrograph Runoff
⊃repare <u>HydroC</u> A	ed by {en AD® 10.00	-26 s/n 0	4015 © 202	0 HydroCAE	re} Printed 2/1/2023 Page 6 Subcatchment E-1: Flow to Existing Basin Hydrograph  Runoff  Type III 24-hr 25-Year Rainfall=6.35"
⊃repare <u>HydroC</u> A	ed by {en	-26 s/n 0	4015 © 202	0 HydroCAE	re} D Software Solutions LLC Printed 2/1/2023 Page 6 Subcatchment E-1: Flow to Existing Basin Hydrograph Type III 24-hr 25-Year Rainfall=6.35" Runoff Area=90,103 sf
Prepare HydroCA	ed by {en AD® 10.00	-26 s/n 0	4015 © 202	0 HydroCAE	re} D Software Solutions LLC Page 6 Subcatchment E-1: Flow to Existing Basin Hydrograph Type III 24-hr 25-Year Rainfall=6.35" Runoff Area=90,103 sf Runoff Volume=24,642 cf
Prepare HydroCA	ed by {en AD® 10.00	-26 s/n 0	4015 © 202	0 HydroCAE	re} D Software Solutions LLC Page 6 Subcatchment E-1: Flow to Existing Basin Hydrograph Type III 24-hr 25-Year Rainfall=6.35" Runoff Area=90,103 sf Runoff Volume=24,642 cf Runoff Depth=3.28"
Prepare HydroCA	7-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1	-26 s/n 0	4015 © 202	0 HydroCAE	re} D Software Solutions LLC Page 6 Subcatchment E-1: Flow to Existing Basin Hydrograph Type III 24-hr 25-Year Rainfall=6.35" Runoff Area=90,103 sf Runoff Volume=24,642 cf Runoff Depth=3.28" Flow Length=553'
⊃repare <u>HydroC</u> A	ed by {en AD® 10.00	-26 s/n 0	4015 © 202	0 HydroCAE	re} D Software Solutions LLC Page 6 Subcatchment E-1: Flow to Existing Basin Hydrograph Type III 24-hr 25-Year Rainfall=6.35" Runoff Area=90,103 sf Runoff Volume=24,642 cf Runoff Depth=3.28"
Prepare HydroCA	7- 6- 5- 4- 3-	-26 s/n 0	4015 © 202	0 HydroCAE	re} D Software Solutions LLC Page 6 Subcatchment E-1: Flow to Existing Basin Hydrograph Type III 24-hr 25-Year Rainfall=6.35" Runoff Area=90,103 sf Runoff Volume=24,642 cf Runoff Depth=3.28" Flow Length=553' Tc=12.0 min
Prepare HydroCA	7-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1	-26 s/n 0	4015 © 202	0 HydroCAE	re} D Software Solutions LLC Page 6 Subcatchment E-1: Flow to Existing Basin Hydrograph Type III 24-hr 25-Year Rainfall=6.35" Runoff Area=90,103 sf Runoff Volume=24,642 cf Runoff Depth=3.28" Flow Length=553'
Prepare HydroCA	7- 6- 5- 4- 3-	-26 s/n 0	4015 © 202	0 HydroCAE	re} D Software Solutions LLC Page 6 Subcatchment E-1: Flow to Existing Basin Hydrograph Type III 24-hr 25-Year Rainfall=6.35" Runoff Area=90,103 sf Runoff Volume=24,642 cf Runoff Depth=3.28" Flow Length=553' Tc=12.0 min

### Summary for Subcatchment E-2: Flow onsite Southeast

Runoff 1.26 cfs @ 12.16 hrs, Volume= 4,727 cf, Depth= 4.31" =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=6.35"

		CN	Decemintien		
-	rea (sf)	-	Description		
*	5,022	98	Paved park	ing	
	6,746	70	Woods, Go	od, HSG C	
	1,391	79	50-75% Gra	ass cover, F	Fair, HSG C
	13.159	82	Weighted A	verage	
	8.137			vious Area	
	5,022			pervious Are	
	0,022		00.1070 111		
Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)		(cfs)	
11.0	50	0.0280	0.08		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.05"
0.1	45	0.1750	6.74		Shallow Concentrated Flow,
0.1	10	0.1100	0.71		Unpaved Kv= 16.1 fps
0.0	11	0.1640	6.52		Shallow Concentrated Flow,
0.0		0.1040	0.52		Unpaved Kv= 16.1 fps
0.2	24	0.0240	3.14		
0.2	34	0.0240	3.14		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
11 3	140	Total			

11.3 140 Total



Type III 24-hr 25-Year Rainfall=6.35" Printed 2/1/2023 Prepared by {enter your company name here} HydroCAD® 10.00-26 s/n 04015 © 2020 HydroCAD Software Solutions LLC Page 8 Subcatchment E-2: Flow onsite Southeast Hydrograph Runoff 1.26 cfs Type III 24-hr 25-Year Rainfall=6.35" Runoff Area=13,159 sf 1 Runoff Volume=4,727 cf Flow (cfs) Runoff Depth=4.31" Flow Length=140' Tc=11.3 min **CN=82** 0 2 4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 34 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70 72 74 76 78 80 Time (hours)

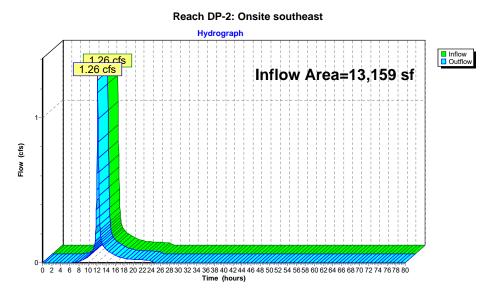
		cfs @ 12.0				f, Depth=							
Runoff by SCS T Type III 24-hr 2				ed-CN, Tim	e Span= 0	0.00-80.00	hrs, dt=	0.05 hrs	6				
Area (sf)		Description											
1,469 636	79		ass cover, F	air, HSG C									
2,105 2,105		Weighted A 100.00% P	verage ervious Area										
Tc Length			Capacity	Descriptior	I								
<u>(min)</u> (feet) 6.0	:) (ft/fi	t) (ft/sec)	(cfs)	Direct Ent	ry, Min.								
				Subcatch	ment E-	3: Flow	off-site	West					
		0.21 0.2 0.19 0.16 0.15 0.16 0.15 0.14 0.13 0.14 0.12 0.14 0.12 0.14 0.12 0.14 0.14 0.12 0.14 0.12 0.14 0.14 0.14 0.15 0.05 0.05 0.05 0.05 0.05 0.05 0.05			1	Runo Runo Runo 42 44 46 46 50 52	ear Raiı off Are ff Volu noff De 7	a=2,10 me=59 pth=3 c=6.0 CN	5.35" 05 sf 93 cf 1.38" min 1=73	Run	off		
										Type II.	l 24-hi		Rainfall=6.35
Prepared by {e				Software So				- 1		Type II	l 24-hı		Rainfall=6.35 rinted 2/1/2023 Page 10
Prepared by {e HydroCAD® 10.00	0-26 s/n	04015 © 202	0 HydroCAD	Software So	lutions LLC ary for F		P-1: Ba	sin		Type II	l 24-hi		rinted 2/1/2023
Prepared by {e <u>HydroCAD® 10.00</u> [40] Hint: Not De Inflow Area = Inflow =	<u>0-26 s/n (</u> escribed ) 90 6.49	04015 © 202 (Outflow=Inf ,103 sf, 6. cfs @ 12.1	0 HydroCAD	Software So Summ ous, Inflow ne=	ary for F	Reach D	or 25-Yea	ar event		Type II	l 24-hi		rinted 2/1/2023
Prepared by {e HydroCAD® 10.00 [40] Hint: Not De Inflow Area = Inflow = Outflow =	0-26 s/n 0 escribed 90 6.49 6.49	04015 © 202 (Outflow=Inf ,103 sf, 6. cfs @ 12.1 cfs @ 12.1	<u>0 HydroCAD</u> low) 06% Impervi 7 hrs, Volur 7 hrs, Volur	Software So Summ ous, Inflow ne= ne= 0.00-80.00	Depth = 24,642 c 24,642 c hrs, dt= 0.	3.28"         fc           f         f           f, Atten=         05 hrs	or 25-Yea 0%, Lag	ar event		Type II	l 24-hı		rinted 2/1/2023
Prepared by {e HydroCAD® 10.00 [40] Hint: Not De Inflow Area = Inflow = Outflow =	0-26 s/n 0 escribed 90 6.49 6.49	04015 © 202 (Outflow=Inf ,103 sf, 6. cfs @ 12.1 cfs @ 12.1	<u>0 HydroCAD</u> low) 06% Impervi 7 hrs, Volur 7 hrs, Volur	Software So Summ ous, Inflow ne= ne= 0.00-80.00	Depth = 24,642 c 24,642 c hrs, dt= 0. <b>Reach E</b>	3.28" fo f f, Atten= 05 hrs <b>DP-1: Ba</b>	or 25-Yea 0%, Lag	ar event		Type II	l 24-hr		rinted 2/1/2023
Prepared by {e HydroCAD® 10.00 [40] Hint: Not De Inflow Area = Inflow = Outflow =	0-26 s/n 0 escribed 90 6.49 6.49	04015 © 202 (Outflow=Inf ,103 sf, 6.1 cfs @ 12.1 cfs @ 12.1 ns method, 7	0 HydroCAD low) 06% Impervi 7 hrs, Volur 7 hrs, Volur îime Span= 1	Software So Summ ous, Inflow ne= ne= 0.00-80.00	Depth = 24,642 c 24,642 c hrs, dt= 0.	3.28" fo f f, Atten= 05 hrs <b>DP-1: Ba</b>	or 25-Yea 0%, Lag	ar event		Type II	124-hr	P1	rinted 2/1/2023 Page 10
Prepared by {e HydroCAD® 10.00 [40] Hint: Not De Inflow Area = Inflow = Outflow =	0-26 s/n 0 escribed 90 6.49 6.49	04015 © 202 (Outflow=Inf ,103 sf, 6. cfs @ 12.1 cfs @ 12.1	0 HydroCAD low) 06% Impervi 7 hrs, Volur 7 hrs, Volur îime Span= 1	Software So Summ ous, Inflow ne= ne= 0.00-80.00	Depth = 24,642 c 24,642 c hrs, dt= 0. <b>Reach E</b>	3.28"         ft           f         Atten=           05 hrs         DP-1: Bah	or 25-Yea 0%, Lag <b>sin</b>	ar event	: in				rinted 2/1/2023 Page 10
	0-26 s/n i escribed i 90, 6.49 6.49 -Ind+Trar	04015 © 202 (Outflow=Inf ,103 sf, 6.1 cfs @ 12.1 cfs @ 12.1 ns method, 7	0 HydroCAD low) 06% Impervi 7 hrs, Volur 7 hrs, Volur îime Span= 1	Software So Summ ous, Inflow ne= ne= 0.00-80.00	Depth = 24,642 c 24,642 c hrs, dt= 0. <b>Reach E</b>	3.28"         ft           f         Atten=           05 hrs         DP-1: Bah	or 25-Yea 0%, Lag	ar event	: in			P1	rinted 2/1/2023 Page 10
Prepared by {e HydroCAD® 10.00 [40] Hint: Not De Inflow Area = Inflow = Outflow =	0-26 s/n ( 900 6.49 6.49 -Ind+Trar	04015 © 202 (Outflow=Inf ,103 sf, 6.1 cfs @ 12.1 cfs @ 12.1 ns method, 7	0 HydroCAD low) 06% Impervi 7 hrs, Volur 7 hrs, Volur îime Span= 1	Software So Summ ous, Inflow ne= ne= 0.00-80.00	Depth = 24,642 c 24,642 c hrs, dt= 0. <b>Reach E</b>	3.28"         ft           f         Atten=           05 hrs         DP-1: Bah	or 25-Yea 0%, Lag <b>sin</b>	ar event	: in			P1	rinted 2/1/2023 Page 10
Prepared by {e <u>HydroCAD® 10.00</u> [40] Hint: Not De Inflow Area = Inflow = Outflow = Routing by Stor-	0-26 s/n 1 escribed 1 90 6.49 6.49 -Ind+Trar	04015 © 202 (Outflow=Inf ,103 sf, 6.1 cfs @ 12.1 cfs @ 12.1 ns method, 7	0 HydroCAD low) 06% Impervi 7 hrs, Volur 7 hrs, Volur îime Span= 1	Software So Summ ous, Inflow ne= ne= 0.00-80.00	Depth = 24,642 c 24,642 c hrs, dt= 0. <b>Reach E</b>	3.28"         ft           f         Atten=           05 hrs         DP-1: Bah	or 25-Yea 0%, Lag <b>sin</b>	ar event	: in			P1	rinted 2/1/2023 Page 10
Prepared by {e <u>HydroCAD® 10.00</u> [40] Hint: Not De Inflow Area = Inflow = Outflow = Routing by Stor-	0-26 s/n 1 escribed 1 90 6.49 6.49 -Ind+Trar	04015 © 202 (Outflow=Inf ,103 sf, 6.1 cfs @ 12.1 cfs @ 12.1 ns method, 7	0 HydroCAD low) 06% Impervi 7 hrs, Volur 7 hrs, Volur îime Span= 1	Software So Summ ous, Inflow ne= ne= 0.00-80.00	Depth = 24,642 c 24,642 c hrs, dt= 0. <b>Reach E</b>	3.28"         ft           f         Atten=           05 hrs         DP-1: Bah	or 25-Yea 0%, Lag <b>sin</b>	ar event	: in			P1	rinted 2/1/2023 Page 10
Prepared by {e HydroCAD® 10.00 [40] Hint: Not De Inflow Area = Inflow = Outflow =	0-26 s/n 1 escribed 1 90 6.49 6.49 -Ind+Trar	04015 © 202 (Outflow=Inf ,103 sf, 6.1 cfs @ 12.1 cfs @ 12.1 ns method, 7	0 HydroCAD low) 06% Impervi 7 hrs, Volur 7 hrs, Volur îime Span= 1	Software So Summ ous, Inflow ne= ne= 0.00-80.00	Depth = 24,642 c 24,642 c hrs, dt= 0. <b>Reach E</b>	3.28"         ft           f         Atten=           05 hrs         DP-1: Bah	or 25-Yea 0%, Lag <b>sin</b>	ar event	: in			P1	rinted 2/1/2023 Page 10
Prepared by {e <u>HydroCAD® 10.00</u> [40] Hint: Not De Inflow Area = Inflow = Outflow = Routing by Stor-	0-26 s/n 1 escribed 1 90 6.49 6.49 -Ind+Trar	04015 © 202 (Outflow=Inf ,103 sf, 6.1 cfs @ 12.1 cfs @ 12.1 ns method, 7	0 HydroCAD low) 06% Impervi 7 hrs, Volur 7 hrs, Volur îime Span= 1	Software So Summ ous, Inflow ne= ne= 0.00-80.00	Depth = 24,642 c 24,642 c hrs, dt= 0. <b>Reach E</b>	3.28"         ft           f         Atten=           05 hrs         DP-1: Bah	or 25-Yea 0%, Lag <b>sin</b>	ar event	: in			P1	rinted 2/1/2023 Page 10
Prepared by {e <u>HydroCAD® 10.00</u> [40] Hint: Not De Inflow Area = Inflow = Outflow = Routing by Stor-	0-26 s/n ( escribed ) 90 6.49 6.49 -Ind+Trar	04015 © 202 (Outflow=Inf ,103 sf, 6.1 cfs @ 12.1 cfs @ 12.1 ns method, 7	0 HydroCAD low) 06% Impervi 7 hrs, Volur 7 hrs, Volur îime Span= 1	Software So Summ ous, Inflow ne= ne= 0.00-80.00	Depth = 24,642 c 24,642 c hrs, dt= 0. <b>Reach E</b>	3.28"         ft           f         Atten=           05 hrs         DP-1: Bah	or 25-Yea 0%, Lag <b>sin</b>	ar event	: in			P1	rinted 2/1/2023 Page 10

#### Summary for Reach DP-2: Onsite southeast

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area	a =	13,159 sf, 38.16% Imperviou	s, Inflow Depth = 4.31" for 25-Year event
Inflow	=	1.26 cfs @ 12.16 hrs, Volume	= 4,727 cf
Outflow	=	1.26 cfs @ 12.16 hrs, Volume	= 4,727 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs



Existing-2

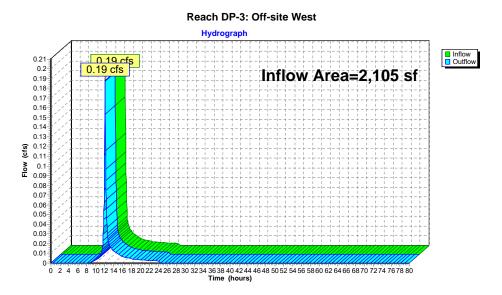
Prepared by {enter your company name here} HydroCAD® 10.00-26 s/n 04015 © 2020 HydroCAD Software Solutions LLC Type III 24-hr 25-Year Rainfall=6.35" Printed 2/1/2023 Page 12

### Summary for Reach DP-3: Off-site West

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area	a =	2,105 sf,	0.00% Impervious,	Inflow Depth = 3.	.38" for 25-Year event
Inflow	=	0.19 cfs @	12.09 hrs, Volume=	593 cf	
Outflow	=	0.19 cfs @	12.09 hrs, Volume=	593 cf,	Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs





# HydroCAD Analysis

# **Existing Conditions - 100 Year Storm**

### Area Listing (all nodes)

Area (sq-ft)	CN	Description (subcatchment-numbers)
9,896	79	50-75% Grass cover, Fair, HSG C (E-1, E-2, E-3)
10,479	98	Paved parking (E-1, E-2)
84,992	70	Woods, Good, HSG C (E-1, E-2, E-3)
105,367	74	TOTAL AREA

Existing-2 Prepared by {enter your company name here} HydroCAD® 10.00-26 s/n 04015 © 2020 HydroCAD Software Solutions LLC

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## Soil Listing (all nodes)

Area (sq-ft)	Soil Group	Subcatchment Numbers
0	HSG A	
0	HSG B	
94,888	HSG C	E-1, E-2, E-3
0	HSG D	
10,479	Other	E-1, E-2
105.367		TOTAL AREA

Existing-2	
Prepared by {enter	your company name here}
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rocAD® 10:00-26 s/n 04015 © 2020 HydroCAD Software Solutions LLC       Page         Time span=0.00-80.00 hrs, dt=0.05 hrs, 1601 points       Runoff by SCS TR-20 method, UH=SCS, Weighted-CN         Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method       Runoff Area=90,103 sf 6.06% Impervious Runoff Depth=4.6         Procetchment E-1: Flow to Existing Basin       Runoff Area=90,103 sf 6.06% Impervious Runoff Depth=4.6         Procetchment E-2: Flow onsite Southeast       Runoff Area=13,159 sf 38.16% Impervious Runoff Depth=6.6         Procetchment E-3: Flow off-site West       Runoff Area=2,105 sf 0.00% Impervious Runoff Depth=4.6         Procetchment E-3: Flow off-site West       Runoff Area=2,105 sf 0.00% Impervious Runoff Depth=4.6         Procetchment E-3: Flow off-site West       Runoff Area=2,105 sf 0.00% Impervious Runoff Depth=4.6         Procetchment E-3: Flow off-site West       Inflow=9.57 cfs 36,305         Procetchment E-3: Flow off-site West       Runoff Area=2,105 sf 0.00% Impervious Runoff Depth=4.6         Procetchment E-3: Flow off-site West       Inflow=9.57 cfs 36,305         Procetchment E-3: Flow off-site West       Inflow=9					Ind Covers (	all nodes)	)	
0         0         9,896         0         0         9,076 (Dass cover, Fair E-1, E-2, E-3)           0         0         0         10,479         10,479         9,896 (Dass cover, Fair E-1, E-2, E-3)           0         0         84,992         0         9,4992         Woods, Good         E-1, E-2, E-3           0         0         94,988         0         10,479         105,367         TOTAL AREA								
0       0       84,992       0       0       84,992       Woods, Good       E-1, E-2, E-3         0       0       94,888       0       10,479       105,367       TOTAL AREA         sting-2       Type III 24-hr       100-Year Rainfall-8.1       100-Year Rainfall-8.1         ared by (enter your company name here)       Type III 24-hr       100-Year Rainfall-8.1         School 10.00-26 is in 04015       Printed 21/120       Printed 21/120         Code 10.00-26 is in 04015       Printed 21/120       Printed 21/120         Time span=0.00-80.00 hrs, dt=0.05 hrs, 1601 points       Runoff Area=0.10.31 f. 0.0% is impervious. Runoff Deptine4 f. Runoff Verser-80, 10.01 f. 0.0% is impervious. Runoff Deptine4 f. Runoff Verser-80, 10.01 f. 0.05% is impervious. Runoff Deptine4 f. Runoff Area=13, 10.91 f. 0.0% is impervious. Runoff Deptine4 f. Te=0.0 min. CN=72 Runoff=3.7 dt 6.5, 0.50 f. Runoff Area=13, 10.91 f. 0.0% is impervious. Runoff Deptine4 f. Te=0.0 min. CN=72 Runoff=2.7 dt 6.5, 0.50 f. Statement E-2: Flow onsite Southeast       Runoff Area=13, 19.91 f. 3.1% is impervious. Runoff Deptine4 f. Te=0.0 min. CN=72 Runoff=2.7 dt 6.5, 0.50 f. Statement E-2: Flow onsite Southeast         Catchment E-3: Flow off-site West       Runoff Area=13, 19.91 f. 3.1% is impervious. Runoff Deptine4 f. Te=0.0 min. CN=72 Runoff=2.7 dt 6.5, 0.50 min. CN=73 Runoff=2.7 dt 6	0	0	9,896	0	0	9,896	50-75% Grass cover, Fair	E-1, E-2, E-3
ting-2 strig-2 ared by (enter your company name here) Scabe 100-28 is Motified by 2020 HydrocAD Software Solutions LLC The span-0 00-80.00 hrs. df-0 05 hrs. ft61 points Runoff by SCS TR-20 method. UH-SCS, Weighted.CD Reach routing by Stort-Ind Trans Houte-SC KD Reach routing by Stort-Ind Ind CM-SC Reacher 2 Runoff-124 cfs 6.592 Runoff Area-13.150 sf 3.002 Runoff Area-13.150 sf								
sting-2       Type III 24-hr 100-Year Rainfall=8.1         iared by (enter your company name here)       Printed 21/120         scADe 10.09-26 sin 04015 @ 2020 HydroCAD Software Solutions LLC       Page         Time span=0.00-80.00 hrs, dt=0.05 hrs, 1601 points       Runoff by SOG TH-20 method. UH=SGS Weighted-CN         Runoff by SOG TH-20 method. UH=SGS Weighted-CN       Runoff by SOG TH-20 method. UH=SGS Year 20 mic NH=72 Runoff=57 dt 53.65         catchmentE-1: Flow to Existing Basin       Runoff Area=13,159 af 36.16% Impervious Runoff Depth=4.6         catchmentE-2: Flow onsite Southeast       Runoff Area=13,159 af 38.16% Impervious Runoff Depth=4.6         catchmentE-3: Flow off-site West       Runoff Area=2,103 af 0.00% Impervious Runoff Depth=0.27 dt 86.55         chtP-1: Basin       Inflow=0.57 dt 93.60         cutower 57 dt 93.600       OutWere-57 dt 93.600         cutower 57 dt 93.600       Cutower 57 dt								E-1, E-2, E-3
hared by {enter your company name here}       Printed 2/1/20         DCAD® 10.00-26 s/n 04015 © 2020 HydroCAD Software Solutions LLC       Printed 2/1/20         Time span=0.00-80.00 hrs, dt=0.05 hrs, 1601 points       Runoff by SCS TR-20 method, UH=SCS, Weighted-CN         Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method       Runoff Area=90,103 sf 6.06% Impervious Runoff Depth=4.8         Flow Length=553' Tc=12.0 min CN=72 Runoff=9.57 cfs 36,305       Runoff Area=13,159 sf 38.16% Impervious Runoff Depth=6.0         catchment E-2: Flow onsite Southeast       Runoff Area=13,159 sf 38.16% Impervious Runoff Depth=4.6         catchment E-3: Flow off-site West       Runoff Area=2,105 sf 0.00% Impervious Runoff Depth=4.5         ch DP-1: Basin       Inflow=9.57 cfs 36,305         ch DP-2: Onsite southeast       Inflow=1.74 cfs 6,592								
hared by {enter your company name here}       Printed 2/1/20         DCAD® 10.00-26 s/n 04015 © 2020 HydroCAD Software Solutions LLC       Printed 2/1/20         Time span=0.00-80.00 hrs, dt=0.05 hrs, 1601 points       Runoff by SCS TR-20 method, UH=SCS, Weighted-CN         Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method       Runoff Area=90,103 sf 6.06% Impervious Runoff Depth=4.8         Flow Length=553' Tc=12.0 min CN=72 Runoff=9.57 cfs 36,305       Runoff Area=13,159 sf 38.16% Impervious Runoff Depth=6.0         catchment E-2: Flow onsite Southeast       Runoff Area=13,159 sf 38.16% Impervious Runoff Depth=4.6         catchment E-3: Flow off-site West       Runoff Area=2,105 sf 0.00% Impervious Runoff Depth=4.5         ch DP-1: Basin       Inflow=9.57 cfs 36,305         ch DP-2: Onsite southeast       Inflow=1.74 cfs 6,592							Type III 24	4-hr 100-Year Rainfall=8.16"
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN         Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method         Acatchment E-1: Flow to Existing Basin       Runoff Area=90,103 sf 6.06% Impervious Runoff Depth=4.6         Flow Length=553' Tc=12.0 min CN=72 Runoff=9.57 cfs 36,305         Acatchment E-2: Flow onsite Southeast       Runoff Area=13,159 sf 38.16% Impervious Runoff Depth=6.0         Acatchment E-3: Flow off-site West       Runoff Area=2,105 sf 0.00% Impervious Runoff Depth=4.6         Acatchment E-3: Flow off-site West       Runoff Area=2,105 sf 0.00% Impervious Runoff Depth=4.6         Acatchment E-3: Flow off-site West       Runoff Area=2,105 sf 0.00% Impervious Runoff Depth=4.6         Acatchment E-3: Flow off-site West       Runoff Area=2,105 sf 0.00% Impervious Runoff Depth=4.6         Acatchment E-3: Flow off-site West       Runoff Area=2,105 sf 0.00% Impervious Runoff Depth=4.6         Acatchment E-3: Flow off-site West       Runoff Area=2,105 sf 0.00% Impervious Runoff Depth=4.6         Acatchment E-3: Flow off-site West       Inflow=9.57 cfs 36,305         Acatchment E-3: Flow off-site Southeast       Inflow=9.57 cfs 36,305         Acatchment E-3: Flow off-site Southeast       Inflow=9.57 cfs 3	pared by {ente	er your comp 26 s/n 04015 ©	2020 HydroCA	D Software Solut		-0.05 bro. 1		Printed 2/1/2023 Page 4
Flow Length=553'       Tc=12.0 min       CN=72       Runoff=9.57 cfs       36,305         pocatchment E-2:       Flow onsite Southeast       Runoff Area=13,159 sf       38.16% Impervious       Runoff Depth=6.0         pocatchment E-3:       Flow off-site West       Runoff Area=2,105 sf       0.00% Impervious       Runoff Depth=4.5         pocatchment E-3:       Flow off-site West       Runoff Area=2,105 sf       0.00% Impervious       Runoff Depth=4.5         pocatchment E-3:       Flow off-site West       Inflow=9.57 cfs       36,305         pocatchment E-3:       Flow off-site West       Runoff Area=2,105 sf       0.00% Impervious       Runoff Depth=4.5         pocatchment E-3:       Flow off-site West       Inflow=9.57 cfs       36,305         pocatchment E-3:       Flow off-site Southeast       Inflow=9.57 cfs       36,305         pocatchment E-3:       Flow off-site Southeast       Inflow=9.57 cfs       36,305			Ru	noff by SCS TF	R-20 method, l	JH=SCS, W Pond rout	/eighted-CN ing by Stor-Ind method	
Flow Length=140'         Tc=11.3 min         CN=82         Runoff=1.74 cfs         6,592           catchment E-3: Flow off-site West         Runoff Area=2,105 sf         0.00%         Impervious         Runoff Depth=4.5           ch DP-1: Basin         Inflow=9.57 cfs         36,305         Outflow=9.57 cfs         36,305           ch DP-2: Onsite southeast         Inflow=1.74 cfs         6,592         Inflow=1.74 cfs         6,592	catchment E-1	I: Flow to Exi	sting Basin			Flow Le	ngth=553' Tc=12.0 min C	N=72 Runoff=9.57 cfs 36,305 cf
Tc=6.0 min         CN=73         Runoff=0.27 cfs         869           Inch DP-1: Basin         Inflow=9.57 cfs         36,305           Outflow=9.57 cfs         36,305           Inch DP-2: Onsite southeast         Inflow=1.74 cfs         6,592	catchment E-2	2: Flow onsite	Southeast					
Outflow=9.57 cfs 36,305 Inflow=1.74 cfs 6,592	catchment E-3	3: Flow off-sit	e West			R		
								Inflow=9.57 cfs 36,305 cf Outflow=9.57 cfs 36,305 cf
								Inflow=1.74 cfs 6,592 cf Outflow=1.74 cfs 6,592 cf
	ach DP-3: Off-s	ite West						Inflow=0.27 cfs 869 cf Outflow=0.27 cfs 869 cf

i ype III			thod, UH=S Rainfall=8.16		ted-CN, Ti	ime Spar	n= 0.00-8	0.00 hrs	, dt= 0.	05 hrs					
A	Area (sf)	CN	Description												_
ł	5,457 76,777		Paved parki Woods, Goo												
	7,869		50-75% Gra Weighted Av		air, HSG	С									_
	84,646 5,457	1	93.94% Per 6.06% Impe	vious Area											
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Descripti	on									
8.6 3.4		0.0530 0.0240			Sheet FI Woods: I Shallow	ight und Concen	erbrush <b>trated Fl</b>		10 P2=	= 3.05"					
12.0	553	Total			Unpaved	Kv= 16	6.1 fps								_
	ed by {en		· company r								Туре	II 24-hr	100-Ye	<i>ar Rainfall=8.1</i> Printed 2/1/202	23
Prepare	ed by {en		• company r 4015 © 2020	) HydroCAD	Software			v to Ex	isting	Basir		II 24-hr	100-Ye		23
Prepare	ed by {en			) HydroCAD	) Software : ubcatch		-1: Flov	v to Ex	isting	Basir		II 24-hr	100-Ye	Printed 2/1/202	23
Prepare HydroCA	ed by {en	-26 s/n 0		) HydroCAD	) Software : ubcatch	ment E	-1: Flov	- 100	)-Ye	ar F	Type Rainfa	24   =8.	-hr 16"	Printed 2/1/202	23
Prepare HydroCA 11	ed by {en AD® 10.00-	-26 s/n 0	4015 © 2020	) HydroCAD	) Software : ubcatch	ment E	-1: Flow	100 R	)-Ye uno	ear F	Type tainfa rea=9	III 24 II=8. 0,103	-hr 16" 8 sf	Printed 2/1/202 Page	23
Prepare HydroCA 11	ed by {en	-26 s/n 0	4015 © 2020	) HydroCAD	) Software : ubcatch	ment E	-1: Flow	100 R	)-Ye uno off V	ear F ff Ai /olu	Type Rainfa rea=9 me=3	III 24 II=8.: 0,103 6,305	-hr 16" 3 sf	Printed 2/1/202 Page	23
Prepare HydroCA	ed by {en <u>AD® 10.00-</u>	-26 s/n 0	4015 © 2020	) HydroCAD	) Software : ubcatch	ment E	-1: Flow	100 R	)-Ye uno off V Ru	ear F ff Ai /olu noff	Type tainfa rea=9	III 24 II=8. 0,103 6,305 h=4.8	-hr 16" 3 sf 5 cf 34"	Printed 2/1/202 Page	23

#### Summary for Subcatchment E-2: Flow onsite Southeast

Runoff 1.74 cfs @ 12.16 hrs, Volume= 6,592 cf, Depth= 6.01" =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=8.16"

	А	rea (sf)	CN	Description		
	ł	5,022	98	Paved park	ina	
		6.746			od, HSG C	
		1,391				Fair, HSG C
-		13.159		Weighted A	,	
		8.137			rvious Area	
		5,022			pervious Area	
		5,022		50. 10 /0 mm		5a
	Тс	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)		(cfs)	
-	11.0	50	0.0280			Sheet Flow.
						Woods: Light underbrush n= 0.400 P2= 3.05"
	0.1	45	0.1750	6.74		Shallow Concentrated Flow,
	0		000	0		Unpaved Kv= 16.1 fps
	0.0	11	0.1640	6.52		Shallow Concentrated Flow,
	0.0		0.1010	0.02		Unpaved Kv= 16.1 fps
	0.2	34	0.0240	3.14		Shallow Concentrated Flow,
	0.2	04	0.0240	0.14		Paved Kv= 20.3 fps
-	11.3	140	Total			

Existing-2

Type III 24-hr 100-Year Rainfall=8.16" Printed 2/1/2023 Prepared by {enter your company name here} HydroCAD® 10.00-26 s/n 04015 © 2020 HydroCAD Software Solutions LLC Page 8 Subcatchment E-2: Flow onsite Southeast Hydrograph Runoff 1.74 cfs Type III 24-hr 100-Year Rainfall=8.16" Runoff Area=13,159 sf Runoff Volume=6,592 cf Flow (cfs) Runoff Depth=6.01" Flow Length=140' Tc=11.3 min **CN=82** 0 2 4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 34 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70 72 74 76 78 80 Time (hours)

Runoff	=	0.27	cfs @	12.09	hrs,	Volum	ne=		8	869 cf	, Dep	th=	4.95	"										
	y SCS TF 24-hr 100					eighte	d-CN,	, Time	Spa	an= 0.	00-80	.00	nrs, c	lt= 0.	05 h	rs								
A	rea (sf)	CN		ription																				
	1,469 636	70 79	50-75	ds, Goo 5% Gra	ss cov	er, Fa	ir, HS	GC																
	2,105 2,105	73		hted Av 00% Pe																				
Тс	Length			elocity	Capa	city I	Descri	iption																
<u>(min)</u> 6.0	(feet)	(ft/f	t) (f	t/sec)	(0	cfs) I	Direct	Entry	/, Mi	in.														
						5	Subca	atchr	nen	nt E-3	3: Flo	w o	off-s	ite V	Vest	t								
				/	1		- !! -!-			irograpi									Runoff					
				0.28 0.26 0.24 0.22 0.18 0.16 0.12 0.18 0.16 0.12 0.19 0.08 0.06 0.04 0.04 0.04 0.04 0.04 0.04 0.04							2444648	Runo	er F off / noff		fall= ne= oth= c=6.	=8.1 105 869 =4.9 :0 m :N=	6" 5f 5" 1in 73							
Existin	a-2																Ty	pe l	11 24	-hr	100-`	Year F	Rainfall=	=8.16"
Prepare	<b>g-2</b> d by {ent D® 10.00-2						Softwar	re Solu mma			each	DP	-1:1	Basi	n		Ту	pe l	ll 24	l-hr	100-`		Rainfall- nted 2/ Pa	
Prepare HydroCAI	d by {ent D® 10.00-:	<u>26 s/n</u>	04015	© 2020	) Hydro		Softwar				each	DP	-1:1	Basi	n		Ту	pe l	II 24	-hr	100-`		nted 2/2	1/2023
HydroCA	d by {ent <u>D® 10.00-</u> ; : Not Des	26 s/n cribed 90 9.57	04015 (Outflo ,103 s cfs @	© 2020	<u>) Hydro</u> ow) 6% Im 7 hrs, '	pervic Volum	Softwar Su Sus, Ir ne=	mma	<b>ry f</b>	or R	4.84"	foi	100	)-Yea	ır eve		Ту	rpe l	<i>II 24</i>	-hr	100-		nted 2/2	1/2023
Prepare HydroCAI [40] Hint: Inflow Ar Inflow Outflow	d by {ent <u>D® 10.00-</u> ; : Not Des ea = =	26 s/n cribed 90 9.57 9.57	(Outfld ,103 s cfs @ cfs @	© 2020 cow=Infl if, 6.0 12.17 12.17	) <u>Hydro</u> ow) 6% Im 7 hrs, 7	pervic Volum	Softwar Su Sus, Ir ne= ne=	mma	<b>ry f</b> Dept 36,3 36,3	<b>or R</b> h = 05 cf	4.84" , Atte	foi n= C	100	)-Yea	ır eve		Ty	rpe l	<i>II 24</i>	-hr	100-`		nted 2/2	1/2023
Prepare HydroCAI [40] Hint: Inflow Ar Inflow Outflow	d by {ent <u>D® 10.00-</u> : Not Des :ea = = =	26 s/n cribed 90 9.57 9.57	(Outfld ,103 s cfs @ cfs @	© 2020 cow=Infl if, 6.0 12.17 12.17	) <u>Hydro</u> ow) 6% Im 7 hrs, 7	pervic Volum	Softwar Su Sus, Ir ne= ne=	mma nflow [ 0.00 hi	<b>ry f</b> Dept 36,3 36,3 rs, d	<b>for R</b> th = 505 cf 505 cf tt= 0.0	4.84" , Atte	foi n= 0	· 100 %, L	)-Yea	ır eve		Ту	pe l	<i>II 24</i>	'-hr	100-`		nted 2/2	1/2023
Prepare HydroCAI [40] Hint: Inflow Ar Inflow Outflow	d by {ent <u>D® 10.00-</u> : Not Des :ea = = =	26 s/n cribed 90 9.57 9.57	(Outfld ,103 s cfs @ cfs @	© 2020 cow=Infl if, 6.0 12.17 12.17	) <u>Hydro</u> ow) 6% Im 7 hrs, 7	pervic Volum	Softwar Su Sus, Ir ne= ne=	mma nflow [ 0.00 hr R	<b>ry f</b> Dept 36,3 36,3 rs, d <b>Reac</b>	<b>for R</b> th = 505 cf 505 cf tt= 0.0	4.84" , Atte )5 hrs <b>P-1:</b>	foi n= 0	· 100 %, L	)-Yea	ır eve		<i>Ty</i>	т <b>ре /</b>		-hr	100-		nted 2/2	1/2023
Prepare HydroCAI [40] Hint: Inflow Ar Inflow Outflow	d by {ent <u>D® 10.00-</u> : Not Des :ea = = =	26 s/n cribed 90 9.57 9.57	(Outfld ,103 s cfs @ cfs @	© 2020 cow=Infl if, 6.0 12.17 12.17 thod, T	ow) 6% Im 7 hrs, 7 ime Sp	pervic Volum	Softwar Su Sus, Ir ne= ne=	mma nflow [ 0.00 hr R	<b>ry f</b> Dept 36,3 36,3 rs, d <b>Reac</b>	or R h = 05 cf 05 cf t= 0.0 ch D	4.84" , Atte 05 hrs <b>P-1:</b>	for n= 0 Bas	• 100 %, L .in	)-Yea _ag=	or eve 0.0 r	nin							nted 2/2	1/2023
Prepare HydroCAI [40] Hint: Inflow Ar Inflow Outflow	d by {ent D® 10.00- ea = = = =	26 s/n cribed 90 9.57 9.57 d+Trat	(Outfld ,103 s cfs @ cfs @	© 202( bw=Infl if, 6.0 12.17 12.17 thod, T	ow) 6% Im 7 hrs, 7 ime Sp	pervic Volum	Softwar Su Sus, Ir ne= ne=	mma nflow [ 0.00 hr R	<b>ry f</b> Dept 36,3 36,3 rs, d <b>Reac</b>	or R h = 05 cf 05 cf t= 0.0 ch D	4.84" , Atte 05 hrs <b>P-1:</b>	for n= 0 Bas	• 100 %, L .in	)-Yea	or eve 0.0 r	nin						Prir	nted 2/2	1/2023
Prepare HydroCAI [40] Hint: Inflow Ar Inflow Outflow	d by {ent D® 10.00- ea = = = =	26 s/n cribed 90 9.57 9.57 d+Trai	(Outfld ,103 s cfs @ cfs @	© 2020 cow=Infl if, 6.0 12.17 12.17 thod, T	ow) 6% Im 7 hrs, 7 ime Sp	pervic Volum	Softwar Su Sus, Ir ne= ne=	mma nflow [ 0.00 hr R	<b>ry f</b> Dept 36,3 36,3 rs, d <b>Reac</b>	or R h = 05 cf 05 cf t= 0.0 ch D	4.84" , Atte 05 hrs <b>P-1:</b>	for n= 0 Bas	• 100 %, L .in	)-Yea _ag=	or eve 0.0 r	nin						Prir	nted 2/2	1/2023
Prepare HydroCAI [40] Hint: Inflow Ar Inflow Outflow	d by {ent D® 10.00- ea = = = =	26 s/n cribed 90 9.57 9.57 d+Trat	(Outfld ,103 s cfs @ cfs @	© 2020 cow=Infl if, 6.0 12.17 12.17 thod, T	ow) 6% Im 7 hrs, 7 ime Sp	pervic Volum	Softwar Su Sus, Ir ne= ne=	mma nflow [ 0.00 hr R	<b>ry f</b> Dept 36,3 36,3 rs, d <b>Reac</b>	or R h = 05 cf 05 cf t= 0.0 ch D	4.84" , Atte 05 hrs <b>P-1:</b>	for n= 0 Bas	• 100 %, L .in	)-Yea _ag=	or eve 0.0 r	nin						Prir	nted 2/2	1/2023
Prepare HydroCAI [40] Hint: Inflow Ar Inflow Outflow	d by {ent D® 10.00-7 ea = = = = by Stor-In	26 <u>s/n</u> cribed 90 9.57 9.57 d+Trai	(Outfld ,103 s cfs @ cfs @	© 2020 cow=Infl if, 6.0 12.17 12.17 thod, T	ow) 6% Im 7 hrs, 7 ime Sp	pervic Volum	Softwar Su Sus, Ir ne= ne=	mma nflow [ 0.00 hr R	<b>ry f</b> Dept 36,3 36,3 rs, d <b>Reac</b>	or R h = 05 cf 05 cf t= 0.0 ch D	4.84" , Atte 05 hrs <b>P-1:</b>	for n= 0 Bas	• 100 %, L .in	)-Yea _ag=	or eve 0.0 r	nin						Prir	nted 2/2	1/2023
Prepare HydroCAI [40] Hint: Inflow Ar Inflow Outflow	d by {ent D® 10.00-7 ea = = = = by Stor-In	26 <u>s/n</u> cribed 90 9.57 9.57 d+Trai	(Outfld ,103 s cfs @ cfs @	© 2020 cow=Infl if, 6.0 12.17 12.17 thod, T	ow) 6% Im 7 hrs, 7 ime Sp	pervic Volum	Softwar Su Sus, Ir ne= ne=	mma nflow [ 0.00 hr R	<b>ry f</b> Dept 36,3 36,3 rs, d <b>Reac</b>	or R h = 05 cf 05 cf t= 0.0 ch D	4.84" , Atte 05 hrs <b>P-1:</b>	for n= 0 Bas	• 100 %, L .in	)-Yea _ag=	or eve 0.0 r	nin						Prir	nted 2/2	1/2023
Prepare HydroCAI [40] Hint: Inflow Ar Inflow Outflow	d by {ent D® 10.00- ea = = = =	26 <u>s/n</u> cribed 90 9.57 9.57 d+Trai	(Outfld ,103 s cfs @ cfs @	© 2020 cow=Infl if, 6.0 12.17 12.17 thod, T	ow) 6% Im 7 hrs, 7 ime Sp	pervic Volum	Softwar Su Sus, Ir ne= ne=	mma nflow [ 0.00 hr R	<b>ry f</b> Dept 36,3 36,3 rs, d <b>Reac</b>	or R h = 05 cf 05 cf t= 0.0 ch D	4.84" , Atte 05 hrs <b>P-1:</b>	for n= 0 Bas	• 100 %, L .in	)-Yea _ag=	or eve 0.0 r	nin						Prir	nted 2/2	1/2023
Prepare HydroCAI [40] Hint: Inflow Ar Inflow Outflow	d by {ent D® 10.00-7 ea = = = = by Stor-In	26 <u>s/n</u> cribed 90 9.57 9.57 d+Trai	(Outfld ,103 s cfs @ cfs @	© 2020 cow=Infl if, 6.0 12.17 12.17 thod, T	ow) 6% Im 7 hrs, 7 ime Sp	pervic Volum	Softwar Su Sus, Ir ne= ne=	mma nflow [ 0.00 hr R	<b>ry f</b> Dept 36,3 36,3 rs, d <b>Reac</b>	or R h = 05 cf 05 cf t= 0.0 ch D	4.84" , Atte 05 hrs <b>P-1:</b>	for n= 0 Bas	• 100 %, L .in	)-Yea _ag=	or eve 0.0 r	nin						Prir	nted 2/2	1/2023
Prepare HydroCAI [40] Hint: Inflow Ar Inflow Outflow	d by {ent D® 10.00-7 ea = = = = by Stor-In	26 <u>s/n</u> cribed 900 9.57 9.57 d+Trai	(Outfld ,103 s cfs @ cfs @	© 2020 cow=Infl if, 6.0 12.17 12.17 thod, T	ow) 6% Im 7 hrs, 7 ime Sp	pervic Volum	Softwar Su Sus, Ir ne= ne=	mma nflow [ 0.00 hr R	<b>ry f</b> Dept 36,3 36,3 rs, d <b>Reac</b>	or R h = 05 cf 05 cf t= 0.0 ch D	4.84" , Atte 05 hrs <b>P-1:</b>	for n= 0 Bas	• 100 %, L .in	)-Yea _ag=	or eve 0.0 r	nin						Prir	nted 2/2	1/2023

#### Summary for Reach DP-2: Onsite southeast

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area	a =	13,159 sf, 38.16% Impervious, Inflow Depth = 6.01" for 100-Year event	
Inflow	=	1.74 cfs @ 12.16 hrs, Volume= 6,592 cf	
Outflow	=	1.74 cfs @ 12.16 hrs, Volume= 6,592 cf, Atten= 0%, Lag= 0.0 min	

Routing by Stor-Ind+Trans method, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs

Participant provide the second second

Existing-2

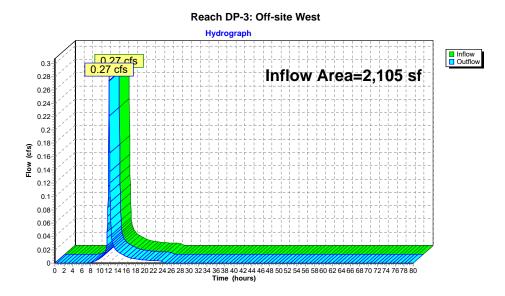
Prepared by {enter your company name here} HydroCAD® 10.00-26 s/n 04015 © 2020 HydroCAD Software Solutions LLC Type III 24-hr 100-Year Rainfall=8.16" Printed 2/1/2023 Page 12

#### Summary for Reach DP-3: Off-site West

[40] Hint: Not Described (Outflow=Inflow)

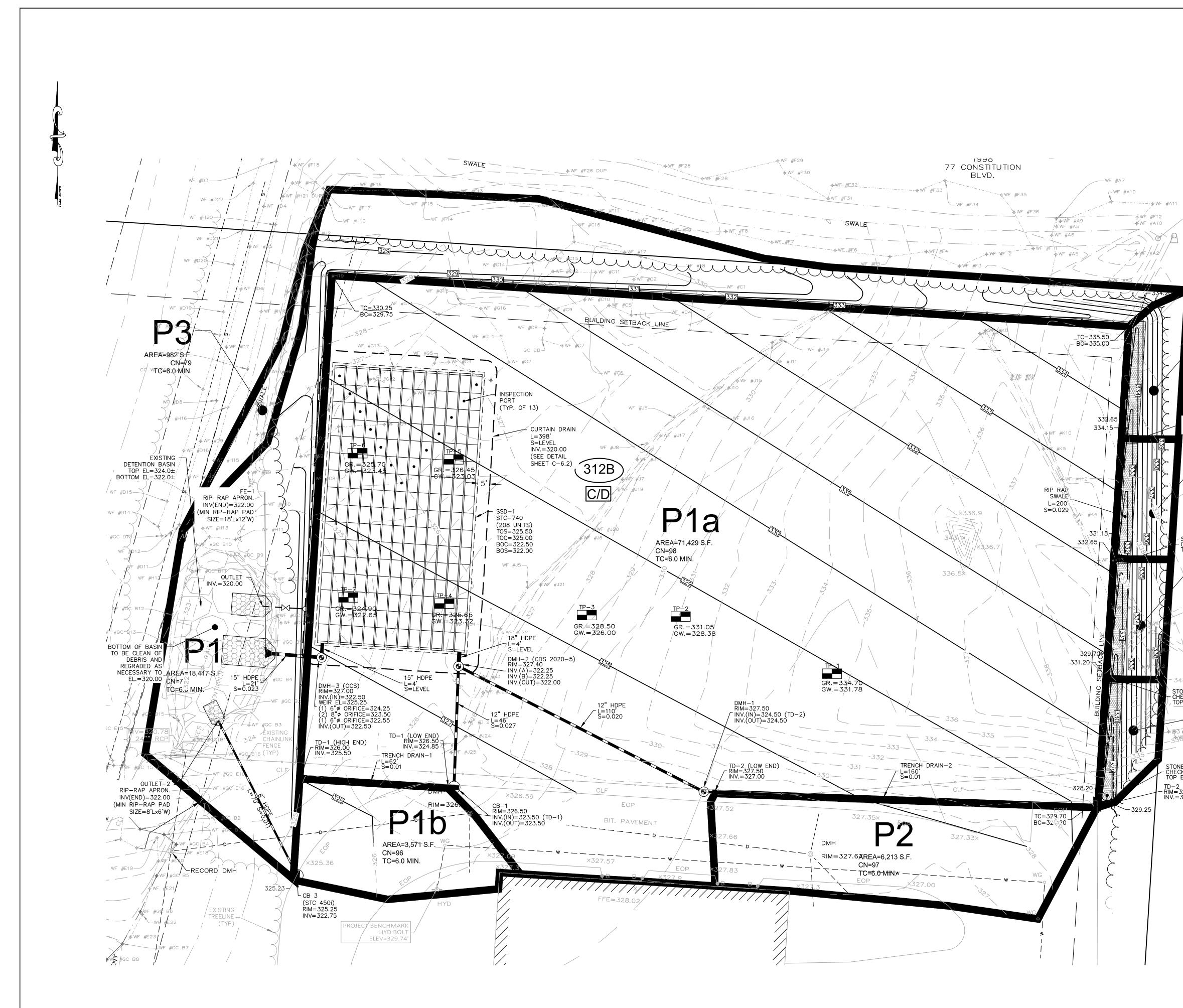
Inflow Area	a =	2,105 sf,	0.00% Impervious,	Inflow Depth = 4.95"	for 100-Year event
Inflow	=	0.27 cfs @ 1	12.09 hrs, Volume=	869 cf	
Outflow	=	0.27 cfs @ 1	12.09 hrs, Volume=	869 cf, Atter	n= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs





### Proposed Drainage Plan & HydroCAD Diagram



# WATERSHED LEGEND



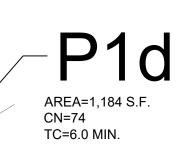
TC=6.0 MIN.

# ONE GABION ECK DAM P EL.=334.05

FES

INV≠335.15

/INV=330.63



STONE GABION CHECK DAM TOP EL.=332.50



AREA=1,184 S.F. ₩F**QN**1 75 TC=6.0 MIN.

STONE GABION CHECK DAM TOP EL.=331.00 P1

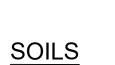
243WF-#L5 AREA=1,071 S.F. CN=74 TC=6.0 MIN.

STONE GABION - CHECK DAM TOP EL.=329.50 TD-2 (HIGH END) - RIM=329.15 INV.=328.60





HYDROLOGIC SOIL GROUP



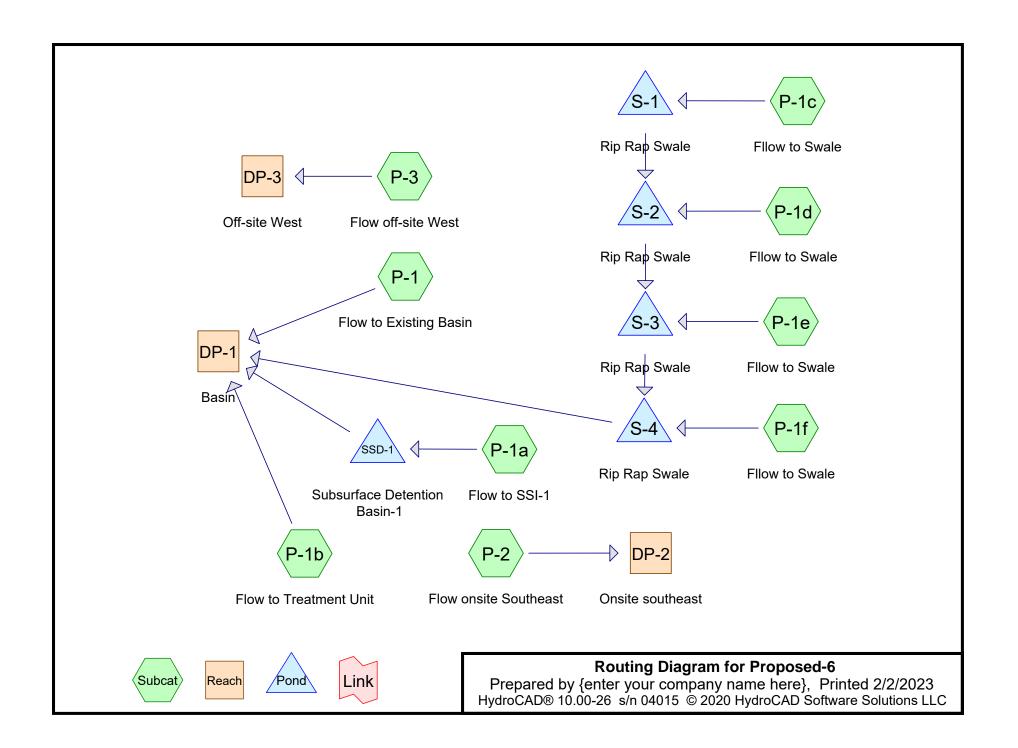


(312B) WOODBRIDGE FINE SANDY LOAM



NO DATE

REVISIONS

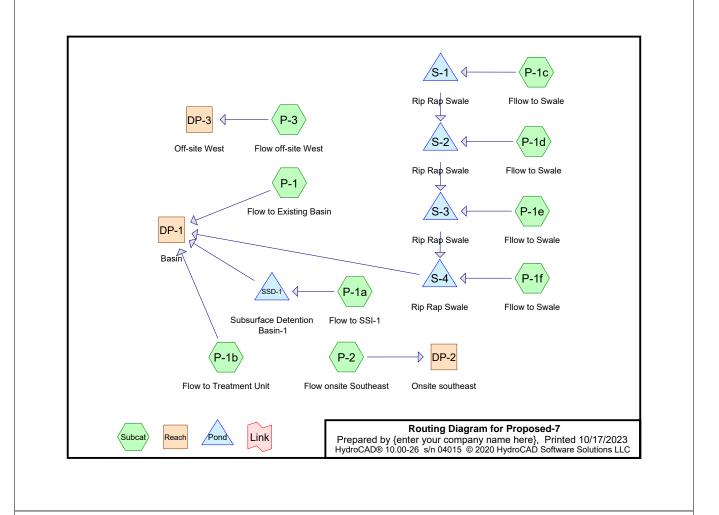




### HydroCAD Analysis

## **Proposed Conditions - 2 Year Storm**

249 SOUTH STREET UNIT 1 PLAINVILLE MA 02762 TEL508 695 2221 FAX508 695 2219 CONTACT@LEVELDG.COM LEVELDG.COM



### Proposed-7

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### Area Listing (all nodes)

Area	CN	Description
(acres)		(subcatchment-numbers)
0.426	79	50-75% Grass cover, Fair, HSG C (P-1, P-1a, P-1b, P-1c, P-1d, P-1e, P-1f, P-2, P-3)
1.838	98	Paved parking (P-1a, P-1b, P-2)
0.032	66	Rip Rap Swale (P-1c, P-1d, P-1e, P-1f)
0.123	70	Woods, Good, HSG C (P-1, P-1c, P-1d, P-1e, P-1f, P-3)
2.419	93	TOTAL AREA

#### Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
0.000	HSG B	
0.549	HSG C	P-1, P-1a, P-1b, P-1c, P-1d, P-1e, P-1f, P-2, P-3
0.000	HSG D	
1.870	Other	P-1a, P-1b, P-1c, P-1d, P-1e, P-1f, P-2
2.419		TOTAL AREA

#### Proposed-7

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#### HSG-A HSG-B HSG-C HSG-D Other Total Ground Subcatchment (acres) (acres) (acres) (acres) (acres) (acres) Cover Numbers 0.000 0.000 0.426 0.000 0.426 50-75% Grass cover, Fair P-1, P-1a, P-1b, P-1c, P-1d, P-1e, P-1f, P-2, P-3 0.000 0.000 0.000 0.000 0.000 1.838 1.838 Paved parking P-1a, P-1b, P-2 0.000 0.000 0.000 0.032 0.032 P-1c, P-1d, P-1e, P-1f 0.000 Rip Rap Swale 0.000 0.000 0.123 0.000 0.000 0.123 Woods, Good P-1, P-1c, P-1d, P-1e, P-1f, P-3 0.000 0.000 0.549 0.000 1.870 2.419 TOTAL AREA

Ground Covers (all nodes)

rija ob, a	10.00 20	0,1101010	© 2020 Hydro	0/12 00111						Pag
Line#	Node	In-Invert	Out-Invert	Length	Slope	e Listin n	<b>ig (all nodes</b> Diam/Width	5) Height	Inside-Fill	
Linon	Number	(feet)	(feet)	(feet)	(ft/ft)		(inches)	(inches)	(inches)	
1	SSD-1	322.50	322.00	21.3	0.0235	0.013	15.0	0.0	0.0	
<b>Propos</b> Prenare	ed-7	r vour com	pany name	herel						Type III 24-hr 2-Year Rainfall=3. Printed 10/17/20
HydroCA	D® 10.00-26	i s/n 04015	© 2020 Hydro	CAD Softw	/are Soluti	ions LLC				Plinted 10/17/20

Runoff Area=18,417 sf 0.00% Impervious Runoff Depth=1.11" Flow Length=461' Tc=10.0 min CN=77 Runoff=0.46 cfs 0.039 af Subcatchment P-1: Flow to Existing Basin Subcatchment P-1a: Flow to SSI-1 Runoff Area=71,428 sf 99.59% Impervious Runoff Depth=2.82" Tc=6.0 min CN=98 Runoff=4.74 cfs 0.385 af Runoff Area=3,571 sf 87.17% Impervious Runoff Depth=2.60" Tc=6.0 min CN=96 Runoff=0.23 cfs 0.018 af Subcatchment P-1b: Flow to Treatment Unit Subcatchment P-1c: Fllow to Swale Runoff Area=1,317 sf 0.00% Impervious Runoff Depth=0.84" Tc=6.0 min CN=72 Runoff=0.03 cfs 0.002 af Runoff Area=1,184 sf 0.00% Impervious Runoff Depth=0.94" Tc=6.0 min CN=74 Runoff=0.03 cfs 0.002 af Subcatchment P-1d: Fllow to Swale Subcatchment P-1e: Fllow to Swale Runoff Area=1,184 sf 0.00% Impervious Runoff Depth=0.99" Tc=6.0 min CN=75 Runoff=0.03 cfs 0.002 af Runoff Area=1,071 sf 0.00% Impervious Runoff Depth=0.94" Tc=6.0 min CN=74 Runoff=0.03 cfs 0.002 af Subcatchment P-1f: Fllow to Swale Runoff Area=6,213 sf 93.87% Impervious Runoff Depth=2.71" Subcatchment P-2: Flow onsite Southeast Tc=6.0 min CN=97 Runoff=0.41 cfs 0.032 af Runoff Area=982 sf 0.00% Impervious Runoff Depth=1.23" Tc=6.0 min CN=79 Runoff=0.03 cfs 0.002 af Subcatchment P-3: Flow off-site West Reach DP-1: Basin Inflow=1.31 cfs 0.292 af Outflow=1.31 cfs 0.292 af Reach DP-2: Onsite southeast

Inflow=0.41 cfs 0.032 af Outflow=0.41 cfs 0.032 af

Reach DP-3: Off-site West

Pond S-1: Rip Rap Swale

Pond S-2: Rip Rap Swale

Pond S-3: Rip Rap Swale

Pond S-4: Rip Rap Swale

Pond SSD-1: Subsurface Detention Basin-1

Inflow=0.03 cfs 0.002 af Outflow=0.03 cfs 0.002 af

Peak Elev=333.17' Storage=92 cf Inflow=0.03 cfs 0.002 af Outflow=0.00 cfs 0.000 af

Peak Elev=331.73' Storage=93 cf Inflow=0.03 cfs 0.002 af Outflow=0.00 cfs 0.000 af

Peak Elev=330.29' Storage=98 cf Inflow=0.03 cfs 0.002 af Outflow=0.00 cfs 0.000 af

Peak Elev=328.70' Storage=84 cf Inflow=0.03 cfs 0.002 af Outflow=0.00 cfs 0.000 af

 Peak Elev=323.55' Storage=7,838 cf
 Inflow=4.74 cfs
 0.385 af

 Discarded=0.08 cfs
 0.149 af
 Primary=0.83 cfs
 0.236 af
 Outflow=0.92 cfs
 0.385 af

Total Runoff Area = 2.419 ac Runoff Volume = 0.485 af Average Runoff Depth = 2.40" 24.00% Pervious = 0.581 ac 76.00% Impervious = 1.838 ac

#### Proposed-7

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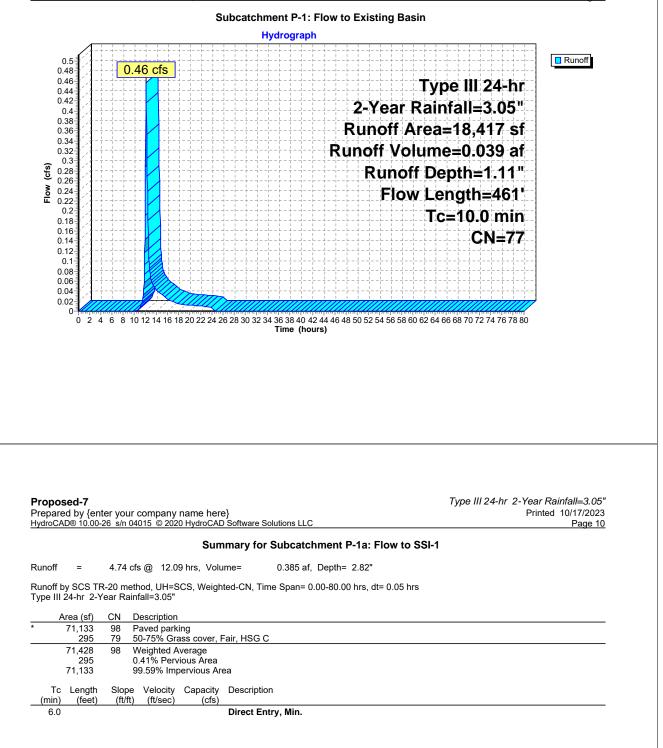
#### Summary for Subcatchment P-1: Flow to Existing Basin

Runoff = 0.46 cfs @ 12.15 hrs, Volume= 0.039 af, Depth= 1.11"

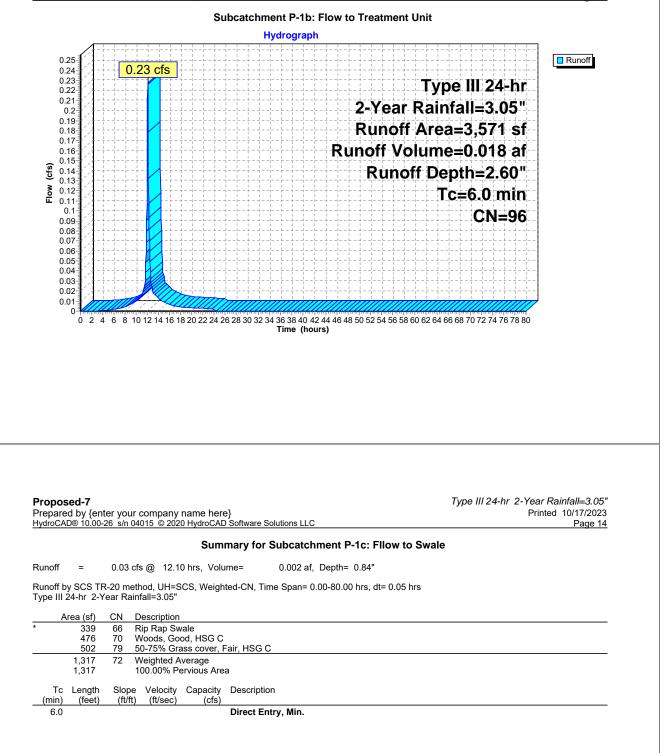
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs Type III 24-hr 2-Year Rainfall=3.05"

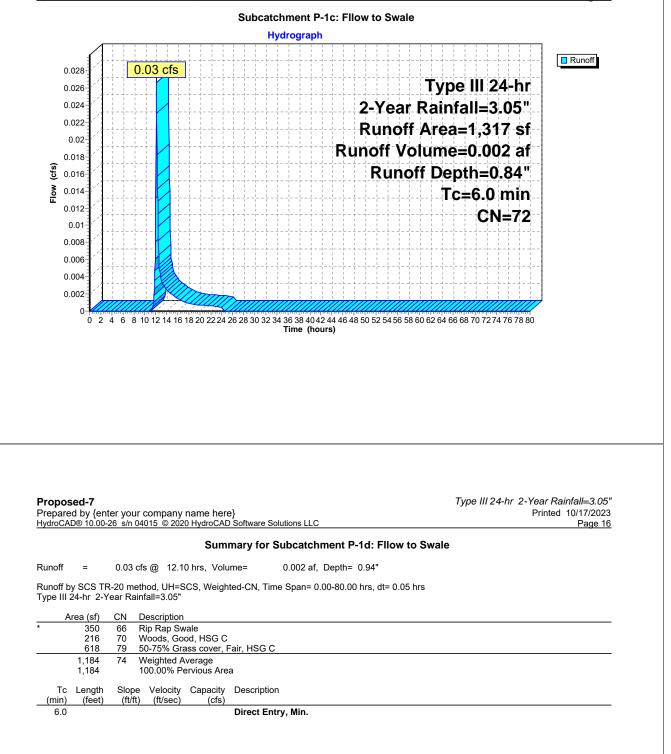
_	A	rea (sf)	CN	Description		
_		4,454	70	Woods, Go		
_		13,963	79	50-75% Gr	ass cover, F	Fair, HSG C
		18,417	77	Weighted A	verage	
		18,417		100.00% P	ervious Are	a
	Тс	Length	Slope	e Velocity	Capacity	Description
	(min)	(feet)	(ft/ft	) (ft/sec)	(cfs)	
-	7.3	50	0.080	0.11		Sheet Flow, Sheet Flow
	2.7	411	0.024	) 2.49		Woods: Light underbrush n= 0.400 P2= 3.05" Shallow Concentrated Flow.
_						Unpaved Kv= 16.1 fps
	40.0	101	<b>T</b> · ·			

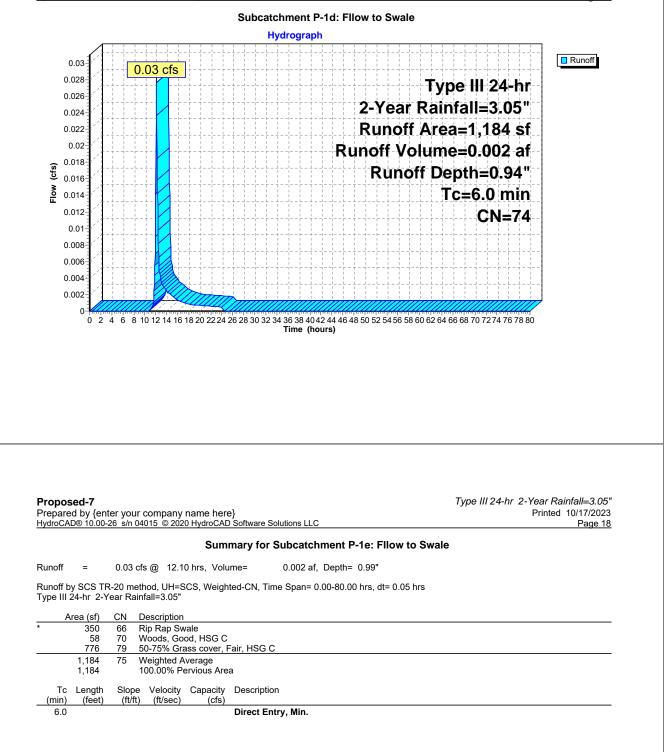
10.0 461 Total

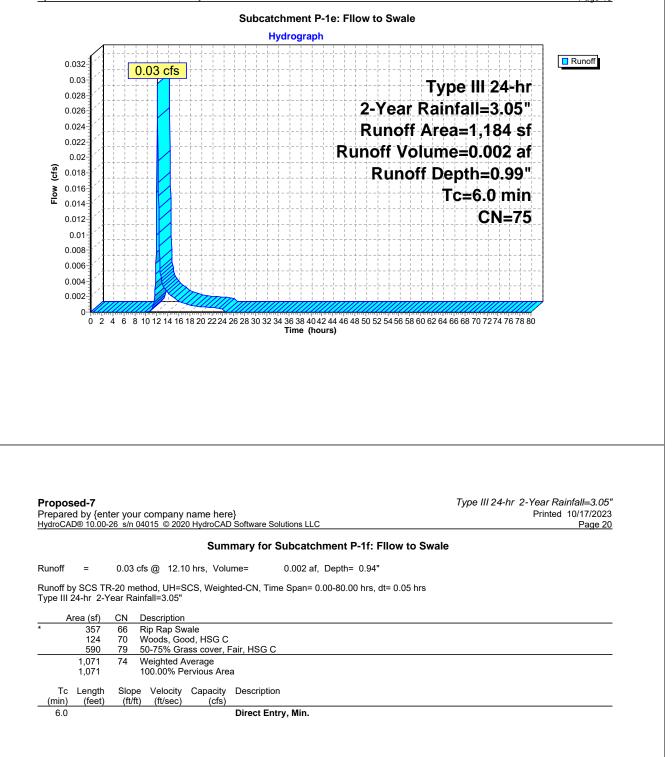


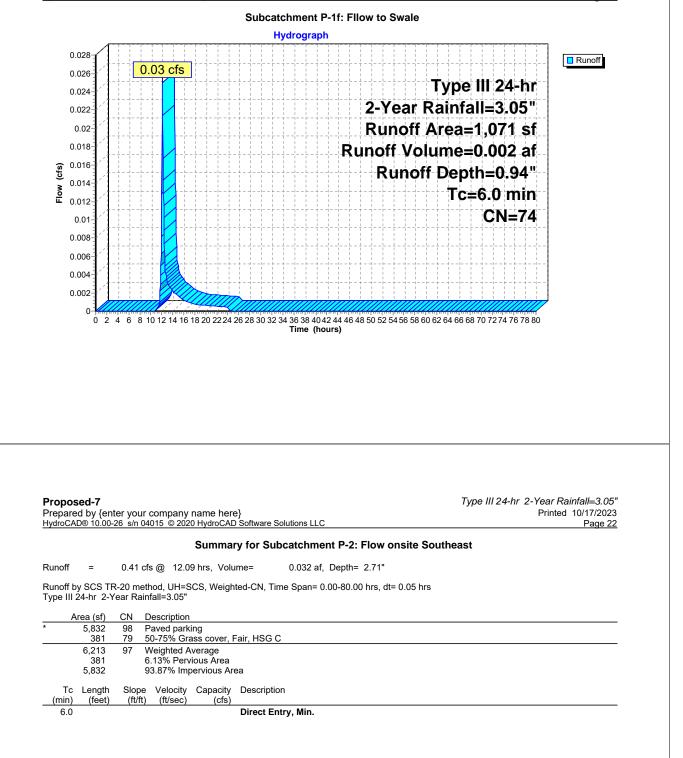
					tchment F Iydrograph		10 331-1						
Elow (cts)		4.74 cfs				2 Ri	-Year inoff off V Runc	<sup>•</sup> Raii Area olum off De	nfal 1=71 1e=0 epth	,428 .385	95" sf af 92" nin	L Ru	inoff
0-4					1 36 38 40 42	44 46 48 50	52 54 56 58	3 60 62 64					
	2468	10 12 14 16 1	8 20 22 24 26	28 30 32 34	Time (hou		02 04 00 00		00 00 /	0 72 74 76	6 78 80		
	2468	10 12 14 16 1	8 20 22 24 26	28 30 32 34			02 04 00 00		00 00 7	0 72 74 76	6 78 80		
	2468	10 12 14 16 1	8 20 22 24 26	28 30 32 34					00 08 7	0 72 74 76	6 78 80		
		10 12 14 16 1	8 20 22 24 26	28 30 32 34					00 00 //	0 72 74 76	57880		
Proposed	<b>7</b> γ {enter yo	bur company	/ name here	∋}	Time (hou						r 2-Yea	ar Rainfai inted 10/	17/2023
Proposed	<b>7</b> γ {enter yo		/ name here 20 HydroCAD	9} 9 Software S	Time (hou	rs)			Туре		r 2-Yea	inted 10/2	
Proposed Prepared by HydroCAD® 1	<b>-7</b> / {enter yc 0.00-26 s/r	our company n 04015 © 202	/ name here 20 HydroCAD <b>Summary</b>	≥} Software S y for Sube	Time (hou	t P-1b: Flo	ow to Tre		Туре		r 2-Yea	inted 10/2	17/2023
Proposed Prepared by HydroCAD® 1 Runoff = Runoff by SC	<b>-7</b> √ {enter yc 0.00-26 s/r 0.2 CS TR-20 r	bur company	y name here 20 HydroCAD <b>Summary</b> 09 hrs, Volu SCS, Weigh	e} <u>Software S</u> <b>/ for Sub</b> o me=	olutions LLC catchmen 0.018 af,	r <b>s)</b> t <b>P-1b: Fl</b> a Depth= 2.6	ow to Tre	eatment	Туре		r 2-Yea	inted 10/2	17/2023
Proposed- Prepared by HydroCAD® 1 Runoff = Runoff by SC Type III 24-h Area	<b>-7</b> / {enter yc 0.00-26 s/i 5 TR-20 r r 2-Year F (sf) CN	Dur company n 04015 © 202 3 cfs @ 12.0 nethod, UH=3 Rainfall=3.05" Descriptior	y name here 20 HydroCAD <b>Summary</b> 09 hrs, Volu SCS, Weigh	e} <u>Software S</u> <b>/ for Sub</b> o me=	olutions LLC catchmen 0.018 af,	r <b>s)</b> t <b>P-1b: Fl</b> a Depth= 2.6	ow to Tre	eatment	Туре		r 2-Yea	inted 10/2	17/2023
Proposed Prepared by HydroCAD® 1 Runoff = Runoff by SC Type III 24-h <u>Area</u> * 3,	-7 √ {enter yc 0.00-26 s/r CS TR-20 r r 2-Year F (sf) CN 113 98	Dur company n 04015 © 202 3 cfs @ 12.0 method, UH=3 Rainfall=3.05" Descriptior Paved parl	y name here 20 HydroCAD <b>Summary</b> 09 hrs, Volu SCS, Weigh n king	e} <u>9 Software S</u> <b>/ for Sub</b> e me= ted-CN, Tin	olutions LLC catchmen 0.018 af, ne Span= 0.	r <b>s)</b> t <b>P-1b: Fl</b> a Depth= 2.6	ow to Tre	eatment	Туре		r 2-Yea	inted 10/2	17/2023
Proposed- Prepared by HydroCAD® f Runoff by SC Type III 24-h Area * 3, <sup>2</sup> 2 3,6	7 / {enter yc 0.00-26 s// CS TR-20 r r 2-Year F (sf) CN 113 98 158 79 771 96 158	our company n 04015 © 202 3 cfs @ 12.0 nethod, UH=: Rainfall=3.05" Descriptior Paved parl 50-75% Gf Weighted / 12.83% Pe	y name here 20 HydroCAD Summary 09 hrs, Volu SCS, Weigh n king rass cover, F Average ervious Area	€} <u>Software S</u> <b>/ for Sub</b> / me= ted-CN, Tin	olutions LLC catchmen 0.018 af, ne Span= 0.	r <b>s)</b> t <b>P-1b: Fl</b> a Depth= 2.6	ow to Tre	eatment	Туре		r 2-Yea	inted 10/2	17/2023
Proposed Prepared by HydroCAD® 1 Runoff = Runoff by SC Type III 24-h Area * 3, 5 3, 5	7 / {enter yc 0.00-26 s/r CS TR-20 r r 2-Year F (sf) CN (sf) CN 1/3 98 1/3 98 1/3 96 1/3	Dur company n 04015 © 202 3 cfs @ 12.0 nethod, UH=: ainfall=3.05" Description Paved part 50-75% Gr Weighted / 12.83% Pe 87.17% Im	y name here 20 HydroCAD <b>Summary</b> 09 hrs, Volu SCS, Weigh n king rass cover, F Average ervious Area opervious Area	e} <u>9 Software S</u> <b>y for Sub</b> e me= ted-CN, Tin Fair, HSG C ea	Olutions LLC catchmen 0.018 af, ne Span= 0.	r <b>s)</b> t <b>P-1b: Fl</b> a Depth= 2.6	ow to Tre	eatment	Туре		r 2-Yea	inted 10/2	17/2023
Proposed Prepared by HydroCAD® 1 Runoff by SC Type III 24-h <u>Area</u> * 3, 2 3, 7 3, 7	7 / (enter yc 0.00-26 s/r CS TR-20 r r 2-Year F (sf) CN 13 98 158 79 571 96 158 13 ngth Slo	our company n 04015 © 202 3 cfs @ 12.0 nethod, UH=: Rainfall=3.05" Descriptior Paved parl 50-75% Gf Weighted / 12.83% Pe	y name here 20 HydroCAD Summary 09 hrs, Volu SCS, Weigh h king rass cover, F Average ervious Area pervious Area pervious Area	€} <u>Software S</u> <b>/ for Sub</b> / me= ted-CN, Tin	Olutions LLC catchmen 0.018 af, ne Span= 0.	r <b>s)</b> t <b>P-1b: Fl</b> a Depth= 2.6	ow to Tre	eatment	Туре		r 2-Yea	inted 10/2	17/2023

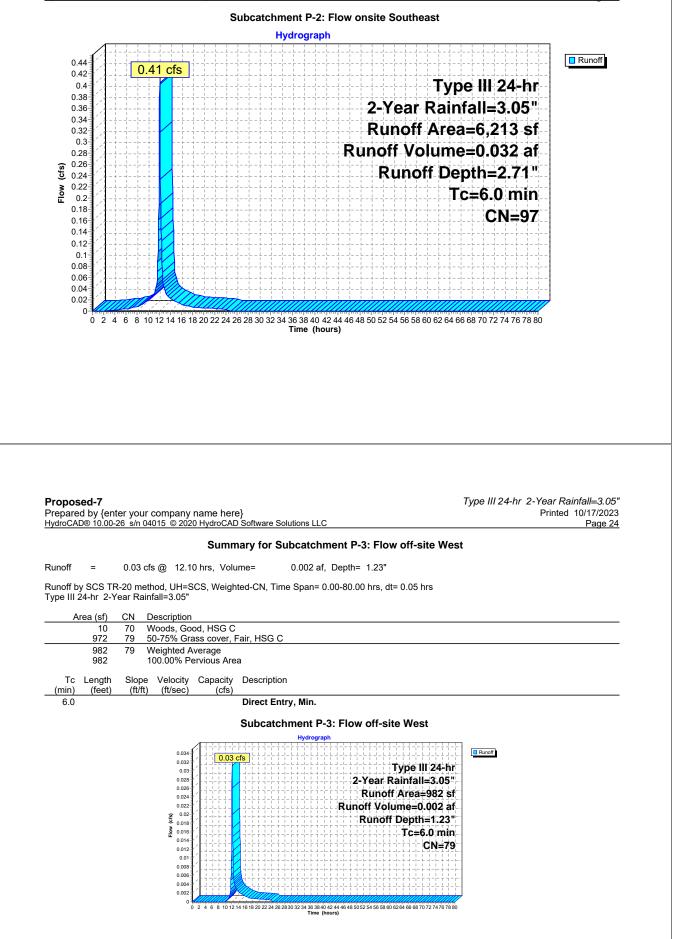










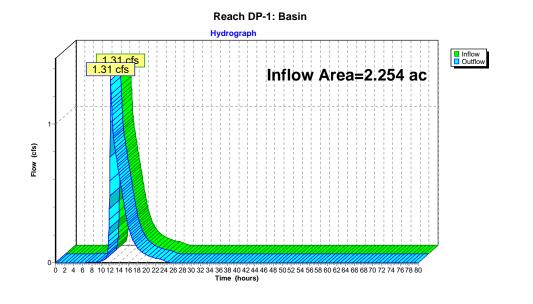


#### Summary for Reach DP-1: Basin

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =	2.254 ac, 75.63% Impervious, Inflow Depth = 1.56" for 2-Year event
Inflow =	1.31 cfs @ 12.16 hrs, Volume= 0.292 af
Outflow =	1.31 cfs @ 12.16 hrs, Volume= 0.292 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs



Proposed-7

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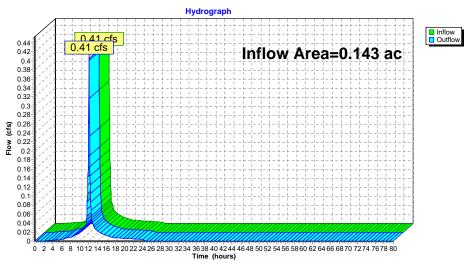
#### Summary for Reach DP-2: Onsite southeast

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area	a =	0.143 ac, 93.87% Impervious, Inflow Depth = 2.71	for 2-Year event
Inflow	=	0.41 cfs @ 12.09 hrs, Volume= 0.032 af	
Outflow	=	0.41 cfs @ 12.09 hrs, Volume= 0.032 af, A	Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs



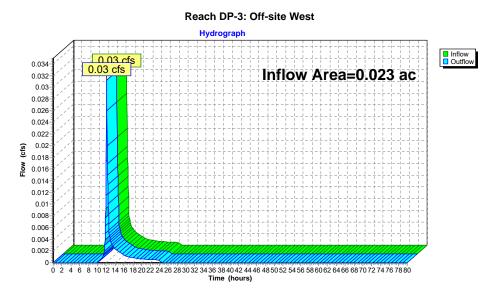


#### Summary for Reach DP-3: Off-site West

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =	0.023 ac,	0.00% Impervious, Inflo	w Depth = 1.23"	for 2-Year event
Inflow =	0.03 cfs @	12.10 hrs, Volume=	0.002 af	
Outflow =	0.03 cfs @	12.10 hrs, Volume=	0.002 af, Atte	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs



Proposed-7

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#### Summary for Pond S-1: Rip Rap Swale

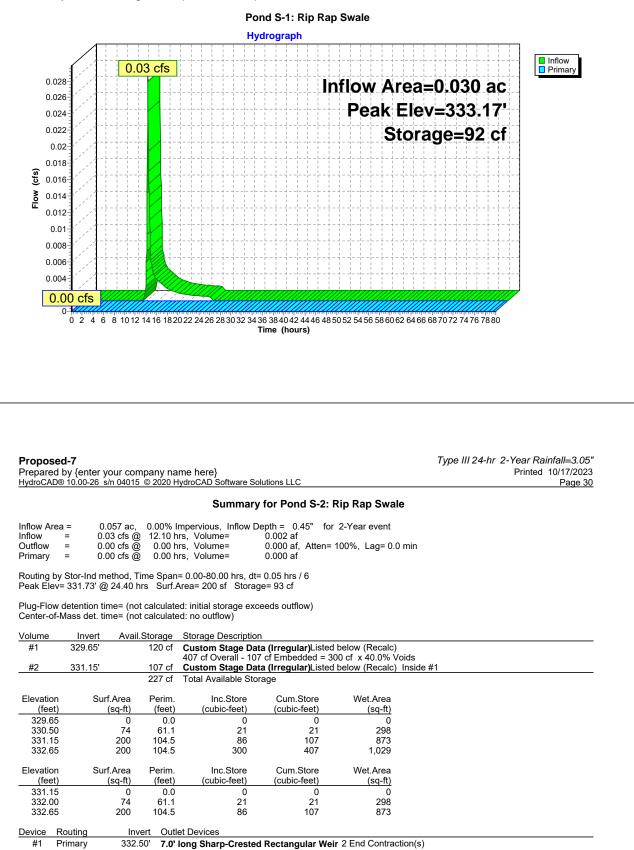
Inflow Area =	0.030 ac,	0.00% Impervious, Inflow D	epth = 0.84" for 2-Year event
Inflow =	0.03 cfs @	12.10 hrs, Volume=	0.002 af
Outflow =	0.00 cfs @	0.00 hrs, Volume=	0.000 af, Atten= 100%, Lag= 0.0 min
Primary =	0.00 cfs @	0.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs / 6 Peak Elev= 333.17' @ 24.40 hrs Surf.Area= 200 sf Storage= 92 cf

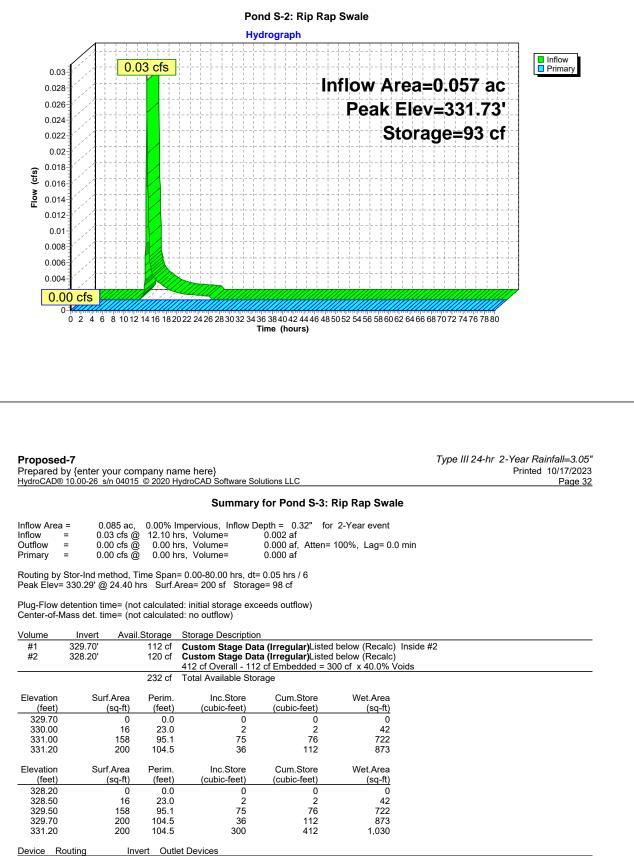
Plug-Flow detention time= (not calculated: initial storage exceeds outflow) Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.S	torage	Storage Description	ı		
#1	331.15'		120 cf	Custom Stage Dat			
#0	222.651		111 -	414 cf Overall - 114			
#2	332.65'		114 cf	Custom Stage Dat	a (irregular)Listed	below (Recalc)	Inside #1
			234 cf	Total Available Stor	age		
Elevation	Surf	.Area	Perim.	Inc.Store	Cum.Store	Wet.Area	
(feet)	(	sq-ft)	(feet)	(cubic-feet)	(cubic-feet)	(sq-ft)	
331.15		0	0.0	0	0	0	
331.50		21	27.2	2	2	59	
332.50		171	99.3	84	86	788	
332.65		200	104.4	28	114	872	
334.15		200	104.4	300	414	1,028	
Elevation	Surf	.Area	Perim.	Inc.Store	Cum.Store	Wet.Area	
(feet)		sq-ft)	(feet)	(cubic-feet)	(cubic-feet)	(sq-ft)	
332.65		0	0.0	0	0	0	
333.00		21	27.2	2	2	59	
334.00		171	99.3	84	86	788	
334.15		200	104.4	28	114	872	
Device Routing Invert Outlet Devices							
#1 Primary 334.05' 7.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)							

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=331.15' (Free Discharge) 1=Sharp-Crested Rectangular Weir ( Controls 0.00 cfs)



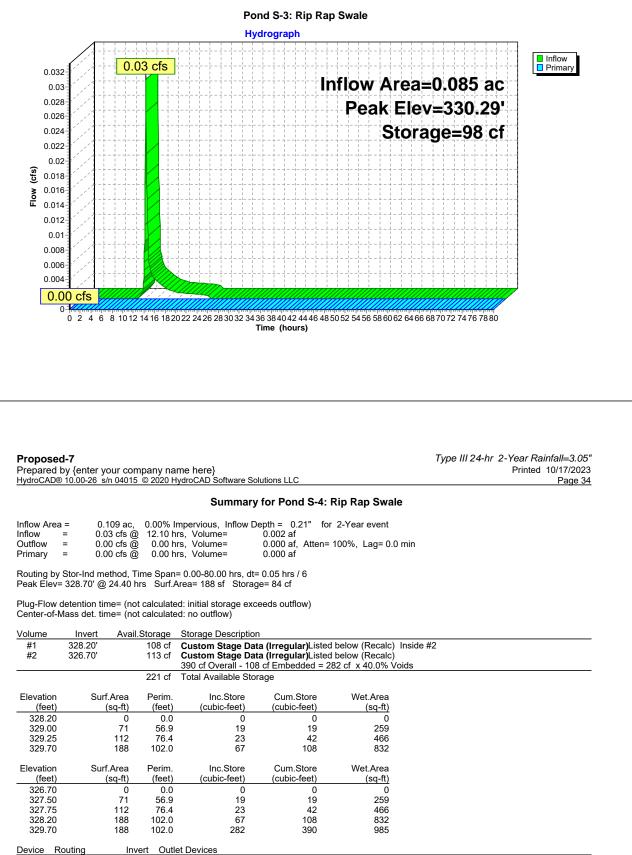
Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=329.65' (Free Discharge) 1=Sharp-Crested Rectangular Weir ( Controls 0.00 cfs)



#1 Primary

<sup>331.00&#</sup>x27; 7.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

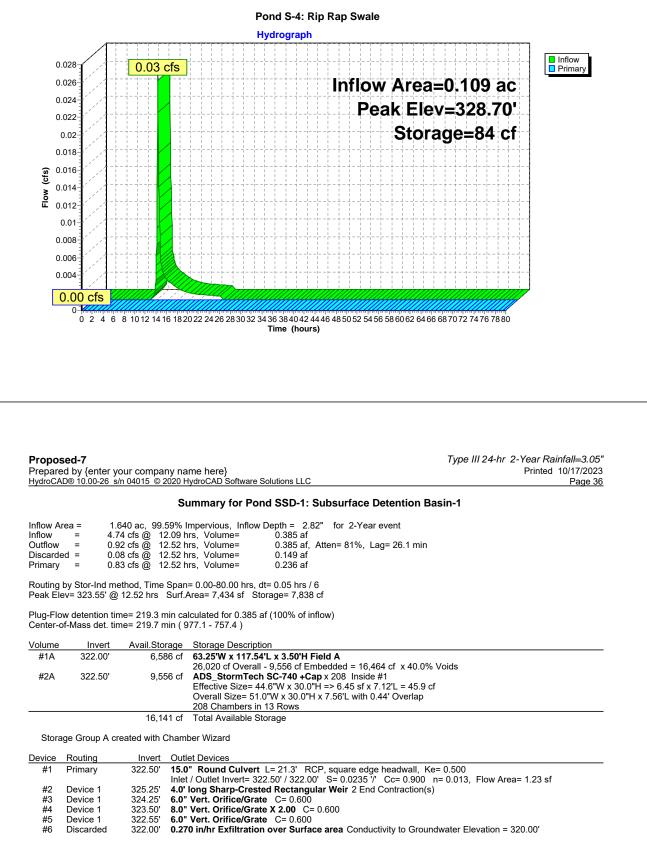
Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=328.20' (Free Discharge) 1=Sharp-Crested Rectangular Weir ( Controls 0.00 cfs)



#1 Primary

<sup>329.25&#</sup>x27; 7.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=326.70' (Free Discharge) 1=Sharp-Crested Rectangular Weir ( Controls 0.00 cfs)



Discarded OutFlow Max=0.08 cfs @ 12.52 hrs HW=323.55' (Free Discharge) 6=Exfiltration (Controls 0.08 cfs)

Primary OutFlow Max=0.83 cfs @ 12.52 hrs HW=323.55' (Free Discharge)

-1=Culvert (Passes 0.83 cfs of 3.82 cfs potential flow)
 -2=Sharp-Crested Rectangular Weir (Controls 0.00 cfs)
 -3=Orifice/Grate (Controls 0.00 cfs)
 -4=Orifice/Grate (Orifice Controls 0.02 cfs @ 0.73 fps)

-5=Orifice/Grate (Orifice Controls 0.82 cfs @ 4.16 fps)

#### Proposed-7

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Type III 24-hr 2-Year Rainfall=3.05" Printed 10/17/2023 Page 38

#### Pond SSD-1: Subsurface Detention Basin-1 - Chamber Wizard Field A

Chamber Model = ADS\_StormTech SC-740 +Cap (ADS StormTech® SC-740 with cap length) Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap

51.0" Wide + 6.0" Spacing = 57.0" C-C Row Spacing

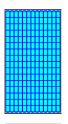
16 Chambers/Row x 7.12' Long +0.81' Cap Length x 2 = 115.54' Row Length +12.0" End Stone x 2 = 117.54' Base Length 13 Rows x 51.0" Wide + 6.0" Spacing x 12 + 12.0" Side Stone x 2 = 63.25' Base Width 6.0" Base + 30.0" Chamber Height + 6.0" Cover = 3.50' Field Height

208 Chambers x 45.9 cf = 9,555.5 cf Chamber Storage

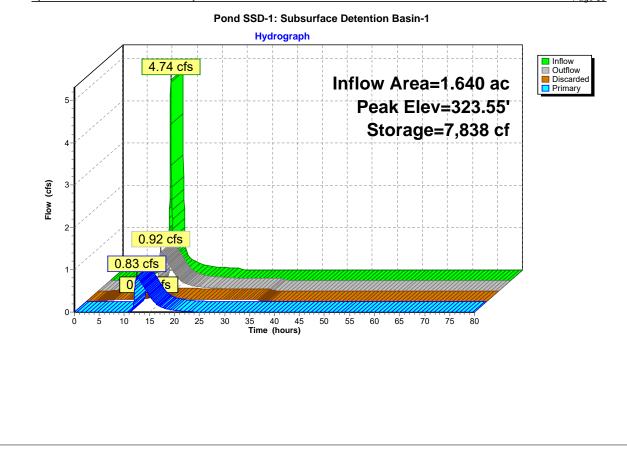
26,019.7 cf Field - 9,555.5 cf Chambers = 16,464.2 cf Stone x 40.0% Voids = 6,585.7 cf Stone Storage

Chamber Storage + Stone Storage = 16,141.2 cf = 0.371 af Overall Storage Efficiency = 62.0% Overall System Size = 117.54' x 63.25' x 3.50'

208 Chambers 963.7 cy Field 609.8 cy Stone



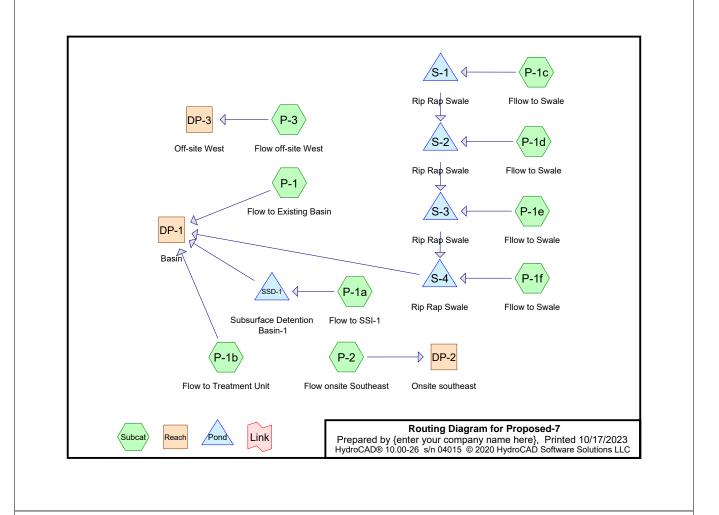
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### HydroCAD Analysis

## **Proposed Conditions - 10 Year Storm**



### Proposed-7

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### Area Listing (all nodes)

Area	CN	Description
(acres)		(subcatchment-numbers)
0.426	79	50-75% Grass cover, Fair, HSG C (P-1, P-1a, P-1b, P-1c, P-1d, P-1e, P-1f, P-2, P-3)
1.838	98	Paved parking (P-1a, P-1b, P-2)
0.032	66	Rip Rap Swale (P-1c, P-1d, P-1e, P-1f)
0.123	70	Woods, Good, HSG C (P-1, P-1c, P-1d, P-1e, P-1f, P-3)
2.419	93	TOTAL AREA

#### Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
0.000	HSG B	
0.549	HSG C	P-1, P-1a, P-1b, P-1c, P-1d, P-1e, P-1f, P-2, P-3
0.000	HSG D	
1.870	Other	P-1a, P-1b, P-1c, P-1d, P-1e, P-1f, P-2
2.419		TOTAL AREA

#### Proposed-7

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#### HSG-A HSG-B HSG-C HSG-D Other Total Ground Subcatchment (acres) (acres) (acres) (acres) (acres) (acres) Cover Numbers 0.000 0.000 0.426 0.000 0.426 50-75% Grass cover, Fair P-1, P-1a, P-1b, P-1c, P-1d, P-1e, P-1f, P-2, P-3 0.000 0.000 0.000 0.000 0.000 1.838 1.838 Paved parking P-1a, P-1b, P-2 0.000 0.000 0.000 0.032 0.032 P-1c, P-1d, P-1e, P-1f 0.000 Rip Rap Swale 0.000 0.000 0.123 0.000 0.000 0.123 Woods, Good P-1, P-1c, P-1d, P-1e, P-1f, P-3 0.000 0.000 0.549 0.000 1.870 2.419 TOTAL AREA

Ground Covers (all nodes)

	® 10.00-20	s/n 04015	© 2020 Hydro	CAD Softv	vare Solut	ions LLC				Page
HydroCAD® 10:00-26 s/n 04015 © 2020 HydroCAD Software Solutions LLC P Pipe Listing (all nodes)										
Line#	Node Number	In-Invert (feet)	Out-Invert (feet)	Length (feet)	Slope (ft/ft)	n	Diam/Width (inches)	Height (inches)	Inside-Fill (inches)	
1	SSD-1	322.50	322.00	21.3	0.0235	0.013	15.0	0.0	0.0	
	d by {enter		ipany name © 2020 Hydro		vare Solut	ions LLC			Type III 24-	<i>hr 10-Year Rainfall</i> =5.15 Printed 10/17/202 Page (
-				Time sp Runoff by	an=0.00- SCS TR	80.00 hr -20 met	rs, dt=0.05 hr hod, UH=SCS	, Weighte		
Subcatch	nment P-1:	Flow to Ex	xisting Basir	ı			Flo			pervious Runoff Depth=2.75 =77 Runoff=1.18 cfs 0.097 a
Subcatch	nment P-1a	: Flow to S	SSI-1				I	Runoff Area		pervious Runoff Depth=4.91 =98 Runoff=8.07 cfs 0.671 a

Runoff Area=3,571 sf 87.17% Impervious Runoff Depth=4.68" Tc=6.0 min CN=96 Runoff=0.40 cfs 0.032 af

Runoff Area=1,317 sf 0.00% Impervious Runoff Depth=2.31" Tc=6.0 min CN=72 Runoff=0.08 cfs 0.006 af

Runoff Area=1,184 sf 0.00% Impervious Runoff Depth=2.48" Tc=6.0 min CN=74 Runoff=0.08 cfs 0.006 af

Runoff Area=1,184 sf 0.00% Impervious Runoff Depth=2.57" Tc=6.0 min CN=75 Runoff=0.08 cfs 0.006 af

Runoff Area=1,071 sf 0.00% Impervious Runoff Depth=2.48" Tc=6.0 min CN=74 Runoff=0.07 cfs 0.005 af

Runoff Area=6,213 sf 93.87% Impervious Runoff Depth=4.80" Tc=6.0 min CN=97 Runoff=0.70 cfs 0.057 af

Runoff Area=982 sf 0.00% Impervious Runoff Depth=2.93" Tc=6.0 min CN=79 Runoff=0.08 cfs 0.006 af

Inflow=4.15 cfs 0.636 af Outflow=4.15 cfs 0.636 af

Inflow=0.70 cfs 0.057 af Outflow=0.70 cfs 0.057 af

Subcatchment P-3: Flow off-site West

Reach DP-1: Basin

Reach DP-2: Onsite southeast

Subcatchment P-1c: Fllow to Swale

Subcatchment P-1d: Fllow to Swale

Subcatchment P-1e: Fllow to Swale

Subcatchment P-1f: Fllow to Swale

Subcatchment P-2: Flow onsite Southeast

Reach DP-3: Off-site West

Pond S-1: Rip Rap Swale

Pond S-2: Rip Rap Swale

Pond S-3: Rip Rap Swale

Pond S-4: Rip Rap Swale

Pond SSD-1: Subsurface Detention Basin-1

Inflow=0.08 cfs 0.006 af Outflow=0.08 cfs 0.006 af

Peak Elev=334.05' Storage=215 cf Inflow=0.08 cfs 0.006 af Outflow=0.00 cfs 0.001 af

Peak Elev=332.50' Storage=198 cf Inflow=0.08 cfs 0.007 af Outflow=0.00 cfs 0.002 af

Peak Elev=331.00' Storage=195 cf Inflow=0.08 cfs 0.008 af Outflow=0.01 cfs 0.003 af

Peak Elev=329.25' Storage=148 cf Inflow=0.07 cfs 0.008 af Outflow=0.01 cfs 0.005 af

Peak Elev=324.17' Storage=11,223 cf Inflow=8.07 cfs 0.671 af Discarded=0.10 cfs 0.169 af Primary=3.05 cfs 0.502 af Outflow=3.15 cfs 0.671 af

Total Runoff Area = 2.419 ac Runoff Volume = 0.885 af Average Runoff Depth = 4.39" 24.00% Pervious = 0.581 ac 76.00% Impervious = 1.838 ac

# Proposed-7

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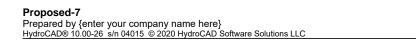
# Summary for Subcatchment P-1: Flow to Existing Basin

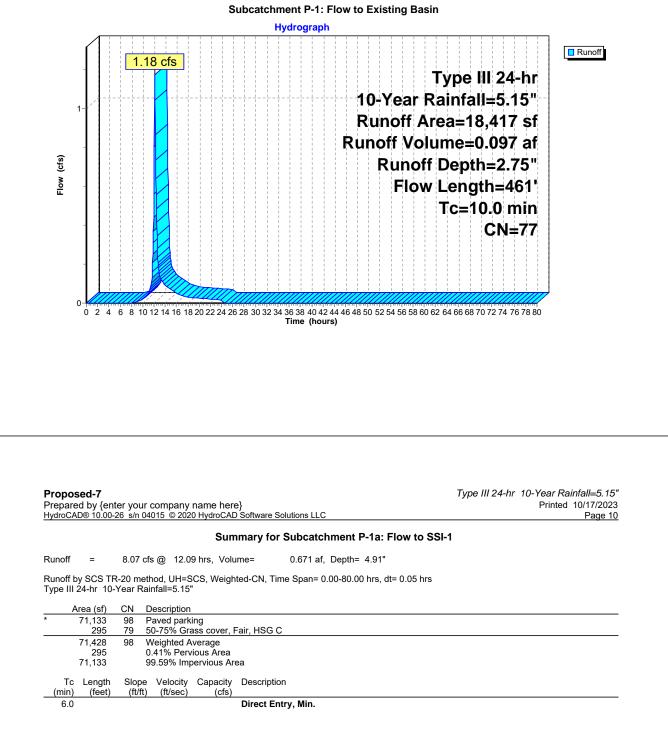
Runoff = 1.18 cfs @ 12.15 hrs, Volume= 0.097 af, Depth= 2.75"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs Type III 24-hr  $\,$  10-Year Rainfall=5.15"

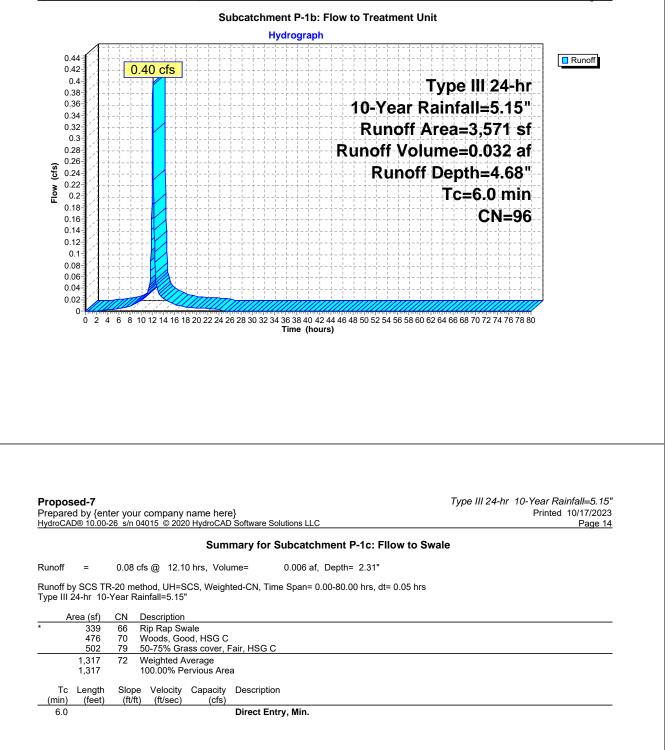
_	A	rea (sf)	CN	Description	l							
		4,454	70	Woods, Go	Voods, Good, HSG C							
_		13,963	79	50-75% Gr	ass cover, F	Fair, HSG C						
		18,417	77	Weighted A	/eighted Average							
		18,417		100.00% P	ervious Are	a						
	Tc (min)	Length (feet)	Slope (ft/ft		Capacity (cfs)	Description						
	7.3	50	0.080	0.11		Sheet Flow, Sheet Flow						
	2.7	411	0.024	) 2.49		Woods: Light underbrush n= 0.400 P2= 3.05" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps						
-	10.0	461	Total									

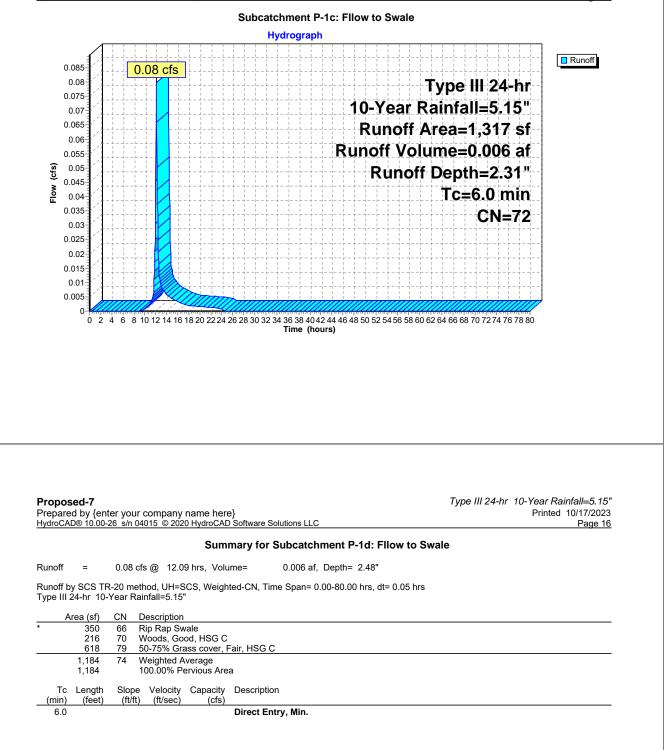
10.0 461 Total

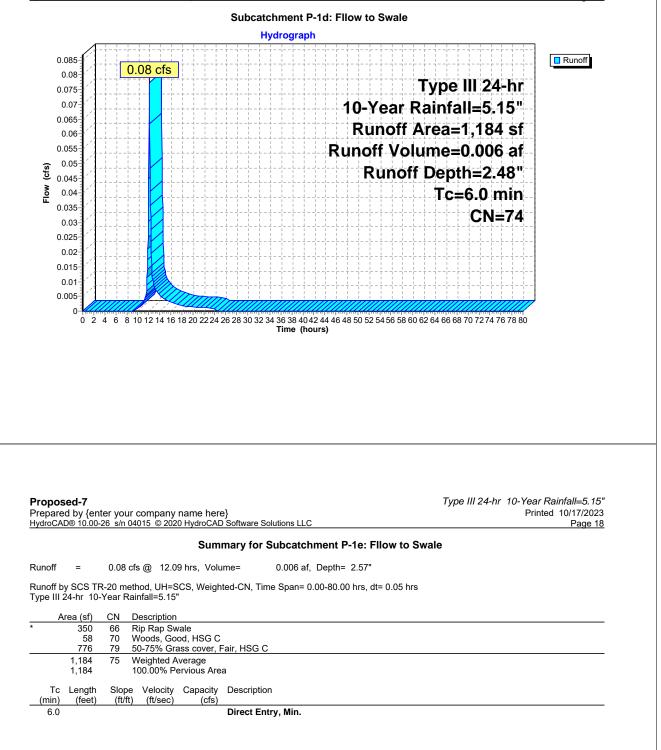


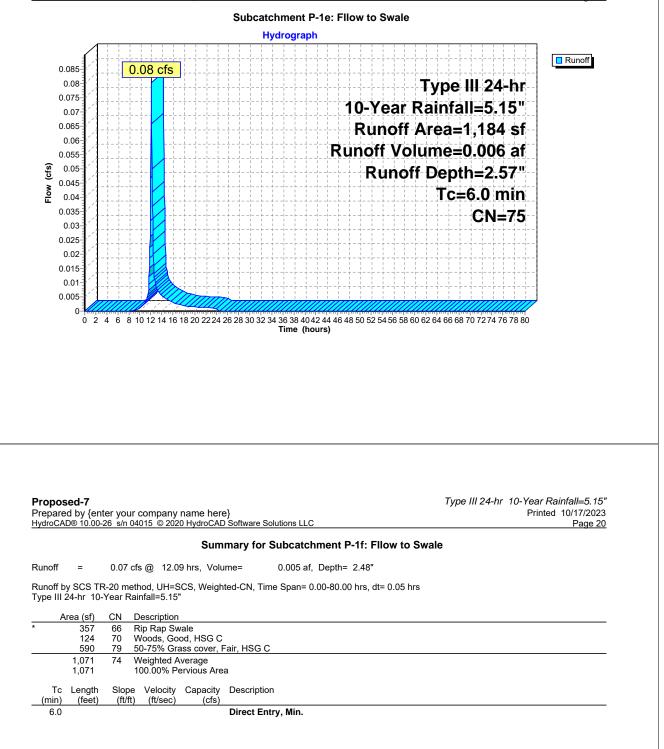


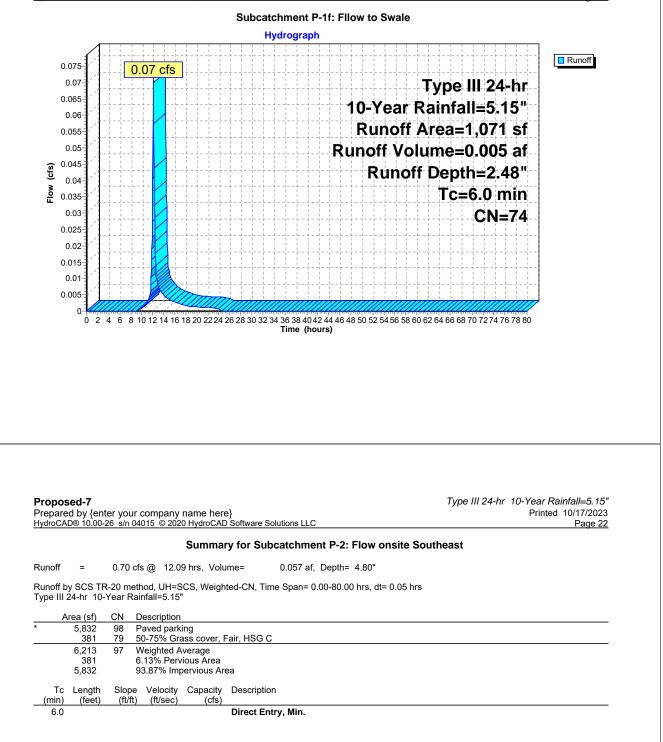
			ubcatchm Hydrog		FIOW to	551-1						
9-	8.07 cfs										Runoff	
8								e III				
7-	10-Year Rainfall=5.15"											
6-	Runoff Area=71,											
	·			R	lunof							
Elow (cfs)						unot			h=4.91"			
<b>앞</b> 4-							10	c=6.	i i	i i l		
3								C	N=	90		
2-	-+								+-	      - 		
1-										11		
		Time										
roposed-7 epared by {enter y							Т	ype III 2	24-hr		ar Rainfall=5. nted 10/17/20	023
epared by {enter y	n 04015 © 2020	HydroCAD Softw			h- Elour (				24-hr			023
epared by {enter y droCAD® 10.00-26 s	<u>'n 04015 © 2020  </u> S	HydroCAD Softw	Subcatch	ment P-1		o Treat			24-hr		nted 10/17/2	023
epared by {enter y droCAD® 10.00-26 s noff = 0.4	n 04015 © 2020 S S 0 cfs @ 12.09 method, UH=SC	HydroCAD Softw Summary for hrs, Volume=	Subcatch	<b>iment P-1</b> 32 af, Depth	n= 4.68"		tment L		24-hr		nted 10/17/2	023
epared by {enter y droCAD® 10.00-26 s inoff = 0.4 inoff by SCS TR-20 pe III 24-hr 10-Yeau <u>Area (sf) CN</u>	<u>'n 04015 © 2020</u> <b>S</b> 0 cfs @ 12.09 method, UH=SC Rainfall=5.15" Description	HydroCAD Softw Summary for hrs, Volume= CS, Weighted-C	Subcatch	<b>iment P-1</b> 32 af, Depth	n= 4.68"		tment L		24-hr		nted 10/17/2	023
epared by {enter y droCAD® 10.00-26 s inoff = 0.4 inoff by SCS TR-20 pe III 24-hr 10-Yeau <u>Area (sf) CN</u> 3,113 98 458 79	n 04015 © 2020 S 0 cfs @ 12.09 method, UH=SC Rainfall=5.15" Description Paved parkin 50-75% Gras	HydroCAD Softw Summary for hrs, Volume= CS, Weighted-C	Subcatch 0.03 N, Time Spa	<b>iment P-1</b> 32 af, Depth	n= 4.68"		tment L		24-hr		nted 10/17/2	023
epared by {enter y droCAD® 10.00-26 s noff = 0.4 inoff by SCS TR-20 pe III 24-hr 10-Yeau <u>Area (sf) CN</u> 3,113 98	n 04015 © 2020 S 0 cfs @ 12.09 method, UH=SC Rainfall=5.15" Description Paved parkin 50-75% Gras	HydroCAD Softw Summary for hrs, Volume= CS, Weighted-C CS S cover, Fair, H erage ious Area	Subcatch 0.03 N, Time Spa	<b>iment P-1</b> 32 af, Depth	n= 4.68"		tment L				nted 10/17/2	023
spared by {enter y           troCAD® 10.00-26 s           noff         =         0.4           noff by SCS TR-20           be III 24-hr         10-Year           Area (sf)         CN           3,113         98           458         79           3,571         96           458         3,113           Tc         Length	n 04015 © 2020 S 0 cfs @ 12.09 method, UH=SC Rainfall=5.15" Description Paved parkin 50-75% Gras Weighted Ave 12.83% Pervi	HydroCAD Softw Summary for hrs, Volume= CS, Weighted-C S cover, Fair, H erage ious Area ervious Area Capacity Des- (cfs)	Subcatch 0.03 N, Time Spa ISG C	ament P-1 32 af, Deptł an= 0.00-80	n= 4.68"		tment L		24-hr		nted 10/17/2	023

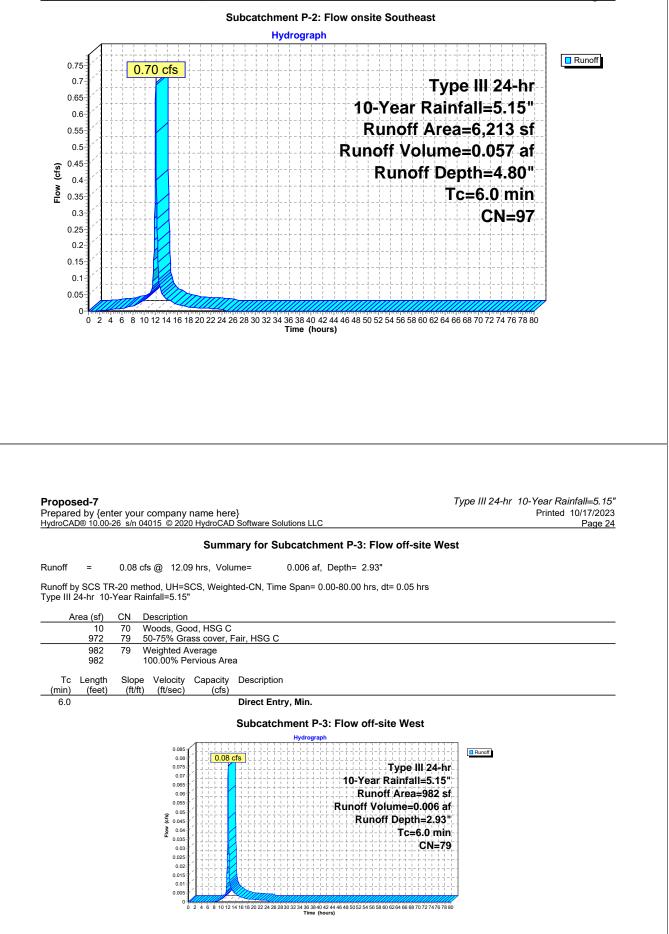










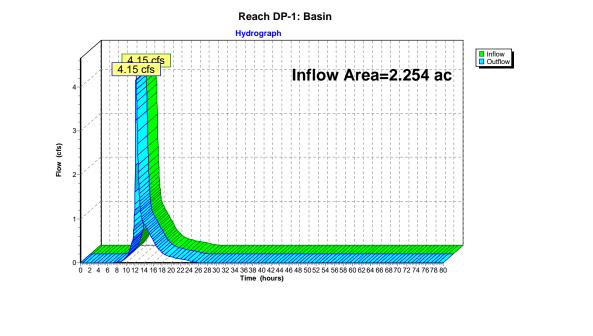


### Summary for Reach DP-1: Basin

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =	2.254 ac, 75.63% Impervious, Inflow Depth = 3.39" for 10-Year event	
Inflow =	4.15 cfs @ 12.21 hrs, Volume= 0.636 af	
Outflow =	4.15 cfs @ 12.21 hrs, Volume= 0.636 af, Atten= 0%, Lag= 0.0 min	

Routing by Stor-Ind+Trans method, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs



Proposed-7

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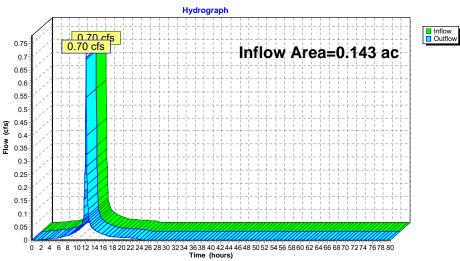
# Summary for Reach DP-2: Onsite southeast

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area	a =	0.143 ac, 9	3.87% Impervious,	Inflow Depth =	4.80"	for 10-Year event
Inflow	=	0.70 cfs @	12.09 hrs, Volume	= 0.057	af	
Outflow	=	0.70 cfs @	12.09 hrs, Volume	= 0.057	af, Atte	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs



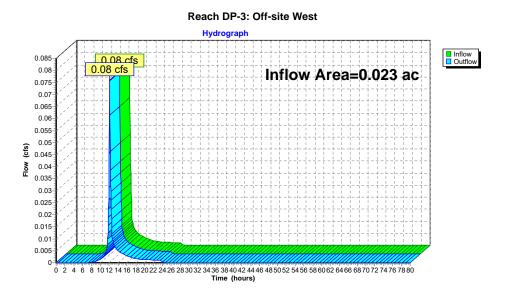


# Summary for Reach DP-3: Off-site West

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area :	=	0.023 ac,	0.00% Impervious, Inflo	ow Depth = 2.93"	for 10-Year event
Inflow =	=	0.08 cfs @	12.09 hrs, Volume=	0.006 af	
Outflow =	=	0.08 cfs @	12.09 hrs, Volume=	0.006 af, Atte	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs



Proposed-7

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# Summary for Pond S-1: Rip Rap Swale

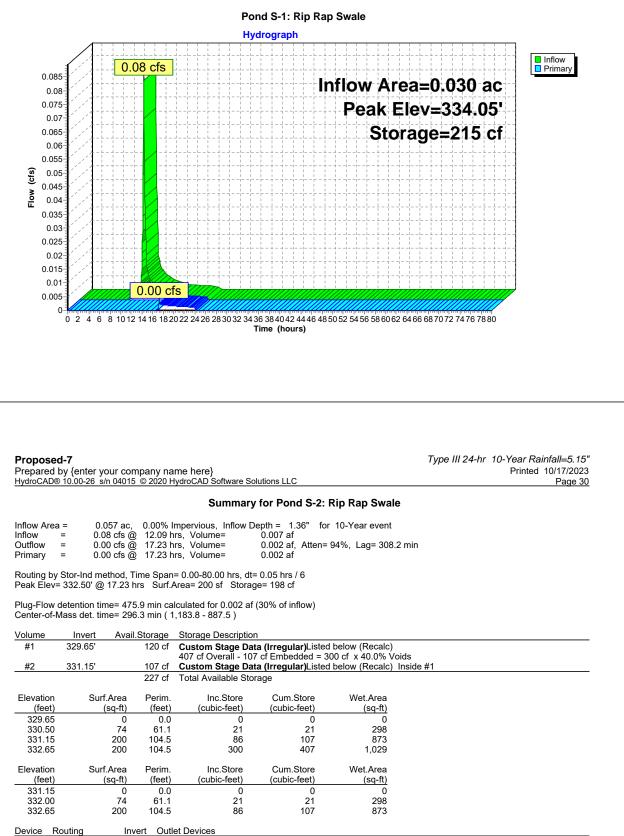
Inflow Area = 0.0	.030 ac, 0.00% Impervious, Inflow	Depth = 2.31" for 10-Year event
Inflow = 0.0	08 cfs @ 12.10 hrs, Volume=	0.006 af
Outflow = 0.0	00 cfs @ 17.20 hrs, Volume=	0.001 af, Atten= 97%, Lag= 306.3 min
Primary = 0.0	00 cfs @ 17.20 hrs, Volume=	0.001 af

Routing by Stor-Ind method, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs / 6 Peak Elev= 334.05' @ 17.20 hrs Surf.Area= 200 sf Storage= 215 cf

Plug-Flow detention time= 517.4 min calculated for 0.001 af (15% of inflow) Center-of-Mass det. time= 369.3 min ( 1,210.3 - 841.0 )

Volume	Invert	Avail.Storag	je	Storage Description								
#1	331.15'	120		Custom Stage Dat								
				414 cf Overall - 114								
#2	332.65'	114	cf	Custom Stage Data (Irregular)Listed below (Recalc) Inside #1								
		234	cf	Total Available Stor	age							
Elevation	Surf	Area Peri	m.	Inc.Store	Cum.Store	Wet.Area						
(feet)	(	(sq-ft) (fee	et)	(cubic-feet)	(cubic-feet)	(sq-ft)						
331.15		0 0	0.0	0	0	0						
331.50		21 27.2		2	2	59						
332.50		171 99	9.3	84	86	788						
332.65		200 104.4		28	114	872						
334.15		200 104	.4	300	414	1,028						
Elevation	Surf	Area Peri	m.	Inc.Store	Cum.Store	Wet.Area						
(feet)	(	(sq-ft) (fee	et)	(cubic-feet)	(cubic-feet)	(sq-ft)						
332.65		0 0	0.0	0	0	0						
333.00		21 27	.2	2	2	59						
334.00		171 99	9.3	84	86	788						
334.15		200 104	.4	28	114	872						
Device Ro	outing	Invert O	outle	t Devices								
#1 Pr	imary	334.05' <b>7</b>	.0' le	ong Sharp-Crested	Rectangular Wei	r 2 End Contrac	ction(s)					

Primary OutFlow Max=0.00 cfs @ 17.20 hrs HW=334.05' (Free Discharge) 1=Sharp-Crested Rectangular Weir (Weir Controls 0.00 cfs @ 0.11 fps)



#1 Primary

332.50' 7.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Device Routing

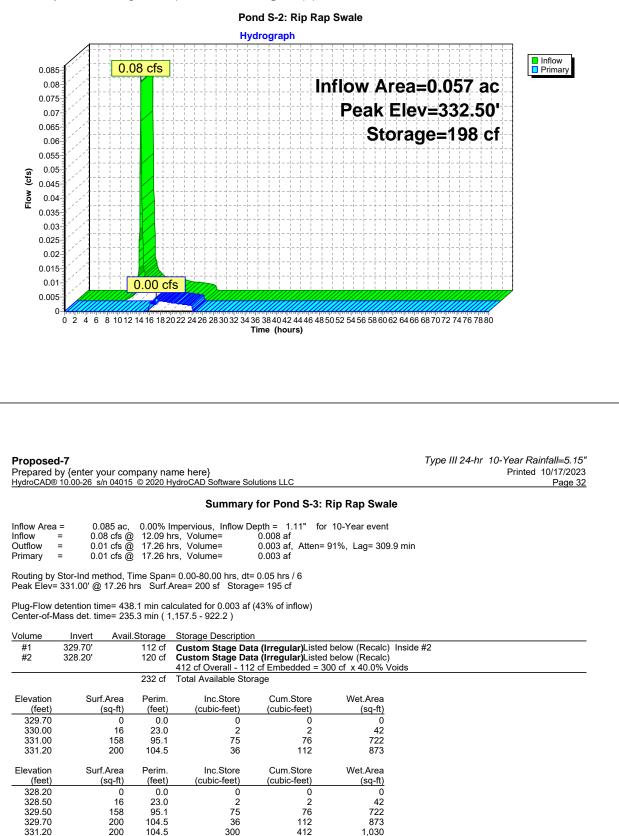
#1 Primary

Invert

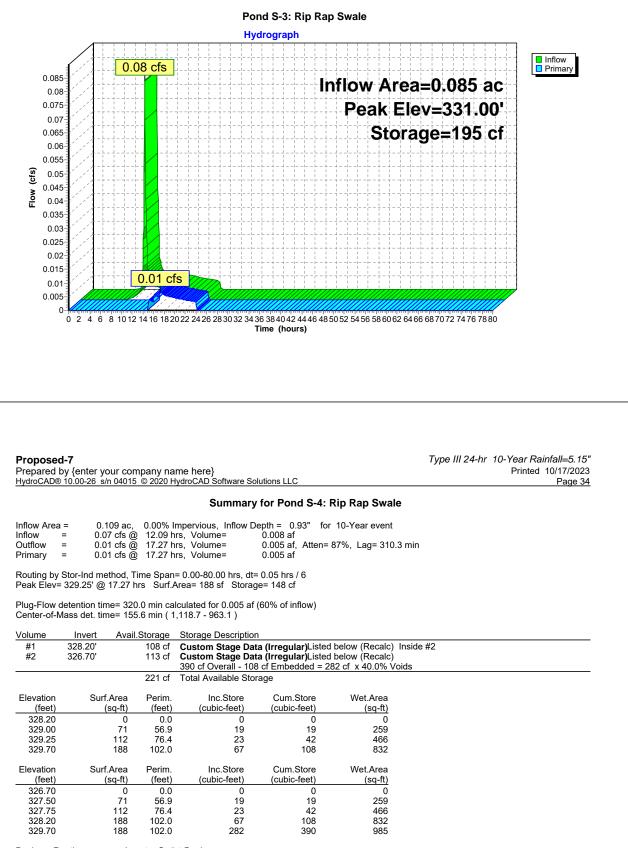
Outlet Devices

331.00' 7.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=0.00 cfs @ 17.23 hrs HW=332.50' (Free Discharge) 1=Sharp-Crested Rectangular Weir (Weir Controls 0.00 cfs @ 0.11 fps)



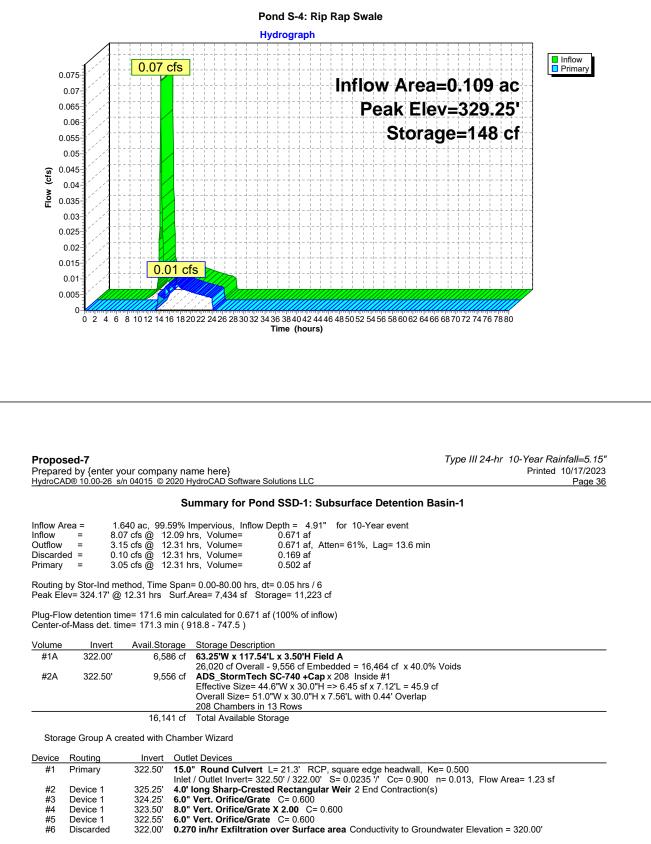
Primary OutFlow Max=0.00 cfs @ 17.26 hrs HW=331.00' (Free Discharge) 1=Sharp-Crested Rectangular Weir (Weir Controls 0.00 cfs @ 0.15 fps)



Device Routing #1 Primary

Invert Outlet Devices 329.25' 7.0' Iong Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=0.00 cfs @ 17.27 hrs HW=329.25' (Free Discharge) 1=Sharp-Crested Rectangular Weir (Weir Controls 0.00 cfs @ 0.15 fps)



Discarded OutFlow Max=0.10 cfs @ 12.31 hrs HW=324.17' (Free Discharge) 6=Exfiltration (Controls 0.10 cfs)

Primary OutFlow Max=3.05 cfs @ 12.31 hrs HW=324.17' (Free Discharge)

-1=Culvert (Passes 3.05 cfs of 6.03 cfs potential flow)
 -2=Sharp-Crested Rectangular Weir ( Controls 0.00 cfs)
 -3=Orifice/Grate ( Controls 0.00 cfs)
 -4=Orifice/Grate (Orifice Controls 1.94 cfs @ 2.78 fps)

- -5=Orifice/Grate (Orifice Controls 1.11 cfs @ 5.63 fps)

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Type III 24-hr 10-Year Rainfall=5.15" Printed 10/17/2023 Page 38

#### Pond SSD-1: Subsurface Detention Basin-1 - Chamber Wizard Field A

Chamber Model = ADS\_StormTech SC-740 +Cap (ADS StormTech® SC-740 with cap length) Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap

51.0" Wide + 6.0" Spacing = 57.0" C-C Row Spacing

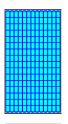
16 Chambers/Row x 7.12' Long +0.81' Cap Length x 2 = 115.54' Row Length +12.0" End Stone x 2 = 117.54' Base Length 13 Rows x 51.0" Wide + 6.0" Spacing x 12 + 12.0" Side Stone x 2 = 63.25' Base Width 6.0" Base + 30.0" Chamber Height + 6.0" Cover = 3.50' Field Height

208 Chambers x 45.9 cf = 9,555.5 cf Chamber Storage

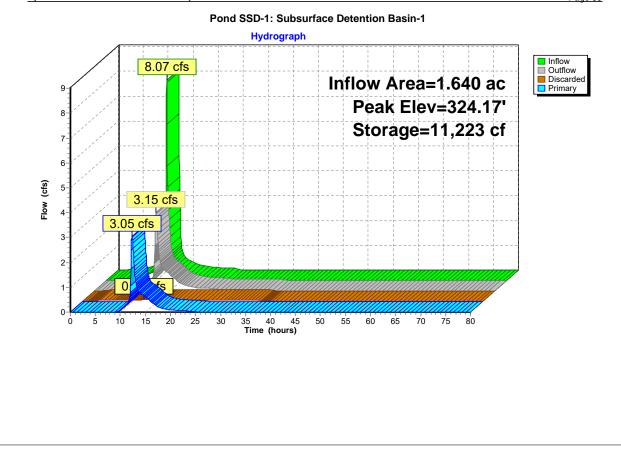
26,019.7 cf Field - 9,555.5 cf Chambers = 16,464.2 cf Stone x 40.0% Voids = 6,585.7 cf Stone Storage

Chamber Storage + Stone Storage = 16,141.2 cf = 0.371 af Overall Storage Efficiency = 62.0% Overall System Size = 117.54' x 63.25' x 3.50'

208 Chambers 963.7 cy Field 609.8 cy Stone



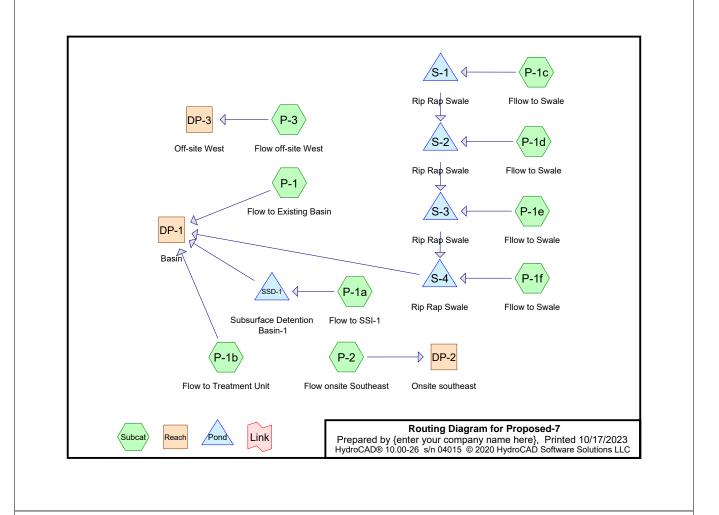
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# HydroCAD Analysis

# **Proposed Conditions - 25 Year Storm**



# Proposed-7

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# Area Listing (all nodes)

Area	CN	Description
(acres)		(subcatchment-numbers)
0.426	79	50-75% Grass cover, Fair, HSG C (P-1, P-1a, P-1b, P-1c, P-1d, P-1e, P-1f, P-2, P-3)
1.838	98	Paved parking (P-1a, P-1b, P-2)
0.032	66	Rip Rap Swale (P-1c, P-1d, P-1e, P-1f)
0.123	70	Woods, Good, HSG C (P-1, P-1c, P-1d, P-1e, P-1f, P-3)
2.419	93	TOTAL AREA

# Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
0.000	HSG B	
0.549	HSG C	P-1, P-1a, P-1b, P-1c, P-1d, P-1e, P-1f, P-2, P-3
0.000	HSG D	
1.870	Other	P-1a, P-1b, P-1c, P-1d, P-1e, P-1f, P-2
2.419		TOTAL AREA

# Proposed-7

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#### HSG-A HSG-B HSG-C HSG-D Other Total Ground Subcatchment (acres) (acres) (acres) (acres) (acres) (acres) Cover Numbers 0.000 0.000 0.426 0.000 0.426 50-75% Grass cover, Fair P-1, P-1a, P-1b, P-1c, P-1d, P-1e, P-1f, P-2, P-3 0.000 0.000 0.000 0.000 0.000 1.838 1.838 Paved parking P-1a, P-1b, P-2 0.000 0.000 0.000 0.032 0.032 P-1c, P-1d, P-1e, P-1f 0.000 Rip Rap Swale 0.000 0.000 0.123 0.000 0.000 0.123 Woods, Good P-1, P-1c, P-1d, P-1e, P-1f, P-3 0.000 0.000 0.549 0.000 1.870 2.419 TOTAL AREA

Ground Covers (all nodes)

	D® 10.00-26											Page
							ig (all nodes					
Line#	Node Number	In-Invert (feet)	Out-Invert (feet)	Length (feet)	Slope (ft/ft)	n	Diam/Width (inches)	Height (inches)	Inside-Fill (inches)			
1	SSD-1	322.50	322.00	21.3	0.0235	0.013	15.0	0.0	0.0			
Propos									Тур	e III 24-hr 25		
Prepare HydroCAI	d by {entei D® 10.00-26	r your com s s/n 04015	pany name © 2020 Hydro	here} CAD Softv	vare Soluti	ions LLC					Printed 1	0/17/202 Page

Runoff Area=18,417 sf 0.00% Impervious Runoff Depth=3.79" Flow Length=461' Tc=10.0 min CN=77 Runoff=1.62 cfs 0.133 af Subcatchment P-1: Flow to Existing Basin Subcatchment P-1a: Flow to SSI-1 Runoff Area=71,428 sf 99.59% Impervious Runoff Depth=6.11" Tc=6.0 min CN=98 Runoff=9.97 cfs 0.835 af Runoff Area=3,571 sf 87.17% Impervious Runoff Depth=5.88" Tc=6.0 min CN=96 Runoff=0.49 cfs 0.040 af Subcatchment P-1b: Flow to Treatment Unit Subcatchment P-1c: Fllow to Swale Runoff Area=1,317 sf 0.00% Impervious Runoff Depth=3.28" Tc=6.0 min CN=72 Runoff=0.11 cfs 0.008 af Runoff Area=1,184 sf 0.00% Impervious Runoff Depth=3.48" Tc=6.0 min CN=74 Runoff=0.11 cfs 0.008 af Subcatchment P-1d: Fllow to Swale Subcatchment P-1e: Fllow to Swale Runoff Area=1,184 sf 0.00% Impervious Runoff Depth=3.58" Tc=6.0 min CN=75 Runoff=0.11 cfs 0.008 af Runoff Area=1,071 sf 0.00% Impervious Runoff Depth=3.48" Tc=6.0 min CN=74 Runoff=0.10 cfs 0.007 af Subcatchment P-1f: Fllow to Swale Runoff Area=6,213 sf 93.87% Impervious Runoff Depth=5.99" Subcatchment P-2: Flow onsite Southeast Tc=6.0 min CN=97 Runoff=0.86 cfs 0.071 af Runoff Area=982 sf 0.00% Impervious Runoff Depth=3.99" Tc=6.0 min CN=79 Runoff=0.10 cfs 0.008 af Subcatchment P-3: Flow off-site West Reach DP-1: Basin Inflow=5.78 cfs 0.846 af Outflow=5.78 cfs 0.846 af Reach DP-2: Onsite southeast Inflow=0.86 cfs 0.071 af Outflow=0.86 cfs 0.071 af

Inflow=0.10 cfs 0.008 af Outflow=0.10 cfs 0.008 af

Peak Elev=334.06' Storage=216 cf Inflow=0.11 cfs 0.008 af Outflow=0.01 cfs 0.003 af

Peak Elev=332.51' Storage=199 cf Inflow=0.11 cfs 0.011 af Outflow=0.02 cfs 0.007 af

Peak Elev=331.01' Storage=196 cf Inflow=0.11 cfs 0.015 af Outflow=0.03 cfs 0.010 af

Peak Elev=329.26' Storage=149 cf Inflow=0.10 cfs 0.017 af Outflow=0.04 cfs 0.014 af

Peak Elev=324.52' Storage=12,891 cf Inflow=9.97 cfs 0.835 af Discarded=0.10 cfs 0.177 af Primary=4.21 cfs 0.658 af Outflow=4.32 cfs 0.835 af

Total Runoff Area = 2.419 ac Runoff Volume = 1.119 af Average Runoff Depth = 5.55" 24.00% Pervious = 0.581 ac 76.00% Impervious = 1.838 ac

# Proposed-7

Reach DP-3: Off-site West

Pond S-1: Rip Rap Swale

Pond S-2: Rip Rap Swale

Pond S-3: Rip Rap Swale

Pond S-4: Rip Rap Swale

Pond SSD-1: Subsurface Detention Basin-1

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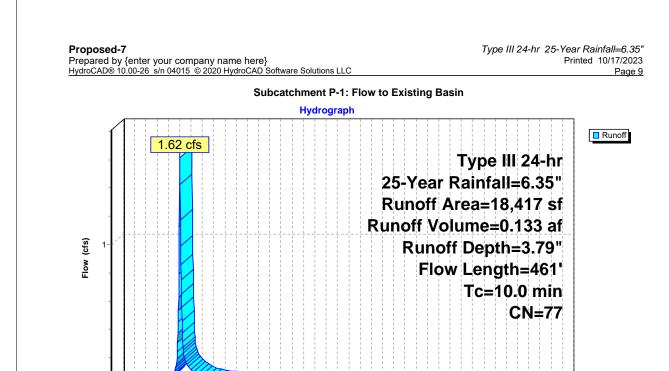
# Summary for Subcatchment P-1: Flow to Existing Basin

Runoff = 1.62 cfs @ 12.14 hrs, Volume= 0.133 af, Depth= 3.79"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=6.35"

A	rea (sf)	CN	Description	Description								
	4,454	70	Woods, Go	Voods, Good, HSG C								
	13,963	79	50-75% Gr	ass cover, F	Fair, HSG C							
	18,417	77	Weighted A	verage								
	18,417		100.00% P	ervious Are	a							
-		~		<b>.</b>								
TC	Length	Slop			Description							
(min)	(feet)	(ft/fl	) (ft/sec)	(cfs)								
7.3	50	0.080	0.11		Sheet Flow, Sheet Flow							
					Woods: Light underbrush n= 0.400 P2= 3.05"							
2.7	411	0.024	) 2.49		Shallow Concentrated Flow,							
					Unpaved Kv= 16.1 fps							
40.0	404	T - 4 - 1										

10.0 461 Total



						لسسان				1	1.0.00	11		1	1		11	11111					1					.1	1	11		1				11	
0	2	4	6	8	10	12 14	4 16	18	20 2	22.2	24 2	26 2	83	03	23	43	6 38	840	) 42	2 4 4	146	48	50	52	54	56	58 6	50 E	32 6	6 4ذ	6 6	870	72 (	74	767	8 80	
																٦	ime	e (ł	nou	ırs)																	

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Type III 24-hr 25-Year Rainfall=6.35" Printed 10/17/2023 Page 10

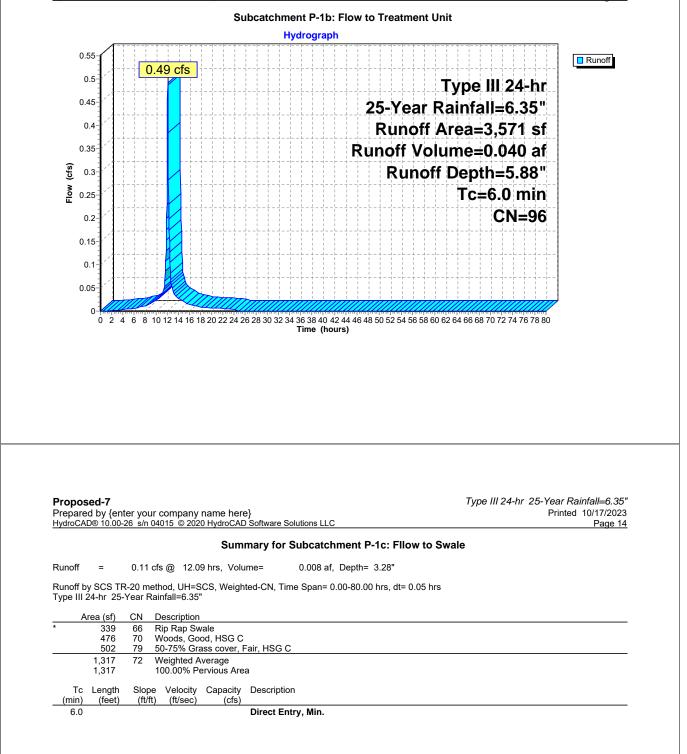
Summary for Subcatchment P-1a: Flow to SSI-1

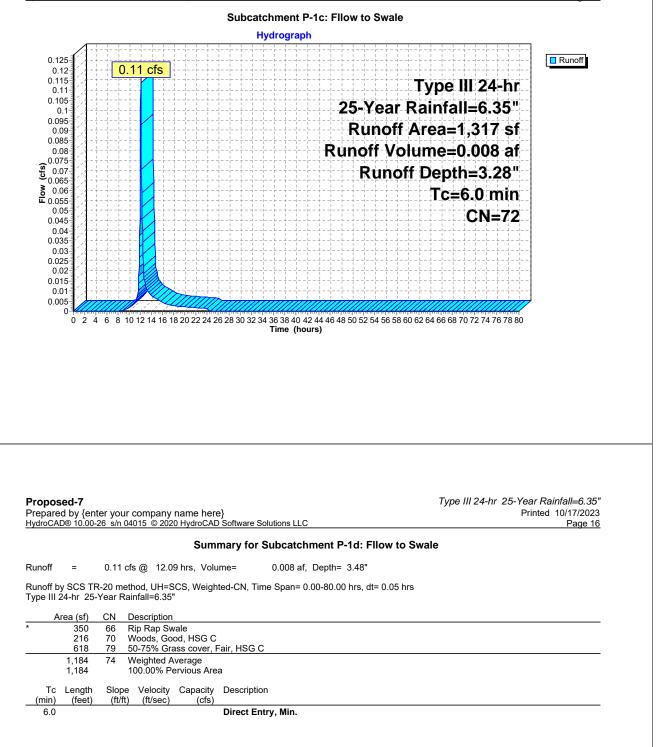
Runoff = 9.97 cfs @ 12.09 hrs, Volume= 0.835 af, Depth= 6.11"

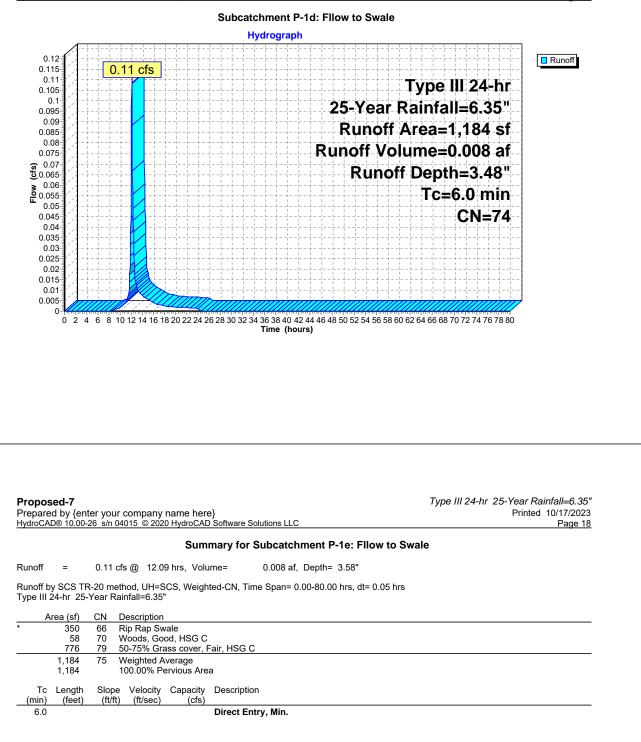
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs Type III 24-hr 25-Year Rainfall=6.35"

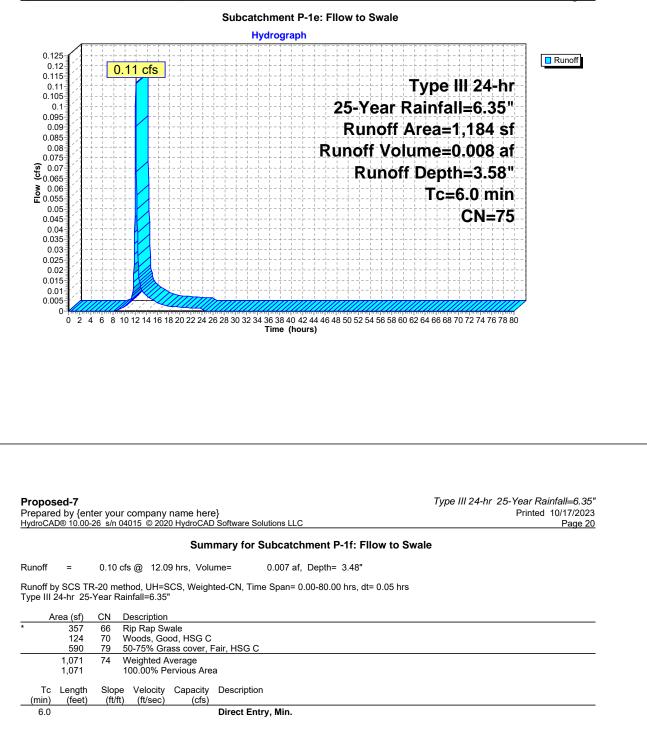
	Area (sf	) CN	Description	1		
*	71,13		Paved park			
	29	5 79	50-75% Gr	ass cover, F	air, HSG C	
	71,428	8 98	Weighted A			
	29	5	0.41% Perv	vious Area		
	71,13	3	99.59% Im	pervious Are	a	
-	Tc Leng	th Slop	e Velocity	Capacity	Description	
(mi			t) (ft/sec)	(cfs)	·	
6	.0				Direct Entry, M	in.

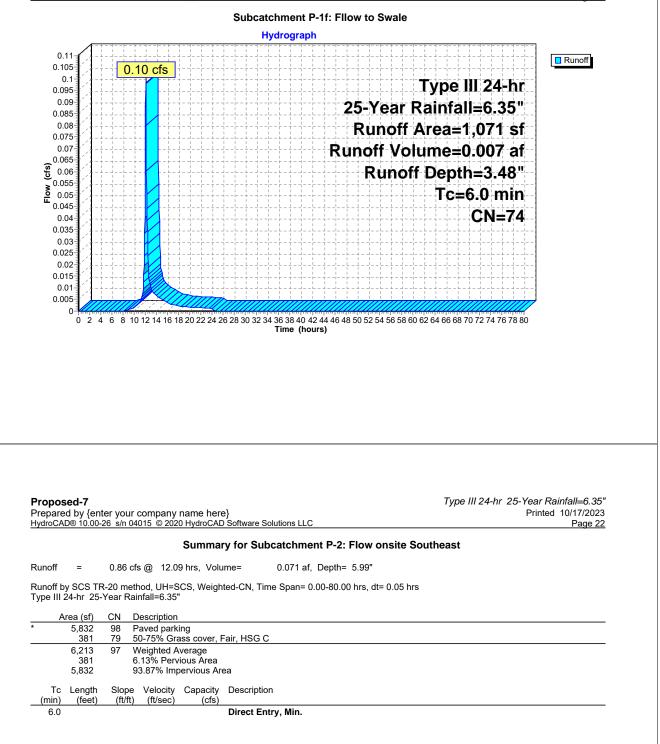
					н	lydrogra	ph								
٤		9.	97 cfs					25-Yo Runc unoff	ear R off Ai	Rainf rea=	71,42	.35" 8 sf	Ru	noff	
Flow (	6- 5- 4- 3-							Rı	Inoff	f Depth=6.11" Tc=6.0 min CN=98					
	2												_		
						Time (he									
Prepare	ed bv {er	iter you -26 s/n		ny name her 020 HydroCA	'€} D Software S					Ту	pe III 24-		ear Rainfal rinted 10/1 F		
Prepare	ed bv {er	1ter you -26 s/n	ır compan <u>04015 ⊚ 2(</u>	020 HydroCA	re} D Software S	iolutions LL	_ <u>C</u>	b: Flow to	o Treatr				rinted 10/1	7/2023	
Prepare HydroCA	ed bv {er	) <u>-26 s/n</u>	04015 © 20	020 HydroCA	D Software S	iolutions Ll	_ <u>C</u>		o Treatr				rinted 10/1	7/2023	
Prepare HydroCA Runoff Runoff b	ed by {er \ <u>D® 10.00</u> = by SCS T	0.49 0.49	04015 © 20	020 HydroCA Summar 09 hrs, Vol SCS, Weigl	<u>D Software S</u> T <b>y for Sub</b> ume=	iolutions Ll catchme 0.040 a	_C ent P-1I	= 5.88"		ment U			rinted 10/1	7/2023	
Prepare HydroCA Runoff Runoff b Type III	ed by {er <u>AD® 10.00</u> = by SCS T 24-hr 25 Area (sf)	0.49 0.49 R-20 m 5-Year F <u>CN</u>	04015 © 20 cfs @ 12 ethod, UH= Rainfall=6.3 _Descriptic	020 HydroCA Summar 09 hrs, Vol SCS, Weigl 55"	<u>D Software S</u> T <b>y for Sub</b> ume=	iolutions Ll catchme 0.040 a	_C ent P-1I	= 5.88"		ment U			rinted 10/1	7/2023	
Prepare HydroCA Runoff Runoff b Type III	ed by {er <u>AD® 10.00</u> = by SCS T 24-hr 25 <u>Area (sf)</u> 3,113 <u>458</u>	0.49 0.49 R-20 m 5-Year F	o4015 © 20 cfs @ 12 ethod, UH= Rainfall=6.3 Descriptic Paved pa	020 HydroCA Summar 09 hrs, Vol SCS, Weigl 55"	<u>D Software S</u> ry for Sub ume= hted-CN, Tir	iolutions Ll catchme 0.040 a me Span=	_C ent P-1I	= 5.88"		ment U			rinted 10/1	7/2023	
HydroCA Runoff Runoff b Type III	ed by {er <u>AD® 10.00</u> = by SCS T 24-hr 25 <u>Area (sf)</u> 3,113	0.49 0.49 R-20 m 5-Year F <u>CN</u> 98	cfs @ 12 ethod, UH= Rainfall=6.3 <u>Descriptic</u> Paved pa 50-75% C Weighted 12.83% P	Summar Summar .09 hrs, Vol =SCS, Weigl 55" on rrking Grass cover,	<u>D Software S</u> <b>ry for Sub</b> ume= hted-CN, Tir <u>Fair, HSG C</u> a	iolutions Ll catchme 0.040 a me Span=	_C ent P-1I	= 5.88"		ment U			rinted 10/1	7/2023	
Prepare HydroCA Runoff Runoff t Type III A	ed by {er <u>D® 10.00</u> = by SCS T 24-hr 25 <u>Area (sf)</u> 3,113 458 3,571 458	0.49 0.49 R-20 m 5-Year F <u>CN</u> 98 79 96 Slop	cfs @ 12 ethod, UH= Rainfall=6.3 Descriptic Paved pa 50-75% C Weighted 12.83% P 87.17% Ir	<u>Summar</u> Summar 09 hrs, Vol S5" Sc, Weigl 55" on rrking Prass cover, Average Pervious Area mpervious Area mpervious Area	<u>D</u> <u>software S</u> <b>ry for Sub</b> ume= hted-CN, Tir <u>Fair, HSG C</u> a rea Descriptic	iolutions Ll catchme 0.040 a ne Span=	_C ent P-1I	= 5.88"		ment U			rinted 10/1	7/2023	

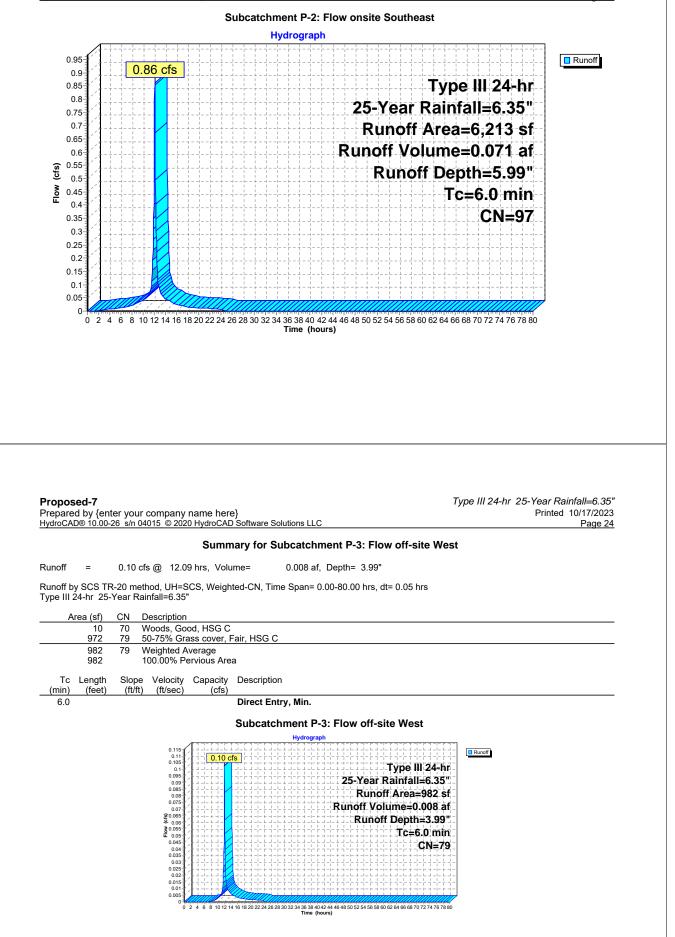










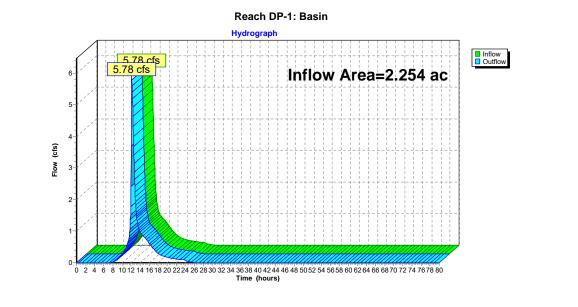


### Summary for Reach DP-1: Basin

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area =	2.254 ac, 75.63% Impervious, Inflow Dep	th = 4.50" for 25-Year event
Inflow =	5.78 cfs @ 12.19 hrs, Volume= 0	.846 af
Outflow =	5.78 cfs @ 12.19 hrs, Volume= 0	.846 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs



Proposed-7

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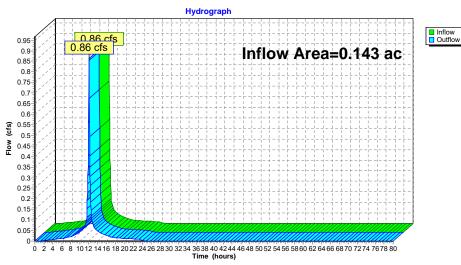
# Summary for Reach DP-2: Onsite southeast

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area	a =	0.143 ac, 9	3.87% Impervious,	Inflow Depth =	5.99"	for 25-Year event
Inflow	=	0.86 cfs @	12.09 hrs, Volume	= 0.071	af	
Outflow	=	0.86 cfs @	12.09 hrs, Volume	= 0.071	af, Atte	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs





# Summary for Reach DP-3: Off-site West

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area	ı =	0.023 ac,	0.00% Impervious, I	Inflow Depth =	3.99"	for 25-Year event
Inflow	=	0.10 cfs @	12.09 hrs, Volume=	0.008 a	af	
Outflow	=	0.10 cfs @	12.09 hrs, Volume=	• 0.008 a	af, Atte	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs

Reach DP-3: Off-site West Hydrograph Inflow
Outflow 0.10 cfs 0.10 cfs 0.115 0.11 Inflow Area=0.023 ac 0.105 0.1 0.095 0.09 0.085 0.08 0.07 දු ව<u>්</u> 0.065 0.06 **8** 0.055 ■ 0.05 0.045 0.04 0.035 0.025 0.015 0.01 0.005 0-0 2 4 6 8 1012 1416 18 2022 2426 28 30 3234 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70 72 74 76 78 80 Time (hours)

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# Summary for Pond S-1: Rip Rap Swale

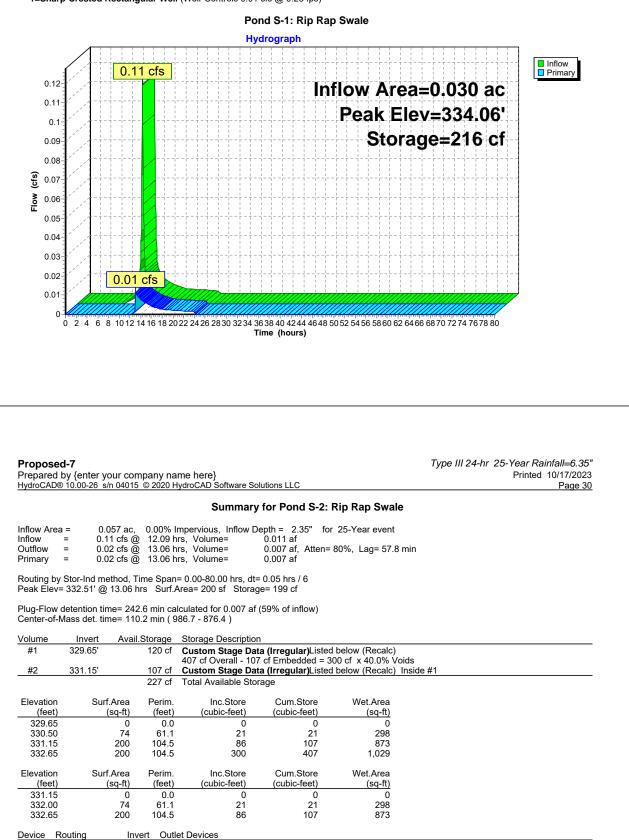
Inflow Area =	0.030 ac, 0.00% Impervious, Inflow	Depth = 3.28" for 25-Year event
Inflow =	0.11 cfs @ 12.09 hrs, Volume=	0.008 af
Outflow =	0.01 cfs @ 13.04 hrs, Volume=	0.003 af, Atten= 90%, Lag= 56.7 min
Primary =	0.01 cfs @ 13.04 hrs, Volume=	0.003 af

Routing by Stor-Ind method, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs / 6 Peak Elev= 334.06' @ 13.04 hrs Surf.Area= 200 sf Storage= 216 cf

Plug-Flow detention time= 288.6 min calculated for 0.003 af (40% of inflow) Center-of-Mass det. time= 164.1 min ( 994.9 - 830.9 )

Volume	Invert	Avail.Sto	rage	Storage Description								
#1	331.15'	1:	20 cf	Custom Stage Data								
					14 cf Overall - 114 cf Embedded = 300 cf x 40.0% Voids							
#2	332.65'	1	14 cf	Custom Stage Data	Istom Stage Data (Irregular)Listed below (Recalc) Inside #1							
		23	34 cf	Total Available Stora	otal Available Storage							
Elevation	Surf.	.Area P	Perim.	Inc.Store	Cum.Store	Wet.Area						
(feet)	(	sq-ft)	(feet)	(cubic-feet)	(cubic-feet)	(sq-ft)						
331.15		0	0.0	0	0	0						
331.50		21	27.2	2	2	59						
332.50		171	99.3	84	86	788						
332.65		200 -	104.4	28	114	872						
334.15		200 -	104.4	300	414	1,028						
Elevation	Surf	.Area P	Perim.	Inc.Store	Cum.Store	Wet Area						
(feet)	(	<i>i</i>	(feet)	(cubic-feet)	(cubic-feet)	(sq-ft)						
332.65		0	0.0	0	0	0						
333.00		21	27.2	2	2	59						
334.00		171	99.3	84	86	788						
334.15		200	104.4	28	114	872						
Device Routing Invert Outlet Devices												
-												

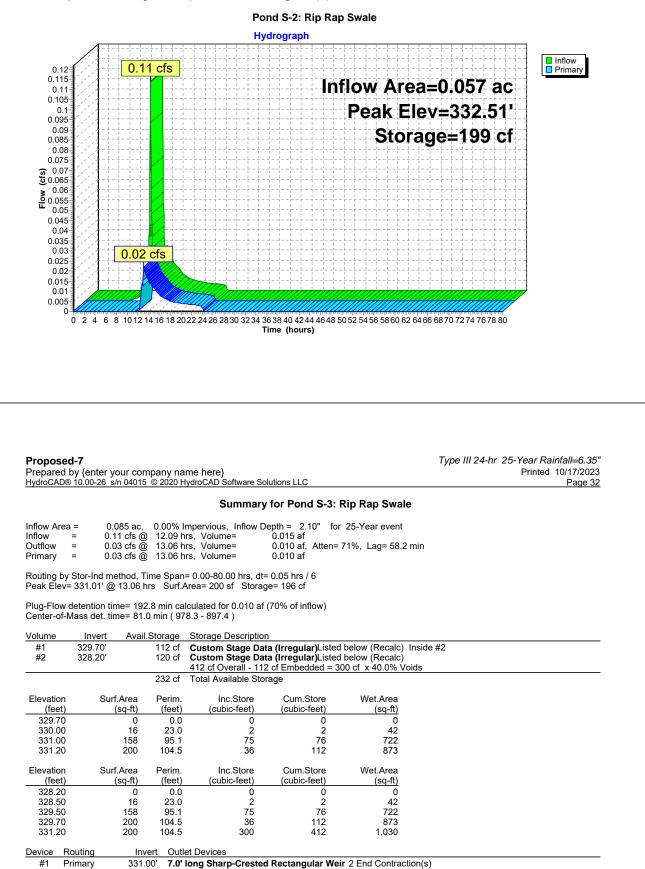
Primary OutFlow Max=0.01 cfs @ 13.04 hrs HW=334.05' (Free Discharge) 1=Sharp-Crested Rectangular Weir (Weir Controls 0.01 cfs @ 0.23 fps)



<sup>#1</sup> Primary

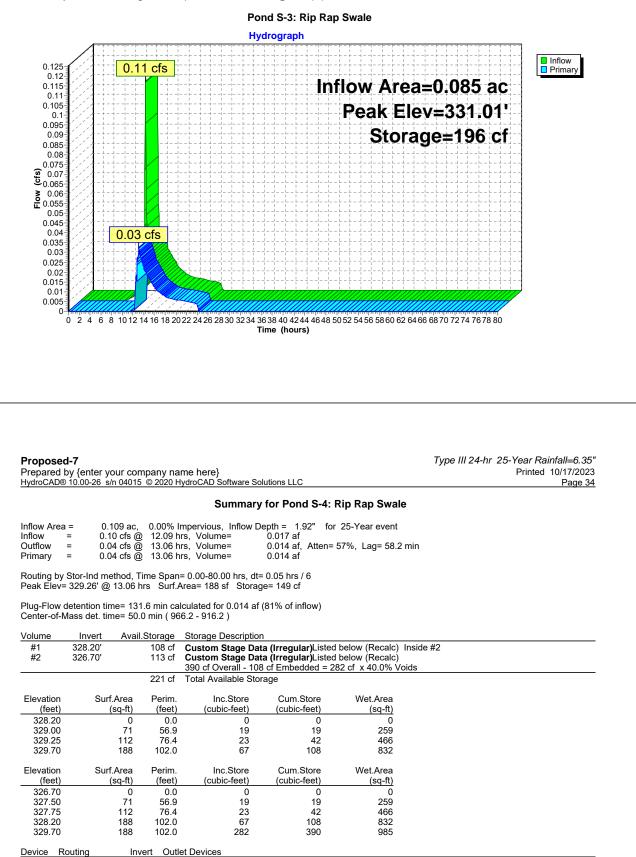
<sup>332.50&#</sup>x27; 7.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=0.01 cfs @ 13.06 hrs HW=332.51' (Free Discharge) 1=Sharp-Crested Rectangular Weir (Weir Controls 0.01 cfs @ 0.24 fps)



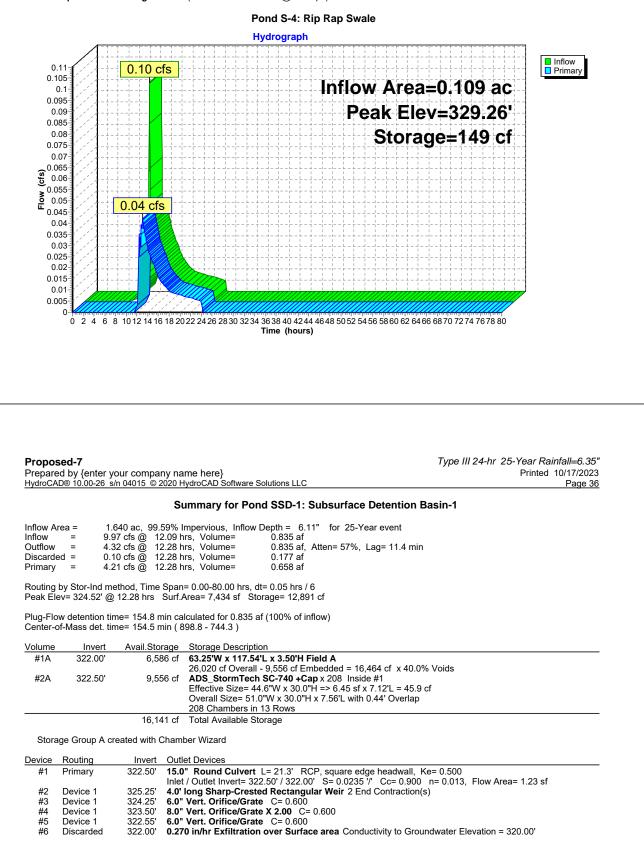
#1 Primary

Primary OutFlow Max=0.02 cfs @ 13.06 hrs HW=331.01' (Free Discharge) 1=Sharp-Crested Rectangular Weir (Weir Controls 0.02 cfs @ 0.33 fps)



329.25' 7.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=0.02 cfs @ 13.06 hrs HW=329.26' (Free Discharge) 1=Sharp-Crested Rectangular Weir (Weir Controls 0.02 cfs @ 0.34 fps)



Discarded OutFlow Max=0.10 cfs @ 12.28 hrs HW=324.52' (Free Discharge) 6=Exfiltration (Controls 0.10 cfs)

Primary OutFlow Max=4.20 cfs @ 12.28 hrs HW=324.52' (Free Discharge) -1=Culvert (Passes 4.20 cfs of 6.97 cfs potential flow)
 -2=Sharp-Crested Rectangular Weir (Controls 0.00 cfs)
 -3=Orifice/Grate (Orifice Controls 0.19 cfs @ 1.76 fps)
 -4=Orifice/Grate (Orifice Controls 2.78 cfs @ 3.98 fps)

-5=Orifice/Grate (Orifice Controls 1.24 cfs @ 6.31 fps)

#### Proposed-7

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Type III 24-hr 25-Year Rainfall=6.35" Printed 10/17/2023 Page 38

#### Pond SSD-1: Subsurface Detention Basin-1 - Chamber Wizard Field A

Chamber Model = ADS\_StormTech SC-740 +Cap (ADS StormTech® SC-740 with cap length) Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap

51.0" Wide + 6.0" Spacing = 57.0" C-C Row Spacing

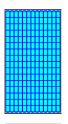
16 Chambers/Row x 7.12' Long +0.81' Cap Length x 2 = 115.54' Row Length +12.0" End Stone x 2 = 117.54' Base Length 13 Rows x 51.0" Wide + 6.0" Spacing x 12 + 12.0" Side Stone x 2 = 63.25' Base Width 6.0" Base + 30.0" Chamber Height + 6.0" Cover = 3.50' Field Height

208 Chambers x 45.9 cf = 9,555.5 cf Chamber Storage

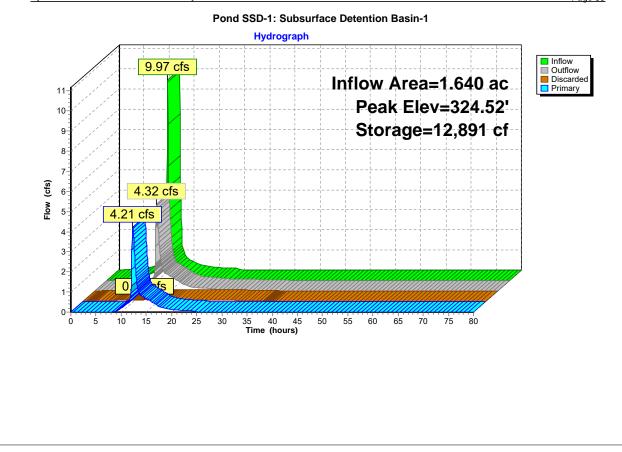
26,019.7 cf Field - 9,555.5 cf Chambers = 16,464.2 cf Stone x 40.0% Voids = 6,585.7 cf Stone Storage

Chamber Storage + Stone Storage = 16,141.2 cf = 0.371 af Overall Storage Efficiency = 62.0% Overall System Size = 117.54' x 63.25' x 3.50'

208 Chambers 963.7 cy Field 609.8 cy Stone



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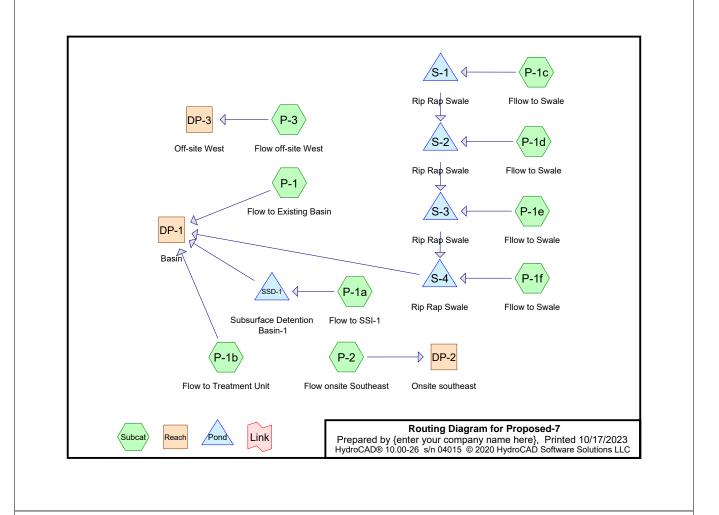




## HydroCAD Analysis

# **Proposed Conditions - 100 Year Storm**

249 SOUTH STREET UNIT 1 PLAINVILLE MA 02762 TEL508 695 2221 FAX508 695 2219 CONTACT@LEVELDG.COM LEVELDG.COM



#### Proposed-7

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#### Area Listing (all nodes)

Area	CN	Description
(acres)		(subcatchment-numbers)
0.426	79	50-75% Grass cover, Fair, HSG C (P-1, P-1a, P-1b, P-1c, P-1d, P-1e, P-1f, P-2, P-3)
1.838	98	Paved parking (P-1a, P-1b, P-2)
0.032	66	Rip Rap Swale (P-1c, P-1d, P-1e, P-1f)
0.123	70	Woods, Good, HSG C (P-1, P-1c, P-1d, P-1e, P-1f, P-3)
2.419	93	TOTAL AREA

#### Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
0.000	HSG B	
0.549	HSG C	P-1, P-1a, P-1b, P-1c, P-1d, P-1e, P-1f, P-2, P-3
0.000	HSG D	
1.870	Other	P-1a, P-1b, P-1c, P-1d, P-1e, P-1f, P-2
2.419		TOTAL AREA

#### Proposed-7

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#### HSG-A HSG-B HSG-C HSG-D Other Total Ground Subcatchment (acres) (acres) (acres) (acres) (acres) (acres) Cover Numbers 0.000 0.000 0.426 0.000 0.426 50-75% Grass cover, Fair P-1, P-1a, P-1b, P-1c, P-1d, P-1e, P-1f, P-2, P-3 0.000 0.000 0.000 0.000 0.000 1.838 1.838 Paved parking P-1a, P-1b, P-2 0.000 0.000 0.000 0.032 0.032 P-1c, P-1d, P-1e, P-1f 0.000 Rip Rap Swale 0.000 0.000 0.123 0.000 0.000 0.123 Woods, Good P-1, P-1c, P-1d, P-1e, P-1f, P-3 0.000 0.000 0.549 0.000 1.870 2.419 TOTAL AREA

Ground Covers (all nodes)

HydroCAE	u by {ente <u>0® 10.00-</u> 26	r your com <u>s/n 0401</u> 5	pany name © 2020 Hydro	nere} <pre>&gt;DCAD Softw</pre>	vare Solut	ions LLC				Printed 10/17/202 Page
					Pip	e Listin	g (all nodes	5)		
Line#	Node Number	In-Invert (feet)	Out-Invert (feet)	Length (feet)	Slope (ft/ft)	n	Diam/Width (inches)	Height (inches)	Inside-Fill (inches)	
1	SSD-1	322.50	322.00	21.3	0.0235	0.013	15.0	0.0	0.0	
Propos Prepareo HydroCAE	d by {ente	r your com s/n 04015	pany name © 2020 Hydro	here} CAD Softw	vare Solut	ions LLC			Type III 24-I	nr 100-Year Rainfall=8.16 Printed 10/17/202 Page
			Reach rou	Runoff by	SCS TR	-20 metł	s, dt=0.05 hrs nod, UH=SCS nod - Pond r	S, Weighte		
Subcatchment P-1: Flow to Existing Basin							Flo			npervious Runoff Depth=5.42 I=77 Runoff=2.30 cfs 0.191 a
Subcatcl	hment P-1a	a: Flow to S	SI-1				I	Runoff Area		npervious Runoff Depth=7.92 98 Runoff=12.83 cfs 1.082 a
Subcatcl	hment P-11	b: Flow to T	Freatment U	nit				Runoff Are		npervious Runoff Depth=7.68 I=96 Runoff=0.64 cfs 0.052 a

Subcatchment P-1c: Fllow to Swale

Subcatchment P-1d: Fllow to Swale

Subcatchment P-1e: Fllow to Swale

Subcatchment P-1f: Fllow to Swale

Subcatchment P-2: Flow onsite Southeast

Subcatchment P-3: Flow off-site West

Reach DP-1: Basin

Reach DP-2: Onsite southeast

Runoff Area=1,317 sf 0.00% Impervious Runoff Depth=4.84" Tc=6.0 min CN=72 Runoff=0.17 cfs 0.012 af

Runoff Area=1,184 sf 0.00% Impervious Runoff Depth=5.07" Tc=6.0 min CN=74 Runoff=0.16 cfs 0.011 af

Runoff Area=1,184 sf 0.00% Impervious Runoff Depth=5.19" Tc=6.0 min CN=75 Runoff=0.16 cfs 0.012 af

Runoff Area=1,071 sf 0.00% Impervious Runoff Depth=5.07" Tc=6.0 min CN=74 Runoff=0.14 cfs 0.010 af

Runoff Area=6,213 sf 93.87% Impervious Runoff Depth=7.80" Tc=6.0 min CN=97 Runoff=1.11 cfs 0.093 af

Runoff Area=982 sf 0.00% Impervious Runoff Depth=5.66" Tc=6.0 min CN=79 Runoff=0.14 cfs 0.011 af

> Inflow=8.73 cfs 1.169 af Outflow=8.73 cfs 1.169 af

> Inflow=1.11 cfs 0.093 af Outflow=1.11 cfs 0.093 af

Reach DP-3: Off-site West

Pond S-1: Rip Rap Swale

Pond S-2: Rip Rap Swale

Pond S-3: Rip Rap Swale

Pond S-4: Rip Rap Swale

Pond SSD-1: Subsurface Detention Basin-1

Inflow=0.14 cfs 0.011 af Outflow=0.14 cfs 0.011 af

Peak Elev=334.07' Storage=219 cf Inflow=0.17 cfs 0.012 af Outflow=0.09 cfs 0.007 af

Peak Elev=332.54' Storage=205 cf Inflow=0.18 cfs 0.019 af Outflow=0.17 cfs 0.014 af

Peak Elev=331.05' Storage=203 cf Inflow=0.27 cfs 0.026 af Outflow=0.25 cfs 0.022 af

Peak Elev=329.31' Storage=156 cf Inflow=0.34 cfs 0.032 af Outflow=0.32 cfs 0.029 af

Peak Elev=325.16' Storage=15,127 cf Inflow=12.83 cfs 1.082 af Discarded=0.12 cfs 0.185 af Primary=6.09 cfs 0.897 af Outflow=6.21 cfs 1.082 af

Total Runoff Area = 2.419 ac Runoff Volume = 1.475 af Average Runoff Depth = 7.32" 24.00% Pervious = 0.581 ac 76.00% Impervious = 1.838 ac

#### Proposed-7

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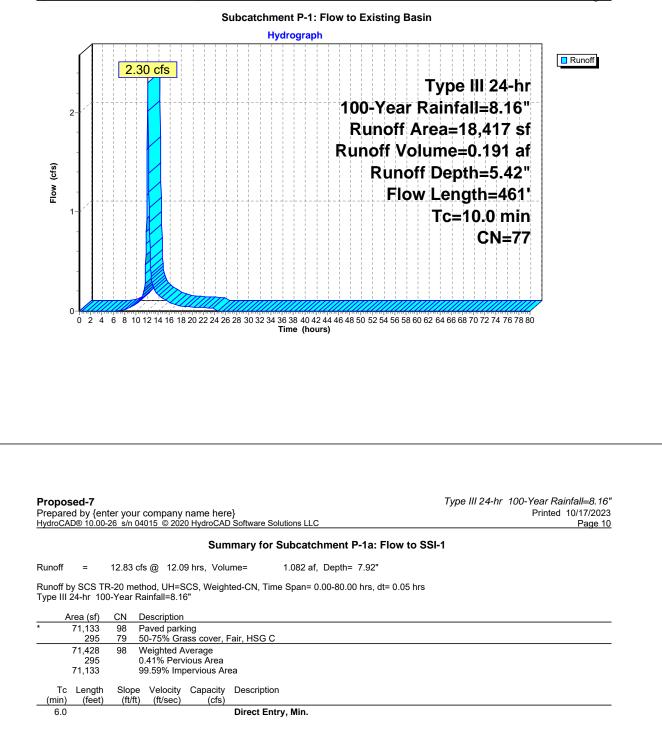
#### Summary for Subcatchment P-1: Flow to Existing Basin

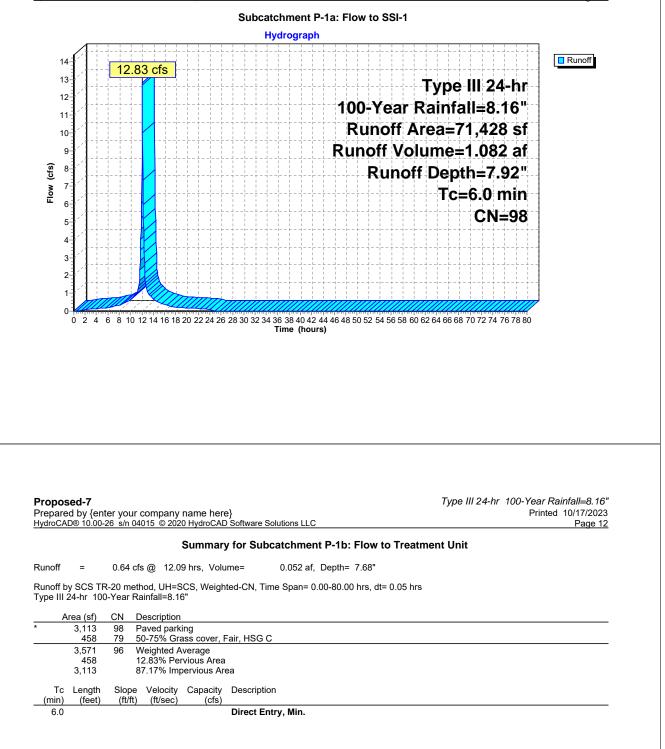
Runoff = 2.30 cfs @ 12.14 hrs, Volume= 0.191 af, Depth= 5.42"

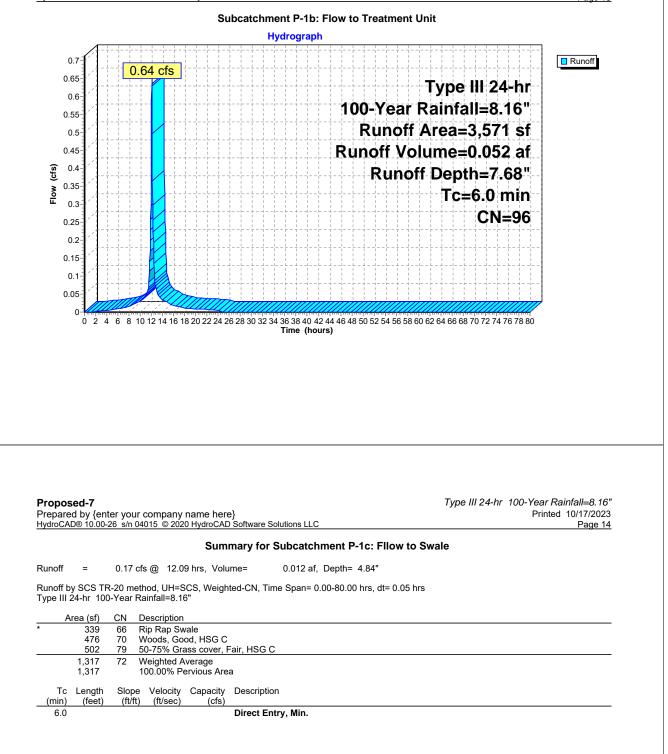
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs Type III 24-hr 100-Year Rainfall=8.16"

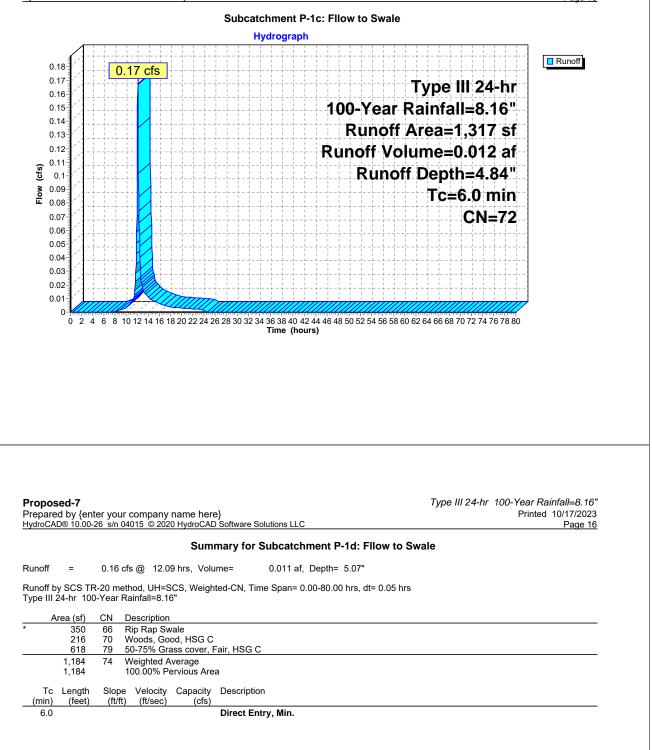
	A	rea (sf)	CN	Description	1							
_		4,454	70	Woods, Go	Woods, Good, HSG C							
_		13,963	79	50-75% Gr	ass cover, l	Fair, HSG C						
		18,417	77	Weighted A	Verage							
		18,417		100.00% P	ervious Are	a						
	Tc (min)	Length (feet)	Slop (ft/fl		Capacity (cfs)	Description						
	7.3	50	0.080	0.11		Sheet Flow, Sheet Flow						
_	2.7	411	0.024	) 2.49		Woods: Light underbrush n= 0.400 P2= 3.05" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps						
_	40.0	404	<b>T</b> ( )									

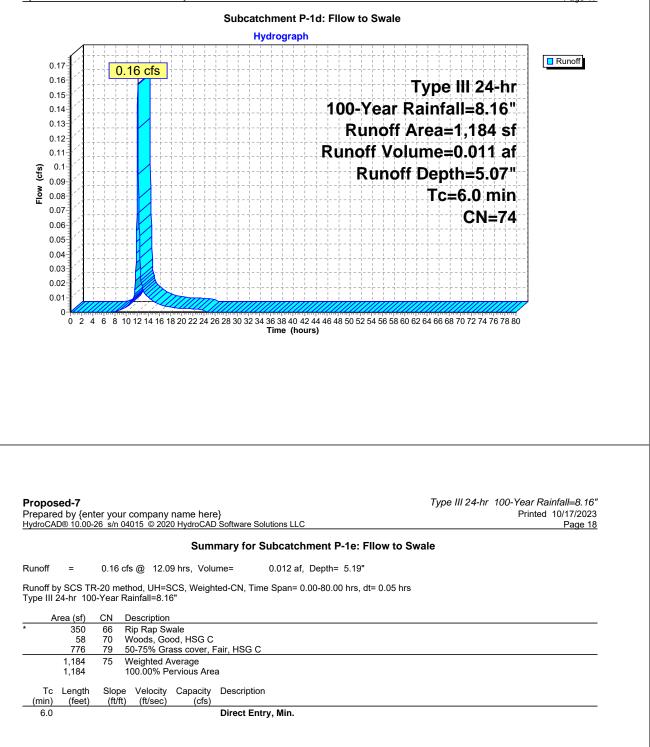
10.0 461 Total

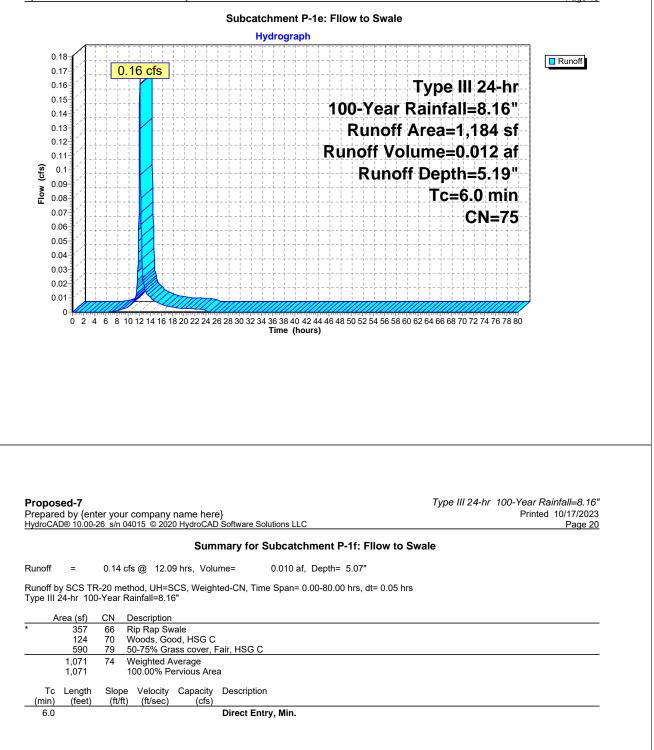


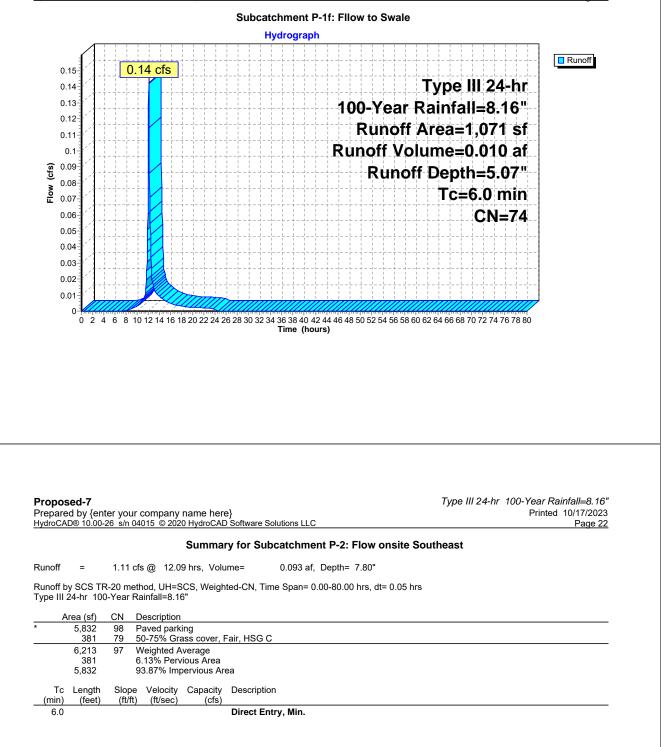


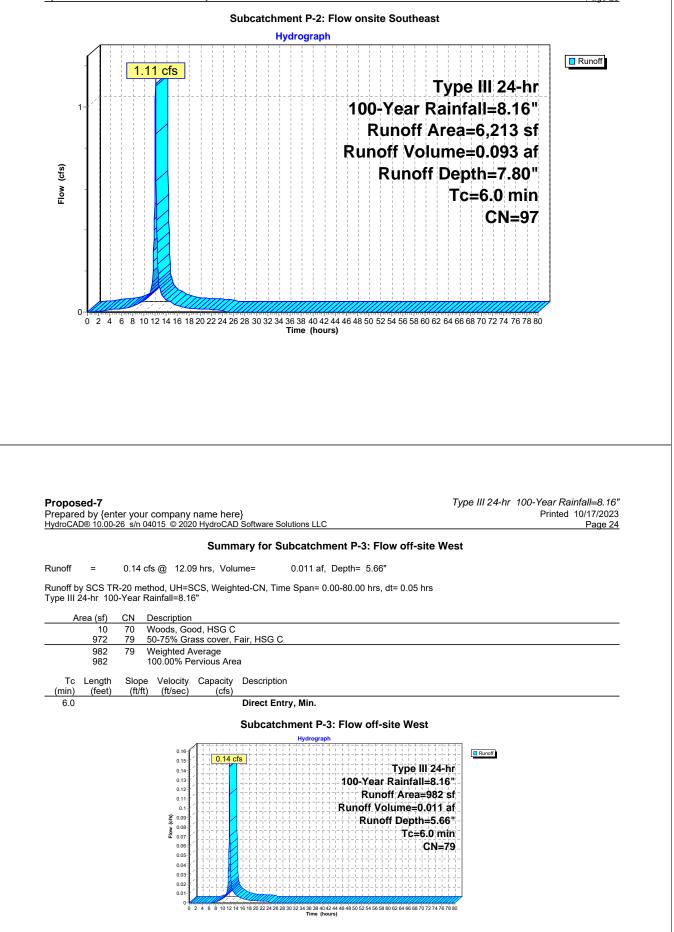












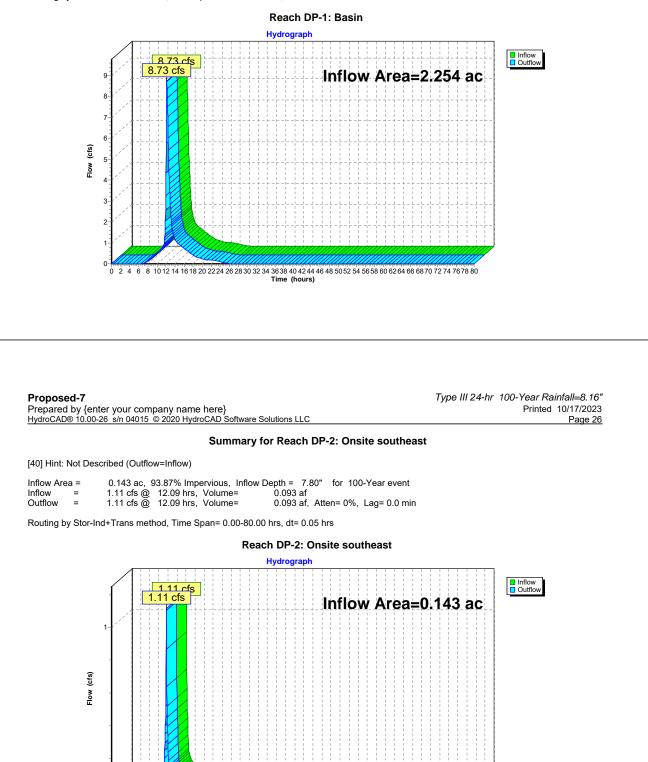
#### Summary for Reach DP-1: Basin

[40] Hint: Not Described (Outflow=Inflow)

0

Inflow Area =	2.254 ac, 75.63% Impervious, Inflow Depth = 6.22" for 100-Year event	
Inflow =	8.73 cfs @ 12.19 hrs, Volume= 1.169 af	
Outflow =	8.73 cfs @ 12.19 hrs, Volume= 1.169 af, Atten= 0%, Lag= 0.0 min	

Routing by Stor-Ind+Trans method, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs



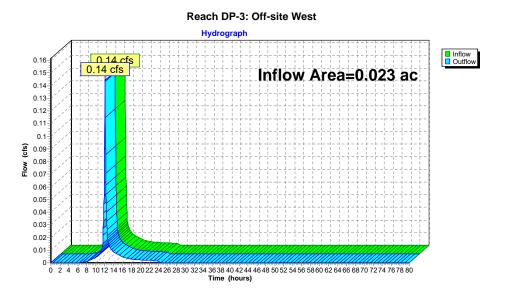
0 2 4 6 8 1012 14 16 18 20 22 24 26 28 30 32 34 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70 72 74 76 78 80 Time (hours)

#### Summary for Reach DP-3: Off-site West

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area	=	0.023 ac,	0.00% Impervious, Inflow	Depth = 5.66"	for 100-Year event
Inflow =	=	0.14 cfs @	12.09 hrs, Volume=	0.011 af	
Outflow =	=	0.14 cfs @	12.09 hrs, Volume=	0.011 af, Atte	en= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs



Proposed-7

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#### Summary for Pond S-1: Rip Rap Swale

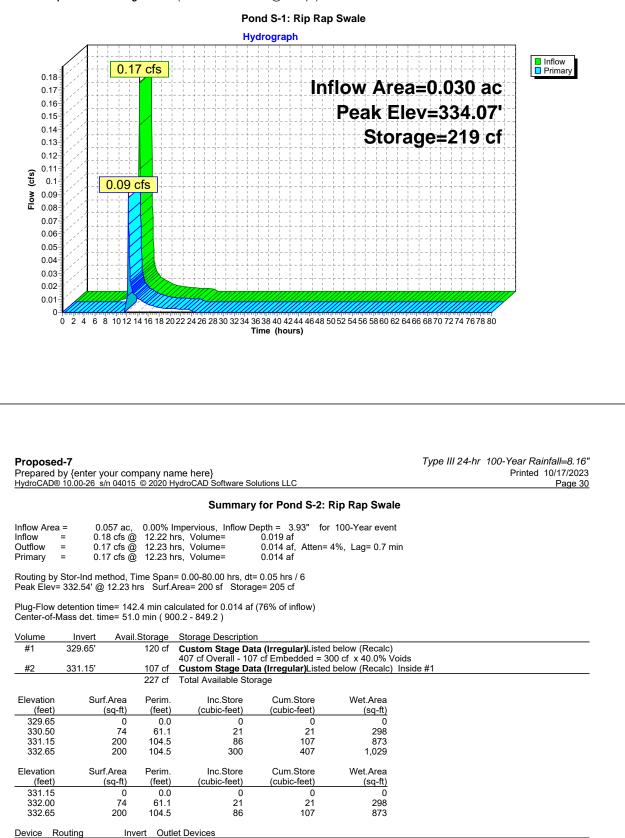
Inflow Area =	0.030 ac,	0.00% Impervious, Inflow E	Depth = 4.84" for 100-Year event
Inflow =	0.17 cfs @	12.09 hrs, Volume=	0.012 af
Outflow =	0.09 cfs @	12.25 hrs, Volume=	0.007 af, Atten= 48%, Lag= 9.4 min
Primary =	0.09 cfs @	12.25 hrs, Volume=	0.007 af

Routing by Stor-Ind method, Time Span= 0.00-80.00 hrs, dt= 0.05 hrs / 6 Peak Elev= 334.07' @ 12.25 hrs Surf.Area= 200 sf Storage= 219 cf

Plug-Flow detention time= 188.5 min calculated for 0.007 af (60% of inflow) Center-of-Mass det. time= 82.2 min ( 901.9 - 819.7 )

Volume	Invert	Avail.S	torage	Storage Description	1		
#1	331.15'		120 cf	Custom Stage Dat			
#2	332.65'		114 cf	414 cf Overall - 114 Custom Stage Dat			
<u></u>	002.00		234 cf	Total Available Stor			
					0		
Elevation	Surf.	.Area	Perim.	Inc.Store	Cum.Store	Wet.Area	
(feet)	(	sq-ft)	(feet)	(cubic-feet)	(cubic-feet)	(sq-ft)	
331.15		0	0.0	0	0	0	
331.50		21	27.2	2	2	59	
332.50		171	99.3	84	86	788	
332.65		200	104.4	28	114	872	
334.15		200	104.4	300	414	1,028	
Elevation	Surf	Area	Perim.	Inc.Store	Cum.Store	Wet.Area	
(feet)	(	sq-ft)	(feet)	(cubic-feet)	(cubic-feet)	(sq-ft)	
332.65		0	0.0	0	0	0	
333.00		21	27.2	2	2	59	
334.00		171	99.3	84	86	788	
334.15		200	104.4	28	114	872	
Device Ro	outing	Inve	rt Outle	et Devices			
#1 Pr	imary	334.05	5' <b>7.0'</b>	long Sharp-Crested	Rectangular Wei	r 2 End Contrac	ction(s)

Primary OutFlow Max=0.08 cfs @ 12.25 hrs HW=334.07' (Free Discharge) 1=Sharp-Crested Rectangular Weir (Weir Controls 0.08 cfs @ 0.49 fps)



#1 Primary

332.50' 7.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Device Routing

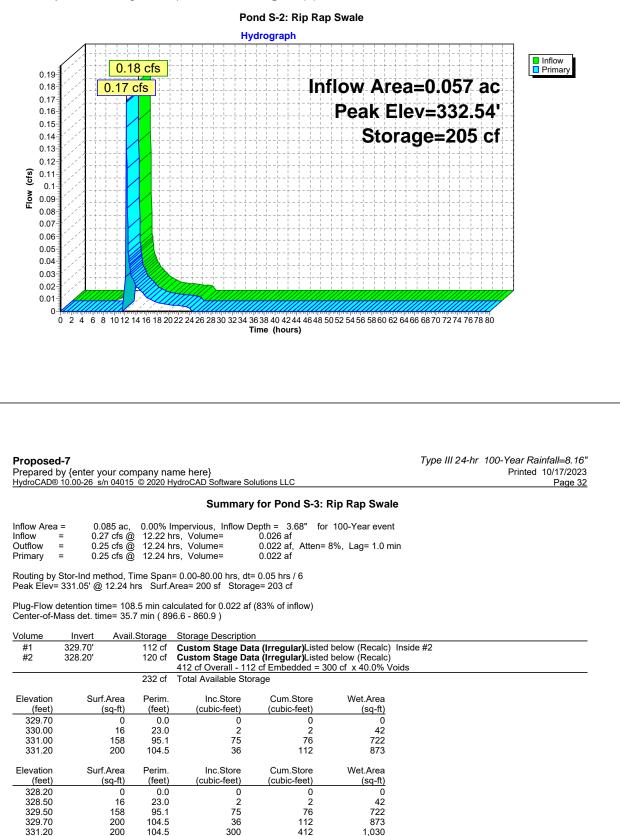
#1 Primary

Invert

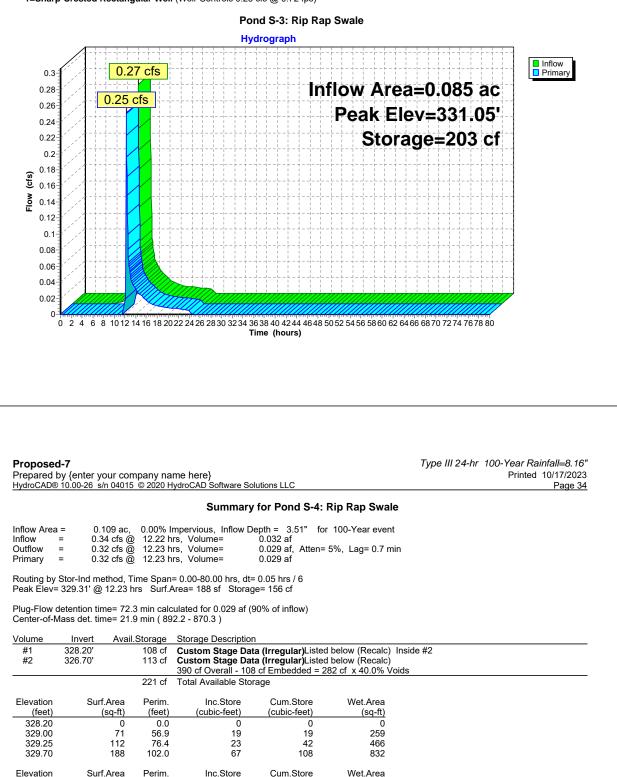
Outlet Devices

331.00' 7.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=0.16 cfs @ 12.23 hrs HW=332.54' (Free Discharge) 1=Sharp-Crested Rectangular Weir (Weir Controls 0.16 cfs @ 0.63 fps)



Primary OutFlow Max=0.25 cfs @ 12.24 hrs HW=331.05' (Free Discharge) 1=Sharp-Crested Rectangular Weir (Weir Controls 0.25 cfs @ 0.72 fps)



(cubic-feet)

0

19

23

67

282

329.25' 7.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

(cubic-feet)

0

19

42

108

390

(sq-ft)

0

259

466

832

985

(sq-ft)

0

71

112

188

188

Invert

(feet)

0.0

56.9

76.4

102.0

102.0

Outlet Devices

(feet)

326 70

327.50

327.75

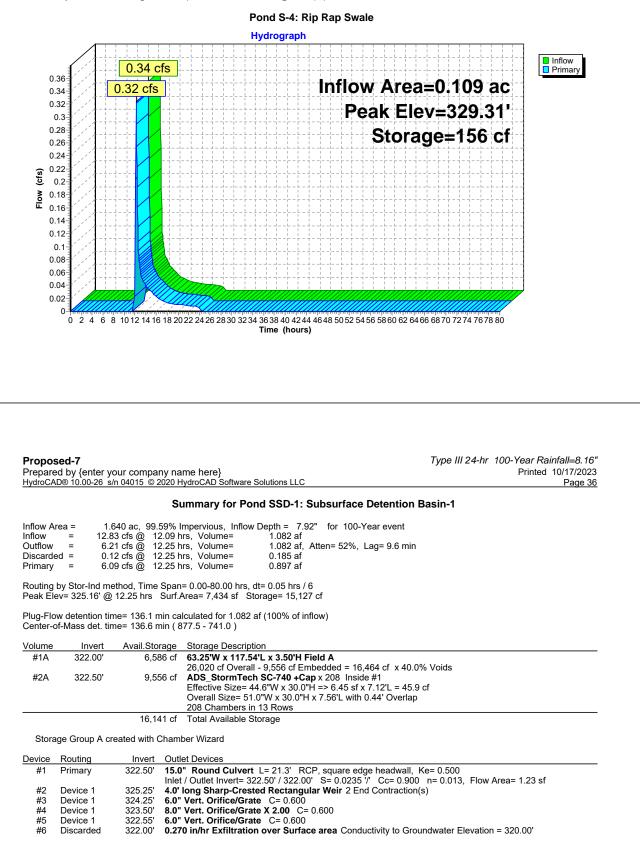
328.20

329.70

Device Routing

#1 Primary

Primary OutFlow Max=0.32 cfs @ 12.23 hrs HW=329.31' (Free Discharge) 1=Sharp-Crested Rectangular Weir (Weir Controls 0.32 cfs @ 0.79 fps)



Discarded OutFlow Max=0.12 cfs @ 12.25 hrs HW=325.16' (Free Discharge) G=Exfiltration (Controls 0.12 cfs)

Primary OutFlow Max=6.09 cfs @ 12.25 hrs HW=325.16' (Free Discharge) 

-5=Orifice/Grate (Orifice Controls 1.45 cfs @ 7.39 fps)

#### Proposed-7

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#### Pond SSD-1: Subsurface Detention Basin-1 - Chamber Wizard Field A

Chamber Model = ADS\_StormTech SC-740 +Cap (ADS StormTech® SC-740 with cap length) Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap

51.0" Wide + 6.0" Spacing = 57.0" C-C Row Spacing

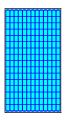
16 Chambers/Row x 7.12' Long +0.81' Cap Length x 2 = 115.54' Row Length +12.0" End Stone x 2 = 117.54' Base Length 13 Rows x 51.0" Wide + 6.0" Spacing x 12 + 12.0" Side Stone x 2 = 63.25' Base Width 6.0" Base + 30.0" Chamber Height + 6.0" Cover = 3.50' Field Height

208 Chambers x 45.9 cf = 9,555.5 cf Chamber Storage

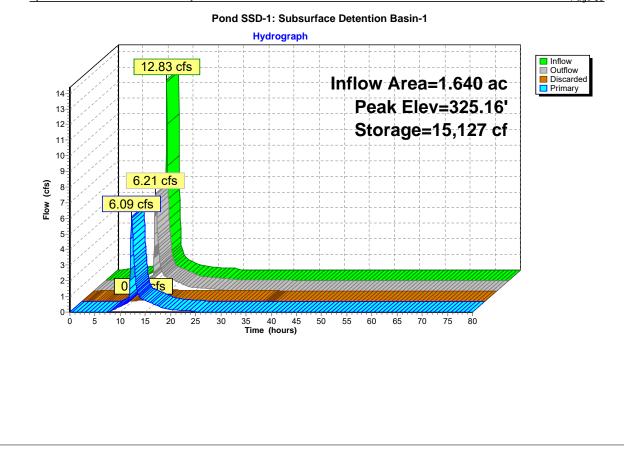
26,019.7 cf Field - 9,555.5 cf Chambers = 16,464.2 cf Stone x 40.0% Voids = 6,585.7 cf Stone Storage

Chamber Storage + Stone Storage = 16,141.2 cf = 0.371 af Overall Storage Efficiency = 62.0% Overall System Size = 117.54' x 63.25' x 3.50'

208 Chambers 963.7 cy Field 609.8 cy Stone



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## **Operation and Maintenance Plan**



## OPERATION AND MAINTENANCE PLAN FOR 15 LIBERTY WAY FRANKLIN, MA

DATED: JANUARY 17, 2023 Revised: October 17, 2023

Prepared By: Level Design Group, L.L.C. 249 South Street, Unit 1 Plainville, MA 02762

Prepared For: Oliver Street Capital 125 High Street, Suite 220 Boston, MA 02110

LDG Project No.: 2081.00



The proposed Stormwater Management System is designed to function properly provided that routine maintenance is performed. It is the responsibility during construction and until purchase of the units and turnover of the project to a Home Owners Association to be formed, that the Owner and Developer, Oliver Street Capital, shall be responsible for the long-term maintenance and to provide the required maintenance outlined in this plan for the site infiltration systems as well as the remainder of the on-site storm drainage system.

Upon completion of construction and the formation of the Home Owners Association, maintenance of driveways and the stormwater appurtenances required to ensure that sedimentation and pollution is controlled and that storm water detention and infiltration capacity is sustained are the on-going responsibility of the Home Owners Association. To ensure the proper functioning of these facilities the following maintenance practices will be used:

#### **DRIVEWAYS AND PARKING AREAS**

#### Spring Maintenance

Driveways and Parking Areas are to be swept monthly to remove sand which has accumulated. Sand shall be removed from the site and legally disposed of.

#### Summer & Fall Maintenance

Leaves and debris which accumulates within the Driveways and Parking Areas during the summer and fall shall be collected and legally disposed of.

#### Winter Maintenance & Snow Removal

Snow removal within Driveways and Parking Area shall be stockpiled in the designated Snow Stockpile Areas outside of the traveled driveways. These areas should be located within or adjacent to the parking surface and should drain to the stormwater management system. Under no circumstances shall snow be directed onto abutting parcels or into the on-site resource areas (wetlands, wetland buffer zone, and riverfront areas).

#### Estimated Yearly Cost <u>\$1,000.00 (not including cost for snow plowing)</u>

#### **DEEP SUMP CATCH BASINS**

Catch basins shall be inspected and cleaned four times per year or when the sumps are 50% full.

#### Spring Maintenance

Catch basins require the removal of sediment each spring. This procedure is comprised of removing the catch basin grate followed by removal of sediment trapped in the structure with a clamshell shovel. The outlet pipe from the catch basin shall be inspected and any obstructions are to be removed. The sediment and debris removed from the catch basin shall be legally disposed of.

#### Fall Maintenance

Catch basin grates shall be cleared of leaves and debris so they may function properly.



Estimated Yearly Cost \$2,000.00

## SUBSURFACE INFILTRATION BASIN

### Spring Maintenance

The subsurface detention basin requires monthly inspections for accumulations of settled solids. If these materials have accumulated to a point where removal is necessary this shall be completed immediately. Accumulated trash and debris shall also be removed and legally disposed of during the monthly inspections.

## Estimated Yearly Cost \$500.00

## PUBLIC SAFETY FEATURES

Many of the Public Safety Features of the Stormwater Management System are incorporated into its design. The Infiltration basin was designed to minimize its depth to 2-feet deep. This combined with sediment forebay being approximately 1-foot deep provide for a safe and effective system.

Despite all the well-designed safety features within the Stormwater Management System all components of the system must be properly maintained to be effective. All maintenance procedures detailed above must be done on schedule and documented. Standing or stagnant water provides mosquito-breeding habitat and increases the potential for disease transmission. The basin is designed to fully infiltrate within 72 hours after a storm even which will prevent standing water from becoming a safety hazard. Routine monitoring for and management of mosquito-breeding conditions by qualified maintenance staff is required during the peak breading season between April and September ensure that unforeseen conditions do not develop.

While risks can be mitigated through proper design and maintenance, it is impossible to entirely eliminate risk. Therefore, education regarding stormwater management facilities and their inherent risks is valuable and should be a part of every community's activity. Employees and tenants of the Facility shall be given an overview of the Stormwater System and which areas to avoid. Public participation also increases the level of maintenance as community members can notify staff if a component of the stormwater system is not functioning properly.

The O&M shall be recorded with the Home Owners Agreement or other approving maintenance agreement to properly notify future owners of maintenance requirements.



## STORMWATER MANAGEMENT OPREATOIN AND MAINTENANCE LOG

It is the responsibility of the owner and developer, Oliver Street Capital, to provide the maintenance of the Stormwater Management System Maintenance in accordance with the Town of Franklin Stormwater Management Standards until such time as an entity is created for overall site management at which time the agreement will spell out responsibility with appropriate contact information for all parties. The log form below is a template and shall be reproduced as needed. Copies of all log forms shall be kept on file for a minimum of three years from the date of inspection.

Name of Inspector:	
Date and Time of Inspection:	
Weather Conditions:	

Stormwater BMP	Observations	Action Required



# Long Term Pollution Prevention Plan



## LONG TERM POLLUTION PREVENTION PLAN FOR

15 LIBERTY WAY FRANKLIN, MA

DATED: JANUARY 13, 2023

Prepared By: Level Design Group, L.L.C. 249 South Street, Unit 1 Plainville, MA 02762

Prepared For: Oliver Street Capital 125 High Street, Suite 220 Boston, MA 02110

LDG Project No.: 2081.00



## **GOOD HOUSEKEEPING PRACTICES**

It is the responsibility of the developer, Oliver Street Capital, to provide for maintenance of the parking areas and the storm drainage system until the site is turned over to the condominium association which will be created prior to the sale of any units. The Owner shall utilize good housekeeping practices as outlined in the Operation and Maintenance Plan required for the maintenance of the Stormwater Management System.

### PROVISIONS FOR STORAGE OF MATERIALS AND WASTE PRODUCTS INSIDE OR UNDER COVER

The storage of hazardous materials and waste is prohibited from being stored outdoor at the site. Any hazardous materials shall be stored under cover.

## VEHICLE WASHING CONTROLS

Outdoor vehicle washing is allowed only for occupants of the condominium development for noncommercial vehicles owned by the residents of the units. No commercial vehicle washing operations is allowed in this area.

#### **REQUIREMENTS FOR ROUTINE INSPECTION AND MAINTENANCE OF STORMWATER BMPS**

The Owner / Operator shall keep a Maintenance Log Sheets of scheduled tasks outlined Operation and Maintenance Plan.

#### SPILL PREVENTION AND RESPONSE PLANS

The risk of significant spills requiring action at this site is limited and will most likely be associated with motor vehicle use or maintenance. In the event of a significant spill contact:

Massachusetts Department of Environmental Protection 24-hour emergency response notification line – (888) 304-1133

## PROVISIONS FOR MAINTENANCE OF LAWNS, GARDENS, AND OTHER LANDSCAPED AREAS

The use of chemical fertilizers shall not be used on-site. If chemical fertilizers are required to be used, the fertilizers must be worked into the soil to prevent washouts and stormwater contamination of fertilizers.



## **REQUIREMENTS FOR STORAGE AND USE OF FERTILIZERS, HERBICIDES, AND PESTICIDES**

If fertilizers, herbicides, and pesticides are to be used and stored on site they are to be stored in their original containers and keep in a dry, safe area where children do not have access to.

### PROVISIONS SOLID WASTE MANAGEMENT

Solid waste and recycling is to be disposed in designated areas in enclosed dumpsters and receptacles with covers and hauled by private certified waste management service operators. Solid waste management systems shall be inspected and maintained in accordance with state, local, and federal solid waste management regulations.

### EMERGENCY AND REGULATORY CONTACTS

Franklin Fire Department:	911 / (508) 528-2323
Franklin Police Department:	911 / (508) 528-1212
Massachusetts Department of Environmental Protection – Central Regional Office:	(508) 792-7650
United State Environmental Protection Agency:	(617) 918-1111



## NPDES Stormwater Pollution Prevention Plan (DRAFT – Under separate cover)