Franklin, Massachusetts

# APPENDIX C – Stormwater Management Report & Checklist





#### Massachusetts Department of Environmental Protection

Bureau of Resource Protection - Wetlands Program

### **Checklist for Stormwater Report**

#### A. Introduction

Important: When filling out forms on the computer, use only the tab key to move your cursor - do not use the return key.





A Stormwater Report must be submitted with the Notice of Intent permit application to document compliance with the Stormwater Management Standards. The following checklist is NOT a substitute for the Stormwater Report (which should provide more substantive and detailed information) but is offered here as a tool to help the applicant organize their Stormwater Management documentation for their Report and for the reviewer to assess this information in a consistent format. As noted in the Checklist, the Stormwater Report must contain the engineering computations and supporting information set forth in Volume 3 of the Massachusetts Stormwater Handbook. The Stormwater Report must be prepared and certified by a Registered Professional Engineer (RPE) licensed in the Commonwealth.

The Stormwater Report must include:

- The Stormwater Checklist completed and stamped by a Registered Professional Engineer (see page 2) that certifies that the Stormwater Report contains all required submittals. This Checklist is to be used as the cover for the completed Stormwater Report.
- Applicant/Project Name
- Project Address
- Name of Firm and Registered Professional Engineer that prepared the Report
- Long-Term Pollution Prevention Plan required by Standards 4-6
- Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan required by Standard 8<sup>2</sup>
- Operation and Maintenance Plan required by Standard 9

In addition to all plans and supporting information, the Stormwater Report must include a brief narrative describing stormwater management practices, including environmentally sensitive site design and LID techniques, along with a diagram depicting runoff through the proposed BMP treatment train. Plans are required to show existing and proposed conditions, identify all wetland resource areas, NRCS soil types, critical areas, Land Uses with Higher Potential Pollutant Loads (LUHPPL), and any areas on the site where infiltration rate is greater than 2.4 inches per hour. The Plans shall identify the drainage areas for both existing and proposed conditions at a scale that enables verification of supporting calculations.

As noted in the Checklist, the Stormwater Management Report shall document compliance with each of the Stormwater Management Standards as provided in the Massachusetts Stormwater Handbook. The soils evaluation and calculations shall be done using the methodologies set forth in Volume 3 of the Massachusetts Stormwater Handbook.

To ensure that the Stormwater Report is complete, applicants are required to fill in the Stormwater Report Checklist by checking the box to indicate that the specified information has been included in the Stormwater Report. If any of the information specified in the checklist has not been submitted, the applicant must provide an explanation. The completed Stormwater Report Checklist and Certification must be submitted with the Stormwater Report.

<sup>&</sup>lt;sup>1</sup> The Stormwater Report may also include the Illicit Discharge Compliance Statement required by Standard 10. If not included in the Stormwater Report, the Illicit Discharge Compliance Statement must be submitted prior to the discharge of stormwater runoff to the post-construction best management practices.

<sup>&</sup>lt;sup>2</sup> For some complex projects, it may not be possible to include the Construction Period Erosion and Sedimentation Control Plan in the Stormwater Report. In that event, the issuing authority has the discretion to issue an Order of Conditions that approves the project and includes a condition requiring the proponent to submit the Construction Period Erosion and Sedimentation Control Plan before commencing any land disturbance activity on the site.



#### Massachusetts Department of Environmental Protection Bureau of Resource Protection - Wetlands Program

### **Checklist for Stormwater Report**

#### **B. Stormwater Checklist and Certification**

The following checklist is intended to serve as a guide for applicants as to the elements that ordinarily need to be addressed in a complete Stormwater Report. The checklist is also intended to provide conservation commissions and other reviewing authorities with a summary of the components necessary for a comprehensive Stormwater Report that addresses the ten Stormwater Standards.

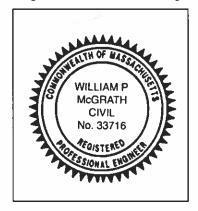
*Note:* Because stormwater requirements vary from project to project, it is possible that a complete Stormwater Report may not include information on some of the subjects specified in the Checklist. If it is determined that a specific item does not apply to the project under review, please note that the item is not applicable (N.A.) and provide the reasons for that determination.

A complete checklist must include the Certification set forth below signed by the Registered Professional Engineer who prepared the Stormwater Report.

#### **Registered Professional Engineer's Certification**

I have reviewed the Stormwater Report, including the soil evaluation, computations, Long-term Pollution Prevention Plan, the Construction Period Erosion and Sedimentation Control Plan (if included), the Long-term Post-Construction Operation and Maintenance Plan, the Illicit Discharge Compliance Statement (if included) and the plans showing the stormwater management system, and have determined that they have been prepared in accordance with the requirements of the Stormwater Management Standards as further elaborated by the Massachusetts Stormwater Handbook. I have also determined that the information presented in the Stormwater Checklist is accurate and that the information presented in the Stormwater Report accurately reflects conditions at the site as of the date of this permit application.

Registered Professional Engineer Block and Signature



Signature and Date 2-10-2023

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<b>Project Type:</b> Is the redevelopment?	application for new development,	redevelopment,	or a mix of new and
☐ New developmen	t		
□ Redevelopment			
☐ Mix of New Deve	opment and Redevelopment		



# **Massachusetts Department of Environmental Protection**Bureau of Resource Protection - Wetlands Program

# **Checklist for Stormwater Report**

#### Checklist (continued)

env	<b>Measures:</b> Stormwater Standards require LID measures to be considered. Document what rironmentally sensitive design and LID Techniques were considered during the planning and design of project:
	No disturbance to any Wetland Resource Areas
	Site Design Practices (e.g. clustered development, reduced frontage setbacks)
	Reduced Impervious Area (Redevelopment Only)
$\boxtimes$	Minimizing disturbance to existing trees and shrubs
	LID Site Design Credit Requested:
	☐ Credit 1
	☐ Credit 2
	☐ Credit 3
$\boxtimes$	Use of "country drainage" versus curb and gutter conveyance and pipe
	Bioretention Cells (includes Rain Gardens)
	Constructed Stormwater Wetlands (includes Gravel Wetlands designs)
$\boxtimes$	Treebox Filter
	Water Quality Swale
	Grass Channel
	Green Roof
	Other (describe):
Sta	ndard 1: No New Untreated Discharges
$\boxtimes$	No new untreated discharges
	Outlets have been designed so there is no erosion or scour to wetlands and waters of the Commonwealth
$\boxtimes$	Supporting calculations specified in Volume 3 of the Massachusetts Stormwater Handbook included.



#### **Massachusetts Department of Environmental Protection**

Bureau of Resource Protection - Wetlands Program

## **Checklist for Stormwater Report**

Checklist (continued) Standard 2: Peak Rate Attenuation Standard 2 waiver requested because the project is located in land subject to coastal storm flowage and stormwater discharge is to a wetland subject to coastal flooding. Evaluation provided to determine whether off-site flooding increases during the 100-year 24-hour storm. Calculations provided to show that post-development peak discharge rates do not exceed predevelopment rates for the 2-year and 10-year 24-hour storms. If evaluation shows that off-site flooding increases during the 100-year 24-hour storm, calculations are also provided to show that post-development peak discharge rates do not exceed pre-development rates for the 100-year 24hour storm. Standard 3: Recharge Soil Analysis provided. Required Recharge Volume calculation provided. Required Recharge volume reduced through use of the LID site Design Credits. Sizing the infiltration, BMPs is based on the following method: Check the method used. Static
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 Simple Dynamic ☐ Dynamic Field¹ Runoff from all impervious areas at the site discharging to the infiltration BMP. Runoff from all impervious areas at the site is *not* discharging to the infiltration BMP and calculations are provided showing that the drainage area contributing runoff to the infiltration BMPs is sufficient to generate the required recharge volume. Recharge BMPs have been sized to infiltrate the Required Recharge Volume. Recharge BMPs have been sized to infiltrate the Required Recharge Volume only to the maximum extent practicable for the following reason: Site is comprised solely of C and D soils and/or bedrock at the land surface M.G.L. c. 21E sites pursuant to 310 CMR 40.0000 Solid Waste Landfill pursuant to 310 CMR 19.000 Project is otherwise subject to Stormwater Management Standards only to the maximum extent practicable. Calculations showing that the infiltration BMPs will drain in 72 hours are provided. Property includes a M.G.L. c. 21E site or a solid waste landfill and a mounding analysis is included.

<sup>&</sup>lt;sup>1</sup> 80% TSS removal is required prior to discharge to infiltration BMP if Dynamic Field method is used.



# **Massachusetts Department of Environmental Protection**Bureau of Resource Protection - Wetlands Program

# **Checklist for Stormwater Report**

Cł	necklist (continued)
Sta	indard 3: Recharge (continued)
	The infiltration BMP is used to attenuate peak flows during storms greater than or equal to the 10-year 24-hour storm and separation to seasonal high groundwater is less than 4 feet and a mounding analysis is provided.
	Documentation is provided showing that infiltration BMPs do not adversely impact nearby wetland resource areas.
Sta	ndard 4: Water Quality
The	E Long-Term Pollution Prevention Plan typically includes the following: Good housekeeping practices; Provisions for storing materials and waste products inside or under cover; Vehicle washing controls; Requirements for routine inspections and maintenance of stormwater BMPs; Spill prevention and response plans; Provisions for maintenance of lawns, gardens, and other landscaped areas; Requirements for storage and use of fertilizers, herbicides, and pesticides; Pet waste management provisions; Provisions for operation and management of septic systems; Provisions for solid waste management; Snow disposal and plowing plans relative to Wetland Resource Areas; Winter Road Salt and/or Sand Use and Storage restrictions; Street sweeping schedules; Provisions for prevention of illicit discharges to the stormwater management system; Documentation that Stormwater BMPs are designed to provide for shutdown and containment in the event of a spill or discharges to or near critical areas or from LUHPPL; Training for staff or personnel involved with implementing Long-Term Pollution Prevention Plan; List of Emergency contacts for implementing Long-Term Pollution Prevention Plan.
	A Long-Term Pollution Prevention Plan is attached to Stormwater Report and is included as an attachment to the Wetlands Notice of Intent.  Treatment BMPs subject to the 44% TSS removal pretreatment requirement and the one inch rule for calculating the water quality volume are included, and discharge:
	is near or to other critical areas
	is within soils with a rapid infiltration rate (greater than 2.4 inches per hour)
	involves runoff from land uses with higher potential pollutant loads.
	The Required Water Quality Volume is reduced through use of the LID site Design Credits.

☐ Calculations documenting that the treatment train meets the 80% TSS removal requirement and, if

applicable, the 44% TSS removal pretreatment requirement, are provided.



#### **Massachusetts Department of Environmental Protection**

Bureau of Resource Protection - Wetlands Program

### **Checklist for Stormwater Report**

Checklist (continued) Standard 4: Water Quality (continued) The BMP is sized (and calculations provided) based on: ☐ The ½" or 1" Water Quality Volume or ☐ The equivalent flow rate associated with the Water Quality Volume and documentation is provided showing that the BMP treats the required water quality volume. The applicant proposes to use proprietary BMPs, and documentation supporting use of proprietary BMP and proposed TSS removal rate is provided. This documentation may be in the form of the propriety BMP checklist found in Volume 2, Chapter 4 of the Massachusetts Stormwater Handbook and submitting copies of the TARP Report, STEP Report, and/or other third party studies verifying performance of the proprietary BMPs. A TMDL exists that indicates a need to reduce pollutants other than TSS and documentation showing that the BMPs selected are consistent with the TMDL is provided. Standard 5: Land Uses With Higher Potential Pollutant Loads (LUHPPLs) ☐ The NPDES Multi-Sector General Permit covers the land use and the Stormwater Pollution Prevention Plan (SWPPP) has been included with the Stormwater Report. ☐ The NPDES Multi-Sector General Permit covers the land use and the SWPPP will be submitted *prior* to the discharge of stormwater to the post-construction stormwater BMPs. The NPDES Multi-Sector General Permit does *not* cover the land use. LUHPPLs are located at the site and industry specific source control and pollution prevention measures have been proposed to reduce or eliminate the exposure of LUHPPLs to rain, snow, snow melt and runoff, and been included in the long term Pollution Prevention Plan. All exposure has been eliminated. All exposure has **not** been eliminated and all BMPs selected are on MassDEP LUHPPL list. The LUHPPL has the potential to generate runoff with moderate to higher concentrations of oil and grease (e.g. all parking lots with >1000 vehicle trips per day) and the treatment train includes an oil grit separator, a filtering bioretention area, a sand filter or equivalent. Standard 6: Critical Areas The discharge is near or to a critical area and the treatment train includes only BMPs that MassDEP has approved for stormwater discharges to or near that particular class of critical area. Critical areas and BMPs are identified in the Stormwater Report.



#### **Massachusetts Department of Environmental Protection**

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### **Checklist for Stormwater Report**

#### Checklist (continued)

Standard 7: Redevelopments and Other Projects Subject to the Standards only to the maximum extent practicable

The project is subject to the Stormwater Management Standards only to the maximum Extent

	acticable as a:
	Limited Project
	Small Residential Projects: 5-9 single family houses or 5-9 units in a multi-family development provided there is no discharge that may potentially affect a critical area.  Small Residential Projects: 2-4 single family houses or 2-4 units in a multi-family development with a discharge to a critical area  Marina and/or boatyard provided the hull painting, service and maintenance areas are protected from exposure to rain, snow, snow melt and runoff
$\boxtimes$	Bike Path and/or Foot Path
$\boxtimes$	Redevelopment Project
	Redevelopment portion of mix of new and redevelopment.
exp The imp in \ the and	rtain standards are not fully met (Standard No. 1, 8, 9, and 10 must always be fully met) and an planation of why these standards are not met is contained in the Stormwater Report. The project involves redevelopment and a description of all measures that have been taken to prove existing conditions is provided in the Stormwater Report. The redevelopment checklist found volume 2 Chapter 3 of the Massachusetts Stormwater Handbook may be used to document that a proposed stormwater management system (a) complies with Standards 2, 3 and the pretreatment of structural BMP requirements of Standards 4-6 to the maximum extent practicable and (b) proves existing conditions.

#### Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control

A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan must include the following information:

- Narrative;
- Construction Period Operation and Maintenance Plan;
- Names of Persons or Entity Responsible for Plan Compliance;
- Construction Period Pollution Prevention Measures;
- Erosion and Sedimentation Control Plan Drawings;
- Detail drawings and specifications for erosion control BMPs, including sizing calculations;
- Vegetation Planning;
- Site Development Plan;
- Construction Sequencing Plan;
- Sequencing of Erosion and Sedimentation Controls;
- Operation and Maintenance of Erosion and Sedimentation Controls;
- Inspection Schedule;
- Maintenance Schedule;
- Inspection and Maintenance Log Form.
- A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan containing the information set forth above has been included in the Stormwater Report.



# **Massachusetts Department of Environmental Protection**Bureau of Resource Protection - Wetlands Program

# **Checklist for Stormwater Report**

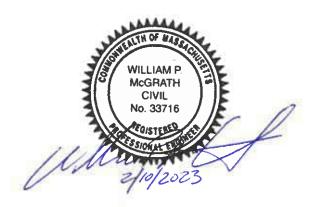
Checklist (continued)

	andard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control ontinued)
	The project is highly complex and information is included in the Stormwater Report that explains why it is not possible to submit the Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan with the application. A Construction Period Pollution Prevention and Erosion and Sedimentation Control has <i>not</i> been included in the Stormwater Report but will be submitted <i>before</i> land disturbance begins.
	The project is <i>not</i> covered by a NPDES Construction General Permit.
	The project is covered by a NPDES Construction General Permit and a copy of the SWPPP is in the Stormwater Report.
$\boxtimes$	·
Sta	andard 9: Operation and Maintenance Plan
$\boxtimes$	The Post Construction Operation and Maintenance Plan is included in the Stormwater Report and includes the following information:
	Name of the stormwater management system owners;
	☑ Party responsible for operation and maintenance;
	Schedule for implementation of routine and non-routine maintenance tasks;
	☐ Plan showing the location of all stormwater BMPs maintenance access areas;
	☐ Description and delineation of public safety features;
	☐ Estimated operation and maintenance budget; and
	☐ Operation and Maintenance Log Form.
	The responsible party is <b>not</b> the owner of the parcel where the BMP is located and the Stormwater Report includes the following submissions:
	A copy of the legal instrument (deed, homeowner's association, utility trust or other legal entity) that establishes the terms of and legal responsibility for the operation and maintenance of the project site stormwater BMPs;
	A plan and easement deed that allows site access for the legal entity to operate and maintain BMP functions.
Sta	andard 10: Prohibition of Illicit Discharges
	The Long-Term Pollution Prevention Plan includes measures to prevent illicit discharges;
	An Illicit Discharge Compliance Statement is attached;
	NO Illicit Discharge Compliance Statement is attached but will be submitted <i>prior to</i> the discharge of any stormwater to post-construction BMPs.

# **Grove Street Improvements – Phase 2**

February 2023

### STORMWATER MANAGEMENT REPORT





701 George Washington Hwy Lincoln, Rhode Island 02865 401.333.2382 www.BETA-Inc.com

# Grove Street Improvements – Phase 2 Franklin, MA

### STORMWATER MANAGEMENT REPORT

Prepared by: BETA GROUP, INC. Prepared for: Town of Franklin

February 2023

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Appendix B – Construction Period Pollution Prevention Plan and Operation and Maintenance Plan

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Appendix I – Environmental Resources Map



#### 1.0 Introduction

In accordance with the Massachusetts Wetlands Protection Act, M.G.L. Chapter 131, Section 40, and the Town of Franklin Wetlands Ordinance, BETA Group, Inc. (BETA) has completed the Stormwater Report for submission to the Massachusetts Department of Environmental Protection (MADEP) on behalf of the Town of Franklin. The proposed project includes the widening, proposed milling and overlay of Grove Street, construction of a shared-use path, installation of new curbing and wheelchair ramps, construction of low retaining walls, and installation of a new closed drainage system with hydrodynamic separators.

A locus map of the project area is shown in Figure 1 – Project Locus Map.

#### 2.0 PROJECT SUMMARY

The proposed project consists of reconstruction of a 1.1-mile segment of Grove Street from Tobacco Road/Rosewood Lane (meeting with the end of Phase 1) to Kenwood Circle. The project limits are shown in Figure 1. The purpose of the project is to construct a shared use path along the north/west side of Grove Street, which will provide improved pedestrian and bicycle access along the corridor and connect to the existing Southern New England Trunkline Trail (SNETT). The existing roadway width is generally between 28 feet and 40 feet wide with 2' shoulders and no sidewalks throughout the project limits.

The improvements will include a cross section with 12-foot travel lanes, 2-foot shoulders, enhanced pavement conditions through a combination of reconstruction/reclamation and resurfacing, and providing bicycle and pedestrian accommodations through an 8-foot to 10-foot shared use path. The project will also include upgrades to the existing drainage system to improve runoff collection and stormwater quality. The new shared use path is proposed along the north/west side of Grove Street.



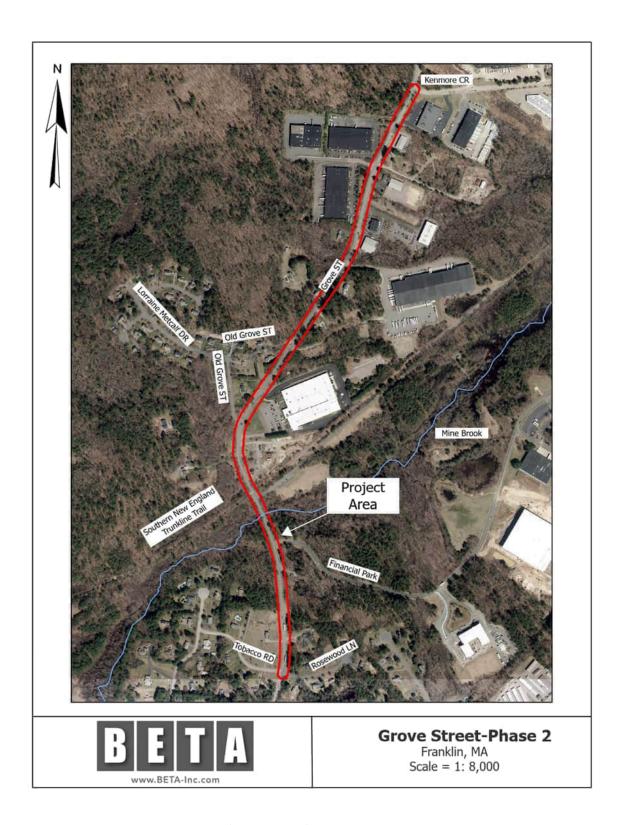


Figure 1 – Project Locus Map



#### 3.0 Existing Conditions

The Phase 2 project area is approximately 7 acres and begins at the intersection of Tobacco Road and Grove Street in Franklin (Figure 1), which meets the end of the Phase 1 Grove Street project. Grove Street is a two-lane bituminous asphalt roadway with various commercial and industrial properties as well as some private residences along its length. The project corridor is adjacent to Town land (for public wellhead protection) as well as State land. There is generally no curbing or berm on either side. At several locations, there are wetlands adjacent to the roadway, and there are several existing culverts. Near the beginning of the project (~STA 23+00 LT), there is an entrance to the Southern New England Trunkline Trail (SNETT), and one major objective of this project is to provide improved access to this existing trail.

There are wetland resource areas within 100 feet of the proposed activities, and the site also includes a wellhead protection area (Zones I and II).

#### SITE PARAMETERS

#### Soil Classification

Please refer to Appendix F – Soil Map. According to the Soil Survey of Norfolk County, Massachusetts, prepared by the US Department of Agriculture, Natural Resources Conservation Service, Underlying soils within the project area consists of nine soil types, which are predominately Hydrologic Soil Group (HSG) A. The project also includes smaller areas of soils that are HSG A/D, B/D, and Urban land. For areas with HSG A/D, A soils were assumed to be dominant within the roadway area, and for areas with HSG B/D, B soils were assumed to be dominant within the roadway. For roadway soils classified as urban land, HSG A was assumed, as that is the classification of soils directly adjacent to that roadway segment.

Detailed individual descriptions of these soils are not provided herein but may be found in the referenced USDA soil survey.

Hydrologic Soil Groups (HSG) are based on estimates of runoff potential. Soils are assigned to one of four groups, according to the rate of water infiltration when 1) the soils are not protected by vegetation, 2) are thoroughly wet, and 3) receive precipitation from long-duration storms.

Per the soil survey, the general characteristics of the four (4) hydrologic soil groups are as follows:

<u>Group A</u> – Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

<u>Group B</u> – Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

<u>Group C</u> – Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

<u>Group D</u> – Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high-water



table, soils that have a clay pan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

As depicted in the Appendix F, the underlying soils within the upland project area belong mostly to HSG A, meaning that the project area likely has a high infiltration rate with a low potential for runoff.

#### Subsurface Investigation

As a part of the Phase 1 work, a subsurface investigation (in the form of a soil evaluation) was performed onsite to confirm the condition of the existing soils as well as determine the seasonal high groundwater levels.

The test pit was performed at the location of what is now the newly-constructed stormwater BMP, off the east side of Grove Street approximately 100' south of Rosewood Lane (~STA 5+00 RT). The soil was classified as sand. Seasonal high groundwater was not found within 10' of the surface. The results from the Phase 1 soil evaluation can be found in Appendix E.

#### **Existing Drainage Collection**

Stormwater runoff along Grove Street currently sheet flows off the roadway into the existing wetlands on both sides of the road. There is a small existing closed drainage system trunkline in the vicinity of the intersection with Old Grove Street as well as some catch basins near Kenwood Circle.

For an overview of existing drainage catchment areas and their characteristics, refer to the Watershed Plans in Appendix C.

Key features in and around the project area include wetland resource areas, FEMA Flood Zones, and Zone II areas.

#### **Wetland Resources**

Wetland resource areas along the project alignment were delineated in 2020 by BETA Group, Inc. A copy of the Wetland Report is included in the Appendix C. The Wetland Report describes wetland resource areas subject to Protection under the Massachusetts Wetlands Protection Act, the federal Clean Water Act, the Massachusetts Clean Waters Act, and local bylaws.

#### Flood Zone Classification

Please refer to Appendix G – FEMA Flood Map. According to the Flood Insurance Rate Maps (FIRM) for Norfolk County, Map Number 25021C0316E, effective date July 17, 2012, the northern portion of Mine Brook, which flows through a culvert under under Grove Street (~STA 21+00), is located within FEMA Floodway and Flood Zone AE. There is a Bordering Land Subject to Flooding (BLSF) associated with this flood zone.

Zone AE Flood Hazard areas indicate the limits of the 100-year floodplain, with an associated Base Flood Elevation (BFE).



#### 4.0 Proposed Conditions

The proposed project includes the addition of a paved shared use pathway along the north/west side of Grove Street, as well as proposed milling and overlay of Grove Street, installation of new curbing and wheelchair ramps, installation of tree wells, installation of a new closed drainage system with hydrodynamic separators, and a connection to a previously constructed infiltration basin.

These measures will improve the stormwater characteristics at the site by providing water quality pretreatment and stormwater recharge for the proposed impervious area.

While the roadway impervious area will be reduced, the overall impervious area for the project will increase due to the addition of shared use path. The Town of Franklin will be responsible for the annual inspection and maintenance of the new stormwater management system.

#### STORMWATER MANAGEMENT

The proposed project is a redevelopment project. The following describes the methodology used in the analysis and design of the stormwater management system for the roadways.

#### PROJECT AREA ANALYSIS AND STORMWATER REQUIREMENTS CALCULATIONS

The overall project area was analyzed to determine the stormwater management requirements for the project; specifically, the groundwater recharge volume (ReV) and water quality volume (WQV) requirements were determined, based on the existing and proposed project-wide impervious areas.

#### Existing, Proposed & Net Impervious Areas

The existing, proposed, and net increase impervious areas within the project limits were determined and the net increase to impervious area was used in the calculations of the required ReV and WQV. Impervious areas consist of existing roadways, bituminous and cement concrete sidewalks, and paved driveways within and to the extents of the project limits of disturbance; impervious areas outside of the project limits of disturbance (e.g. driveways, buildings, walls, impervious site features) were not included in the determinations of existing and proposed impervious areas.

The net (new) impervious area for the project is 33,270 s.f. This represents a net increase of 14%.

Table 1 Changes to Impervious Areas

Existing Impervious	New Impervious (Pathway)	New Impervious (Roadway)	Net New Impervious	Total Impervious
204,362 SF	43,038 SF	-9,769 SF	33,270 SF	237,632 SF



#### Minimum ReV Requirement

The required recharge volume (ReV) is the product of the total new impervious area created by the project and a target recharge factor (measured in inches of rainfall per square foot of impervious area) for the project area. The target recharge factor is based on the HSG(s) of the underlying soil(s) present within the project area.

The impervious area within the project site is located where the soil type is predominantly HSG A with a relatively small impervious area within HSG B soils. The recharge target for A soils is 0.6 in/s.f., while B is 0.35 in/s.f. Based on 26,145 s.f. of new impervious area in A soils and 7,125 s.f. in B soils, the minimum ReV required calculates to 1,521 c.f.

#### Minimum WQV Requirement

The Franklin Bylaw 21-867 states that redevelopment projects are required to retain the volume of runoff equivalent to 0.8 inches multiplied by the post construction impervious area. This bylaw applies for 22,775 s.f. of the project. However, since 19,246 s.f. of the project area is classified as a Zone II well protection area, the required water quality treatment volume (WQV) for that area must be equal to 1.0 inch of rainfall over the total net impervious area created by the proposed project. Based on the new impervious areas, the minimum WQV for the project is 3,198 c.f. Pre-treatment will be provided by tree wells and deep sump catch basins while hydrodynamic separators and an existing infiltration basin will provide a portion of the water quality treatment. The required water quality volume of 3,198 c.f. is greater than the required recharge volume of 1,521 c.f. and will be used as the target treatment volume.

The Phase 1 proposed site stormwater management system was designed to provide excess storage capacity (more than 4,000 c.f. total). Therefore, there is additional capacity available for water quality treatment in this recently constructed basin. Due to site grading constraints, only a portion of the Phase 2 proposed stormwater water quality volume (~628 c.f.) can be directed to the Infiltration Basin for treatment.

#### Drawdown

The required drawdown for an infiltration BMP is 72 hours to ensure that the BMP drains completely between storm events. Using a Hydraulic Conductivity factor of 8.27 inches/hour (See Table 2.3.3 of the Stormwater Manual), it was determined that the drawdown of the infiltration system is 2.63 hours (based on drawing down the sum of the design volumes from Phase 1 and new impervious volume contributing to the basin from Phase 2), which complies with the 72-hour threshold.

#### STORMWATER MANAGEMENT SYSTEM ANALYSIS AND DESIGN

The proposed stormwater management system will collect, pretreat, and treat surface runoff from Grove Street to discharge into a recently constructed infiltration basin as well as two hydrodynamic separators and several tree wells. As there are no existing stormwater treatment measures on site, the implementation of the proposed system will result in an overall decrease in overall post development peak runoff from the site for design storms including the 2-year, 10-year, 25-year, and 100-year events.



Two proposed hydrodynamic separators and the existing infiltration basin will treat the required water quality volume for the proposed impervious areas.

#### **Closed Drainage Systems**

The proposed closed system is designed with deep sump catch basins and hydrodynamic separators to provide initial TSS removal. It is anticipated that this train of pretreatment devices at each of the two proposed outfalls will provide 96% TSS removal prior to the discharge to design points. Depending on the closed system, TSS removal varies from 25% to 96%. For TSS removal worksheets, please refer to Appendix D.

#### Infiltration Basin System

A portion of the proposed drainage system will discharge to an existing infiltration basin located on the east side of Grove Street and south of Rosewood Lane. This recently-constructed stormwater infiltration basin from the Grove Street Phase 1 project has excess capacity and will be modified to accept a portion of additional flows from Phase 2 areas. From Phase 2, the infiltration basin is anticipated to provide infiltration from approximately 7,535 s.f. of impervious area (about 3,193 s.f. from the proposed shared use path).

For an overview of proposed drainage catchment areas and their characteristics, refer to the Watershed Plans in Appendix C.

Table 5 lists the proposed BMPs and provides a description of each.

Table 2 Existing/Proposed BMPs

BMP	Description
BMP 1 – Existing Infiltration Basin	Grove Street Station 5+00 RT
BMP 2 – Hydrodynamic Separator	Grove Street Station 20+52 LT
BMP 3 – Hydrodynamic Separator	Grove Street Station 47+08 LT
Tree Filters	Various Locations – See Plans



#### 5.0 IMPAIRED WATERS AND TMDLS

A portion of this project will discharge to Mine Brook. This water body has the following impairments based on MassDEP Year 2018/2020 Integrated List of Waters, also known as the 303(d) list:

Table 3 Impaired Waters and TMDL Information

Water Body	Water Body ID	Impairments
Mine Brook	MA72-14	(Habitat Assessment*); E. Coli, Temperature

<sup>\*</sup>TMDL not required

#### **6.0 STORMWATER MANAGEMENT STANDARDS**

As demonstrated below, the proposed Project complies with the MassDEP Stormwater Management Standards (the Standards) to the maximum extent practicable. The Project is a redevelopment project, therefore, per 310 CMR 10.05(6)(k)(7), the project must only meet Standards 2, 3, 4, 5 and 6 to the maximum extent practicable. Existing stormwater discharges shall comply with Standard 1 only to the maximum extent practicable.

#### 6.1 STANDARD 1 - MET (TO THE MAXIMUM EXTENT PRACTICABLE)

No new stormwater conveyances (e.g. outfalls) may discharge untreated stormwater directly to or cause erosion in wetlands or waters of the Commonwealth.

The Project has been designed to comply with Standard 1 to the maximum extent practicable. All new outfalls are designed with headwalls and stone for pipe ends to prevent erosion to the receiving water bodies and wetlands.

There will be no new untreated discharges created as part of this project. Existing discharges will be improved to the maximum extent practicable through the installation of deep sump catch basins. Stormwater generated from the site will be captured by the closed drainage system and treated through proposed deep sump catch basins and hydrodynamic separators at new discharge locations. A portion of the project area will also be infiltrated through the stormwater basin constructed during Phase 1.

#### 6.2 STANDARD 2 – MET (TO THE MAXIMUM EXTENT PRACTICABLE)

Stormwater management systems shall be designed so that post-development peak discharge rates do not exceed pre-development peak discharge rates. This Standard may be waived for discharges to land subject to coastal storm flowage as defined in 310 CMR 10.04.

The Project has been designed to comply with Standard 2 to the maximum extent practicable. There will be an increase to the impervious area as a result of this project. There will be several changes to the drainage collection and conveyance system in order to incorporate water quality treatment measures and conform to roadway standards. Two new BMPs are proposed as part of the drainage improvements, and



several tree filters will also be used as well as a reduction in roadway impervious area. However, the new shared use path will result in a net increase in impervious area.

In the proposed condition, the roadway and shared use path will be collected in a closed drainage network and routed to deep sump catch basins and hydrodynamic separators. A portion will also be routed to the existing stormwater basin that was recently constructed in Phase 1. The basin retains and infiltrates all the Phase 1 stormwater runoff up to the 10-year storm as well as a portion of the Phase 2 stormwater runoff.

In order to provide adequate room for the proposed shared use path and guardrail, a few small areas of existing wetland will be permanently disturbed in the vicinity of Sta 46+30 LT to Sta 48+00 LT (504 s.f. total). Wetland replication that amounts to at least double the permanent impact will be provided in vicinity of the impacts. Additionally, while there is no permanent wetland impact near Sta 23+50 LT, compensatory flood storage will be provided in this area due to impacts on the 100-yr floodplain by the proposed rockfill slope at this location.

Hydrologic analyses of the site were conducted under existing and proposed conditions for the 2, 10, 25, and 100-year storms.

The results of the analyses indicate that there will be an increase of the proposed peak runoff rates and volumes to the adjacent wetlands. Therefore, this standard is not fully met. However, due to the project being a shared use path construction, this standard only needs to be met to the greatest extent practicable. Due to Right-of-Way (ROW) constraints and abutting state-owned forest (which falls under Article 97 protection), areas for potential BMPs for infiltration and attenuation are limited within the project. Although the peak discharges increase slightly, no impact to the 100-year flood elevation is anticipated since the overall size of the receiving watershed is comparatively much larger than the increase in impervious area from the project.

Refer to Appendix D for full results of the existing and proposed Autodesk Storm and Sanitary Sewers analysis as well as partial HydroCAD analysis for the area contributing to the infiltration basin from Phase 1.

To verify that the existing basin from Phase 1 has adequate capacity to treat a portion of the Phase 2 water quality volume, a limited HydroCAD analysis was performed using a modified version of the Phase 1 HydroCAD analysis. This modified model includes the addition of flows from subcatchment area PR-sub-1 into Basin #1 via a catch basin with a flow diversion weir. The flow diversion is present to ensure only flows from the water quality storm will be directed to the existing infiltration basin. Rainfall depths used in the HydroCAD model are listed below:

#### Rainfall Depths (in)

Design Storm Event	Rainfall Depth (in)
2-year	3.36
_10-year	5.23
25-year	6.39
100-year	8.19



Drainage system pipes were designed utilizing peak flows from the Rational Method for the 10-year storm event utilizing AutoCAD Storm and Sanitary Analysis 2020.

The table below provides a summary of peak rates for each design point under existing and proposed conditions. Appendix D provides computations and supporting information regarding the hydraulic and hydrologic modeling.

	Existing				Pro	posed		
Design Point	2-year	10-year	25-year	100- year	2-year	10-year	25-year	100- year
DP-1*	0.34	0.72	0.99	1.44	0.61	1.07	1.38	1.88
DP-5	0.81	1.23	1.50	1.90	2.47	3.79	4.63	5.86
DP-6	0.40	0.61	0.74	0.93	0.51	0.75	0.90	1.11
DP-7	1.24	1.89	2.28	2.92	1.35	2.01	2.40	3.00
DP-10	0.56	0.85	1.03	1.31	0.71	1.08	1.30	1.63
DP-13	1.04	1.59	1.92	2.45	1.03	1.58	1.92	2.43
DP-16	1.76	2.69	3.26	4.14	2.03	3.10	3.70	3.82
DP-18	2.30	3.51	4.27	5.41	2.39	3.65	4.43	5.66
DP-20	1.00	1.52	1.85	2.35	2.12	3.24	3.92	4.99

Peak Discharge Rates (cfs)

The results of the analysis indicate that post-development peak discharge rates will increase at most design points from pre-development discharge rates due to the increase in impervious area from the shared use pathway and addition of a closed drainage system. It should be noted that for DP-1, the increase in peak flow is less than it would be due to a portion of the flow being directed to the infiltration basin from Phase 1. The watershed figures and supporting analysis can be found in Appendix C.

#### 6.3 STANDARD 3 – MET (TO THE MAXIMUM EXTENT PRACTICABLE)

Loss of annual recharge to groundwater shall be eliminated or minimized through the use of infiltration measures including environmentally sensitive site design, low impact development techniques, stormwater best management practices, and good operation and maintenance. At a minimum, the annual recharge from the post-development site shall approximate the annual recharge from predevelopment conditions based on soil type. This Standard is met when the stormwater management system is designed to infiltrate the required recharge volume as determined in accordance with the Massachusetts Stormwater Handbook.

The Project has been designed to comply with Standard 3 to the maximum extent practicable. The stormwater management design infiltrates a portion of the required recharge volume to groundwater in the infiltration basin that was constructed as part of Phase 1. While this basin has adequate capacity to provide an additional recharge volume from Phase 2, the site grading and surface cover will only allow around 628 c.f. to be directed to the infiltration basin for treatment. Assuming 7.6 c.f. of recharge volume per tree filter leads to an additional 45.8 c.f. of recharge volume that can be provided.



<sup>\*</sup>For DP-1, Peak Discharge Rates were calculated using HydroCAD, in order to model that a portion of proposed flows being directed to the Phase 1 infiltration basin BMP.

So, while 1,521 c.f. of recharge is required, only 673.8 c.f. of recharge volume is able to be provided as part of this project. It is worth noting, however that there is more than 3,000 linear feet of proposed grass buffer that will be able to intercept stormwater flowing off the new pavement of the shared use path. Some portion of this flow will infiltrate into groundwater before reaching the roadway gutter.

#### 6.4 STANDARD 4 – MET (TO THE MAXIMUM EXTENT PRACTICABLE)

Stormwater management systems shall be designed to remove 80% of the average annual post-construction load of Total Suspended Solids (TSS). This Standard is met when:

- a. Suitable practices for source control and pollution prevention are identified in a long-term pollution prevention plan, and thereafter are implemented and maintained;
- b. Structural stormwater best management practices are sized to capture the required water quality volume determined in accordance with the Massachusetts Stormwater Handbook; and c. Pretreatment is provided in accordance with the Massachusetts Stormwater Handbook.

The Project has been designed to comply with Standard 4 to the maximum extent practicable as this is a redevelopment project. Stormwater control measures have been sized to treat a portion of the required water quality volume (WQV). The addition of off-line deep sump catch basins and tree filters will also provide some water quality treatment to stormwater entering the resource areas. While the proposed tree filters do not directly connect to catch basins, they do intercept the gutter flow prior to it reaching the downstream catch basin. This ensures that treatment of gutter flows are provided until the tree filter becomes bypassed by larger storm events or clogging. Where existing closed systems are being modified, a TSS removal of at least 25% is achieved, assuming installation of deep-sump catch basins. For areas where entirely new closed systems are present, the TSS removal rates range from 85-96%. TSS Removal worksheets can be found in Appendix D.

It should be noted that the runoff leaving the roadway and ultimately entering the wetland resource areas currently receives no treatment at all; therefore, the proposed mitigation features, while not achieving the entire treatment standard, will still result in a significant improvement to the water quality of the runoff.

#### 6.5 STANDARD 5 - N/A

For land uses with higher potential pollutant loads, source control and pollution prevention shall be implemented in accordance with the Massachusetts Stormwater Handbook to eliminate or reduce the discharge of stormwater runoff from such land uses to the maximum extent practicable. If through source control and/or pollution prevention all land uses with higher potential pollutant loads cannot be completely protected from exposure to rain, snow, snow melt, and stormwater runoff, the proponent shall use the specific structural stormwater BMPs determined by the Department to be suitable for such uses as provided in the Massachusetts Stormwater Handbook. Stormwater discharges from land uses with higher potential pollutant loads shall also comply with the requirements of the Massachusetts Clean Waters Act, M.G.L. c. 21, §§ 26-53 and the regulations promulgated thereunder at 314 CMR 3.00, 314 CMR 4.00 and 314 CMR 5.00.



The project area does not qualify as an area with higher potential pollutant loads; therefore, this standard is not applicable.

#### 6.6 STANDARD 6 - MET

Stormwater discharges within the Zone II or Interim Wellhead Protection Area of a public water supply, and stormwater discharges near or to any other critical area, require the use of the specific source control and pollution prevention measures and the specific structural stormwater best management practices determined by the Department to be suitable for managing discharges to such areas, as provided in the Massachusetts Stormwater Handbook. A discharge is near a critical area if there is a strong likelihood of a significant impact occurring to said area, taking into account site-specific factors. Stormwater discharges to Outstanding Resource Waters and Special Resource Waters shall be removed and set back from the receiving water or wetland and receive the highest and best practical method of treatment. A "storm water discharge" as defined in 314 CMR 3.04(2)(a)1 or (b) to an Outstanding Resource Water or Special Resource Water shall comply with 314 CMR 3.00 and 314 CMR 4.00. Stormwater discharges to a Zone I or Zone A are prohibited unless essential to the operation of a public water supply.

Approximately 51% of the project is located within Zone II Wellhead Protection Area. The new outfalls located at Station 20+65 LT (within Zone II) and 47+06 LT (outside Zone II) are designed with headwalls and stone for pipe ends to prevent erosion to the receiving wetlands. The proposed outfalls are set back from the existing wetlands. Hydrodynamic separators and deep sump catch basins are proposed as part of this system. Stormwater BMPs were considered in these locations but were determined to be impractical due to close proximity to wetlands and limited area within the right-of-way.

Appendix H shows the Wellhead Protection Areas in the vicinity of the project site.

The work within the Zone II area of the project consists of full depth path construction, milling and overlay, slope grading, and construction of guardrail and retaining walls/moment slab. Minor roadway widening is proposed to provide a consistent cross section meeting minimum MassDOT requirements. No stormwater discharges are proposed within Zone I areas.

#### 6.7 STANDARD 7 - MFT

A redevelopment project is required to meet the following Stormwater Management Standards only to the maximum extent practicable: Standard 2, Standard 3, and the pretreatment and structural best management practice requirements of Standards 4, 5, and 6. Existing stormwater discharges shall comply with Standard 1 only to the maximum extent practicable. A redevelopment project shall also comply with all other requirements of the Stormwater Management Standards and improve existing conditions.

The proposed project is a redevelopment project. As discussed above, the standard has been met to the maximum extent practicable.



#### 6.8 STANDARD 8 - MET

A plan to control construction-related impacts including erosion, sedimentation and other pollutant sources during construction and land disturbance activities (construction period erosion, sedimentation, and pollution prevention plan) shall be developed and implemented.

Soil and erosion control shall be provided during construction by means of compost filter socks and catch basin silt sacks. A Construction Period Pollution Prevention and Erosion and Sediment Control Plan has been developed for the project site and is included in Appendix B.

#### 6.9 STANDARD 9 - MFT

All stormwater management systems must have an operation and maintenance plan to ensure that systems function as designed.

The long-term post-construction implementation of the Operation and Maintenance (O&M) plan for the stormwater structures within the project area will be the responsibility of the Town of Franklin. The O&M plan is attached to this report in Appendix H.

#### 6.10 STANDARD 10 - MET

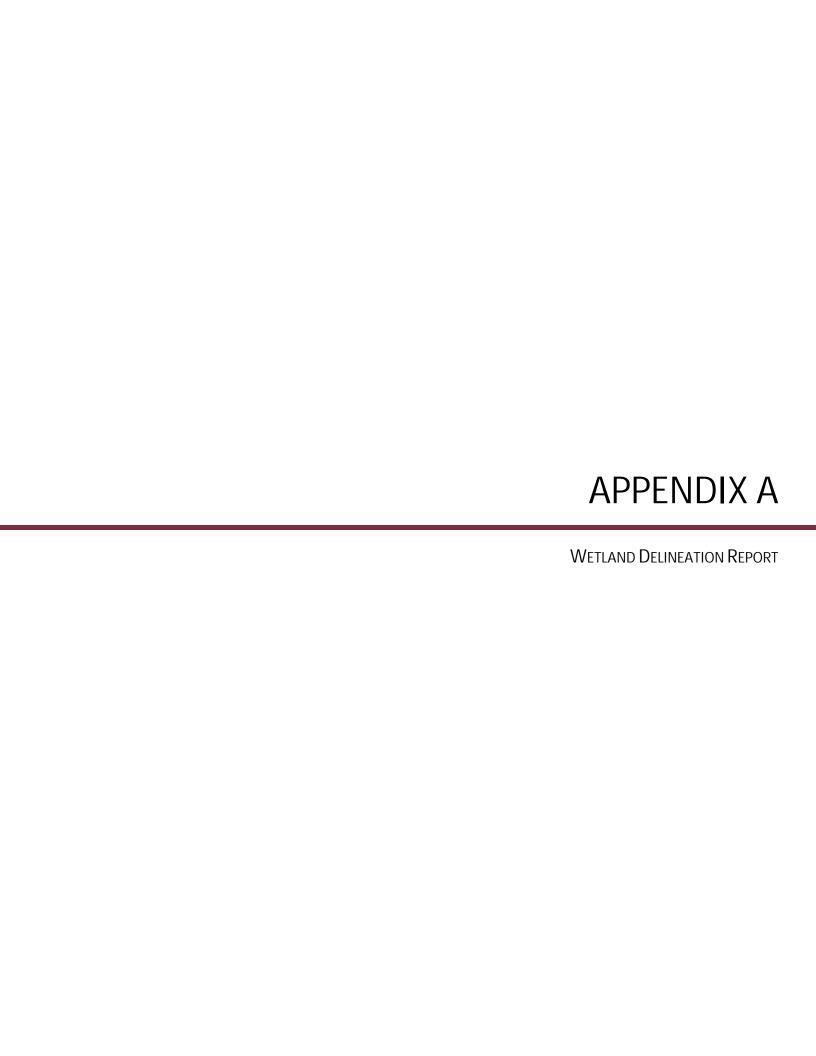
All illicit discharges to the stormwater management system are prohibited.

The project's stormwater management system, as shown on the plans submitted with this report, have been designed in full compliance with Standard 10. The project area does not have any known illicit connections.

#### 7.0 CONCLUSION

While the Grove Street Improvements Phase 2 project will result in a net increase in impervious areas, this is due wholly to the addition of a paved shared use path. By using a combination of hydrodynamic separators, tree wells, and taking advantage of excess treatment capacity within an existing stormwater basin, the effects of the project on adjacent wetlands will be mitigated to the greatest extent practicable. Treatment of stormwater runoff has been provided and meets the requirements set forth by the Massachusetts Department of Environmental Protection and Town of Franklin Bylaws to the greatest extent practicable. Any unavoidable impacts to Resource Areas are to be mitigated by replicating new wetlands.







#### Resource Area Boundary Delineation Grove Street Franklin, Massachusetts

#### January 4, 2021

On May 13, 2021, BETA Group, Inc. (BETA) conducted resource area boundary delineations along a portion of the Grove Street public right-of-way in Franklin, Massachusetts. This report describes resource areas Subject to Protection under the Massachusetts Wetlands Protection Act (M.G.L. Chapter 131 Section 40) (the Act), the federal Clean Water Act (33 U.S.C. §1251 et seq (1972)), the Massachusetts Clean Waters Act (MGL Chapter 21 Section 26-53), and the Town of Franklin Wetlands Protection Bylaw (Chapter 181) (the Bylaw) that exist on the site and methodology used to delineate their boundaries.

#### **Site Description**

The Site consists of an approximately 6,500-linear foot portion of the Grove Street public right-of-way in Franklin, Massachusetts, from its intersection with Washington Street to its intersection with Kenwood Circle. Land uses along the Site corridor generally consist of residential and commercial parcels. In addition, the Franklin State Forest abuts portions of the west side of the Site and Town of Franklin public water supply wells exist to the east of the Site (Figure 1 – Site Locus). The Site is bisected by Mine Brook (Figure 2 – Environmental Resources) as well as the Southern New England Trunkline Trail (SNETT), an improved but unpaved multi-use path. Existing improvements at the Site include a two-lane bituminous roadway, guardrails, stormwater management infrastructure, and vegetated roadway shoulders.

According to the USDA Natural Resources Conservation Service – Soil Survey, mapped soils on the Site and in the vicinity of the Site are classified as Udorthents-sandy, Urban land, Merrimac fine sandy loam, Sudbury fine sandy loam, Hinckley loamy sand, Hollis-Rock outcrop-Charlton complex, Carlton-Hollis-Rock outcrop complex, Whitman fine sandy loam, Ridgebury fine sandy loam, Swansea muck, and Scarboro/Birdsall soils. Our field work generally confirmed the soil types within the Site. The *Custom Soil Resource Report for Norfolk and Suffolk Counties, Massachusetts* is attached.

State jurisdictional resource areas identified on the Site include Bank (to perennial and intermittent streams), Bordering Vegetated Wetlands (BVW), Land Under Water (LUW), Bordering Land Subject to Flooding (BLSF), and Riverfront Area (RA). The MassGIS database was used as the initial step in identifying critical areas on or within proximity to the Site that would be examined more closely if construction activities are proposed. The table below describes selected environmentally critical categories as determined through MassGIS.

**Table 1: Selected MassGIS Environmental Data Layers** 

Mapped Resource On or Within Proximity to Site	Yes	No
Area of Critical Environmental Concern		✓
NHESP Certified Vernal Pool	1	✓
NHESP Potential Vernal Pool	<b>✓</b>	
NHESP Estimated Habitat of Rare Wildlife		✓
NHESP Priority Habitat of Rare Species		✓
Outstanding Resource Waters		✓
FEMA Flood Zones	✓	
Surface Water Protection Area (Zones A and B)		✓

Mapped Resource On or Within Proximity to Site	Yes	No
Interim Wellhead Protection Area		<b>✓</b>
Zone I Wellhead Protection Area	✓	
Zone II Wellhead Protection Area	✓	
Wild and Scenic River		✓
DFW Coldwater Fisheries Resource	<b>√</b> 1	

Source: MassGIS

#### Jurisdictional Wetland Resource Areas - Massachusetts Wetlands Protection Act

A Site inspection was conducted by BETA's Wetland Scientists on May 13, 2021 to identify and delineate the boundary of resource areas on the Site and in the immediate vicinity of the Site. Resource area boundaries were identified and delineated in accordance with methods developed by the Massachusetts Department of Environmental Protection's *Delineating Bordering Vegetated Wetlands Under the Massachusetts Wetlands Protection Act*, dated 1995, as well as definitions set forth in the Wetland Regulations, 310 CMR 10.00. Five (5) Areas Subject to Protection under the Act exist at the Site and are described below.

#### Bank (Inland) - 310 CMR 10.54

According to 310 CMR 10.54(2), the definition of a Bank is the portion of the land surface which normally abuts and confines a water body, occurring between a water body and a vegetated bordering wetland and adjacent floodplain, or, in the absence of these, it occurs between a water body and an upland. The upper boundary of a Bank is the first observable break in the slope or the mean annual flood level, whichever is lower.

BETA identified the resource Bank associated to one (1) intermittent stream and three (3) perennial streams in proximity to the Site. The Banks within 100 feet of the Site were delineated in the field with blue flagging as described below in Table 2: Bank Boundary Description.

**Table 2: Bank Boundary Description** 

Table 2. Balik boundary Description				
Flag Series	Stream Type & Location	Description / Notes		
B1 & B2 Series  Flags B1-100 to B1-102 & B2-100 to B2-102	Intermittent stream interior to the WF4 Series BVW, north of 352 Grove Street	The southern ( <i>B1 Series</i> ) and northern ( <i>B2 Series</i> ) Banks of an intermittent stream interior to the WF4 Series BVW were delineated based on a coincident first observable break in slope and mean annual flood level. This channel is approximately two (2) feet wide with approximately six (6) inches of standing water at the time of the Site visit; no flow was observed. This stream is not depicted on USGS topographic maps or the USGS StreamStats program.		
B3 & B4 Series Flags B3-100 to B3-108 & B4-100 to B4-109	Mine Brook crossing at Grove Street, north of 352 Grove Street	The southern (B3 Series) and northern (B4 Series) Banks of Mine Brook, a perennial stream (River), were delineated in the vicinity of the crossing under Grove Street via a stone arch bridge with a span of approximately ten (10) feet. Mine Brook flows easterly and is approximately ten (10) feet wide with eight (8) inches of water near the stone culvert at the time of the Site visit. Bank is coincident with the Mean Annual High Water (MAHW) mark; the		



<sup>&</sup>lt;sup>1</sup>Mine Brook is a tributary to Dix Brook, which is mapped by the DFW as a Coldwater Fishery. The confluence of Mine Brook and Dix Brook is located approximately 1,350 feet northeast of the Site. Miscoe Brook, a tributary to Mine Brook, is also mapped as a Coldwater Fishery; their confluence is located approximately 2,100 feet southwest of the Site.

Flag Series	Stream Type & Location	Description / Notes
		MAHW mark/mean annual flood level are upgradient of the first observable break in slope and were delineated as Bank*. The substrate of Mine Brook consists of sand with small stones, and vegetation along the Banks include red maple ( <i>Acer rubrum</i> ), poison ivy ( <i>Toxicodendron radicans</i> ), and skunk cabbage ( <i>Symplocarpus foetidus</i> ).
B5 Series Flags B5-87 to B5-114	West side of Grove Street, north and south sides of the SNETT	The eastern (B5 Series) Bank of an unnamed perennial tributary to Mine Brook was delineated from its confluence with Mine Brook to a point approximately 500 feet north. The tributary flows south through a four (4)-foot-wide stone culvert under the SNETT and is approximately five (5) feet wide with a water depth varying from four (4) to twelve (12) inches at the time of the Site visit. The substrate consists of pebbles and sand, and vegetation along the Bank includes skunk cabbage (Symplocarpus foetidus) and cinnamon fern (Osmundastrum cinnamomeum). Bank was delineated along the mean annual flood level/MAHW where it was observed upgradient of the first observable break in slope*.
B6 & B7 Series Flags B6-100 to B6-103 B7-100 to B7-102	East side of Grove Street, between the WF8 and WF9 Series BVWs	The southern ( <i>B6 Series</i> ) and northern ( <i>B7 Series</i> ) Banks/MAHW of an unnamed perennial stream connecting the WF8 and WF9 BVWs were delineated at the east side of Grove Street. Banks of the stream west of Grove Street were not visible due to water levels within the WF8 BVW. The first observable break in slope is coincident with the mean annual flood level. This easterly flowing channel is approximately four (4) feet wide and had a water depth of three (3) inches the time of the Site visit. Vegetation along the Banks includes oriental bittersweet ( <i>Celastrus orbiculatus</i> ) and slippery elm ( <i>Ulmus rubra</i> ).

<sup>\*</sup>Bank was delineated per the Bylaw definition as discussed later in this report.

#### Bordering Vegetated Wetlands – 310 CMR 10.55

According to 310 CMR 10.55(2), the definition of BVW are freshwater wetlands which border on creeks, rivers, streams, ponds and lakes and are areas where the soils are saturated and/or inundated such that they support a predominance of wetland indicator plants. The boundary of BVW is the line within which 50% or more of the vegetation community consists of wetland indicator plants and saturated or inundated conditions exist.

BETA identified seven (7) areas of BVW at the Site. The boundaries of these wetlands were delineated in the field with pink flagging. US Army Corps of Engineers' *Vegetated Wetland Boundary Delineation Field Data Sheets* are attached documenting BETA's observed evidence of hydrology, soils, and hydrophytic vegetation at specific data plots.



**Table 3: BVW Boundary Description** 

Table 3: BVW Bou	Location	Description / Notes
WF2 Series Flags WF2-100 to WF2-106	Northeast of the intersection of Grove Street and Washington Street	The WF2 Series BVW is a scrub shrub wetland located at the toe of a steep slope along the east side of Grove Street. Inundation was observed within the interior of the wetland and waterstained leaves were present at the outer extents. Dominant vegetation within the BVW includes skunk cabbage, jewelweed ( <i>Impatiens capensis</i> ), and sensitive fern ( <i>Onoclea sensibilis</i> ). This wetland boundary was established based on evidence hydrology, as well as the presence of hydrophytic vegetation and hydric soils. A formal data plot was not performed at this location.
WF3 Series Flags WF3-100 to WF3-124	East of Grove Street, adjacent to a public well pump house at 352 Grove Street	The WF3 Series BVW is a red maple swamp with significant ponding present within the interior of the wetland. The wetland boundary was established based on evidence hydrology, as well as the presence of hydrophytic vegetation and hydric soils as documented on the attached U.S. Army Corps of Engineers Field Data Sheet.
WF4 Series Flags WF4-100 to WF4-104	East of Grove Street, along Mine Brook	This BVW is a forested swamp that borders on Mine Brook. An interior intermittent stream was observed to the south of Mine Brook. Dominant vegetation within the BVW includes red maple and skunk cabbage. This wetland boundary was established based on evidence hydrology, as well as the presence of hydrophytic vegetation and hydric soils. A formal data plot was not performed at this location.
WF5 Series Flags WF5-100 to WF5-105	East of Grove Street, north of the WF4 Series BVW and south of the SNETT	The WF5 Series BVW is a forested swamp located north of Mine Brook. The portion of this BVW along Grove Street is separated from the WF4 Series BVW along Grove Street by an upland hummock. Dominant vegetation within the BVW includes red maple. This wetland boundary was established based on evidence hydrology, as well as the presence of hydrophytic vegetation and hydric soils. A formal data plot was not performed at this location.
WF6 Series Flags WF6-100 to WF6-128	West of Grove Street, south and north of Mine Brook	The WF6 Series BVW borders on Mine Brook and is bisected by the SNETT. The BVW to the south of the SNETT is a scrub shrub swamp, while the BVW to the north of the trail is a red maple swamp. Sediment accumulation was observed within a ponded portion of the BVW along Grove Street to the south of Mine Brook. The wetland boundary was established based on evidence hydrology, as well as the presence of hydrophytic vegetation and hydric soils as documented on the attached U.S. Army Corps of Engineers Field Data Sheet.
WF8 Series Flags WF8-100 to WF8-109	Along the frontage of 177 Grove Street	This BVW is a deep marsh that abruptly transitions to the filled side slopes along Grove Street. Fencing is present upgradient of, and within, a portion of this wetland which restricted access for the delineation. The WF8 Series BVW borders on a perennial stream; the associated culvert was submerged on the west side of Grove Street. This wetland boundary was established based on evidence hydrology, as well as the presence of hydrophytic vegetation and hydric soils. A formal data plot was not performed



Flag Series	Location	Description / Notes
		at this location.
WF9 Series Flags WF9-100 to WF9-105	East of Grove Street, north of 176 Grove Street	The WF9 Series BVW is a red maple swamp that borders on an unnamed perennial stream that flows east under Grove Street from the WF8 Series BVW. This wetland boundary was established based on evidence hydrology, as well as the presence of hydrophytic vegetation and hydric soils. A formal data plot was not performed at this location.

#### Land Under Water – 310 CMR 10.56

According to 310 CMR 10.56(2), the definition of LUW is the land beneath any creek, river, stream, pond or lake and may be composed of organic muck or peat, fine sediments, rocks or bedrock. LUW exists between the Bank boundaries below the mean annual low water level of Mine Brook and the two (2) unnamed perennial streams. The boundary of LUW is the mean annual low water level. This boundary was not delineated in the field.

#### Bordering Land Subject to Flooding – 310 CMR 10.57

According to the FEMA FIRM Numbers 25021C0316E and 25021C0308Edated July 17, 2012, a Zone AE Flood Hazard and Regulatory Floodway associated with Mine Brook are present at the Site. Base Flood Elevations (BFEs) associated with the Zone AE Flood Hazard range from 241.4 feet (NAVD88) to 246 feet (NAVD88). Any work performed below the BFE is subject to jurisdiction under the Act.

#### Riverfront Area - 310 CMR 10.58

According to its definition at 310 CMR 10.58(3), the boundary of RA is the area of land between as River's mean annual high-water (MAHW) line measured horizontally outward from the River and a parallel line located 200 feet away. A River is any natural flowing body of water that empties to any ocean, lake, pond, or other River flowing throughout the year and is shown as perennial on the current USGS or more recent map provided by the Department, has a watershed size of at least one (1) square mile, or has a watershed size of at least 0.50 square miles and a predicted flow rate greater than or equal to 0.01 cubic feet per second at the 99% flow duration using the USGS Stream Stats Method.

Mine Brook (B3 & B4 Series Banks), its unnamed tributary (B5 Series Bank), and the stream connecting the WF8 Series and WF9 Series BVWs (B6 & B7 Series Banks) are depicted as perennial streams (Rivers) on USGS topographic maps and are afforded 200-foot RAs. The MAHW mark is coincident with all Bank delineations described above in Table 2.

#### Jurisdictional Wetland Resource Areas - Town of Franklin

The Bylaw maintains many regulatory definitions consistent with the Act, with the exception of the following:

#### **Isolated Vegetated Wetlands**

The Bylaw protects all freshwater wetlands, whether or not they border surface waters. BETA identified four (4) areas that qualify as Isolated Vegetated Wetlands (IVWs) as described below in Table 4.



**Table 4: IVW Boundary Description** 

Flag Series	Location	Description / Notes
WF1 Series Flags WF1-100 to WF1-108	Northwest of the intersection of Grove Street and Washington Street	The WF1 Series IVW is a defined depression that was inundated at the time of the Site visit. MassGIS depicts a PVP at this location. The wetland boundary was established based on evidence hydrology, as well as the presence of hydrophytic vegetation and hydric soils as documented on the attached U.S. Army Corps of Engineers Field Data Sheet.
WF7 Series Flags WF7-100 to WF7-104	Southwest of 191 Grove Street	The WF7 Series IVW is a shallow depression depicted as a stream on MassGIS, though no stream or channel was observed in the field. Dominant vegetation within this depression includes skunk cabbage, elderberry ( <i>Sambucus canadensis</i> ), and cinnamon fern. This wetland boundary was established based on evidence hydrology, as well as the presence of hydrophytic vegetation and hydric soils. A formal data plot was not performed at this location.
WF10 Series Flags WF10-100 to WF10-103	Southwest of the intersection of Grove Street and Kenwood Circle	The WF10 Series IVW is a small roadside depression that receives stormwater runoff from Grove Street. Vegetation within the IVW includes highbush blueberry ( <i>Vaccinium corymbosum</i> ), greenbrier ( <i>Smilax rotundifolia</i> ), and red maple. This wetland boundary was established based on evidence hydrology (including the presence of Hydrogen Sulfide Odor), as well as the presence of hydrophytic vegetation and hydric soils. A formal data plot was not performed at this location.
WF11 Series Flags WF11-100 to WF11-104	Along Grove Street at 161 Grove Street	This IVW is located within a stormwater basin that was constructed between 2001 and 2005 based on historic aerial imagery. The basin appears to not have been maintained in accordance with the MassDEP Stormwater Handbook as evidenced by the growth of substantial woody and herbaceous vegetation including cattail ( <i>Typha latifolia</i> ). Nearby basins appear to be maintained through mowing. This wetland boundary was established based on evidence hydrology, as well as the presence of hydrophytic vegetation and hydric soils. A formal data plot was not performed at this location.

#### **Bank**

Bank is defined as the land area which normally abuts and confines a water body; the lower boundary being the mean annual low flow level, and the upper boundary being the first observable break in the slope or the mean annual flood level, whichever is higher.

The mean annual flood level was delineated as Bank wherever it occurred upgradient of the first observable break in slope. Therefore, the Bank delineation complies with the Bylaw definition.

#### **Rare Species**

The Bylaw states that Rare Species includes, without limitation, all vertebrate and invertebrate animal and all plant species listed as endangered, threatened, or of special concern by the Massachusetts Division of Fisheries and Wildlife, regardless of whether the site in which they occur has been previously identified by the Division.



The Site is located outside of Priority Habitat of Rare Species as identified by the Division. Coordination with the Conservation Commission will be required through the Notice of Intent filing process to determine if the Site qualifies as Rare Species habitat under the Bylaw.

#### Vernal Pool

The Bylaw defines a vernal pool as a confined basin depression which, at least in most years, holds water for a minimum of two continuous months during the spring and/or summer and which is free of adult fish populations, regardless of whether the site has been certified by the Massachusetts Division of Wildlife and Fisheries.

MassGIS depicts Potential Vernal Pools (PVPs) within the WF1 Series IVW and the WF2, WF4, and WF6 Series BVWs. The PVP depicted within the WF1 Series IVW most closely meets this definition based on topography and hydrology; however, the time of year did not facilitate the investigation of vernal pool species. A determination will need to be made by the Conservation Commission regarding the status of these areas as vernal pools under the Bylaw.

#### **Buffer Zone**

Under the Bylaw, Buffer Zones are protected as Resource Areas and are subject to local Buffer Zone Performance Standards.

The Bylaw Regulations protect a 25-foot No Disturb Zone from the boundary of Resource Areas excluding Bordering/Isolated Lands Subject to Flooding (BLSF/ILSF) and RA. Applicants may work within this No Disturb Zone if the activity is considered minor or if a variance is sought.

The Bylaw Regulations also prohibit structures within 50 feet from the boundary of Resource Areas excluding BLSF/ILSF and RA. Structures may be permitted within this setback if the area was disturbed prior to June 29, 2006 or if a variance is sought.

Additional mitigation may be required by the Conservation Commission when a project results in more than 30% of the 50-100-foot Buffer Zone being converted to impervious area.

#### Jurisdictional Wetland Resource Areas – Federal Clean Water Act (Section 404)

The wetlands and streams located on the Site are "Waters of the United States," and are therefore subject to the federal Clean Water Act, 33 U.S.C. §1251 et seq (1972). The boundary to "Waters of the United States" is the Vegetated Wetlands boundary, or, in the absence of Vegetated Wetlands, is the Ordinary High Water Mark (OHWM) for non-tidal rivers and streams, as specified at 33 CFR §328.4.

According to 33 CFR §328.3(c)(4), Vegetated Wetlands are defined as "those areas that are inundated or saturated by surface or groundwater at a frequency and duration sufficient to support, and that under normal circumstances do support, a prevalence of vegetation typically adapted for life in saturated soil conditions." The wetland boundary previously described in this report was delineated in accordance with this definition. The US Army Corps of Engineers' *Vegetated Wetland Boundary Delineation Field Data Sheets* are attached documenting BETA's observed evidence of hydrology, soils, and hydrophytic vegetation at specific data plots.

The OHWM of the streams, as defined at 33 CFR §328.3(c)(6), is coincident with the Bank.

The boundary of Vegetated Wetlands is consistent with the delineated BVW and IVW boundaries and would be considered the extent of Federal Section 404 Jurisdiction for most of the Site, except for areas where there are no Vegetated Wetlands along Streambanks. In those locations, such as to the east of Grove Street near the B6/B7 Series Stream and along portions of the B3/B4 Series Stream, the OHWM is the extent of Federal Section 404 Jurisdiction. Work conducted below the boundary of Vegetated Wetlands or the OHWM is Subject to Jurisdiction under Section 404 of the Clean Water Act.



#### Jurisdictional Wetland Resource Areas - Massachusetts Clean Waters Act (Section 401)

The limit of jurisdiction under Massachusetts Clean Waters Act (Section 401), as specified in 314 CMR 9.00, is the limit of Section 404 jurisdiction under the federal Clean Water Act. Exceedances of the jurisdictional threshold under 314 CMR 9.00 require filing for a Water Quality Certification under Section 401.

#### **Findings and Recommendations**

BETA has identified areas Subject to Protection and/or Jurisdiction under the Massachusetts Wetlands Protection Act, the federal Clean Water Act, the Massachusetts Clean Waters Act, and the Town of Franklin Wetlands Protection Bylaw on or within 100 feet of the Site and has delineated the boundaries of BVW, IVW, and Bank. In order to definitively determine the extent of Conservation Commission jurisdiction, Army Corps of Engineers jurisdiction, and MassDEP jurisdiction, the boundary flags would need to be located and depicted on a to-scale plan of the Site.

Attachments: Figure 1 – Site Locus

Figure 2 – Environmental Resources Map

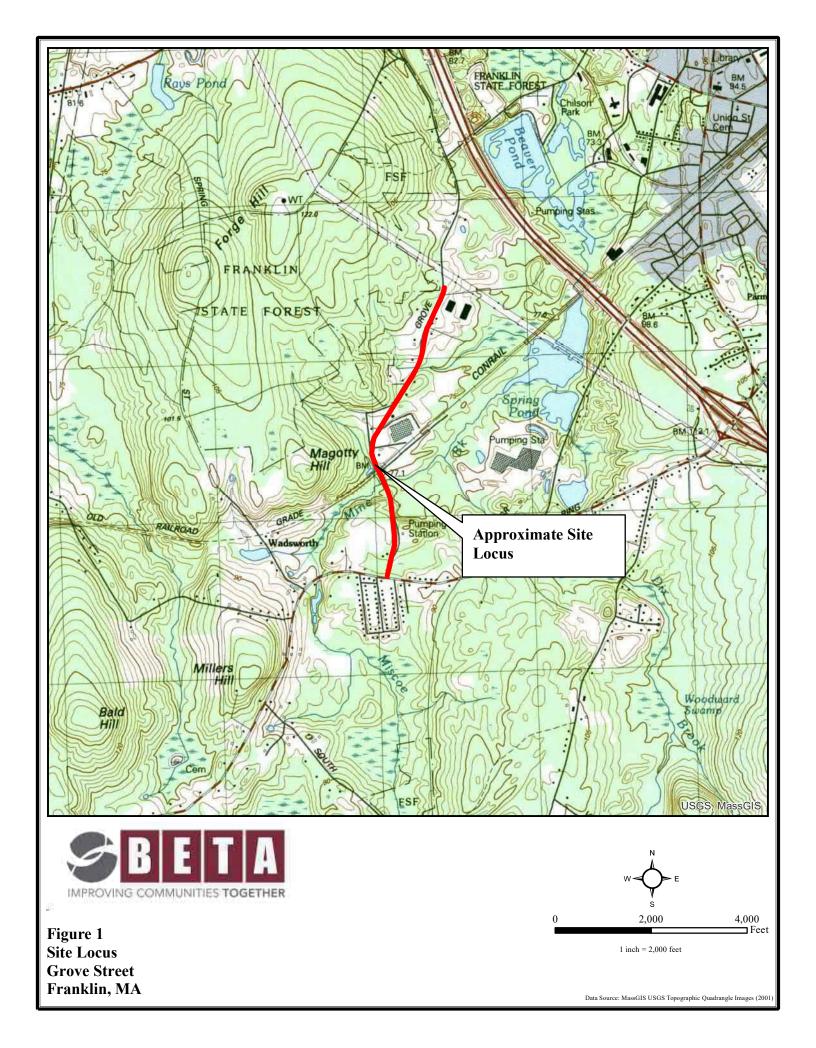
Figure 3 – FEMA FIRMette Photographic Documentation

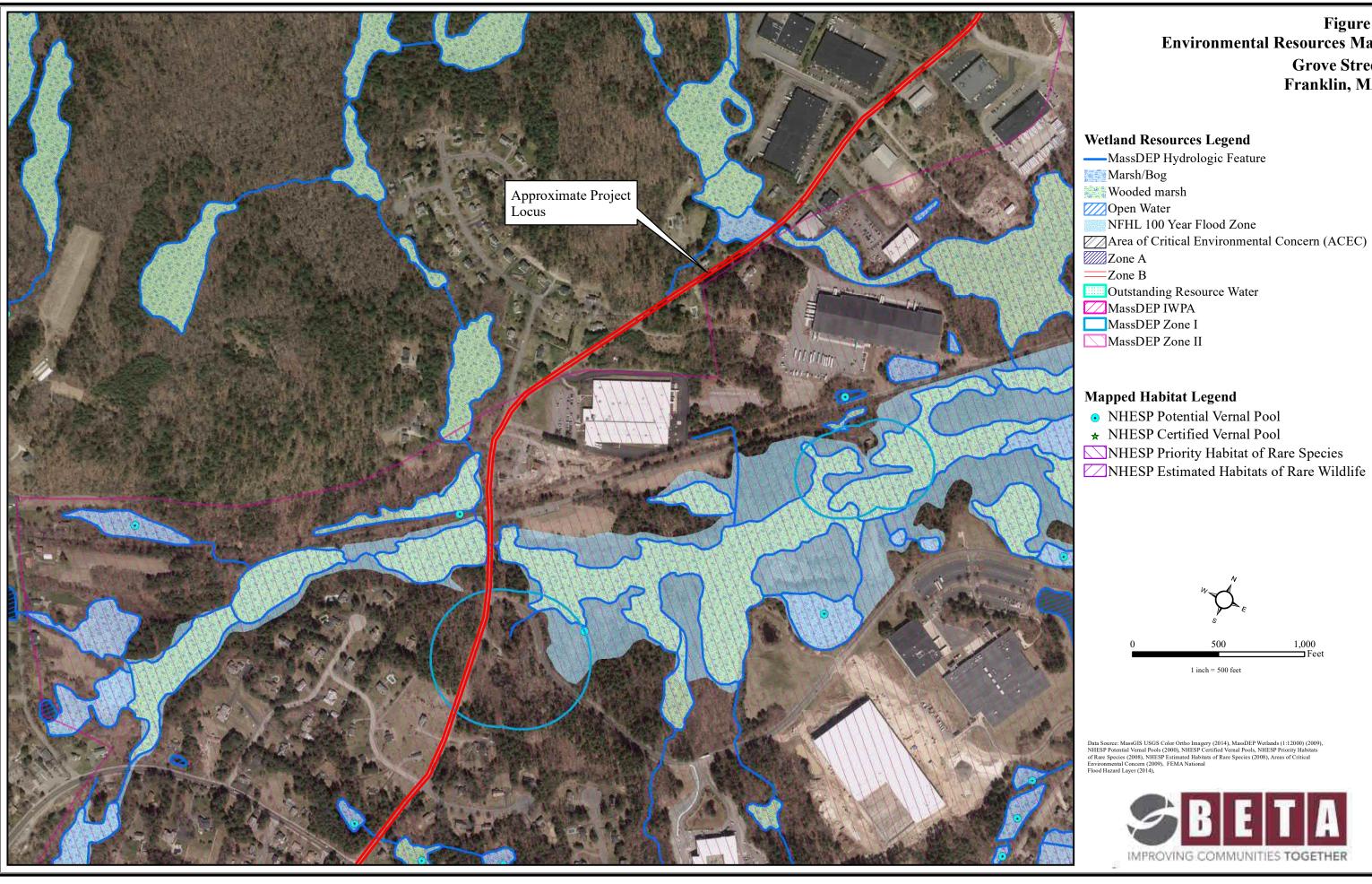
US Army Corps of Engineers' Vegetated Wetland Boundary Delineation Field Data Sheets

Custom Soil Report for Norfolk and Suffolk Counties, Massachusetts

Job No: 21.07548.00

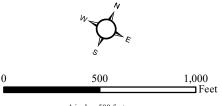






## Figure 2 **Environmental Resources Map Grove Street** Franklin, MA

- NHESP Priority Habitat of Rare Species





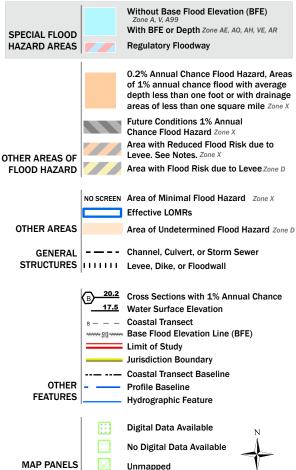


Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020



#### Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT



This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The pin displayed on the map is an approximate point selected by the user and does not represent

an authoritative property location.

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 5/12/2021 at 4:47 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

250

500

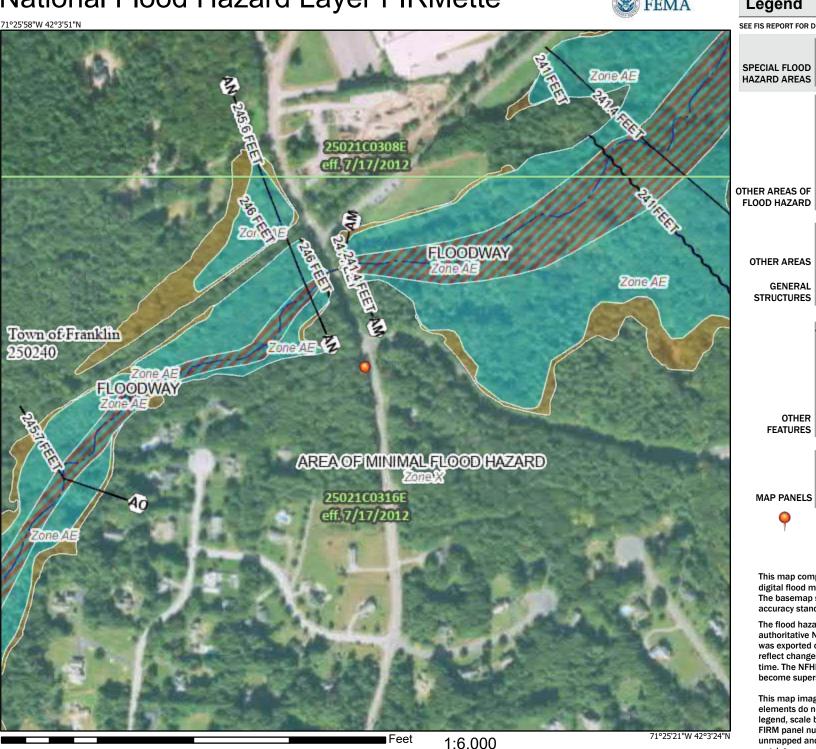
1,000

1.500

2.000

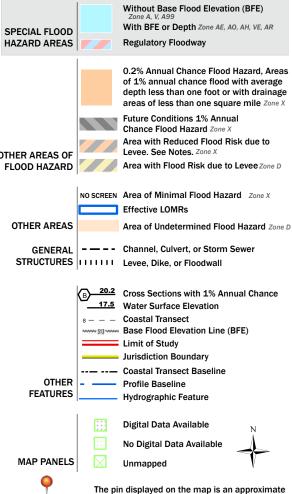
Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020





#### Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT



This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

point selected by the user and does not represent

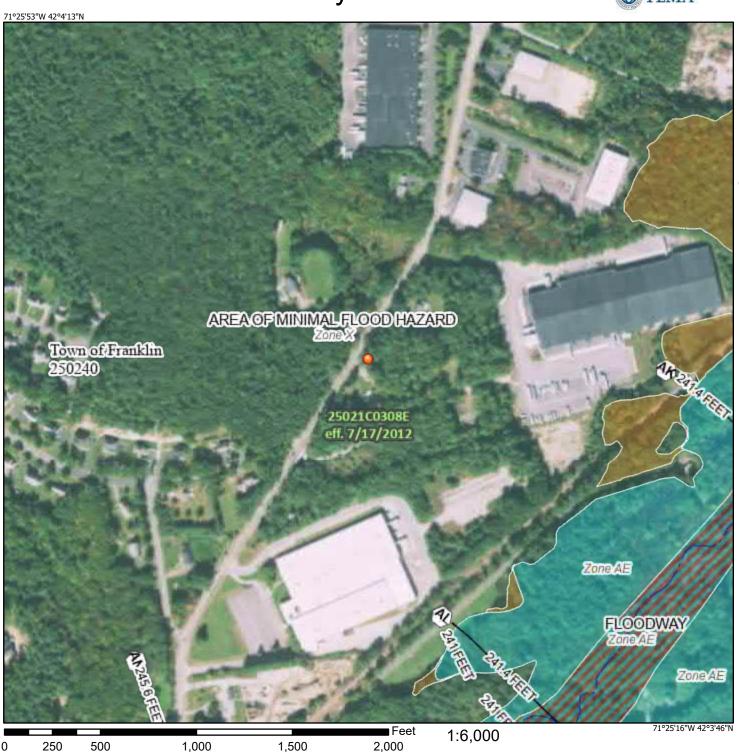
an authoritative property location.

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 5/12/2021 at 4:45 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

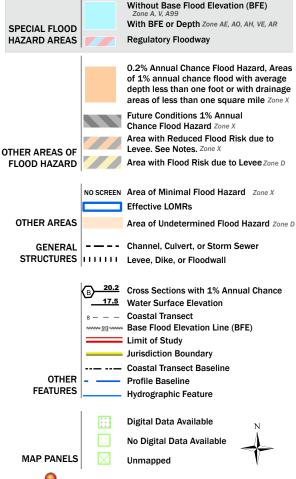


Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020



#### Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT



This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The pin displayed on the map is an approximate point selected by the user and does not represent

an authoritative property location.

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 5/12/2021 at 4:44 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

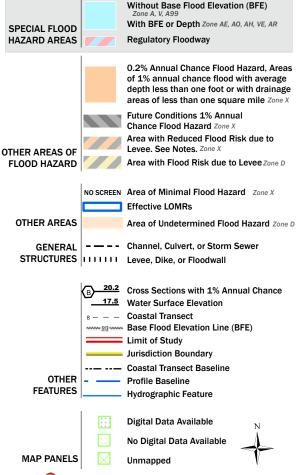


Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020



#### Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT



This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap

accuracy standards

The pin displayed on the map is an approximate point selected by the user and does not represent

an authoritative property location.

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 5/12/2021 at 4:42 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.



View of the WF1 Series IVW—facing west.

## Photo 2



View of the interior of the WF2 Series BVW—facing southeast.

### PHOTOGRAPHIC DOCUMENTATION



View of the WF3 Series BVW and adjacent public well pump house—facing northeast.

### Photo 4



View of Mine Brook, taken from Grove Street—facing east.

### PHOTOGRAPHIC DOCUMENTATION



View of the culvert carrying Mine Brook, taken from the east side of Grove Street—facing west.

## Photo 6



View of Mine Brook, taken from Grove Street—facing west.

### PHOTOGRAPHIC DOCUMENTATION



View of the WF6 Series BVW; note the sediment deposition in the foreground—facing west.

### Photo 8



View of the unnamed tributary to Mine Brook flowing through a culvert under the Southern New England Trunkline Trail—facing northeast.

#### PHOTOGRAPHIC DOCUMENTATION



View of the unnamed tributary to Mine Brook, north of the Southern New England Trunkline Trail—facing north.

### Photo 10



View of cinnamon fern (Osmundastrum cinnamomeum) within the WF7 Series IVW—facing west.

#### PHOTOGRAPHIC DOCUMENTATION



View of a forested portion of the WF8 Series BVW—facing west.

### Photo 12



View of the unnamed perennial stream connecting the WF8 and WF9 Series BVWs at the east side of Grove Street; note the damaged infrastructure—facing east.

### PHOTOGRAPHIC DOCUMENTATION



Typical view of a maintained stormwater basin at the northern end of the Site (157/161 Grove Street)—facing south.

### Photo 14



View of an unmaintained stormwater basin (WF11 Series IVW) at the northern end of the Site (157/ 161 Grove Street)—facing west.

### PHOTOGRAPHIC DOCUMENTATION



View of a small pocket IVW (WF10 Series) formed from roadway stormwater runoff—facing east.

### PHOTOGRAPHIC DOCUMENTATION

Project/Site: Grove Street	City/County: Franklin Sampling Date: 5/13/2021					
Applicant/Owner: Town of Franklin	State: MA Sampling Point: Upland					
Investigator(s): Jonathan Niro & Julia Stearns (BETA Group, Inc.)	Section, Township, Range: Norfolk County					
	al relief (concave, convex, none): Concave Slope %: 0					
Subregion (LRR or MLRA): LRR R, MLRA 144A Lat: 42.066353	Long: -71.426820 Datum: WGS84					
Soil Map Unit Name: Hinckley loamy sand, 8 to 15 percent slopes	NWI classification: N/A					
Are climatic / hydrologic conditions on the site typical for this time of year?						
Are Vegetation, Soil, or Hydrology significantly distu						
Are Vegetation, Soil, or Hydrologynaturally problem	natic? (If needed, explain any answers in Remarks.)					
SUMMARY OF FINDINGS – Attach site map showing sar	mpling point locations, transects, important features, etc.					
Hydrophytic Vegetation Present?         Yes         No         X           Hydric Soil Present?         Yes         No         X           Wetland Hydrology Present?         Yes         No         X	Is the Sampled Area within a Wetland? Yes No X If yes, optional Wetland Site ID: WF1-106					
HYDROLOGY						
Wetland Hydrology Indicators:	Secondary Indicators (minimum of two required)					
Primary Indicators (minimum of one is required; check all that apply)	Surface Soil Cracks (B6)					
Surface Water (A1)  Water-Stained Leaves						
High Water Table (A2)  Aquatic Fauna (B13)	Moss Trim Lines (B16)					
Saturation (A3) Marl Deposits (B15)	Dry-Season Water Table (C2)					
Water Marks (B1) Hydrogen Sulfide Odor						
Sediment Deposits (B2) Oxidized Rhizospheres	s on Living Roots (C3) Saturation Visible on Aerial Imagery (C9)					
Drift Deposits (B3) Presence of Reduced I	Iron (C4) Stunted or Stressed Plants (D1)					
Algal Mat or Crust (B4)Recent Iron Reduction	in Tilled Soils (C6) Geomorphic Position (D2)					
Iron Deposits (B5) Thin Muck Surface (C7	Shallow Aquitard (D3)					
Inundation Visible on Aerial Imagery (B7) Other (Explain in Rema	arks)Microtopographic Relief (D4)					
Sparsely Vegetated Concave Surface (B8)	FAC-Neutral Test (D5)					
Field Observations:						
Surface Water Present? Yes No X Depth (inches						
Water Table Present? Yes No X Depth (inches						
Saturation Present? Yes No X Depth (inches)	s): Wetland Hydrology Present? Yes No X					
(includes capillary fringe)						
Describe Recorded Data (stream gauge, monitoring well, aerial photos, pr	revious inspections), if available:					
Remarks:						
Remarks.						

**VEGETATION** – Use scientific names of plants. Sampling Point: Upland Absolute Dominant Indicator <u>Tree Stratum</u> (Plot size: 30' radius ) % Cover Species? Status **Dominance Test worksheet: FACU** 1. Pinus strobus Yes Number of Dominant Species 2. Acer rubrum 40 FAC Yes That Are OBL, FACW, or FAC: (A) 20 3. Tsuga canadensis Yes **FACU Total Number of Dominant** 4. Species Across All Strata: 4 (B) 5. Percent of Dominant Species That Are OBL, FACW, or FAC: 6. 25.0% (A/B) Prevalence Index worksheet: 100 =Total Cover Total % Cover of: Multiply by: **OBL** species Sapling/Shrub Stratum (Plot size: 15' radius ) **FACW** species 0 x 2 = 1. 0 2. FAC species 40 x 3 = 120 3. FACU species 100 x 4 = 400 4. **UPL** species 0 x 5 = Column Totals: 140 (A) 520 6. Prevalence Index = B/A = **Hydrophytic Vegetation Indicators:** 1 - Rapid Test for Hydrophytic Vegetation =Total Cover Herb Stratum (Plot size: 5' radius ) 2 - Dominance Test is >50% Maianthemum canadense 3 - Prevalence Index is ≤3.01 2. 4 - Morphological Adaptations (Provide supporting data in Remarks or on a separate sheet) 3. 4. Problematic Hydrophytic Vegetation<sup>1</sup> (Explain) 5. <sup>1</sup>Indicators of hydric soil and wetland hydrology must 6. be present, unless disturbed or problematic. 7. **Definitions of Vegetation Strata:** 8. Tree - Woody plants 3 in. (7.6 cm) or more in 9. diameter at breast height (DBH), regardless of height. Sapling/shrub – Woody plants less than 3 in. DBH and greater than or equal to 3.28 ft (1 m) tall. Herb - All herbaceous (non-woody) plants, regardless 40 =Total Cover of size, and woody plants less than 3.28 ft tall. Woody Vine Stratum (Plot size: 15' radius ) Woody vines - All woody vines greater than 3.28 ft in height. 2. Hydrophytic 3. Vegetation Present? Yes No X =Total Cover Remarks: (Include photo numbers here or on a separate sheet.)

SOIL Sampling Point Upland

Profile Desc	ription: (Describe t	o the depth				tor or co	nfirm the absence of indicators.)	
Depth	Matrix			Featur		. 2		
(inches)	Color (moist)	<u>%</u>	Color (moist)	<u>%</u>	Type <sup>1</sup>	Loc <sup>2</sup>	Texture Remarks	
0-1	10YR 2/1						Organic "duff" la	
1-16	10YR 3/3						Fine sandy loa	ım
16-20	10YR 4/3						Fine sandy loa	ım
					<u>-</u>	:		
<del></del>							<del></del>	_
	ncentration, D=Depl	etion, RM=F	Reduced Matrix, M	IS=Mas	ked Sand	Grains.	<sup>2</sup> Location: PL=Pore Lining, M=Matrix.	2
Black His Hydroger Stratified Depleted Thick Da Sandy M Sandy G Sandy Re Stripped Dark Sur	(A1) ipedon (A2) stic (A3) n Sulfide (A4) Layers (A5) Below Dark Surface rk Surface (A12) ucky Mineral (S1) leyed Matrix (S4) edox (S5) Matrix (S6) face (S7)	-	Polyvalue Belor MLRA 149B) Thin Dark Surfa High Chroma S Loamy Mucky N Loamy Gleyed Depleted Matrix Redox Dark Su Depleted Dark Redox Depress Marl (F10) (LRI	ace (S9) sands (S Mineral Matrix ( (F3) rface (F Surface sions (F8 R K, L)	(LRR R, 611) (LRF (F1) (LRF F2) (6) (F7)	MLRA 14 R K, L) R K, L)	Polyvalue Below Surface (S8) (LRR K, L Thin Dark Surface (S9) (LRR K, L Iron-Manganese Masses (F12) (LI Piedmont Floodplain Soils (F19) (I Mesic Spodic (TA6) (MLRA 144A, Red Parent Material (F21) Very Shallow Dark Surface (F22) Other (Explain in Remarks)	A 149B) K, L, R) RR K, L, R) R K, L) ) RR K, L, R) MLRA 149B)
	hydrophytic vegetati ayer (if observed):	on and wetl	and hydrology mu	ist be pr	esent, un	less distu	rbed or problematic.	
Type:	ayer (ii observeu).							
Depth (in	ches):		<u> </u>				Hydric Soil Present? Yes	No X
	n is revised from Noi 2015 Errata. (http://w						2.0 to include the NRCS Field Indicators of Hydp2_051293.docx)	lric Soils,

Project/Site: Grove Street	City/County: Franklin Sampling Date: 5/13/2021				
Applicant/Owner: Town of Franklin	State: MA Sampling Point: Wetland				
Investigator(s): Jonathan Niro & Julia Stearns (BETA Group, Inc.)	Section, Township, Range: Norfolk County				
<del>-</del>	I relief (concave, convex, none): Concave Slope %: 0				
Subregion (LRR or MLRA): LRR R, MLRA 144A Lat: 42.066353	Long: -71.426820 Datum: WGS84				
Soil Map Unit Name: Hinckley loamy sand, 8 to 15 percent slopes	NWI classification: PEM1E				
Are climatic / hydrologic conditions on the site typical for this time of year?	Yes X No (If no, explain in Remarks.)				
Are Vegetation, Soil, or Hydrologysignificantly distur	<del></del> -				
Are Vegetation, Soil, or Hydrology naturally problems					
	npling point locations, transects, important features, etc.				
Hydrophytic Vegetation Present?  Hydric Soil Present?  Yes X No  Wetland Hydrology Present?  Yes X No	Is the Sampled Area within a Wetland?  Yes X No No If yes, optional Wetland Site ID: WF1-106				
HYDROLOGY					
Wetland Hydrology Indicators:	Secondary Indicators (minimum of two required)				
Primary Indicators (minimum of one is required; check all that apply)	Surface Soil Cracks (B6)				
X Surface Water (A1) Water-Stained Leaves (					
X High Water Table (A2) Aquatic Fauna (B13)	Moss Trim Lines (B16)				
X Saturation (A3) Marl Deposits (B15)	Dry-Season Water Table (C2)				
Water Marks (B1) Hydrogen Sulfide Odor					
Sediment Deposits (B2)Oxidized Rhizospheres Drift Deposits (B3) Presence of Reduced Ir					
Algal Mat or Crust (B4)  Recent Iron Reduction i	<u> </u>				
Iron Deposits (B5)  Thin Muck Surface (C7)	• • • • • • • • • • • • • • • • • • • •				
X Inundation Visible on Aerial Imagery (B7) Other (Explain in Remai					
Sparsely Vegetated Concave Surface (B8)	X FAC-Neutral Test (D5)				
Field Observations:					
Surface Water Present? Yes X No Depth (inches)	):12				
Water Table Present? Yes X No Depth (inches)	): 2				
Saturation Present? Yes X No Depth (inches)	: 0 Wetland Hydrology Present? Yes X No				
(includes capillary fringe)					
Describe Recorded Data (stream gauge, monitoring well, aerial photos, pre	evious inspections), if available:				
Remarks:					

**VEGETATION** – Use scientific names of plants. Sampling Point: Wetland Absolute Dominant Indicator <u>Tree Stratum</u> (Plot size: 30' radius ) % Cover Species? Status **Dominance Test worksheet:** FAC 1. Acer rubrum Yes Number of Dominant Species 2. That Are OBL, FACW, or FAC: (A) 3. **Total Number of Dominant** 4. Species Across All Strata: 2 (B) 5. Percent of Dominant Species That Are OBL, FACW, or FAC: 6. 100.0% (A/B) Prevalence Index worksheet: 30 =Total Cover Total % Cover of: Multiply by: **OBL** species Sapling/Shrub Stratum (Plot size: 15' radius ) **FACW** species 5 x 2 = 1. 10 30 2. FAC species x 3 = 3. FACU species 0 x 4 = 4. **UPL** species x 5 = Column Totals: 35 100 6. Prevalence Index = B/A = 2.86 **Hydrophytic Vegetation Indicators:** =Total Cover 1 - Rapid Test for Hydrophytic Vegetation Herb Stratum (Plot size: 5' radius ) X 2 - Dominance Test is >50% X 3 - Prevalence Index is ≤3.0<sup>1</sup> Spiraea tomentosa 4 - Morphological Adaptations (Provide supporting 2. data in Remarks or on a separate sheet) 3. 4. Problematic Hydrophytic Vegetation<sup>1</sup> (Explain) 5. <sup>1</sup>Indicators of hydric soil and wetland hydrology must 6. be present, unless disturbed or problematic. 7. **Definitions of Vegetation Strata:** 8. Tree - Woody plants 3 in. (7.6 cm) or more in 9. diameter at breast height (DBH), regardless of height. Sapling/shrub – Woody plants less than 3 in. DBH and greater than or equal to 3.28 ft (1 m) tall. Herb - All herbaceous (non-woody) plants, regardless 5 =Total Cover of size, and woody plants less than 3.28 ft tall. Woody Vine Stratum (Plot size: 15' radius ) Woody vines - All woody vines greater than 3.28 ft in height. 2. Hydrophytic 3. Vegetation Present? No \_ Yes X =Total Cover Remarks: (Include photo numbers here or on a separate sheet.)

SOIL Sampling Point Wetland

		o the dep				tor or co	nfirm the absence o	f indicators.)
Depth (inches)	Matrix Color (moist)	%	Color (moist)	x Featur %	es Type <sup>1</sup>	Loc <sup>2</sup>	Texture	Remarks
0-2	10YR 3/2	100	Color (molot)		1,700		Toxidio	Fine sandy loam
2-6	10YR 4/3	100						Fine sandy loam
6-18	10YR 3/2	90	10YR 4/3	10	С			Faint redox concentrations
		:		_ _ _	<u> </u>			
¹Type: C=Cc	oncentration, D=Depl	etion, RM	Reduced Matrix, N	/S=Mas	ked Sand	Grains.	<sup>2</sup> Location: P	L=Pore Lining, M=Matrix.
Histosol Histic Ep Black His Hydroger Stratified Depleted Thick Da Sandy M Sandy G X Sandy Re Stripped Dark Sur	Type: C=Concentration, D=Depletion, RM=Reduced Matrix, MS=Masked Sand Grains Hydric Soil Indicators:  Histosol (A1)  Histic Epipedon (A2)  Black Histic (A3)  Hydrogen Sulfide (A4)  Stratified Layers (A5)  Depleted Below Dark Surface (A11)  Thick Dark Surface (A12)  Sandy Mucky Mineral (S1)  Sandy Gleyed Matrix (S4)  Stripped Matrix (S6)  Dark Surface (S7)  Polyvalue Below Surface (S8) (LRR R, MLRA MLRA High Chroma Sands (S11) (LRR K, L)  Loamy Mucky Mineral (F1) (LRR K, L)  Depleted Matrix (F2)  Depleted Matrix (F3)  Redox Dark Surface (F6)  Depleted Dark Surface (F7)  Redox Depressions (F8)  Marl (F10) (LRR K, L)				, MLRA 14 R K, L) R K, L)	2 cm Mu Coast Pr 5 cm Mu Polyvalu Thin Dar Iron-Mar Piedmor Mesic Sp Red Pare Very Sha Other (E	or Problematic Hydric Soils <sup>3</sup> : ck (A10) (LRR K, L, MLRA 149B) rairie Redox (A16) (LRR K, L, R) cky Peat or Peat (S3) (LRR K, L, R) e Below Surface (S8) (LRR K, L) k Surface (S9) (LRR K, L) riganese Masses (F12) (LRR K, L, R) at Floodplain Soils (F19) (MLRA 149B) codic (TA6) (MLRA 144A, 145, 149B) ent Material (F21) allow Dark Surface (F22) xplain in Remarks)	
Type:	.ayer (if observed):							
Depth (in	iches):						Hydric Soil Preser	nt? Yes X No
	m is revised from No 2015 Errata. (http://w							CS Field Indicators of Hydric Soils,

Project/Site: Grove Street	City/County: Franklin Sampling Date: 5/13/202						
Applicant/Owner: Town of Franklin	State: MA	Sampling Point: Upland					
Investigator(s): Jonathan Niro & Julia Stearns (BETA Group, Inc.)	Section, Township, Range: Norfolk (	County					
Landform (hillside, terrace, etc.): Toe of roadside slope Local	relief (concave, convex, none): Concave	Slope %: 0					
Subregion (LRR or MLRA): LRR R, MLRA 144A Lat: 42.066353	Long: -71.426820	Datum: WGS84					
Soil Map Unit Name: Hinckley loamy sand, 3 to 8 percent slopes	NWI classification:						
Are climatic / hydrologic conditions on the site typical for this time of year?		explain in Remarks.)					
Are Vegetation, Soil, or Hydrology significantly distur							
Are Vegetation, Soil, or Hydrologynaturally problems		Remarks.)					
SUMMARY OF FINDINGS – Attach site map showing sam		nportant features, etc.					
Hydrophytic Vegetation Present? Yes No _X	Is the Sampled Area						
Hydric Soil Present?  Yes No X	within a Wetland? Yes	No X					
Wetland Hydrology Present? Yes No X	If yes, optional Wetland Site ID: WF3-118						
Remarks: (Explain alternative procedures here or in a separate report.)							
HYDROLOGY							
Wetland Hydrology Indicators:	Secondary Indicators (r	minimum of two required)					
Primary Indicators (minimum of one is required; check all that apply)	Surface Soil Crack	· · · ·					
Surface Water (A1) Water-Stained Leaves (		` '					
High Water Table (A2)  Aquatic Fauna (B13)		Moss Trim Lines (B16)					
Saturation (A3) Marl Deposits (B15)	Dry-Season Water	Dry-Season Water Table (C2)					
Water Marks (B1) Hydrogen Sulfide Odor (	(C1) Crayfish Burrows (	C8)					
Sediment Deposits (B2)  Oxidized Rhizospheres	on Living Roots (C3) Saturation Visible of	on Aerial Imagery (C9)					
Drift Deposits (B3) Presence of Reduced In	on (C4)Stunted or Stresse	d Plants (D1)					
Algal Mat or Crust (B4) Recent Iron Reduction in	• • • • • • • • • • • • • • • • • • • •	` '					
Iron Deposits (B5) Thin Muck Surface (C7)		Shallow Aquitard (D3)					
Inundation Visible on Aerial Imagery (B7)Other (Explain in Remar							
Sparsely Vegetated Concave Surface (B8)	FAC-Neutral Test (	D5)					
Field Observations:							
Surface Water Present? Yes No X Depth (inches):  Water Table Present? Yes No X Depth (inches):  Soturation Present? Yes No X Depth (inches):	·						
Water Table Present? Yes No X Depth (inches):		V N- V					
Saturation Present? Yes No _X Depth (inches): (includes capillary fringe)	Wetland Hydrology Present?	Yes No _X					
Describe Recorded Data (stream gauge, monitoring well, aerial photos, pre	evious inspections) if available:						
Bosonibo Nocoraca Bata (choani gaago, memoring won, achai priotoc, pro	wilde inepections), if available.						
Remarks:							

**VEGETATION** – Use scientific names of plants. Sampling Point: Upland Absolute Dominant Indicator Tree Stratum (Plot size: 30' radius ) % Cover Species? Status **Dominance Test worksheet:** FAC 1. Acer rubrum Yes Number of Dominant Species 2. That Are OBL, FACW, or FAC: (A) 3. **Total Number of Dominant** 4. Species Across All Strata: 3 (B) 5. Percent of Dominant Species That Are OBL, FACW, or FAC: 6. 33.3% (A/B) Prevalence Index worksheet: 40 =Total Cover Total % Cover of: Multiply by: **OBL** species Sapling/Shrub Stratum (Plot size: 15' radius ) **FACW** species 0 x 2 = 1. Prunus serotina **FACU** 0 10 Yes 2. FAC species 40 x 3 = 120 3. FACU species 10 x 4 = 40 4. **UPL** species 15 x 5 = 75 5. Column Totals: 65 235 6. Prevalence Index = B/A = **Hydrophytic Vegetation Indicators:** 1 - Rapid Test for Hydrophytic Vegetation 10 =Total Cover Herb Stratum (Plot size: 5' radius ) 2 - Dominance Test is >50% Dennstaedtia punctilobula 3 - Prevalence Index is ≤3.01 2. 4 - Morphological Adaptations (Provide supporting data in Remarks or on a separate sheet) 3. 4. Problematic Hydrophytic Vegetation<sup>1</sup> (Explain) 5. <sup>1</sup>Indicators of hydric soil and wetland hydrology must 6. be present, unless disturbed or problematic. 7. **Definitions of Vegetation Strata:** 8. Tree - Woody plants 3 in. (7.6 cm) or more in 9. diameter at breast height (DBH), regardless of height. Sapling/shrub – Woody plants less than 3 in. DBH and greater than or equal to 3.28 ft (1 m) tall. Herb - All herbaceous (non-woody) plants, regardless 15 =Total Cover of size, and woody plants less than 3.28 ft tall. Woody Vine Stratum (Plot size: 15' radius ) Woody vines - All woody vines greater than 3.28 ft in height. 2. Hydrophytic 3. Vegetation Present? Yes No X =Total Cover Remarks: (Include photo numbers here or on a separate sheet.)

SOIL Sampling Point Upland

	•	o the de				tor or co	nfirm the absence of indicators.)	
Depth	Matrix			(Featur		1 2	Tourism	Demode
(inches)	Color (moist)	<u>%</u>	Color (moist)	%	Type <sup>1</sup>	Loc <sup>2</sup>	Texture	Remarks
0-2	10YR 2/1	100					Orga	anic "duff" layer
2-18	10YR 4/4	100					Fir	ne sandy loam
			<u> </u>					
						—		
						·	_	
						—		
						·		
1 <sub>Tymes</sub> C. Co	oncentration, D=Depl	otion DM	Doduced Metrix N		Lod Cond	Croins	<sup>2</sup> Location: PL=Pore Lining	NA Motrix
Hydric Soil I		ellon, Kiv	=Reduced Matrix, iv	io=ivias	keu Sano	Giailis.	Indicators for Problemati	
Histosol			Polyvalue Belo	w Surfa	ce (S8) (I	RR R,	2 cm Muck (A10) (LRF	•
	ipedon (A2)		MLRA 149B)		. , .		Coast Prairie Redox (A	
Black His			Thin Dark Surfa				The state of the s	
	n Sulfide (A4)		High Chroma S			-	Polyvalue Below Surfa	
	Layers (A5)	(111)	Loamy Mucky I			R K, L)	Thin Dark Surface (S9	
	Below Dark Surface rk Surface (A12)	(A11)	Loamy Gleyed Depleted Matrix		(FZ)			es (F12) ( <b>LRR K, L, R</b> ) Soils (F19) ( <b>MLRA 149B</b> )
	ucky Mineral (S1)		Redox Dark Su		<del>-</del> 6)			ILRA 144A, 145, 149B)
	leyed Matrix (S4)		Depleted Dark				Red Parent Material (F	· ·
Sandy Re	edox (S5)		Redox Depress	sions (F	8)		Very Shallow Dark Sur	
	Matrix (S6)		Marl (F10) ( <b>LR</b>	R <b>K</b> , <b>L</b> )			Other (Explain in Remains	arks)
Dark Sur	face (S7)							
<sup>3</sup> Indicators of	hydrophytic vegetati	on and w	etland hydrology mu	ist ha ni	rasant ur	lace dieti	urhed or problematic	
	.ayer (if observed):	on and w	cualia nyarology ma	iot bo pi	rosont, ur	ilooo diot	indea of problematio.	
Type:	,							
Depth (in	ches):						Hydric Soil Present? Ye	es No_X_
Remarks:								
							2.0 to include the NRCS Field Indica	ators of Hydric Soils,
version 7.0, 2	2015 Errata. (http://w	ww.nrcs.	usda.gov/internet/F3	SE_DO(	JUMENT	5/nrcs142	p2_051293.docx)	

Project/Site: Grove Street	City/County: Franklin Sampling Date: 5/13/2021					
Applicant/Owner: Town of Franklin	State: MA Sampling Point: Wetland					
Investigator(s): Jonathan Niro & Julia Stearns (BETA Group, Inc.)	Section, Township, Range: Norfolk County					
	I relief (concave, convex, none): Concave Slope %: 0					
Subregion (LRR or MLRA): LRR R, MLRA 144A Lat: 42.066353	Long: -71.426820 Datum: WGS84					
Soil Map Unit Name: Hinckley loamy sand, 3 to 8 percent slopes	NWI classification: N/A					
Are climatic / hydrologic conditions on the site typical for this time of year?	Yes X No (If no, explain in Remarks.)					
Are Vegetation, Soil, or Hydrologysignificantly distur	rbed? Are "Normal Circumstances" present? Yes X No					
Are Vegetation, Soil, or Hydrologynaturally problems						
	npling point locations, transects, important features, etc.					
Hydrophytic Vegetation Present?         Yes X         No           Hydric Soil Present?         Yes X         No           Wetland Hydrology Present?         Yes X         No	Is the Sampled Area within a Wetland?  If yes, optional Wetland Site ID: WF3-118					
HYDROLOGY						
Wetland Hydrology Indicators:	Secondary Indicators (minimum of two required)					
Primary Indicators (minimum of one is required; check all that apply)	Surface Soil Cracks (B6)					
X Surface Water (A1) X Water-Stained Leaves (						
X High Water Table (A2) Aquatic Fauna (B13)	Moss Trim Lines (B16)					
X Saturation (A3) Marl Deposits (B15)	Dry-Season Water Table (C2)					
Water Marks (B1) Hydrogen Sulfide Odor						
Sediment Deposits (B2)  Oxidized Rhizospheres  Presence of Reduced Ir						
Drift Deposits (B3) Presence of Reduced Ir  Algal Mat or Crust (B4) Recent Iron Reduction i						
Iron Deposits (B5)  Thin Muck Surface (C7)	· / · · · · · · · · · · · · · · · · · ·					
Inundation Visible on Aerial Imagery (B7)  Other (Explain in Remainder (B7)						
Sparsely Vegetated Concave Surface (B8)	FAC-Neutral Test (D5)					
Field Observations:						
Surface Water Present? Yes X No Depth (inches)	): 12					
Water Table Present? Yes X No Depth (inches)						
Saturation Present? Yes X No Depth (inches)						
(includes capillary fringe)						
Describe Recorded Data (stream gauge, monitoring well, aerial photos, pro	evious inspections), if available:					
Remarks:						

**VEGETATION** – Use scientific names of plants. Sampling Point: Wetland Absolute Dominant Indicator Tree Stratum (Plot size: 30' radius ) % Cover Species? Status **Dominance Test worksheet:** FAC 1. Acer rubrum Yes Number of Dominant Species 2. That Are OBL, FACW, or FAC: (A) 3. **Total Number of Dominant** 4. Species Across All Strata: 3 (B) 5. Percent of Dominant Species That Are OBL, FACW, or FAC: 6. 66.7% (A/B) Prevalence Index worksheet: 40 =Total Cover Total % Cover of: Multiply by: **OBL** species Sapling/Shrub Stratum (Plot size: 15' radius ) **FACW** species 20 x 2 = 1. 40 2. FAC species 40 x 3 = 10 3. FACU species x 4 = 4. **UPL** species 0 x 5 = 5. Column Totals: 70 (A) 200 6. Prevalence Index = B/A = 2.86 **Hydrophytic Vegetation Indicators:** =Total Cover 1 - Rapid Test for Hydrophytic Vegetation Herb Stratum (Plot size: 5' radius ) X 2 - Dominance Test is >50% X 3 - Prevalence Index is ≤3.0<sup>1</sup> Maianthemum canadense 10 **FACU** 20 Yes **FACW** 4 - Morphological Adaptations (Provide supporting 2. Osmundastrum cinnamomeum data in Remarks or on a separate sheet) 3. 4. Problematic Hydrophytic Vegetation<sup>1</sup> (Explain) 5. <sup>1</sup>Indicators of hydric soil and wetland hydrology must 6. be present, unless disturbed or problematic. 7. **Definitions of Vegetation Strata:** 8. Tree – Woody plants 3 in. (7.6 cm) or more in 9. diameter at breast height (DBH), regardless of height. Sapling/shrub – Woody plants less than 3 in. DBH and greater than or equal to 3.28 ft (1 m) tall. Herb - All herbaceous (non-woody) plants, regardless 30 =Total Cover of size, and woody plants less than 3.28 ft tall. Woody Vine Stratum (Plot size: 15' radius ) Woody vines - All woody vines greater than 3.28 ft in height. 2. Hydrophytic 3. Vegetation Present? Yes X No =Total Cover Remarks: (Include photo numbers here or on a separate sheet.)

SOIL Sampling Point Wetland

		o the dep				tor or co	nfirm the absence of	f indicators.)
Depth	Matrix			x Featur	_	1 2	Tautuma	Domonto
(inches)	Color (moist)	<u>%</u>	Color (moist)	<u>%</u>	Type <sup>1</sup>	Loc <sup>2</sup>	Texture	Remarks
0-3	10YR 2/1	100						Organic "duff" layer
3-8	10YR 2/1	100		—		—		Sapric
8-18	10YR 4/3	80	10YR 4/2	20	<u>C</u>	<u>M</u>		Sandy with redox
1- 0.0			<u> </u>				21	
Hydric Soil I	ncentration, D=Deple	etion, Rivi	=Reduced Matrix, N	/IS=IVIas	ked Sand	Grains.		L=Pore Lining, M=Matrix.  or Problematic Hydric Soils <sup>3</sup> :
Histosol (		_	Polyvalue Belo	w Surfa	ce (S8) (I	LRR R,		ck (A10) ( <b>LRR K, L, MLRA 149B</b> )
	ipedon (A2)	_	MLRA 149B	•				airie Redox (A16) (LRR K, L, R)
Black His		-	Thin Dark Surf	, ,	•		· —	cky Peat or Peat (S3) (LRR K, L, R)
	Sulfide (A4)	-	High Chroma S			-		e Below Surface (S8) (LRR K, L)
	Layers (A5) Below Dark Surface	- (Δ11)	Loamy Mucky Loamy Gleyed			Χ N, L)		k Surface (S9) ( <b>LRR K, L</b> ) ganese Masses (F12) ( <b>LRR K, L, R</b> )
	rk Surface (A12)	(Δ11)	Depleted Matri		1 2)			t Floodplain Soils (F19) (MLRA 149B)
	ucky Mineral (S1)	-	Redox Dark Su		6)			podic (TA6) ( <b>MLRA 144A, 145, 149B</b> )
	leyed Matrix (S4)	-	Depleted Dark					ent Material (F21)
Sandy Re	edox (S5)	_	Redox Depres	sions (F	B)		Very Sha	allow Dark Surface (F22)
	Matrix (S6)	_	Marl (F10) ( <b>LR</b>	R K, L)			Other (E	xplain in Remarks)
X Dark Sur	face (S7)							
<sup>3</sup> Indicators of	hydrophytic vegetati	on and we	tland hydrology m	ust be pr	esent, ur	nless distu	urbed or problematic.	
Restrictive L	ayer (if observed):		,		·		•	
Type:								v
Depth (in	ches):						Hydric Soil Preser	nt? Yes X No
Remarks:	n is revised from Nor	theentral	and Northeast Rea	ional Su	nnlemen	t Varsion	2.0 to include the NPC	CS Field Indicators of Hydric Soils,
	2015 Errata. (http://w							53 Field indicators of Frydric Soils,

Project/Site: Grove Street	City/County: Franklin Sampling Date: 5/13/2021						
Applicant/Owner: Town of Franklin	<u> </u>						
Investigator(s): Jonathan Niro & Julia Stearns (BETA Group, Inc.)	Section, Township, Range: Norfolk C	County					
Landform (hillside, terrace, etc.): Floodplain Local	relief (concave, convex, none): Concave	Slope %: 0					
Subregion (LRR or MLRA): LRR R, MLRA 144A Lat: 42.066353	Long: -71.426820	Datum: WGS84					
Soil Map Unit Name: Hinckley loamy sand, 3 to 8 percent slopes	NWI classification:						
Are climatic / hydrologic conditions on the site typical for this time of year?		explain in Remarks.)					
Are Vegetation, Soil, or Hydrology significantly distu							
Are Vegetation, Soil, or Hydrology naturally problem		Remarks.)					
SUMMARY OF FINDINGS – Attach site map showing san		portant features, etc.					
Hydrophytic Vegetation Present? Yes No _X	Is the Sampled Area						
Hydric Soil Present?  Yes No X	within a Wetland? Yes	No X					
Wetland Hydrology Present?  Yes  No X	If yes, optional Wetland Site ID: WF6-111						
Remarks: (Explain alternative procedures here or in a separate report.)	<u> </u>						
HYDROLOGY							
Wetland Hydrology Indicators:	Secondary Indicators (n	ninimum of two required)					
Primary Indicators (minimum of one is required; check all that apply)	Surface Soil Cracks						
Surface Water (A1) Water-Stained Leaves (		, ,					
High Water Table (A2)  Aquatic Fauna (B13)	· · · · · · · · · · · · · · · · · · ·	Moss Trim Lines (B16)					
Saturation (A3) Marl Deposits (B15)	Dry-Season Water <sup>-</sup>	Dry-Season Water Table (C2)					
Water Marks (B1) Hydrogen Sulfide Odor	(C1) Crayfish Burrows (C	28)					
Sediment Deposits (B2)  Oxidized Rhizospheres	on Living Roots (C3) Saturation Visible o	n Aerial Imagery (C9)					
Drift Deposits (B3) Presence of Reduced I	ron (C4)Stunted or Stressed	d Plants (D1)					
Algal Mat or Crust (B4) Recent Iron Reduction i	. , :	• • • • • • • • • • • • • • • • • • • •					
Iron Deposits (B5)  Thin Muck Surface (C7)		Shallow Aquitard (D3)					
Inundation Visible on Aerial Imagery (B7) Other (Explain in Rema							
Sparsely Vegetated Concave Surface (B8)	FAC-Neutral Test (I	D5)					
Field Observations:							
Surface Water Present? Yes No X Depth (inches)  Water Table Present? Yes No X Depth (inches)  Soturation Present? Yes No X Depth (inches)	·——						
Water Table Present? Yes No X Depth (inches)	:	Waa Na V					
Saturation Present? Yes No _X Depth (inches) (includes capillary fringe)	Wetland Hydrology Present?	Yes NoX					
Describe Recorded Data (stream gauge, monitoring well, aerial photos, pr	evious inspections) if available:						
Bosonibo Nosoridod Balla (elrodini gadgo, monitorini ginologi, pr	evicus inspections, in available.						
Remarks:							

**VEGETATION** – Use scientific names of plants. Sampling Point: Upland Absolute Dominant Indicator Tree Stratum (Plot size: 30' radius ) % Cover Species? Status **Dominance Test worksheet:** FAC 1. Acer rubrum 50 Yes Number of Dominant Species 2. Pinus strobus 10 FACU No That Are OBL, FACW, or FAC: (A) 3. **Total Number of Dominant** 4. Species Across All Strata: 4 (B) 5. Percent of Dominant Species That Are OBL, FACW, or FAC: 6. 25.0% (A/B) Prevalence Index worksheet: 60 =Total Cover Total % Cover of: Multiply by: **OBL** species Sapling/Shrub Stratum (Plot size: 15' radius ) **FACW** species 0 x 2 = 1. Berberis thunbergii 10 FACU 0 Yes 2. Rosa multiflora **FACU** FAC species 50 x 3 = 150 3. **FACU** species 130 x 4 = 520 4. **UPL** species 0 x 5 = 5. Column Totals: 180 670 6. Prevalence Index = B/A = **Hydrophytic Vegetation Indicators:** 1 - Rapid Test for Hydrophytic Vegetation 40 =Total Cover Herb Stratum (Plot size: 5' radius ) 2 - Dominance Test is >50% Maianthemum canadense **FACU** 3 - Prevalence Index is ≤3.01 2. 4 - Morphological Adaptations (Provide supporting data in Remarks or on a separate sheet) 3. 4. Problematic Hydrophytic Vegetation<sup>1</sup> (Explain) 5. <sup>1</sup>Indicators of hydric soil and wetland hydrology must 6. be present, unless disturbed or problematic. 7. **Definitions of Vegetation Strata:** 8. Tree - Woody plants 3 in. (7.6 cm) or more in 9. diameter at breast height (DBH), regardless of height. Sapling/shrub - Woody plants less than 3 in. DBH and greater than or equal to 3.28 ft (1 m) tall. Herb - All herbaceous (non-woody) plants, regardless 80 =Total Cover of size, and woody plants less than 3.28 ft tall. Woody Vine Stratum (Plot size: 15' radius ) Woody vines - All woody vines greater than 3.28 ft in height. 2. Hydrophytic 3. Vegetation Present? Yes No X =Total Cover Remarks: (Include photo numbers here or on a separate sheet.)

SOIL Sampling Point Upland

Profile Desc		to the de				tor or co	onfirm the absence of indicators.)
Depth	Matrix	0/		k Featur		1 2	Tartius
(inches) 0-2	Color (moist) 10YR 2/1	100	Color (moist)	<u>%</u>	Type <sup>1</sup>	Loc <sup>2</sup>	Texture Remarks  Organic "duff" layer
2-3	10YR 3/3	100					Loamy sand
3-7	10YR 3/4	100					Fine sandy loam
7-18	7.5YR 4/4	100					Sand
7-10	7.51K 4/4	100					Sanu
							<del></del>
		-					
<sup>1</sup> Type: C=Co	ncentration, D=Depl	etion. RM	=Reduced Matrix. N	 IS=Mas	ked Sand	Grains.	<sup>2</sup> Location: PL=Pore Lining, M=Matrix.
Hydric Soil I							Indicators for Problematic Hydric Soils <sup>3</sup> :
Histosol (			Polyvalue Belo		ce (S8) ( <b>I</b>	_RR R,	2 cm Muck (A10) (LRR K, L, MLRA 149B)
	ipedon (A2)		MLRA 149B		\	MIDAA	Coast Prairie Redox (A16) (LRR K, L, R)
Black His	stic (A3) n Sulfide (A4)		Thin Dark Surfa High Chroma S				149B) 5 cm Mucky Peat or Peat (S3) (LRR K, L, R) Polyvalue Below Surface (S8) (LRR K, L)
	Layers (A5)		Loamy Mucky			-	Thin Dark Surface (S9) (LRR K, L)
	Below Dark Surface	(A11)	Loamy Gleyed			, ,	Iron-Manganese Masses (F12) (LRR K, L, R)
Thick Da	rk Surface (A12)		Depleted Matri	x (F3)			Piedmont Floodplain Soils (F19) (MLRA 149E
Sandy M	ucky Mineral (S1)		Redox Dark Su	ırface (F	<del>-</del> 6)		Mesic Spodic (TA6) ( <b>MLRA 144A, 145, 149B</b> )
	eyed Matrix (S4)		Depleted Dark				Red Parent Material (F21)
	edox (S5)		Redox Depress	,	8)		Very Shallow Dark Surface (F22)
Stripped Dark Suri	Matrix (S6)		Marl (F10) ( <b>LR</b>	R K, L)			Other (Explain in Remarks)
Dark Suit	iace (Sr)						
<sup>3</sup> Indicators of	hydrophytic vegetat	ion and w	etland hydrology mu	ıst be pı	resent, ur	less dist	turbed or problematic.
	ayer (if observed):						
Type:	ahaa):						Hydric Soil Present? Yes No X
Depth (in	cnes).						Hydric Soil Present? Yes No _X
Remarks: This data forr	n is revised from No	rthcentral	and Northeast Regi	onal Su	pplement	Version	2.0 to include the NRCS Field Indicators of Hydric Soils,
	2015 Errata. (http://w						

Project/Site: Grove Street	City/County: Franklin Sampling Date: 5/13/202					
Applicant/Owner: Town of Franklin	State: MA Sampling Point: Wetla					
Investigator(s): Jonathan Niro & Julia Stearns (BETA Group, Inc.)	Section, Township, Range: Norfolk County					
<del>-</del>	relief (concave, convex, none): Concave Slope %: 0					
Subregion (LRR or MLRA): LRR R, MLRA 144A Lat: 42.066353	Long: -71.426820 Datum: WGS84					
Soil Map Unit Name: Hinckley loamy sand, 3 to 8 percent slopes	NWI classification: PFO1E					
Are climatic / hydrologic conditions on the site typical for this time of year?	Yes X No (If no, explain in Remarks.)					
Are Vegetation, Soil, or Hydrologysignificantly distur	rbed? Are "Normal Circumstances" present? Yes X No					
Are Vegetation, Soil, or Hydrologynaturally problems	<del></del> -					
SUMMARY OF FINDINGS – Attach site map showing sam						
Hydrophytic Vegetation Present?  Hydric Soil Present?  Wetland Hydrology Present?  Yes X No  Yes X No	Is the Sampled Area within a Wetland?  If yes, optional Wetland Site ID: WF6-111					
HYDROLOGY						
Wetland Hydrology Indicators:	Secondary Indicators (minimum of two required)					
Primary Indicators (minimum of one is required; check all that apply)	Surface Soil Cracks (B6)					
Surface Water (A1) — Water-Stained Leaves (						
High Water Table (A2)  — Aquatic Fauna (B13)  — Marl Deposits (B15)	Moss Trim Lines (B16)					
X Saturation (A3) — Marl Deposits (B15) Water Marks (B1) Hydrogen Sulfide Odor	Crayfish Burrows (C8)					
Sediment Deposits (B2)  Sediment Deposits (B2)  Oxidized Rhizospheres						
Drift Deposits (B3)  Presence of Reduced In						
Algal Mat or Crust (B4)  Recent Iron Reduction is						
Iron Deposits (B5)  Iron Deposits (B5)  Thin Muck Surface (C7)	• • • • • • • • • • • • • • • • • • • •					
Inundation Visible on Aerial Imagery (B7)  Other (Explain in Remainder (B7)						
Sparsely Vegetated Concave Surface (B8)	FAC-Neutral Test (D5)					
	TAO Neutral Test (E5)					
Field Observations: Surface Water Present? Yes No X Depth (inches):						
' ` ` '						
Water Table Present? Yes No X Depth (inches): Saturation Present? Yes X No Depth (inches):						
(includes capillary fringe)	wettand right ology riesent: res_x_No					
Describe Recorded Data (stream gauge, monitoring well, aerial photos, pre	evious inspections), if available:					
Janger, and Janes, and	,					
Remarks:						

**VEGETATION** – Use scientific names of plants. Sampling Point: Wetland Absolute Dominant Indicator Tree Stratum (Plot size: 30' radius ) % Cover Species? Status **Dominance Test worksheet:** FAC 1. Acer rubrum 50 Yes Number of Dominant Species 2. Pinus strobus 10 FACU No That Are OBL, FACW, or FAC: (A) 3. **Total Number of Dominant** 4. Species Across All Strata: 5 (B) 5. Percent of Dominant Species That Are OBL, FACW, or FAC: 6. 60.0% (A/B) Prevalence Index worksheet: 60 =Total Cover Total % Cover of: Multiply by: Sapling/Shrub Stratum (Plot size: 15' radius ) **OBL** species **FACW** species 0 x 2 = 1. FAC 0 Frangula alnus 10 Yes 2. Rosa multiflora **FACU** FAC species 60 x 3 = 180 3. **FACU** species 100 x 4 = 400 4. **UPL** species 0 x 5 = 0 5. Column Totals: 175 595 (B) 6. Prevalence Index = B/A = 3.40 **Hydrophytic Vegetation Indicators:** 40 =Total Cover 1 - Rapid Test for Hydrophytic Vegetation Herb Stratum (Plot size: 5' radius ) X 2 - Dominance Test is >50% Maianthemum canadense FACU 3 - Prevalence Index is ≤3.0<sup>1</sup> 15 OBL 4 - Morphological Adaptations (Provide supporting 2. Symplocarpus foetidus Yes data in Remarks or on a separate sheet) 3. 4. Problematic Hydrophytic Vegetation<sup>1</sup> (Explain) 5. <sup>1</sup>Indicators of hydric soil and wetland hydrology must 6. be present, unless disturbed or problematic. 7. **Definitions of Vegetation Strata:** 8. Tree – Woody plants 3 in. (7.6 cm) or more in 9. diameter at breast height (DBH), regardless of height. Sapling/shrub - Woody plants less than 3 in. DBH and greater than or equal to 3.28 ft (1 m) tall. Herb - All herbaceous (non-woody) plants, regardless 75 =Total Cover of size, and woody plants less than 3.28 ft tall. Woody Vine Stratum (Plot size: 15' radius ) Woody vines - All woody vines greater than 3.28 ft in height. 2. Hydrophytic 3. Vegetation Present? No\_ Yes X =Total Cover Remarks: (Include photo numbers here or on a separate sheet.)

SOIL Sampling Point Wetland

		to the dep				tor or co	nfirm the absence of	f indicators.)
Depth (inches)	Matrix Color (moist)	%	Color (moist)	x Featur %	res Type <sup>1</sup>	Loc <sup>2</sup>	Texture	Remarks
0-4	10YR 3/2	100	Color (moist)	70	Туре	LOC	rexture	20% organic material
4-10	10YR 2/1	100					-	Organic
10-20	10YR 3/2	80	10YR 4/1	20	С	<u></u>		Redox concentrations
10 20	10111072		1011(1)1			<del></del> -		Trodox componerations
							-	
¹Type: C=Co	oncentration, D=Depl	etion. RM:	=Reduced Matrix. N	 ∕IS=Mas	ked Sand	Grains.	<sup>2</sup> Location: P	L=Pore Lining, M=Matrix.
Hydric Soil I			, , , , , , , , , , , , , , , , , , , ,					or Problematic Hydric Soils <sup>3</sup> :
Histosol	• •	•	Polyvalue Belo		ce (S8) (I	LRR R,		ck (A10) ( <b>LRR K, L, MLRA 149B</b> )
	ipedon (A2)		MLRA 149B	,				airie Redox (A16) (LRR K, L, R)
Black His			Thin Dark Surf					cky Peat or Peat (S3) (LRR K, L, R)
	n Sulfide (A4)		High Chroma S Loamy Mucky			-		e Below Surface (S8) (LRR K, L)
	Layers (A5) Below Dark Surface	. (Δ11)	Loamy Gleyed			Χ <b>N</b> , L)		k Surface (S9) ( <b>LRR K, L</b> ) ganese Masses (F12) ( <b>LRR K, L, R</b> )
	rk Surface (A12)	(A11)	Depleted Matri		12)			t Floodplain Soils (F19) (MLRA 149B)
	ucky Mineral (S1)	•	Redox Dark Su		<del>-</del> 6)			podic (TA6) (MLRA 144A, 145, 149B)
	leyed Matrix (S4)	•	Depleted Dark					ent Material (F21)
	edox (S5)	•	Redox Depress					allow Dark Surface (F22)
	Matrix (S6)	•	 Marl (F10) ( <b>LR</b>	R K, L)	,			xplain in Remarks)
X Dark Sur	face (S7)	•						
<sup>3</sup> Indicators of	hydrophytic vegetati	ion and we	atland hydrology mi	ist ha ni	recent ur	alace dietu	urhed or problematic	
	.ayer (if observed):	on and we	etiana nyarology mi	ust be pi	eseni, ui	iless dist	inded of problematic.	
Type:								
Depth (in	ches):						Hydric Soil Preser	nt? Yes <u>X</u> No
Remarks:								
	m is revised from No 2015 Errata. (http://w							CS Field Indicators of Hydric Soils,
version 7.0, 2	2013 Ellata. (III.p.//w	www.iiics.c	sua.gov/internet/1	JL_DOC	JOIVILIVI	0/11103142	.pz_031293.d0cx)	

Project/Site: Grove Street	City/County: Franklin Sampling Date: 5/13/2021				
Applicant/Owner: Town of Franklin	State: MA Sampling Point: Upland				
Investigator(s): Jonathan Niro & Julia Stearns (BETA Group, Inc.)	Section, Township, Range: Norfolk County				
Landform (hillside, terrace, etc.): Toe of roadside slope Local	relief (concave, convex, none): Concave Slope %: 0				
Subregion (LRR or MLRA): LRR R, MLRA 144A Lat: 42.066353	Long: -71.426820 Datum: WGS84				
Soil Map Unit Name: Swansea muck, 0 to 1 percent slopes	NWI classification: N/A				
Are climatic / hydrologic conditions on the site typical for this time of year?	Yes X No (If no, explain in Remarks.)				
Are Vegetation, Soil, or Hydrology significantly distur	<del></del>				
Are Vegetation, Soil, or Hydrologynaturally problems					
SUMMARY OF FINDINGS – Attach site map showing sam	npling point locations, transects, important features, etc.				
Hydrophytic Vegetation Present? Yes No _X	Is the Sampled Area				
Hydric Soil Present?  Yes No X	within a Wetland? Yes No_X_				
Wetland Hydrology Present? Yes No X	If yes, optional Wetland Site ID: WF9-103				
Remarks: (Explain alternative procedures here or in a separate report.)					
romano. (Explain anomalivo proceduros noto el in a coparato roporti)					
HYDROLOGY					
Wetland Hydrology Indicators:	Secondary Indicators (minimum of two required)				
Primary Indicators (minimum of one is required; check all that apply)	Surface Soil Cracks (B6)				
Surface Water (A1) Water-Stained Leaves (	(B9) Drainage Patterns (B10)				
High Water Table (A2) Aquatic Fauna (B13)	Moss Trim Lines (B16)				
Saturation (A3) Marl Deposits (B15)	Dry-Season Water Table (C2)				
Water Marks (B1) Hydrogen Sulfide Odor	(C1) Crayfish Burrows (C8)				
Sediment Deposits (B2)  Oxidized Rhizospheres	on Living Roots (C3) Saturation Visible on Aerial Imagery (C9)				
Drift Deposits (B3) Presence of Reduced Ir	ron (C4) Stunted or Stressed Plants (D1)				
Algal Mat or Crust (B4)Recent Iron Reduction in	n Tilled Soils (C6) Geomorphic Position (D2)				
Iron Deposits (B5)Thin Muck Surface (C7)	Shallow Aquitard (D3)				
Inundation Visible on Aerial Imagery (B7) Other (Explain in Remarks) Microtopographic Relief (D4)					
Sparsely Vegetated Concave Surface (B8)	FAC-Neutral Test (D5)				
Field Observations:					
Surface Water Present? Yes No X Depth (inches):  Water Table Present? Yes No X Depth (inches):  Soturation Present? Yes No X Depth (inches):	: <u> </u>				
Water Table Present? Yes No X Depth (inches):	:				
Saturation Present? Tes No _X Deptir (inches).	:   Wetland Hydrology Present? Yes No _X				
(includes capillary fringe)  Describe Recorded Data (stream gauge, monitoring well, aerial photos, pre	evious inspections) if available:				
Describe Necorded Data (stream gauge, monitoring well, aerial priotos, pre	evious inspections), ii available.				
Remarks:					

**VEGETATION** – Use scientific names of plants. Sampling Point: Upland Absolute Dominant Indicator Tree Stratum (Plot size: 30' radius ) % Cover Species? Status **Dominance Test worksheet:** FAC 1. Acer rubrum 50 Yes Number of Dominant Species 2. Pinus strobus 15 FACU Yes That Are OBL, FACW, or FAC: (A) Betula populifolia 3 3. No FAC **Total Number of Dominant** 4. Species Across All Strata: 4 (B) 5. Percent of Dominant Species That Are OBL, FACW, or FAC: 6. 25.0% (A/B) Prevalence Index worksheet: 68 =Total Cover Total % Cover of: Multiply by: **OBL** species Sapling/Shrub Stratum (Plot size: 15' radius ) **FACW** species 0 x 2 = 1. Euonymus alatus UPL 0 2. FAC species 68 x 3 = 204 3. FACU species 105 x 4 = 420 4. **UPL** species 5 x 5 = 25 5. Column Totals: 178 (A) 649 6. Prevalence Index = B/A = 3.65 **Hydrophytic Vegetation Indicators:** 1 - Rapid Test for Hydrophytic Vegetation 5 =Total Cover Herb Stratum (Plot size: 5' radius ) 2 - Dominance Test is >50% Maianthemum canadense 80 **FACU** 3 - Prevalence Index is ≤3.01 15 No FAC 4 - Morphological Adaptations (Provide supporting 2. Toxicodendron radicans data in Remarks or on a separate sheet) 3. Pteridium aquilinum 10 FACU 4. Problematic Hydrophytic Vegetation<sup>1</sup> (Explain) 5. <sup>1</sup>Indicators of hydric soil and wetland hydrology must 6. be present, unless disturbed or problematic. 7. **Definitions of Vegetation Strata:** 8. Tree – Woody plants 3 in. (7.6 cm) or more in 9. diameter at breast height (DBH), regardless of height. Sapling/shrub – Woody plants less than 3 in. DBH and greater than or equal to 3.28 ft (1 m) tall. Herb - All herbaceous (non-woody) plants, regardless 105 =Total Cover of size, and woody plants less than 3.28 ft tall. Woody Vine Stratum (Plot size: 15' radius ) Woody vines - All woody vines greater than 3.28 ft in height. 2. Hydrophytic 3. Vegetation Present? Yes No X =Total Cover Remarks: (Include photo numbers here or on a separate sheet.)

SOIL Sampling Point Upland

		o the depti				tor or co	onfirm the absence of indicators.)
Depth	Matrix			x Featur		. 2	
(inches)	Color (moist)	<u>%</u>	Color (moist)	<u>%</u>	Type <sup>1</sup>	Loc <sup>2</sup>	Texture Remarks
0-6	10YR 3/2	100					Gravelly/sandy loam (fill)
6-15	10YR 4/3						Gravelly/sandy loam (fill)
	ncentration, D=Deple	etion, RM=F	Reduced Matrix, N	/IS=Masl	ked Sand	Grains.	<sup>2</sup> Location: PL=Pore Lining, M=Matrix.
Hydric Soil Ir Histosol (			Polyvalue Belo	w Surfa	oo (S9) (I	DD D	Indicators for Problematic Hydric Soils <sup>3</sup> : 2 cm Muck (A10) (LRR K, L, MLRA 149B)
	pedon (A2)	_	MLRA 149B		Le (30) (I	-NN N,	Coast Prairie Redox (A16) (LRR K, L, R)
Black His			Thin Dark Surf	•	(LRR R,	MLRA 1	
	Sulfide (A4)	_	High Chroma S			-	Polyvalue Below Surface (S8) (LRR K, L)
	Layers (A5)		Loamy Mucky			R K, L)	Thin Dark Surface (S9) (LRR K, L)
	Below Dark Surface	(A11) _	Loamy Gleyed		F2)		Iron-Manganese Masses (F12) (LRR K, L, R)
	k Surface (A12) ucky Mineral (S1)	_	Depleted Matri Redox Dark Su		·e)		Piedmont Floodplain Soils (F19) (MLRA 1498 Mesic Spodic (TA6) (MLRA 144A, 145, 1498)
	eyed Matrix (S4)	_	Depleted Dark				Red Parent Material (F21)
Sandy Re		_	Redox Depress				Very Shallow Dark Surface (F22)
	Matrix (S6)		Marl (F10) (LR	,	3,		Other (Explain in Remarks)
Dark Surf				, ,			
3							
	hydrophytic vegetation ayer (if observed):	on and wet	land hydrology mi	ust be pr	esent, ur	iless disti	turbed or problematic.
Type:	ayer (ii observed).						
Depth (inc	ches):						Hydric Soil Present? Yes No _X_
Remarks:							
	n is revised from Nor 2015 Errata. (http://w						2.0 to include the NRCS Field Indicators of Hydric Soils,
V C 1 3 1 0 1 1	.010 Enata. (http://w	ww.iiios.us	da.gov/internet/1	JL_DOC	OWILIVI	5/11103142	2P2_001233.d00x)

Project/Site: Grove Street	City/County: Franklin Sampling Date: 5/13/2021
Applicant/Owner: Town of Franklin	State: MA Sampling Point: Wetland
Investigator(s): Jonathan Niro & Julia Stearns (BETA Group, Inc.)	Section, Township, Range: Norfolk County
	relief (concave, convex, none): Concave Slope %: 0
Subregion (LRR or MLRA): LRR R, MLRA 144A Lat: 42.066353	Long: -71.426820 Datum: WGS84
Soil Map Unit Name: Swansea muck, 0 to 1 percent slopes	NWI classification: PFO1E
Are climatic / hydrologic conditions on the site typical for this time of year?	Yes X No (If no, explain in Remarks.)
Are Vegetation, Soil, or Hydrologysignificantly distur	rbed? Are "Normal Circumstances" present? Yes X No
Are Vegetation, Soil, or Hydrologynaturally problems	
SUMMARY OF FINDINGS – Attach site map showing sam	
Hydrophytic Vegetation Present?         Yes X         No           Hydric Soil Present?         Yes X         No           Wetland Hydrology Present?         Yes X         No	Is the Sampled Area within a Wetland?  If yes, optional Wetland Site ID: WF9-103
HYDROLOGY	
Wetland Hydrology Indicators:	Secondary Indicators (minimum of two required)
Primary Indicators (minimum of one is required; check all that apply)	Surface Soil Cracks (B6)
Surface Water (A1) X Water-Stained Leaves (	
High Water Table (A2)  Aquatic Fauna (B13)	Moss Trim Lines (B16)
X Saturation (A3) Marl Deposits (B15)	Dry-Season Water Table (C2)
Water Marks (B1) Hydrogen Sulfide Odor	(C1) Crayfish Burrows (C8)
Sediment Deposits (B2)  Oxidized Rhizospheres	
Drift Deposits (B3) Presence of Reduced Ir	· · · · · · · · · · · · · · · · · · ·
Algal Mat or Crust (B4)  Recent Iron Reduction in	
Iron Deposits (B5) Thin Muck Surface (C7)	
Inundation Visible on Aerial Imagery (B7) Other (Explain in Remai	
Sparsely Vegetated Concave Surface (B8)	FAC-Neutral Test (D5)
Field Observations:	
Surface Water Present? Yes No X Depth (inches): Water Table Present? Yes No X Depth (inches):	
Water Table Present? Yes No X Depth (inches): Saturation Present? Yes X No Depth (inches):	
(includes capillary fringe)	Wettalia Hydrology Freschi: Tes _X_ No
Describe Recorded Data (stream gauge, monitoring well, aerial photos, pre	evious inspections), if available:
Remarks:	

**VEGETATION** – Use scientific names of plants. Sampling Point: Wetland Absolute Dominant Indicator Tree Stratum (Plot size: 30' radius ) % Cover Species? Status **Dominance Test worksheet:** FAC 1. Acer rubrum 80 Yes Number of Dominant Species 2. Pinus strobus 3 FACU No That Are OBL, FACW, or FAC: (A) 3. **Total Number of Dominant** 4. Species Across All Strata: 3 (B) 5. Percent of Dominant Species That Are OBL, FACW, or FAC: 6. 100.0% (A/B) Prevalence Index worksheet: 83 =Total Cover Total % Cover of: Multiply by: Sapling/Shrub Stratum (Plot size: 15' radius ) **OBL** species **FACW** species 10 x 2 = 1. Viburnum dentatum FAC 20 2. FAC species 88 x 3 = 3. **FACU** species 3 x 4 = 12 4. **UPL** species 0 x 5 = 0 5. Column Totals: 181 376 6. Prevalence Index = B/A = 2.08 **Hydrophytic Vegetation Indicators:** 8 =Total Cover 1 - Rapid Test for Hydrophytic Vegetation Herb Stratum (Plot size: 5' radius ) X 2 - Dominance Test is >50% Symplocarpus foetidus 80 OBL X 3 - Prevalence Index is ≤3.0<sup>1</sup> Osmundastrum cinnamomeum 10 **FACW** 4 - Morphological Adaptations (Provide supporting 2. No data in Remarks or on a separate sheet) 3. 4. Problematic Hydrophytic Vegetation<sup>1</sup> (Explain) 5. <sup>1</sup>Indicators of hydric soil and wetland hydrology must 6. be present, unless disturbed or problematic. 7. **Definitions of Vegetation Strata:** 8. Tree – Woody plants 3 in. (7.6 cm) or more in 9. diameter at breast height (DBH), regardless of height. Sapling/shrub - Woody plants less than 3 in. DBH and greater than or equal to 3.28 ft (1 m) tall. Herb - All herbaceous (non-woody) plants, regardless 90 =Total Cover of size, and woody plants less than 3.28 ft tall. Woody Vine Stratum (Plot size: 15' radius ) Woody vines - All woody vines greater than 3.28 ft in height. 2. Hydrophytic 3. Vegetation Present? No\_ Yes X =Total Cover Remarks: (Include photo numbers here or on a separate sheet.)

SOIL Sampling Point Wetland

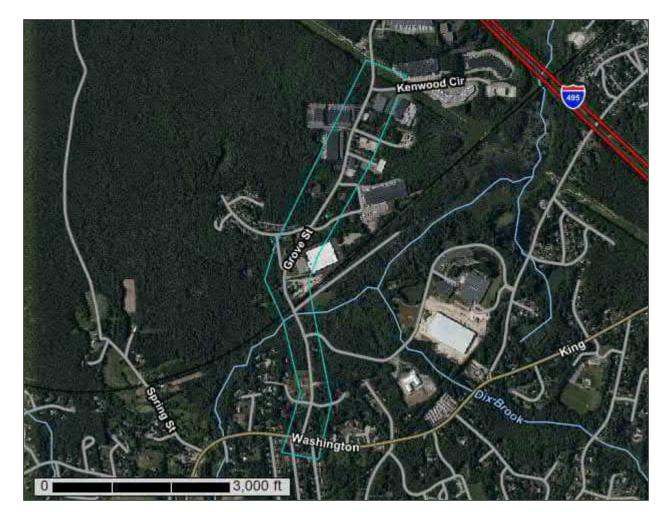
		the depth				tor or co	onfirm the absence of indicators.)
Depth	Matrix			k Feature	-	. 2	
(inches)	Color (moist)	<u>%</u>	Color (moist)	<u>%</u>	Type	Loc <sup>2</sup>	Texture Remarks
0-16	10YR 2/1	100					Sapric
		— –					
							·
<sup>1</sup> Type: C=Cor	ncentration, D=Deple	tion RM-R	educed Matrix M	IS=Masl	ed Sand	Grains	<sup>2</sup> Location: PL=Pore Lining, M=Matrix.
Hydric Soil In		tion, rawi–ra	Saucea Matrix, IV	io-iviasi	ca cana	Oranis.	Indicators for Problematic Hydric Soils <sup>3</sup> :
X Histosol (A			Polyvalue Belo	w Surfac	ce (S8) ( <b>I</b>	RR R.	2 cm Muck (A10) (LRR K, L, MLRA 149B)
	pedon (A2)		MLRA 149B)		() (-	· · · · · · · · · · · · · · · · ·	Coast Prairie Redox (A16) (LRR K, L, R)
Black Hist			Thin Dark Surfa		(LRR R,	MLRA 1	
	Sulfide (A4)		– High Chroma S				Polyvalue Below Surface (S8) (LRR K, L)
Stratified	Layers (A5)		Loamy Mucky I	Mineral (	F1) (LRF	R K, L)	Thin Dark Surface (S9) (LRR K, L)
Depleted	Below Dark Surface	(A11)	Loamy Gleyed	Matrix (I	<del>-</del> 2)		Iron-Manganese Masses (F12) (LRR K, L, R)
Thick Dar	k Surface (A12)		Depleted Matrix	k (F3)			Piedmont Floodplain Soils (F19) (MLRA 149B)
Sandy Mu	cky Mineral (S1)	_	_Redox Dark Su	rface (F	6)		Mesic Spodic (TA6) ( <b>MLRA 144A, 145, 149B</b> )
	eyed Matrix (S4)	_	_Depleted Dark				Red Parent Material (F21)
Sandy Re		_	_Redox Depress	,	3)		Very Shallow Dark Surface (F22)
	Matrix (S6)	_	_Marl (F10) ( <b>LR</b> l	R K, L)			Other (Explain in Remarks)
Dark Surf	ace (S7)						
31						باعدال مدا	unbaad au muablaas at'a
	ayer (if observed):	n and wella	na nyarology mu	ist be pr	esent, ur	iless dist	urbed or problematic.
Type:	ayer (ii observed).						
-	shoo).						Hydric Soil Present? Yes X No
Depth (inc	nes).						Hydric Soil Present? Yes X No
Remarks: This data form	is revised from Nort	thcentral an	d Northeast Regi	onal Su <sub>l</sub>	oplement	Version 2	2.0 to include the NRCS Field Indicators of Hydric Soils,
Version 7.0, 2	015 Errata. (http://ww	ww.nrcs.usd	a.gov/Internet/FS	SE_DOC	UMENT	S/nrcs142	2p2_051293.docx)



**VRCS** 

Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

# Custom Soil Resource Report for Norfolk and Suffolk Counties, Massachusetts



# **Preface**

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2 053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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# **How Soil Surveys Are Made**

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

# Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



#### MAP LEGEND

#### Area of Interest (AOI)

Area of Interest (AOI)

#### Soils

Soil Map Unit Polygons

Soil Map Unit Lines

Soil Map Unit Points

#### **Special Point Features**

(o)

Blowout

Borrow Pit

Clay Spot

**Closed Depression** 

Gravel Pit

**Gravelly Spot** 

Landfill Lava Flow

Marsh or swamp

Mine or Quarry

Miscellaneous Water Perennial Water

Rock Outcrop

Saline Spot

Sandy Spot

Severely Eroded Spot

Sinkhole

Slide or Slip

Sodic Spot

Spoil Area



Stony Spot

Very Stony Spot

Ŷ

Wet Spot Other

Δ

Special Line Features

#### Water Features

Streams and Canals

#### Transportation

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Rails

Interstate Highways

**US Routes** 

Major Roads

00

Local Roads

#### Background

Aerial Photography

#### MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:25.000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Norfolk and Suffolk Counties, Massachusetts Survey Area Data: Version 16, Jun 11, 2020

Soil map units are labeled (as space allows) for map scales 1:50.000 or larger.

Date(s) aerial images were photographed: Jul 5, 2019—Jul 8, 2019

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

# Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
10	Scarboro and Birdsall soils, 0 to 3 percent slopes	3.2	2.9%
51	Swansea muck, 0 to 1 percent slopes	4.8	4.4%
71B	Ridgebury fine sandy loam, 3 to 8 percent slopes, extremely stony	1.4	1.2%
73A	Whitman fine sandy loam, 0 to 3 percent slopes, extremely stony	3.2	2.9%
103B	Charlton-Hollis-Rock outcrop complex, 3 to 8 percent slopes	6.4	5.8%
104D	Hollis-Rock outcrop-Charlton complex, 15 to 35 percent slopes	5.6	5.1%
245B	Hinckley loamy sand, 3 to 8 percent slopes	4.2	3.9%
245C	Hinckley loamy sand, 8 to 15 percent slopes	13.9	12.6%
253D	Hinckley loamy sand, 15 to 35 percent slopes	5.3	4.8%
254A	Merrimac fine sandy loam, 0 to 3 percent slopes	6.2	5.6%
254B	Merrimac fine sandy loam, 3 to 8 percent slopes	39.7	35.9%
260B	Sudbury fine sandy loam, 2 to 8 percent slopes	3.7	3.4%
602	Urban land, 0 to 15 percent slopes	6.1	5.6%
653	Udorthents, sandy	6.6	6.0%
Totals for Area of Interest		110.3	100.0%

# **Map Unit Descriptions**

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the

characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered

practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

# Norfolk and Suffolk Counties, Massachusetts

# 10—Scarboro and Birdsall soils, 0 to 3 percent slopes

# **Map Unit Setting**

National map unit symbol: vkxw Elevation: 0 to 2,100 feet

Mean annual precipitation: 45 to 54 inches
Mean annual air temperature: 43 to 54 degrees F

Frost-free period: 145 to 240 days

Farmland classification: Not prime farmland

# **Map Unit Composition**

Scarboro and similar soils: 65 percent Birdsall and similar soils: 25 percent Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

# **Description of Scarboro**

# Setting

Landform: Terraces

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Loose sandy glaciofluvial deposits

# Typical profile

H1 - 0 to 9 inches: mucky fine sandy loam

H2 - 9 to 60 inches: stratified loamy fine sand to gravelly coarse sand

# Properties and qualities

Slope: 0 to 3 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Very poorly drained

Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat): High to very high (6.00

to 20.00 in/hr)

Depth to water table: About 0 inches

Frequency of flooding: None Frequency of ponding: Frequent

Available water capacity: Low (about 5.1 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 5w

Hydrologic Soil Group: A/D

Ecological site: F144AY031MA - Very Wet Outwash

Hydric soil rating: Yes

# **Description of Birdsall**

# Setting

Landform: Terraces

Landform position (two-dimensional): Toeslope

Landform position (three-dimensional): Tread

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Soft coarse-silty glaciolacustrine deposits

# **Typical profile**

H1 - 0 to 8 inches: very fine sandy loam H2 - 8 to 16 inches: very fine sandy loam

H3 - 16 to 60 inches: silt loam

# Properties and qualities

Slope: 0 to 3 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Very poorly drained

Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to

moderately high (0.06 to 0.20 in/hr) Depth to water table: About 0 inches

Frequency of flooding: None Frequency of ponding: Frequent

Available water capacity: Very high (about 12.8 inches)

# Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 5w

Hydrologic Soil Group: C/D

Ecological site: F144AY031MA - Very Wet Outwash

Hydric soil rating: Yes

# **Minor Components**

#### Swansea

Percent of map unit: 5 percent

Landform: Bogs Hydric soil rating: Yes

# Raynham

Percent of map unit: 3 percent Landform: Depressions Hydric soil rating: Yes

# Walpole

Percent of map unit: 2 percent

Landform: Terraces
Hydric soil rating: Yes

# 51—Swansea muck, 0 to 1 percent slopes

# **Map Unit Setting**

National map unit symbol: 2trl2 Elevation: 0 to 1,140 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

# **Map Unit Composition**

Swansea and similar soils: 80 percent *Minor components:* 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

# **Description of Swansea**

# Setting

Landform: Bogs, swamps

Landform position (three-dimensional): Dip

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Highly decomposed organic material over loose sandy and

gravelly glaciofluvial deposits

# Typical profile

Oa1 - 0 to 24 inches: muck
Oa2 - 24 to 34 inches: muck
Cg - 34 to 79 inches: coarse sand

# Properties and qualities

Slope: 0 to 1 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Very poorly drained

Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: About 0 to 6 inches

Frequency of flooding: Rare Frequency of ponding: Frequent

Available water capacity: Very high (about 16.5 inches)

# Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8w

Hydrologic Soil Group: B/D

Ecological site: F144AY043MA - Acidic Organic Wetlands

Hydric soil rating: Yes

# **Minor Components**

# Freetown

Percent of map unit: 10 percent Landform: Swamps, bogs

Landform position (three-dimensional): Dip

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

# Whitman

Percent of map unit: 5 percent

Landform: Depressions, drainageways

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

,

# Scarboro

Percent of map unit: 5 percent

Landform: Depressions, drainageways

Landform position (two-dimensional): Toeslope

Landform position (three-dimensional): Base slope, tread, dip

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

# 71B—Ridgebury fine sandy loam, 3 to 8 percent slopes, extremely stony

# **Map Unit Setting**

National map unit symbol: 2w69c

Elevation: 0 to 1,290 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

# **Map Unit Composition**

Ridgebury, extremely stony, and similar soils: 80 percent

Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

# **Description of Ridgebury, Extremely Stony**

# Setting

Landform: Drumlins, drainageways, hills, ground moraines, depressions

Landform position (two-dimensional): Toeslope, footslope Landform position (three-dimensional): Base slope, head slope

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Coarse-loamy lodgment till derived from gneiss, granite, and/or

schist

# Typical profile

Oe - 0 to 1 inches: moderately decomposed plant material

A - 1 to 6 inches: fine sandy loam Bw - 6 to 10 inches: sandy loam

Bg - 10 to 19 inches: gravelly sandy loam Cd - 19 to 66 inches: gravelly sandy loam

# **Properties and qualities**

Slope: 3 to 8 percent

Surface area covered with cobbles, stones or boulders: 9.0 percent

Depth to restrictive feature: 15 to 35 inches to densic material

Drainage class: Poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.14 in/hr)

Depth to water table: About 0 to 6 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm) Available water capacity: Low (about 3.0 inches)

# Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: D

Ecological site: F144AY009CT - Wet Till Depressions

Hydric soil rating: Yes

# **Minor Components**

# Woodbridge, extremely stony

Percent of map unit: 10 percent

Landform: Hills, ground moraines, drumlins

Landform position (two-dimensional): Footslope, summit, backslope

Landform position (three-dimensional): Crest, side slope

Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

# Whitman, extremely stony

Percent of map unit: 8 percent Landform: Depressions Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

# Paxton, extremely stony

Percent of map unit: 2 percent

Landform: Drumlins, hills, ground moraines

Landform position (two-dimensional): Shoulder, summit, backslope

Landform position (three-dimensional): Crest, side slope

Down-slope shape: Linear, convex Across-slope shape: Convex, linear

Hydric soil rating: No

# 73A—Whitman fine sandy loam, 0 to 3 percent slopes, extremely stony

# **Map Unit Setting**

National map unit symbol: 2w695

Elevation: 0 to 1,580 feet

Mean annual precipitation: 36 to 71 inches

Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

# **Map Unit Composition**

Whitman, extremely stony, and similar soils: 81 percent

Minor components: 19 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

# **Description of Whitman, Extremely Stony**

# Setting

Landform: Drainageways, hills, ground moraines, drumlins, depressions

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Coarse-loamy lodgment till derived from gneiss, granite, and/or

schist

# **Typical profile**

Oi - 0 to 1 inches: peat

A - 1 to 10 inches: fine sandy loam

*Bg - 10 to 17 inches:* gravelly fine sandy loam *Cdg - 17 to 61 inches:* fine sandy loam

# Properties and qualities

Slope: 0 to 3 percent

Surface area covered with cobbles, stones or boulders: 9.0 percent Depth to restrictive feature: 7 to 38 inches to densic material

Drainage class: Very poorly drained

Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.14 in/hr)

Depth to water table: About 0 to 6 inches

Frequency of flooding: None Frequency of ponding: Frequent

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm) Available water capacity: Low (about 3.0 inches)

# Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: D

Ecological site: F144AY041MA - Very Wet Till Depressions

Hydric soil rating: Yes

# **Minor Components**

# Ridgebury, extremely stony

Percent of map unit: 10 percent

Landform: Drumlins, drainageways, hills, ground moraines, depressions

Landform position (two-dimensional): Toeslope, footslope Landform position (three-dimensional): Base slope, head slope

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

# Scarboro

Percent of map unit: 5 percent

Landform: Depressions, drainageways, outwash deltas, outwash terraces

Landform position (three-dimensional): Tread

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

#### Swansea

Percent of map unit: 3 percent Landform: Marshes, swamps, bogs Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

# Woodbridge, extremely stony

Percent of map unit: 1 percent

Landform: Drumlins, hills, ground moraines

Landform position (two-dimensional): Backslope, footslope, summit

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

# 103B—Charlton-Hollis-Rock outcrop complex, 3 to 8 percent slopes

# **Map Unit Setting**

National map unit symbol: vktd

Elevation: 0 to 480 feet

Mean annual precipitation: 32 to

Mean annual precipitation: 32 to 54 inches Mean annual air temperature: 43 to 54 degrees F

Frost-free period: 120 to 240 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Charlton and similar soils: 40 percent Hollis and similar soils: 25 percent

Rock outcrop: 20 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

# **Description of Charlton**

#### Setting

Landform: Hills

Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Friable coarse-loamy ablation till derived from granite

# Typical profile

H1 - 0 to 6 inches: fine sandy loam H2 - 6 to 36 inches: fine sandy loam H3 - 36 to 60 inches: fine sandy loam

# **Properties and qualities**

Slope: 3 to 8 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.60 to 6.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Moderate (about 7.8 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: A

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

# **Description of Hollis**

# Setting

Landform: Hills

Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Shallow, friable loamy ablation till derived from igneous rock

#### Typical profile

H1 - 0 to 3 inches: fine sandy loam

H2 - 3 to 14 inches: gravelly fine sandy loam H3 - 14 to 18 inches: unweathered bedrock

# **Properties and qualities**

Slope: 3 to 8 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: 10 to 20 inches to lithic bedrock

Drainage class: Well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.14 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Very low (about 1.8 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: D

Ecological site: F144AY033MA - Shallow Dry Till Uplands

Hydric soil rating: No

# **Description of Rock Outcrop**

# **Setting**

Parent material: Igneous and metamorphic rock

# **Properties and qualities**

Slope: 3 to 8 percent

Depth to restrictive feature: 0 inches to lithic bedrock

# Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8s

Hydric soil rating: Unranked

# **Minor Components**

# Canton

Percent of map unit: 7 percent

Hydric soil rating: No

#### Chatfield

Percent of map unit: 5 percent

Hydric soil rating: No

# **Scituate**

Percent of map unit: 2 percent

Hydric soil rating: No

# **Whitman**

Percent of map unit: 1 percent Landform: Depressions

Hydric soil rating: Yes

# 104D—Hollis-Rock outcrop-Charlton complex, 15 to 35 percent slopes

# **Map Unit Setting**

National map unit symbol: vkvh

Elevation: 20 to 610 feet

Mean annual precipitation: 32 to 54 inches Mean annual air temperature: 43 to 54 degrees F

Frost-free period: 120 to 240 days

Farmland classification: Not prime farmland

# **Map Unit Composition**

Hollis and similar soils: 35 percent

Rock outcrop: 30 percent

Charlton and similar soils: 25 percent

Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

# **Description of Hollis**

# Setting

Landform: Hills

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Linear Across-slope shape: Convex

Parent material: Shallow, friable loamy ablation till derived from igneous and

metamorphic rock

# **Typical profile**

H1 - 0 to 3 inches: fine sandy loam

H2 - 3 to 14 inches: gravelly fine sandy loam H3 - 14 to 18 inches: unweathered bedrock

# **Properties and qualities**

Slope: 15 to 35 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: 10 to 20 inches to lithic bedrock

Drainage class: Well drained Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.14 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Very low (about 1.8 inches)

# Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: D

Ecological site: F144AY033MA - Shallow Dry Till Uplands

Hydric soil rating: No

# **Description of Rock Outcrop**

# Setting

Parent material: Igneous and metamorphic rock

#### **Properties and qualities**

Slope: 15 to 35 percent

Depth to restrictive feature: 0 inches to lithic bedrock

# Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8s

Hydric soil rating: Unranked

# **Description of Charlton**

#### Setting

Landform: Hills

Landform position (two-dimensional): Backslope

Landform position (three-dimensional): Side slope

Down-slope shape: Linear Across-slope shape: Convex

Parent material: Friable coarse-loamy ablation till derived from granite

# **Typical profile**

H1 - 0 to 6 inches: fine sandy loam H2 - 6 to 36 inches: fine sandy loam H3 - 36 to 60 inches: fine sandy loam

# Properties and qualities

Slope: 15 to 35 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.60 to 6.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Moderate (about 7.8 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: A

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

# **Minor Components**

#### Canton

Percent of map unit: 5 percent

Hydric soil rating: No

# Chatfield

Percent of map unit: 5 percent

Hydric soil rating: No

# 245B—Hinckley loamy sand, 3 to 8 percent slopes

# **Map Unit Setting**

National map unit symbol: 2svm8

Elevation: 0 to 1,430 feet

Mean annual precipitation: 36 to 53 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 250 days

Farmland classification: Farmland of statewide importance

#### **Map Unit Composition**

Hinckley and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

# **Description of Hinckley**

# Setting

*Landform:* Moraines, kame terraces, kames, outwash terraces, outwash deltas, outwash plains, eskers

Landform position (two-dimensional): Summit, backslope, footslope, shoulder Landform position (three-dimensional): Nose slope, side slope, base slope, crest, tread, riser

Down-slope shape: Linear, convex, concave Across-slope shape: Convex, linear, concave

Parent material: Sandy and gravelly glaciofluvial deposits derived from gneiss and/or granite and/or schist

# **Typical profile**

Oe - 0 to 1 inches: moderately decomposed plant material

A - 1 to 8 inches: loamy sand

Bw1 - 8 to 11 inches: gravelly loamy sand Bw2 - 11 to 16 inches: gravelly loamy sand BC - 16 to 19 inches: very gravelly loamy sand C - 19 to 65 inches: very gravelly sand

C - 19 to 05 inches. Very grave

# **Properties and qualities**

Slope: 3 to 8 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Excessively drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very

high (1.42 to 99.90 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm) Available water capacity: Very low (about 3.0 inches)

# Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3s

Hydrologic Soil Group: A

Ecological site: F144AY022MA - Dry Outwash

Hydric soil rating: No

# **Minor Components**

#### Windsor

Percent of map unit: 8 percent

Landform: Outwash plains, kames, eskers, moraines, outwash terraces, outwash deltas, kame terraces

Landform position (two-dimensional): Summit, shoulder, backslope, footslope Landform position (three-dimensional): Nose slope, side slope, base slope, crest, tread. riser

Down-slope shape: Linear, convex, concave

Across-slope shape: Convex, linear, concave

Hydric soil rating: No

# Sudbury

Percent of map unit: 5 percent

Landform: Moraines, outwash terraces, outwash deltas, kame terraces, outwash

plains

Landform position (two-dimensional): Backslope, footslope

Landform position (three-dimensional): Side slope, base slope, head slope, tread

Down-slope shape: Concave, linear Across-slope shape: Linear, concave

Hydric soil rating: No

# Agawam

Percent of map unit: 2 percent

Landform: Eskers, moraines, outwash terraces, outwash deltas, kame terraces,

outwash plains, kames

Landform position (two-dimensional): Summit, shoulder, backslope, footslope Landform position (three-dimensional): Nose slope, side slope, base slope, crest,

riser, tread

Down-slope shape: Linear, convex, concave Across-slope shape: Convex, linear, concave

Hydric soil rating: No

# 245C—Hinckley loamy sand, 8 to 15 percent slopes

# **Map Unit Setting**

National map unit symbol: 2svm9

Elevation: 0 to 1,480 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Farmland of statewide importance

#### **Map Unit Composition**

Hinckley and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

# **Description of Hinckley**

# Setting

Landform: Outwash deltas, kame terraces, outwash plains, kames, eskers, moraines, outwash terraces

Landform position (two-dimensional): Shoulder, toeslope, footslope, backslope Landform position (three-dimensional): Nose slope, side slope, crest, head slope, riser

Down-slope shape: Convex, concave, linear Across-slope shape: Concave, linear, convex

Parent material: Sandy and gravelly glaciofluvial deposits derived from gneiss and/or granite and/or schist

# Typical profile

Oe - 0 to 1 inches: moderately decomposed plant material

A - 1 to 8 inches: loamy sand

Bw1 - 8 to 11 inches: gravelly loamy sand Bw2 - 11 to 16 inches: gravelly loamy sand BC - 16 to 19 inches: very gravelly loamy sand

C - 19 to 65 inches: very gravelly sand

# Properties and qualities

Slope: 8 to 15 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Excessively drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very

high (1.42 to 99.90 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm) Available water capacity: Low (about 3.1 inches)

# Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: A

Ecological site: F144AY022MA - Dry Outwash

Hydric soil rating: No

# **Minor Components**

#### Merrimac

Percent of map unit: 5 percent

Landform: Eskers, moraines, outwash terraces, outwash plains, kames

Landform position (two-dimensional): Shoulder, backslope, footslope, toeslope

Landform position (three-dimensional): Side slope, head slope, nose slope, crest,
riser

Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

#### Windsor

Percent of map unit: 5 percent

Landform: Moraines, kame terraces, outwash plains, outwash terraces, outwash deltas, kames, eskers

Landform position (two-dimensional): Shoulder, backslope, footslope, toeslope Landform position (three-dimensional): Nose slope, side slope, crest, head slope, riser

Down-slope shape: Convex, linear, concave Across-slope shape: Linear, convex, concave

Hydric soil rating: No

#### Sudbury

Percent of map unit: 5 percent

Landform: Outwash terraces, kame terraces, outwash plains, moraines, outwash

deltas

Landform position (two-dimensional): Backslope, footslope Landform position (three-dimensional): Base slope, tread

Down-slope shape: Concave, linear Across-slope shape: Linear, concave

Hydric soil rating: No

# 253D—Hinckley loamy sand, 15 to 35 percent slopes

# **Map Unit Setting**

National map unit symbol: 2svmd

Elevation: 0 to 860 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

# **Map Unit Composition**

Hinckley and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

# **Description of Hinckley**

# Setting

Landform: Outwash plains, kames, eskers, moraines, outwash terraces, outwash

deltas, kame terraces

Landform position (two-dimensional): Backslope

Landform position (three-dimensional): Crest, nose slope, side slope, head slope,

riser

Down-slope shape: Concave, convex, linear Across-slope shape: Linear, convex, concave

Parent material: Sandy and gravelly glaciofluvial deposits derived from gneiss

and/or granite and/or schist

# Typical profile

Oe - 0 to 1 inches: moderately decomposed plant material

A - 1 to 8 inches: loamy sand

Bw1 - 8 to 11 inches: gravelly loamy sand Bw2 - 11 to 16 inches: gravelly loamy sand BC - 16 to 19 inches: very gravelly loamy sand

C - 19 to 65 inches: very gravelly sand

# **Properties and qualities**

Slope: 15 to 35 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Excessively drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very

high (1.42 to 99.90 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm) Available water capacity: Low (about 3.1 inches)

# Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6e

Hydrologic Soil Group: A

Ecological site: F144AY022MA - Dry Outwash

Hydric soil rating: No

# **Minor Components**

#### Windsor

Percent of map unit: 10 percent

Landform: Moraines, kame terraces, outwash plains, outwash terraces, outwash

deltas, kames, eskers

Landform position (two-dimensional): Backslope

Landform position (three-dimensional): Nose slope, crest, side slope, head slope,

riser

Down-slope shape: Convex, linear, concave Across-slope shape: Convex, linear, concave

Hydric soil rating: No

#### Merrimac

Percent of map unit: 3 percent

 $\textit{Landform:} \ \mathsf{Kames}, \ \mathsf{eskers}, \ \mathsf{moraines}, \ \mathsf{outwash} \ \mathsf{terraces}, \ \mathsf{outwash} \ \mathsf{plains}, \ \mathsf{kame}$ 

terraces

Landform position (two-dimensional): Backslope

Landform position (three-dimensional): Side slope, crest, head slope, nose slope,

risei

Down-slope shape: Convex, concave, linear Across-slope shape: Concave, convex, linear

Hydric soil rating: No

# Sudbury

Percent of map unit: 2 percent

Landform: Moraines, outwash terraces, kame terraces, outwash plains, outwash

deltas

Landform position (two-dimensional): Backslope, footslope, toeslope

Landform position (three-dimensional): Base slope, tread

Down-slope shape: Linear, concave Across-slope shape: Concave, linear

Hydric soil rating: No

# 254A—Merrimac fine sandy loam, 0 to 3 percent slopes

# **Map Unit Setting**

National map unit symbol: 2tyqr Elevation: 0 to 1,100 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: All areas are prime farmland

# Map Unit Composition

Merrimac and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

# **Description of Merrimac**

# Setting

Landform: Moraines, outwash terraces, outwash plains, kames, eskers Landform position (two-dimensional): Backslope, footslope, summit, shoulder

Landform position (three-dimensional): Side slope, crest, riser, tread

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Loamy glaciofluvial deposits derived from granite, schist, and gneiss over sandy and gravelly glaciofluvial deposits derived from granite, schist, and gneiss

#### Typical profile

Ap - 0 to 10 inches: fine sandy loam Bw1 - 10 to 22 inches: fine sandy loam

Bw2 - 22 to 26 inches: stratified gravel to gravelly loamy sand 2C - 26 to 65 inches: stratified gravel to very gravelly sand

#### Properties and qualities

Slope: 0 to 3 percent

Depth to restrictive feature: More than 80 inches Drainage class: Somewhat excessively drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very

high (1.42 to 99.90 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum content: 2 percent Maximum salinity: Nonsaline (0.0 to 1.4 mmhos/cm)

Sodium adsorption ratio, maximum: 1.0

Available water capacity: Low (about 4.6 inches)

# Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2s

Hydrologic Soil Group: A

Ecological site: F145XY008MA - Dry Outwash

Hydric soil rating: No

# **Minor Components**

# Sudbury

Percent of map unit: 5 percent

Landform: Outwash plains, terraces, deltas Landform position (two-dimensional): Footslope Landform position (three-dimensional): Tread, dip

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

# Hinckley

Percent of map unit: 5 percent

Landform: Outwash plains, eskers, kames, deltas

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Nose slope, side slope, crest, head slope,

rise

Down-slope shape: Convex

Across-slope shape: Linear, convex

Hydric soil rating: No

# **Agawam**

Percent of map unit: 3 percent

Landform: Outwash plains, outwash terraces, stream terraces, kames, eskers,

moraines

Landform position (three-dimensional): Rise

Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

#### Windsor

Percent of map unit: 2 percent

Landform: Outwash terraces, deltas, dunes, outwash plains

Landform position (two-dimensional): Summit Landform position (three-dimensional): Tread, riser

Down-slope shape: Linear, convex Across-slope shape: Linear, convex

Hydric soil rating: No

# 254B—Merrimac fine sandy loam, 3 to 8 percent slopes

#### Map Unit Setting

National map unit symbol: 2tyqs

Elevation: 0 to 1,290 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: All areas are prime farmland

# **Map Unit Composition**

Merrimac and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

# **Description of Merrimac**

# Setting

Landform: Kames, eskers, moraines, outwash terraces, outwash plains Landform position (two-dimensional): Backslope, footslope, shoulder, summit Landform position (three-dimensional): Side slope, crest, riser, tread

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Loamy glaciofluvial deposits derived from granite, schist, and gneiss over sandy and gravelly glaciofluvial deposits derived from granite, schist, and gneiss

# **Typical profile**

Ap - 0 to 10 inches: fine sandy loam Bw1 - 10 to 22 inches: fine sandy loam

Bw2 - 22 to 26 inches: stratified gravel to gravelly loamy sand 2C - 26 to 65 inches: stratified gravel to very gravelly sand

# Properties and qualities

Slope: 3 to 8 percent

Depth to restrictive feature: More than 80 inches Drainage class: Somewhat excessively drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very

high (1.42 to 99.90 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum content: 2 percent Maximum salinity: Nonsaline (0.0 to 1.4 mmhos/cm)

Sodium adsorption ratio, maximum: 1.0

Available water capacity: Low (about 4.6 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2s

Hydrologic Soil Group: A

Ecological site: F145XY008MA - Dry Outwash

Hydric soil rating: No

# **Minor Components**

# Sudbury

Percent of map unit: 5 percent

Landform: Outwash plains, terraces, deltas
Landform position (two-dimensional): Footslope
Landform position (three-dimensional): Tread, dip

Down-slope shape: Concave Across-slope shape: Linear

Hydric soil rating: No

# Hinckley

Percent of map unit: 5 percent

Landform: Deltas, outwash plains, eskers, kames

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Nose slope, side slope, crest, head slope,

rise

Down-slope shape: Convex

Across-slope shape: Convex, linear

Hydric soil rating: No

#### Windsor

Percent of map unit: 3 percent

Landform: Outwash terraces, outwash plains, deltas, dunes

Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Tread, riser

Down-slope shape: Linear, convex Across-slope shape: Linear, convex

Hydric soil rating: No

# **Agawam**

Percent of map unit: 2 percent

Landform: Moraines, outwash terraces, outwash plains, kames, eskers, stream

terraces

Landform position (three-dimensional): Rise

Down-slope shape: Convex Across-slope shape: Convex

Hydric soil rating: No

# 260B—Sudbury fine sandy loam, 2 to 8 percent slopes

# **Map Unit Setting**

National map unit symbol: vky4 Elevation: 0 to 2,100 feet

Mean annual precipitation: 45 to 54 inches Mean annual air temperature: 43 to 54 degrees F

Frost-free period: 145 to 240 days

Farmland classification: All areas are prime farmland

# **Map Unit Composition**

Sudbury and similar soils: 85 percent *Minor components*: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

# **Description of Sudbury**

# Setting

Landform: Outwash plains

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Riser

Down-slope shape: Linear Across-slope shape: Concave

Parent material: Friable coarse-loamy eolian deposits over loose sandy

glaciofluvial deposits

# **Typical profile**

H1 - 0 to 11 inches: sandy loam H2 - 11 to 22 inches: sandy loam

H3 - 22 to 60 inches: gravelly coarse sand

# Properties and qualities

Slope: 2 to 8 percent

Depth to restrictive feature: 18 to 36 inches to strongly contrasting textural

stratification

Drainage class: Moderately well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00

in/hr)

Depth to water table: About 18 to 36 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Low (about 4.0 inches)

# Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: B

Ecological site: F144AY027MA - Moist Sandy Outwash

Hydric soil rating: No

# **Minor Components**

# Walpole

Percent of map unit: 5 percent

Landform: Terraces
Hydric soil rating: Yes

# Deerfield

Percent of map unit: 5 percent Landform: Outwash plains

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Tread

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: No

# Merrimac

Percent of map unit: 5 percent

Hydric soil rating: No

# 602—Urban land, 0 to 15 percent slopes

# **Map Unit Setting**

National map unit symbol: vkyj

Mean annual precipitation: 32 to 50 inches Mean annual air temperature: 45 to 50 degrees F

Frost-free period: 120 to 200 days

Farmland classification: Not prime farmland

# **Map Unit Composition**

Urban land: 99 percent Minor components: 1 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

# **Description of Urban Land**

# Setting

Parent material: Excavated and filled land

# **Minor Components**

# **Rock outcrops**

Percent of map unit: 1 percent Hydric soil rating: Unranked

# 653—Udorthents, sandy

# **Map Unit Setting**

National map unit symbol: vky8 Elevation: 0 to 3,000 feet

Mean annual precipitation: 45 to 54 inches Mean annual air temperature: 43 to 54 degrees F

Frost-free period: 145 to 240 days

Farmland classification: Not prime farmland

# **Map Unit Composition**

Udorthents and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

# **Description of Udorthents**

# Setting

Landform position (two-dimensional): Summit, shoulder

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Landform position (three-dimensional): Tread, riser

Down-slope shape: Linear, convex Across-slope shape: Linear, convex

Parent material: Excavated and filled sandy glaciofluvial deposits

# **Typical profile**

H1 - 0 to 6 inches: variable H2 - 6 to 60 inches: variable

### **Properties and qualities**

Slope: 0 to 25 percent

Depth to restrictive feature: More than 80 inches

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to very

high (0.06 to 20.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: A Hydric soil rating: Unranked

### **Minor Components**

### **Udorthents**

Percent of map unit: 8 percent Hydric soil rating: Unranked

### **Urban land**

Percent of map unit: 5 percent Hydric soil rating: Unranked

### **Swansea**

Percent of map unit: 2 percent

Landform: Bogs Hydric soil rating: Yes

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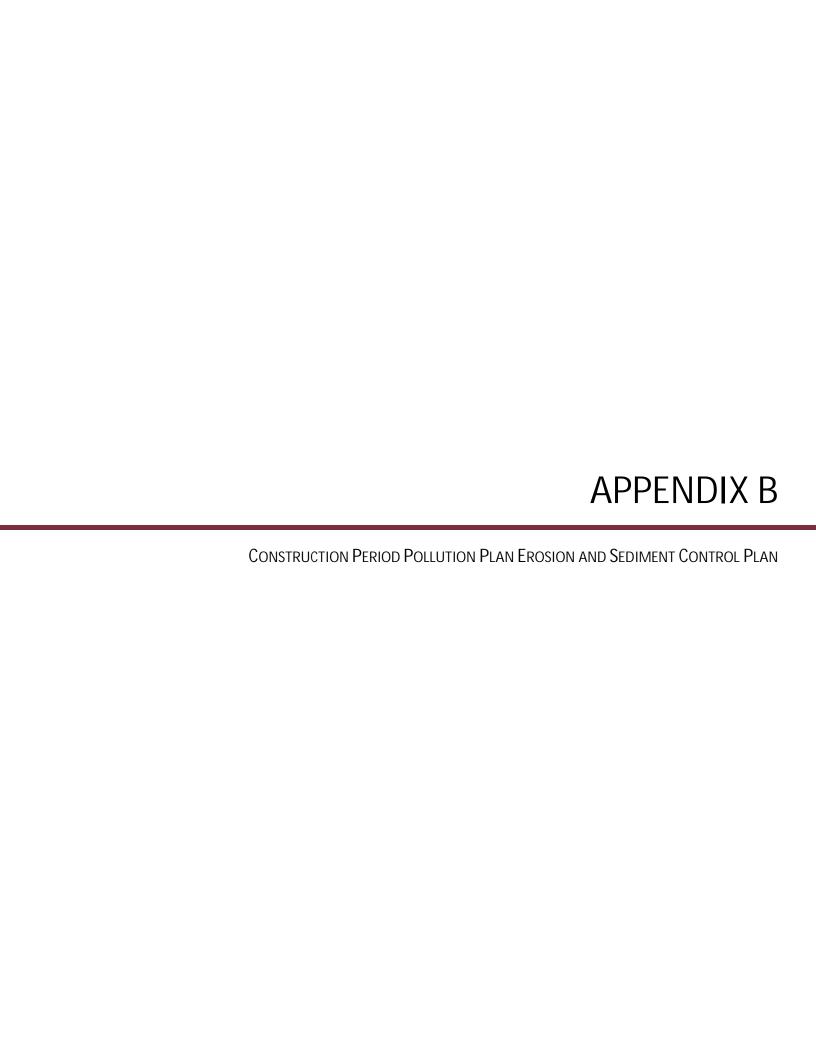
United States Department of Agriculture, Natural Resources Conservation Service. National range and pasture handbook. http://www.nrcs.usda.gov/wps/portal/nrcs/detail/national/landuse/rangepasture/?cid=stelprdb1043084

### Custom Soil Resource Report

United States Department of Agriculture, Natural Resources Conservation Service. National soil survey handbook, title 430-VI. http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/scientists/?cid=nrcs142p2\_054242

United States Department of Agriculture, Natural Resources Conservation Service. 2006. Land resource regions and major land resource areas of the United States, the Caribbean, and the Pacific Basin. U.S. Department of Agriculture Handbook 296. http://www.nrcs.usda.gov/wps/portal/nrcs/detail/national/soils/?cid=nrcs142p2\_053624

United States Department of Agriculture, Soil Conservation Service. 1961. Land capability classification. U.S. Department of Agriculture Handbook 210. http://www.nrcs.usda.gov/Internet/FSE\_DOCUMENTS/nrcs142p2\_052290.pdf



# CONSTRUCTION PERIOD POLLUTION PREVENTION AND EROSION AND SEDIMENTATION CONTROL PLAN

SITE DESCRIPTION					
Project Name and Location; (Latitude, Longitude, or Address	Grove Street Improvements (42.062019, -71.428375) Franklin, MA	Owner Name and Address:	Town of Franklin 355 E Central Street Franklin, MA 02038		
Description: (Purpose and Types of Soil Disturbing Activities)	The following information is based documents prepared by BETA Gro		d from the project plans and supporting		
path, new drainage network, storr installation, retaining walls, new a	nwater treatment, milling and overlay	areas of full depth pave rete wheelchair ramps a	proposed work includes paved shared use ement reconstruction, moment slab and sidewalk, new crosswalks, pavement		
Runoff Coefficient	Approximately 0.98 (mostly imper	vious)			
Site Area:	The project area is approximately	7.0 acres.			
Sequence of Major Activities					
The order of activities will be as follows: See attached construction sequence and project plans for additional information.					
Type of Receiving Resource Area:	Bordering Vegetated Wetland (BV 30-FT No Alteration Zone, 50-ft N				
	CONTR	OLS			
	Erosion and Sedin	nent Controls			
Stabilization Practices					
Temporary Stabilization - Topsoil stockpiles and disturbed portions of the site where construction activity temporarily ceases for at least 21 days will be stabilized with temporary seed and mulch no later than 14 days from the last construction activity in that area. The temporary seed shall be Rye (grain) applied at the rate of 50 pounds per 1000 sq. ft. After seeding, erosion control matting shall be installed over the seeded area.					
permanent seed mix no later than	ed portions of the site where construct 14 days after the last construction act be properly maintained by the contra	ivity. The permanent see			
Disturbed areas with slopes of 2:1 plantings to stabilize slopes while		ermanent geotextile slop	pe reinforcement (as appropriate) and/or		

### **CONTROLS (Continued)**

#### Structural Practices

Compost Filter Tubes – Erosion of or sedimentation from disturbed areas will be prevented by installation of compost filter tubes during construction. Compost filter tubes conform more naturally to existing ground topography, require no excavation or ground disturbance for installation, and may be cut open and left in place at the conclusion of the project rather than removed and disposed of.

### Storm Water Management

All components of the drainage system have been designed to duplicate existing stormwater flow patterns (flow rates and volumes) to the maximum extent practicable, in order to avoid adverse impacts to adjacent properties and/or environmental resource areas which could result from substantial alterations to the existing stormwater flow patterns. The installation of a proposed drainage system will provide additional water quality pretreatment to the existing wetland resource area where none was provided before.

### OTHER CONTROLS

### Waste Disposal:

### **Waste Materials**

All waste materials will be collected and stored in securely lidded metal dumpsters (number and locations as required). The dumpster(s) will meet all local Town and any State solid waste management regulations. All trash and construction debris from the site will be deposited in the dumpster(s), which shall be emptied as needed, and the trash hauled from and legally disposed of off-site. No construction waste materials will be buried onsite. All personnel will be instructed regarding the correct procedure for waste disposal. Notices stating these practices will be posted in the office trailer, and the individual who manages the day-to-day site operations will be responsible for seeing that these procedures are followed by all personnel.

### **Hazardous Waste**

All hazardous waste materials will be disposed of in the manner specified by local or State regulations, or by the manufacturer. Site personnel will be instructed in these practices, and the individual who manages day-to-day site operations will be responsible for seeing that these practices are followed by all personnel.

### Sanitary Waste

Adequate sanitary waste units ("port-a-johns") for all site personnel shall be provided for the duration of the work. All sanitary waste will be collected from the portable units and removed from the site as often as needed, but at a minimum of once a week by a licensed sanitary waste management contractor, as required by local regulation.

### Offsite Vehicle Tracking:

All impervious areas (paved roadways, driveways, sidewalks, etc.) within and/or adjacent to the site will be swept as needed to remove any excess mud, dirt or rock tracked from the site onto same.

Beds of dump trucks or any construction vehicles hauling material from the construction site will be completely covered with a tarpaulin. When leaving unpaved areas to enter paved areas (whether on or off-site), all construction vehicles shall pass over designated and adequately-sized construction pads consisting of coarse angular uniform graded crushed stone gravel. Construction pads shall be maintained regularly by the contractor, and stone refreshed/replaced as needed to provide its intended function.

### TIMING OF CONTROLS/MEASURES

As indicated in the Plans, structural erosion control measures (compost filter socks) will be established prior to clearing or grading of any other portions of the site. Areas where construction activity temporarily ceases for more than 21 days will be stabilized with temporary seed and mulch within 14 days of the last disturbance. Once construction activity ceases permanently the area will be stabilized with permanent seed and mulch.

### CERTIFICATION OF COMPLIANCE WITH FEDERAL, STATE, AND LOCAL REGULATIONS

The construction period pollution prevention and erosion and sedimentation control plan reflect the requirements established by the Massachusetts Stormwater Handbook for all construction activities.

### MAINTENANCE/INSPECTION PROCEDURES

### Erosion and Sediment Control Inspection and Maintenance Practices

These are the inspection and maintenance practices that will be used to maintain erosion and sediment controls.

- All control measures will be inspected at least once every seven calendar days and within 24 hours after any storm event of 0.25 inches or greater in a 24-hour period, or upon the request of the owner or engineer.
- All measures will be maintained in good working order; if a repair is necessary, it will be initiated within 24 hours of report.
- If ponding becomes excessive, and sediment reaches to the midpoint of the compost filter sock, additional compost filter sock should be added in the areas without disturbance of soil or collected sediment.
- Any sediment deposits remaining in place after the compost filter sock has been removed should be dressed to conform to the
  existing grade, prepared, and seeded.
- · Temporary and permanent seeding and planting will be inspected for bare spots, washouts, and healthy growth.
- A maintenance inspection report will be made after each inspection. A copy of the report form to be completed by the inspector
  is attached.
- The site superintendent will select one individual who will be responsible for inspections, maintenance and repair activities, and filling out the inspection and maintenance report.
- Personnel selected for inspection and maintenance responsibilities will receive training from site superintendent. They will be
  trained in all the inspection and maintenance practices necessary for keeping the erosion and sediment controls used onsite in
  good working order.

### MAINTENANCE /INSPECTION PROCEDURES (Continued)

### Non-Storm-Water Discharges

It is expected that the following non-storm water discharges may occur from the site during the construction period:

Pavement wash waters (where no spills or leaks of toxic or hazardous materials have occurred).

### INVENTORY FOR POLLUTION PREVENTION PLAN

The materials or substances, but not limited to those listed below, will potentially be present onsite during construction:

- Paints (enamel and latex)
- Fertilizers
- Petroleum Based Products
- Cleaning Solvents
- Asphalt

- Detergents
- Wood
- Tar
- Concrete

### SPILL PREVENTION

### Material Management Practices

The following are the material management practices that will be used to reduce the risk of spills or other accidental exposure of materials and substances to storm water runoff.

### Good Housekeeping

The following good housekeeping practices will be followed onsite during the construction project

- An effort will be made to store on-site only enough products and materials required to do the job.
- All materials stored onsite will be stored in a neat, orderly manner in their appropriate containers and, if possible, under a roof or other enclosure.
- Products will be kept in their original containers with the original manufacturer's label.
- · Substances will not be mixed with one another unless recommended by the manufacturer.
- Whenever possible, all of a product will be used up before disposing of the container.
- Manufacturers' recommendations for proper use and disposal will be followed.
- The site superintendent will inspect daily to ensure proper use and disposal of materials onsite.

### Hazardous Products:

These practices are used to reduce the risks associated with hazardous materials.

- Products will be kept in original containers unless they are not re-sealable.
- Original labels and material safety data will be retained; they contain important product information.
- If surplus product must be disposed of, manufacturers' or local and State recommended methods for proper disposal will be followed

### **SPILL PREVENTION (Continued)**

#### Product Specific Practices

The following product specific practices will be followed onsite:

### Petroleum Products

All onsite vehicles will be monitored for leaks and receive regular preventive maintenance to reduce the chance of leakage. Petroleum products will be stored in tightly sealed containers which are clearly labeled. Any asphalt substances used onsite will be applied according to the manufacturer's recommendations.

### Fertilizers:

Fertilizers used will be applied only in the minimum amounts recommended by the manufacturer. Once applied, fertilizer will be worked into the soil to limit exposure to storm water. Storage will be in a covered shed. The contents of any partially used bags of fertilizer will be transferred to a sealable plastic bin to avoid spills.

### Paints:

All containers will be tightly sealed and stored when not required for use. Excess paint will not be discharged to the storm sewer system but will be properly disposed of according to manufacturers' instructions or State and local regulations.

### Concrete Trucks:

Concrete trucks will be allowed to wash out or discharge surplus concrete or drum wash water to a dedicated area (or areas) on site. The contractor shall designate concrete wash-out areas and shall maintain adequate controls within and around the areas to prevent the migration of concrete from the wash-out area(s).

### Spill Control Practices

In addition to the good housekeeping and material management practices discussed in the previous sections of this plan, the following practices will be followed for spill prevention and cleanup:

- Manufacturers' recommended methods for spill cleanup will be clearly posted and site personnel will be made aware of the procedures
  and the location of the information and cleanup supplies.
- Materials and equipment necessary for spill cleanup will be kept in a storage area onsite. Equipment and materials will include but not
  be limited to brooms, dust pans, mops, rags, gloves, goggles, kitty litter, sand, sawdust, and plastic and metal trash containers
  specifically for this purpose.
- · All spills will be cleaned up immediately after discovery.
- The spill area will be kept well ventilated and personnel will wear appropriate protective clothing to prevent injury from contact with a hazardous substance.
- Spills of toxic or hazardous material will be reported to the appropriate State or local government agency, regardless of the size.
- The spill prevention plan will be adjusted to include measures to prevent this type of spilt from reoccurring and how to clean up the spill if there is another one. A description of the spill, what caused it, and the cleanup measures will also be included.
- The site superintendent responsible for the day-to-day site operations will be the spill prevention and cleanup coordinator. He will
  designate at least three other site personnel who will receive spill prevention and cleanup training. The individual will each become
  responsible for a particular phase of prevention and cleanup. The names of responsible spill personnel will be posted in the office
  trailer onsite.

# GROVE STREET IMPROVEMENTS PROJECT CONSTRUCTION PERIOD POLLUTION PREVENTION AND EROSION AND SEDIMENTATION CONTROL PLAN INSPECTION AND MAINTENANCE REPORT FORM

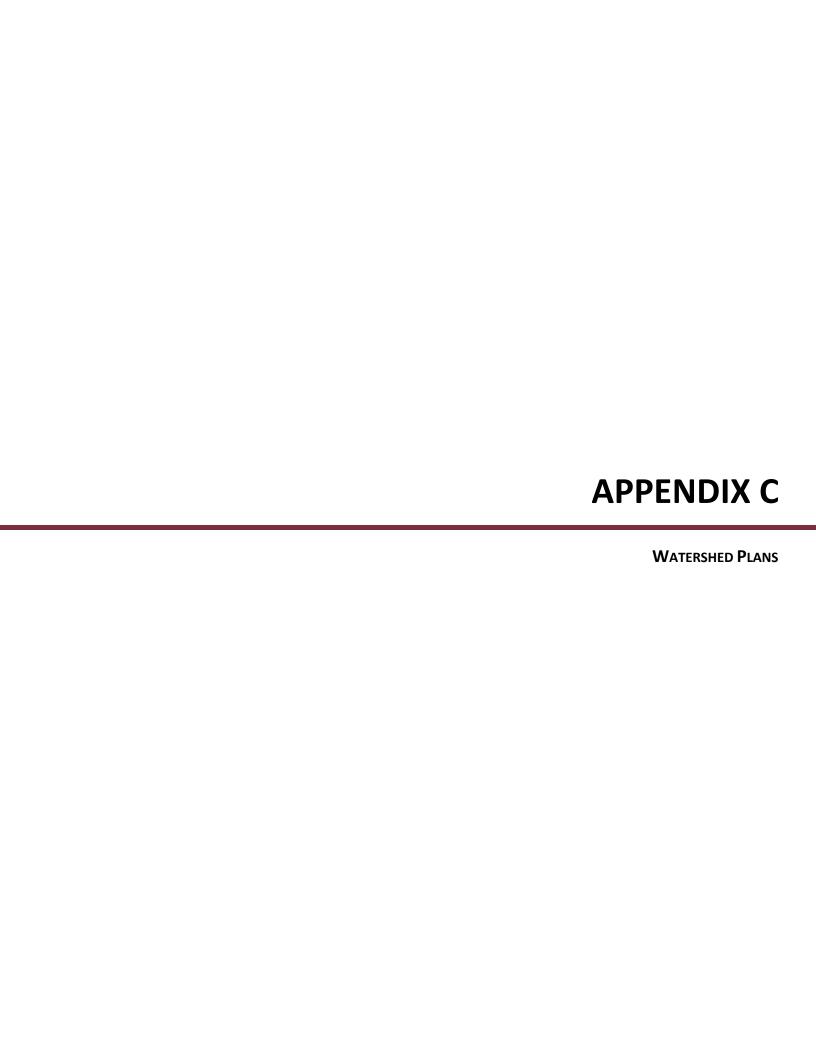
# TO BE COMPLETED EVERY 7 DAYS AND WITHIN 24 HOURS OF A RAINFALL EVENT OF 0.25 INCHES OR MORE

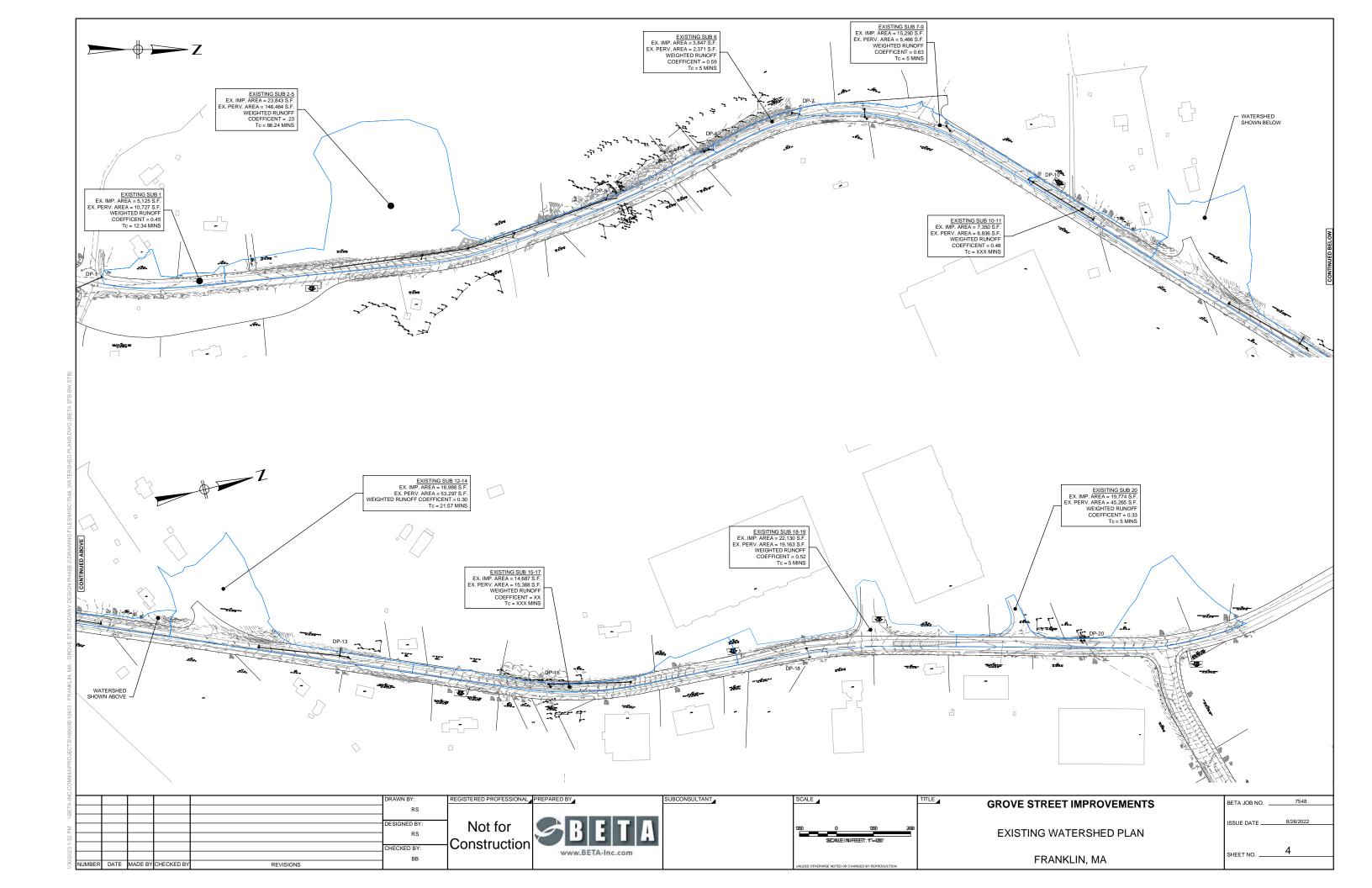
INSPECTOR:			DATE:		
INSPECTOR'S Q	UALIFICATIONS:				
DAYS SINCE LA	ST RAINFALL:	AM	OUNT OF LAST RAIN	NFALL:	INCHES
	S	TABILIZATION	MEASURES		
AREA	DATE SINCE LAST DISTURBANCE	DATE OF NEXT DISTURBANCE	STABILIZED? (YES/NO)	STABILIZED WITH	CONDITION
STABILIZATION	N REQUIRED:				
TO BE PERFORM	MED BY:		ON OR BEFOR	E:	

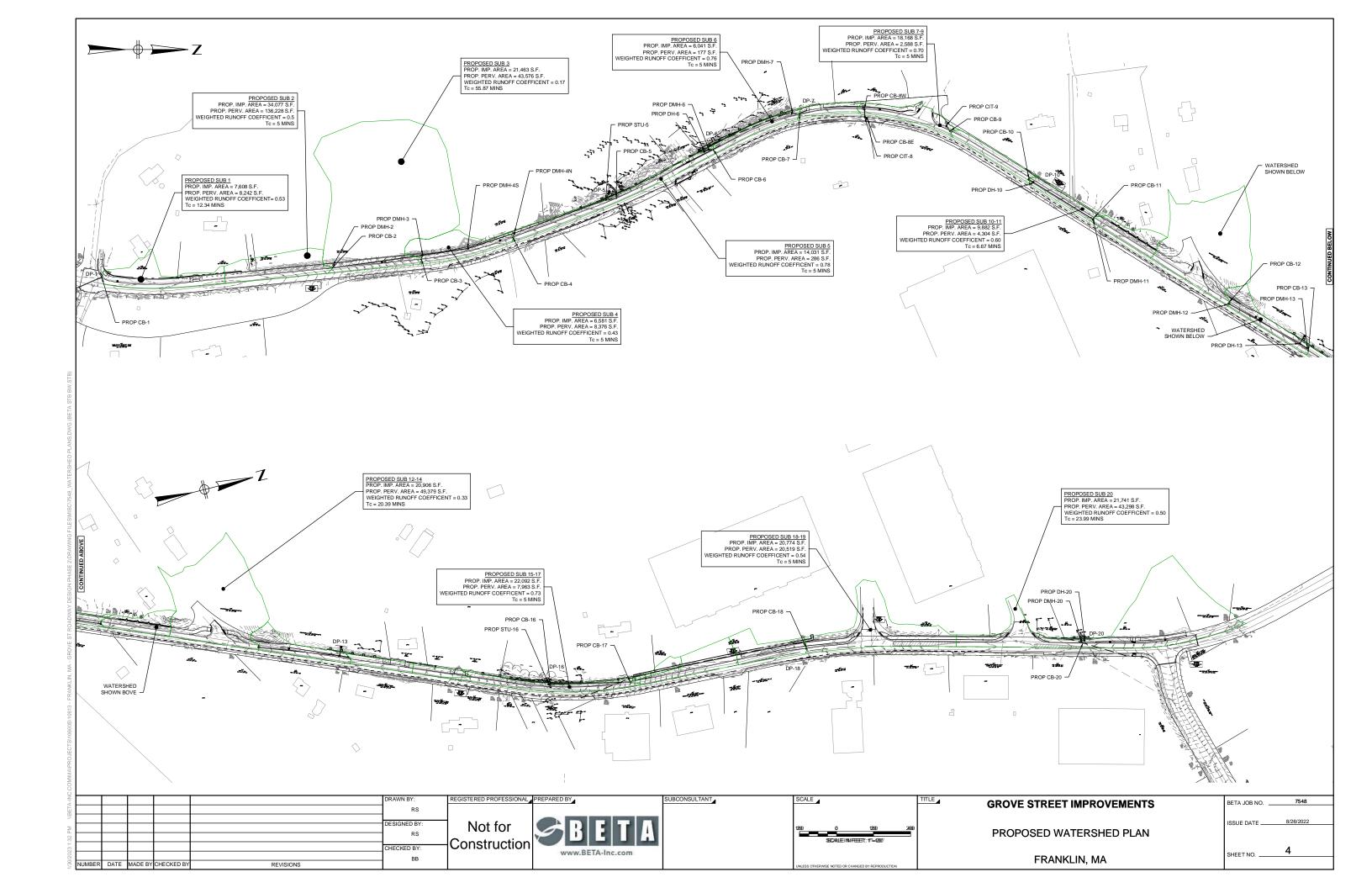
# GROVE STREET IMPROVEMENTS PROJECT CONSTRUCTION PERIOD POLLUTION PREVENTION AND EROSION AND SEDIMENTATION CONTROL PLAN INSPECTION AND MAINTENANCE REPORT FORM

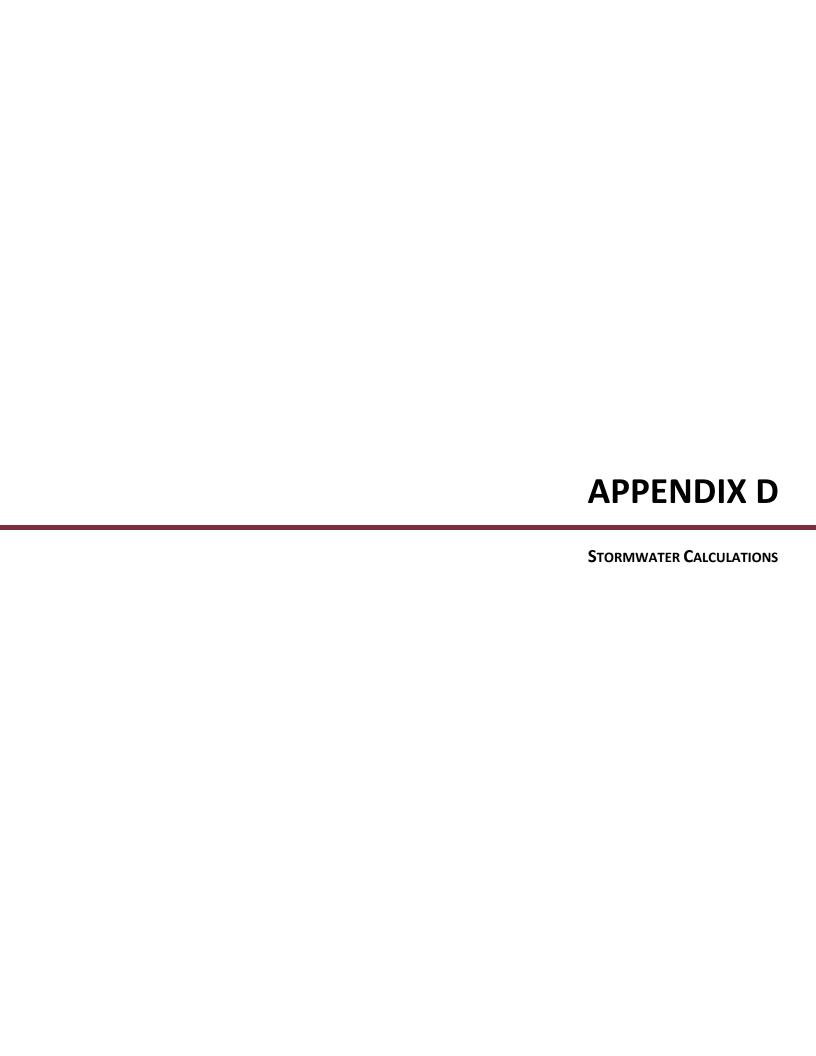
# STRUCTURAL CONTROLS (Compost Filter Sock)

DATE:			
DRAINAGE AREA PERIMETER	HAS SILT REACHED 1/2 OF FILTER SOCK HEIGHT?	IS FILTER SOCK PROPERLY SECURED?	IS THERE EVIDENCE OF WASHOUT OR OVERTOPPING?
MAINTENANCE REQUIRED	FOR COMPOST FILTER SOCK:		
TO BE PERFORMED BY:		ON OR BEFORE:	









Version 1, Automated: Mar. 4, 2008

- 1. In BMP Column, click on Blue Cell to Activate Drop Down Menu
- 2. Select BMP from Drop Down Menu
- 3. After BMP is selected, TSS Removal and other Columns are automatically completed.

Location: Grove Street - 7+00 LT

	В	С	D	E	F
	BMP <sup>1</sup>	TSS Removal	Starting TSS	Amount	Remaining
	BIVIP	Rate <sup>1</sup>	Load*	Removed (C*D)	Load (D-E)
heet	Treebox Filter	0.80	1.00	0.80	0.20
Removal on Worksheet	Deep Sump and Hooded Catch Basin	0.25	0.20	0.05	0.15
Rem on W		0.00	0.15	0.00	0.15
TSS culati		0.00	0.15	0.00	0.15
T		0.00	0.15	0.00	0.15
					Separate Form Needs to

Total TSS Removal =

Separate Form Needs to be Completed for Each Outlet or BMP Train

Project: Grove Street Phase 2
Prepared By: CML
Date: 1/25/2023

\*Equals remaining load from previous BMP (E) which enters the BMP

85%

Version 1, Automated: Mar. 4, 2008

- 1. In BMP Column, click on Blue Cell to Activate Drop Down Menu
- 2. Select BMP from Drop Down Menu
- 3. After BMP is selected, TSS Removal and other Columns are automatically completed.

Location: Grove Street - 20+64 LT

	В	С	D	Е	F
		TSS Removal	Starting TSS	Amount	Remaining
	BMP <sup>1</sup>	Rate <sup>1</sup>	Load*	Removed (C*D)	Load (D-E)
neet	Treebox Filter	0.80	1.00	0.80	0.20
Removal on Worksheet	Deep Sump and Hooded Catch Basin	0.25	0.20	0.05	0.15
Re	Proprietary Treatment Practice	0.75	0.15	0.11	0.04
TSS sulati					
Calc					_
			<u> </u>		Separate Form Needs to

Total TSS Removal =

96% Separate Form Needs to be Completed for Each Outlet or BMP Train

Project: Grove Street Phase 2
Prepared By: CML
Date: 1/25/2023

\*Equals remaining load from previous BMP (E) which enters the BMP

Version 1, Automated: Mar. 4, 2008

- 1. In BMP Column, click on Blue Cell to Activate Drop Down Menu
- 2. Select BMP from Drop Down Menu
- 3. After BMP is selected, TSS Removal and other Columns are automatically completed.

Location: Grove Street - 23+50 LT

	В	С	D	Е	F
		TSS Removal	Starting TSS	Amount	Remaining
	BMP <sup>1</sup>	Rate <sup>1</sup>	Load*	Removed (C*D)	Load (D-E)
neet	Deep Sump and Hooded Catch Basin	0.25	1.00	0.25	0.75
Removal on Worksheet		0.00	0.75	0.00	0.75
Rem on W		0.00	0.75	0.00	0.75
TSS ReCalculation		0.00	0.75	0.00	0.75
Calc		0.00	0.75	0.00	0.75
					Separate Form Needs to

Total TSS Removal =

25%

Separate Form Needs to be Completed for Each Outlet or BMP Train

Project: Grove Street Phase 2
Prepared By: CML
Date: 1/25/2023

\*Equals remaining load from previous BMP (E) which enters the BMP

Version 1, Automated: Mar. 4, 2008

- 1. In BMP Column, click on Blue Cell to Activate Drop Down Menu
- 2. Select BMP from Drop Down Menu
- 3. After BMP is selected, TSS Removal and other Columns are automatically completed.

Location: Grove Street - 26+05 LT

	В	C TSS Removal	D Starting TSS	E Amount	F Remaining
	BMP <sup>1</sup>	Rate <sup>1</sup>	Load*	Removed (C*D)	Load (D-E)
neet	Deep Sump and Hooded Catch Basin	0.25	1.00	0.25	0.75
oval orksl		0.00	0.75	0.00	0.75
Removal on Worksheet		0.00	0.75	0.00	0.75
TSS Re Calculation		0.00	0.75	0.00	0.75
Calc		0.00	0.75	0.00	0.75
	Total TSS Removal =			25%	Separate Form Needs to be Completed for Each Outlet or BMP Train

Project: Grove Street Phase 2 Prepared By: CML Date: 1/25/2023

\*Equals remaining load from previous BMP (E) which enters the BMP

Version 1, Automated: Mar. 4, 2008

- 1. In BMP Column, click on Blue Cell to Activate Drop Down Menu
- 2. Select BMP from Drop Down Menu
- 3. After BMP is selected, TSS Removal and other Columns are automatically completed.

Location: Grove Street - 27+98 LT

	В	С	D	E	F
		TSS Removal	Starting TSS	Amount	Remaining
	BMP <sup>1</sup>	Rate <sup>1</sup>	Load*	Removed (C*D)	Load (D-E)
te.	Treebox Filter	0.00	4.00		0.00
<u>ک</u>	Treebox Filter	0.80	1.00	0.80	0.20
Removal on Worksheet	Deep Sump and Hooded Catch Basin	0.25	0.20	0.05	0.15
ĔΖ					
TSS Re		0.00	0.15	0.00	0.15
SS					
		0.00	0.15	0.00	0.15
<u>re</u>					
		0.00	0.15	0.00	0.15
					Separate Form Needs to

Total TSS Removal =

be Completed for Each
Outlet or BMP Train

Project: Grove Street Phase 2
Prepared By: CML
Date: 1/25/2023

\*Equals remaining load from previous BMP (E) which enters the BMP

85%

Version 1, Automated: Mar. 4, 2008

- 1. In BMP Column, click on Blue Cell to Activate Drop Down Menu
- 2. Select BMP from Drop Down Menu
- 3. After BMP is selected, TSS Removal and other Columns are automatically completed.

Location: Grove Street - 30+17 LT

	B BMP <sup>1</sup>	C TSS Removal Rate <sup>1</sup>	D Starting TSS Load*	E Amount Removed (C*D)	F Remaining Load (D-E)
<b>*</b>	Deep Sump and Hooded Catch Basin	0.25	1.00	0.25	0.75
Removal		0.00	0.75	0.00	0.75
S Ren		0.00	0.75	0.00	0.75
TSS Re		0.00	0.75	0.00	0.75
ز	5	0.00	0.75	0.00	0.75
					Separate Form Needs to

Total TSS Removal =

be Completed for Each
Outlet or BMP Train

Project: Grove Street Phase 2
Prepared By: CML
Date: 1/25/2023

\*Equals remaining load from previous BMP (E) which enters the BMP

Version 1, Automated: Mar. 4, 2008

- 1. In BMP Column, click on Blue Cell to Activate Drop Down Menu
- 2. Select BMP from Drop Down Menu
- 3. After BMP is selected, TSS Removal and other Columns are automatically completed.

Location: Grove Street - 33+94 LT

	В	C TSS Removal	D Starting TSS	E Amount	F Remaining
	BMP <sup>1</sup>	Rate <sup>1</sup>	Load*	Removed (C*D)	Load (D-E)
neet	Deep Sump and Hooded Catch Basin	0.25	1.00	0.25	0.75
oval orksl		0.00	0.75	0.00	0.75
Removal on Worksheet		0.00	0.75	0.00	0.75
TSS Re Calculation		0.00	0.75	0.00	0.75
Calc		0.00	0.75	0.00	0.75
	Total TSS Removal =			25%	Separate Form Needs to be Completed for Each Outlet or BMP Train

Project: Grove Street Phase 2 Prepared By: CML Date: 1/25/2023

\*Equals remaining load from previous BMP (E) which enters the BMP

Version 1, Automated: Mar. 4, 2008

- 1. In BMP Column, click on Blue Cell to Activate Drop Down Menu
- 2. Select BMP from Drop Down Menu
- 3. After BMP is selected, TSS Removal and other Columns are automatically completed.

Date: 1/25/2023

Location: Grove Street - 41+37 LT

	В	C TSS Removal	D Starting TSS	E Amount	F Remaining
	BMP <sup>1</sup>	Rate <sup>1</sup>	Load*	Removed (C*D)	Load (D-E)
heet	Deep Sump and Hooded Catch Basin	0.25	1.00	0.25	0.75
Removal on Worksheet	Treebox Filter	0.80	0.75	0.60	0.15
4	Proprietary Treatment Practice	0.75	0.15	0.11	0.04
TSS Re Calculation					
Calc					
		Total 1	96%	Separate Form Needs to be Completed for Each Outlet or BMP Train	
	Project: Prepared By:	Grove Street Phase 2	'	*Equals remaining load from	n previous BMP (E)

Non-automated TSS Calculation Sheet must be used if Proprietary BMP Proposed 1. From MassDEP Stormwater Handbook Vol. 1 which enters the BMP

Version 1, Automated: Mar. 4, 2008

- 1. In BMP Column, click on Blue Cell to Activate Drop Down Menu
- 2. Select BMP from Drop Down Menu
- 3. After BMP is selected, TSS Removal and other Columns are automatically completed.

Location: Grove Street - 54+18 LT

	В	С	D	Е	F
		TSS Removal	Starting TSS	Amount	Remaining
	BMP <sup>1</sup>	Rate <sup>1</sup>	Load*	Removed (C*D)	Load (D-E)
•	Deep Sump and Hooded Catch Basin	0.25	1.00	0.25	0.75
Removal	Orksr	0.00	0.75	0.00	0.75
Rem		0.00	0.75	0.00	0.75
TSS	Calculat	0.00	0.75	0.00	0.75
-					
		0.00	0.75	0.00	0.75
					Separate Form Needs to

Total TSS Removal =

Separate Form Needs to be Completed for Each Outlet or BMP Train

Project: Grove Street Phase 2
Prepared By: CML
Date: 1/25/2023

\*Equals remaining load from previous BMP (E) which enters the BMP

25%

Version 1, Automated: Mar. 4, 2008

- 1. In BMP Column, click on Blue Cell to Activate Drop Down Menu
- 2. Select BMP from Drop Down Menu
- 3. After BMP is selected, TSS Removal and other Columns are automatically completed.

Location: Grove Street - 61+69 LT

	В	С	D	Е	F
		TSS Removal	Starting TSS	Amount	Remaining
	BMP <sup>1</sup>	Rate <sup>1</sup>	Load*	Removed (C*D)	Load (D-E)
1	Treebox Filter	0.80	1.00	0.80	0.20
Removal	Deep Sump and Hooded Catch Basin	0.25	0.20	0.05	0.15
Rem		0.00	0.15	0.00	0.15
TSS	Calculat	0.00	0.15	0.00	0.15
Č	Ca				
		0.00	0.15	0.00	0.15
					Senarate Form Needs to

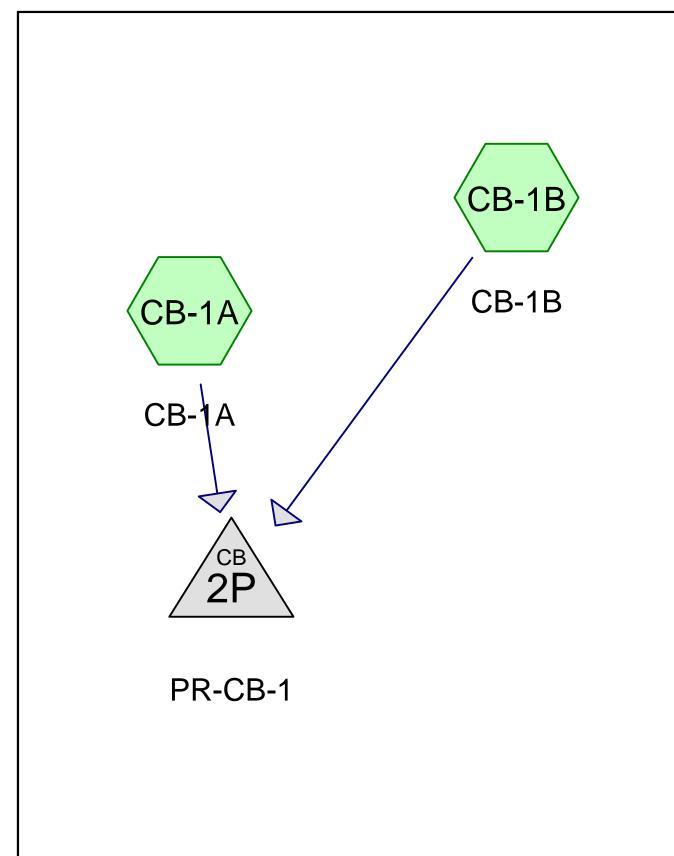
Total TSS Removal =

Separate Form Needs to be Completed for Each Outlet or BMP Train

Project: Grove Street Phase 2
Prepared By: CML
Date: 1/25/2023

\*Equals remaining load from previous BMP (E) which enters the BMP

85%











# **Exist - Constr Rev-MODIFIED**

Prepared by BETA Group, Inc. HydroCAD® 10.00-22 s/n 01895 © 2018 HydroCAD Software Solutions LLC

Printed 2/9/2023 Page 2

# **Area Listing (selected nodes)**

Area	CN	Description
(sq-ft)		(subcatchment-numbers)
11,826	61	1/4 acre lots, 38% imp, HSG A (CB-1B)
4,026	98	Paved roads w/curbs & sewers, HSG A (CB-1A)

Page 3

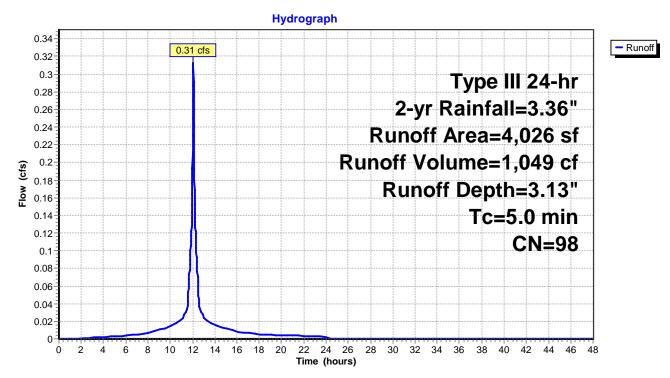
# Summary for Subcatchment CB-1A: CB-1A

Runoff = 0.31 cfs @ 12.07 hrs, Volume= 1,049 cf, Depth= 3.13"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 2-yr Rainfall=3.36"

	Α	rea (sf)	CN D	CN Description					
*		4,026	98 F	98 Paved roads w/curbs & sewers, HSG A					
		4,026	1	100.00% Impervious Area					
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
	5.0	( )	( 2 3/	( /	()	Direct Entry,			

### Subcatchment CB-1A: CB-1A



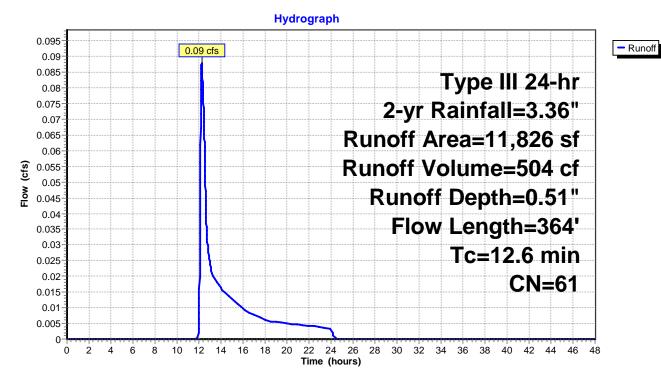
# Summary for Subcatchment CB-1B: CB-1B

Runoff 0.09 cfs @ 12.23 hrs, Volume= 504 cf, Depth= 0.51"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 2-yr Rainfall=3.36"

	Α	rea (sf)	CN E	<b>Description</b>							
		11,826	61 1	61 1/4 acre lots, 38% imp, HSG A							
		7,332	6	62.00% Pervious Area							
		4,494	3	8.00% lmp	ervious Are	ea					
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description					
_	9.7	34	0.0153	0.06		Sheet Flow,					
	2.9	330	0.0090	1.93		Grass: Bermuda n= 0.410 P2= 3.60" <b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps					
_	12 6	364	Total								

# Subcatchment CB-1B: CB-1B



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# Summary for Pond 2P: PR-CB-1

Inflow Area = 15,852 sf, 53.75% Impervious, Inflow Depth = 1.18" for 2-yr event Inflow = 0.34 cfs @ 12.08 hrs. Volume= 1.553 cf

Outflow = 0.34 cfs @ 12.08 hrs, Volume= 1,553 cf, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3

Peak Elev= 276.49' @ 12.08 hrs

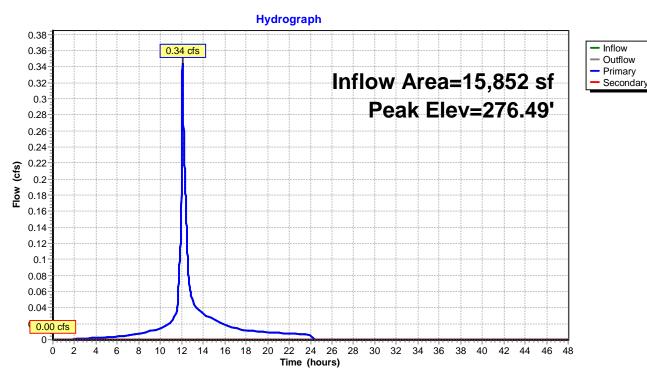
Flood Elev= 280.40'

Device	Routing	Invert	Outlet Devices
#1	Secondary	280.40'	<b>24.0" x 24.0" Horiz. CB Grate</b> C= 0.600
	•		Limited to weir flow at low heads
#2	Primary	276.20'	12.0" Round Culvert
	-		L= 37.4' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 276.20' / 275.00' S= 0.0321 '/' Cc= 0.900
			n= 0.013. Flow Area= 0.79 sf

**Primary OutFlow** Max=0.34 cfs @ 12.08 hrs HW=276.49' (Free Discharge) **2=Culvert** (Inlet Controls 0.34 cfs @ 1.83 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=276.20' (Free Discharge) 1=CB Grate (Controls 0.00 cfs)

## Pond 2P: PR-CB-1



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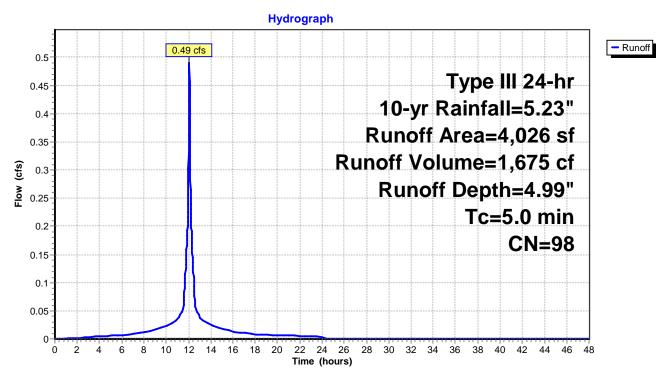
# Summary for Subcatchment CB-1A: CB-1A

Runoff = 0.49 cfs @ 12.07 hrs, Volume= 1,675 cf, Depth= 4.99"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-yr Rainfall=5.23"

	Α	rea (sf)	CN D	CN Description					
*		4,026	98 F	98 Paved roads w/curbs & sewers, HSG A					
		4,026	1	100.00% Impervious Area					
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
	5.0	( )	( 2 3/	( /	()	Direct Entry,			

### Subcatchment CB-1A: CB-1A



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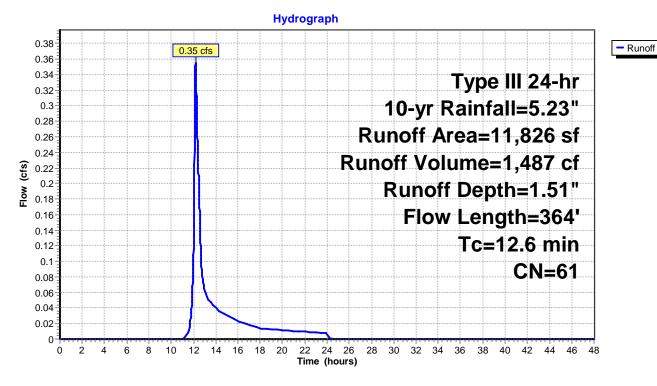
# Summary for Subcatchment CB-1B: CB-1B

Runoff = 0.35 cfs @ 12.19 hrs, Volume= 1,487 cf, Depth= 1.51"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 10-yr Rainfall=5.23"

_	Aı	rea (sf)	CN D	escription							
		11,826	61 1	61 1/4 acre lots, 38% imp, HSG A							
		7,332	6	2.00% Per	vious Area						
		4,494	3	8.00% lmp	ervious Are	ea					
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description					
-	9.7	34	0.0153	0.06		Sheet Flow,					
	2.9	330	0.0090	1.93		Grass: Bermuda n= 0.410 P2= 3.60" <b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps					
_	12.6	364	Total	•							

# Subcatchment CB-1B: CB-1B



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# **Summary for Pond 2P: PR-CB-1**

Inflow Area = 15,852 sf, 53.75% Impervious, Inflow Depth = 2.39" for 10-yr event

Inflow = 0.72 cfs @ 12.10 hrs, Volume= 3,162 cf

Outflow = 0.72 cfs @ 12.10 hrs, Volume= 3,162 cf, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3

Peak Elev= 276.63' @ 12.10 hrs

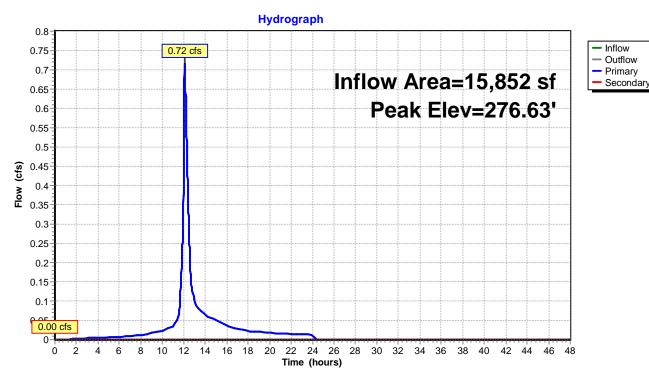
Flood Elev= 280.40'

Device	Routing	Invert	Outlet Devices
#1	Secondary	280.40'	<b>24.0" x 24.0" Horiz. CB Grate</b> C= 0.600
	·		Limited to weir flow at low heads
#2	Primary	276.20'	12.0" Round Culvert
	•		L= 37.4' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 276.20' / 275.00' S= 0.0321 '/' Cc= 0.900
			n= 0.013 Flow Area= 0.79 sf

**Primary OutFlow** Max=0.72 cfs @ 12.10 hrs HW=276.63' (Free Discharge) **2=Culvert** (Inlet Controls 0.72 cfs @ 2.23 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=276.20' (Free Discharge) 1=CB Grate (Controls 0.00 cfs)

## Pond 2P: PR-CB-1



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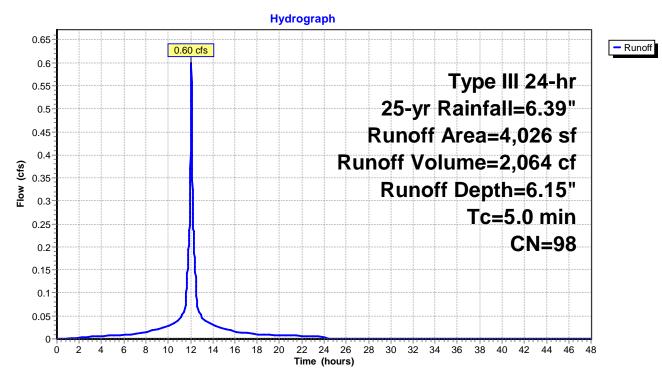
# Summary for Subcatchment CB-1A: CB-1A

Runoff = 0.60 cfs @ 12.07 hrs, Volume= 2,064 cf, Depth= 6.15"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 25-yr Rainfall=6.39"

_	Α	rea (sf)	CN [	CN Description					
*		4,026	98 F	98 Paved roads w/curbs & sewers, HSG A					
		4,026	1	100.00% Impervious Area					
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
_	5.0	(icci)	(1011)	(10300)	(013)	Direct Entry,			

### Subcatchment CB-1A: CB-1A



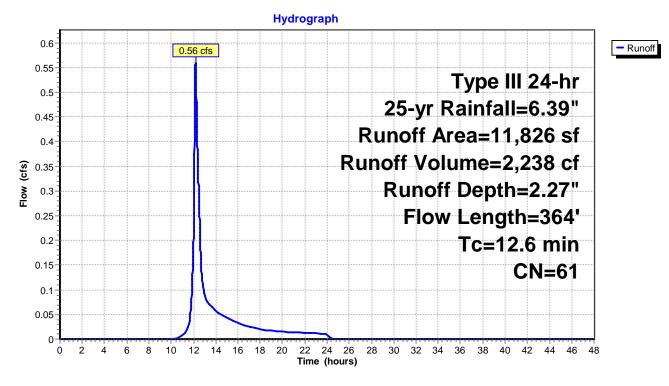
# Summary for Subcatchment CB-1B: CB-1B

Runoff = 0.56 cfs @ 12.19 hrs, Volume= 2,238 cf, Depth= 2.27"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 25-yr Rainfall=6.39"

_	Aı	rea (sf)	CN E	escription							
		11,826	61 1	61 1/4 acre lots, 38% imp, HSG A							
		7,332	6	2.00% Per	vious Area						
		4,494	3	8.00% lmp	ervious Ar	ea					
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description					
-	9.7	34	0.0153	0.06	,	Sheet Flow,					
	2.9	330	0.0090	1.93		Grass: Bermuda n= 0.410 P2= 3.60" <b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps					
Ī	12.6	364	Total								

# Subcatchment CB-1B: CB-1B



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# **Summary for Pond 2P: PR-CB-1**

Primary = 0.99 cfs @ 12.10 hrs, Volume= 4,302 cf Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0 cf

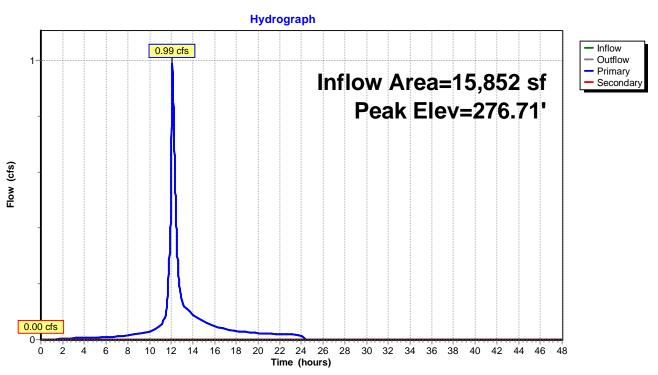
Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 276.71' @ 12.10 hrs Flood Elev= 280.40'

Device	Routing	Invert	Outlet Devices
#1	Secondary	280.40'	<b>24.0" x 24.0" Horiz. CB Grate</b> C= 0.600
	·		Limited to weir flow at low heads
#2	Primary	276.20'	12.0" Round Culvert
	•		L= 37.4' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 276.20' / 275.00' S= 0.0321 '/' Cc= 0.900
			n= 0.013 Flow Area= 0.79 sf

Primary OutFlow Max=0.99 cfs @ 12.10 hrs HW=276.71' (Free Discharge) —2=Culvert (Inlet Controls 0.99 cfs @ 2.44 fps)

**Secondary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=276.20' (Free Discharge) **1=CB Grate** (Controls 0.00 cfs)

## Pond 2P: PR-CB-1



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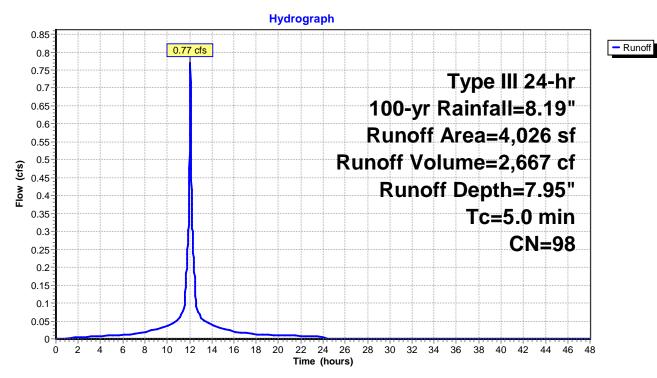
## Summary for Subcatchment CB-1A: CB-1A

Runoff = 0.77 cfs @ 12.07 hrs, Volume= 2,667 cf, Depth= 7.95"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 100-yr Rainfall=8.19"

	Α	rea (sf)	CN [	Description			
*		4,026	98 F	8 Paved roads w/curbs & sewers, HSG A			
		4,026	1	100.00% Impervious Area			
,		Length	•	•	Capacity	Description	
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
	5.0					Direct Entry,	

#### Subcatchment CB-1A: CB-1A



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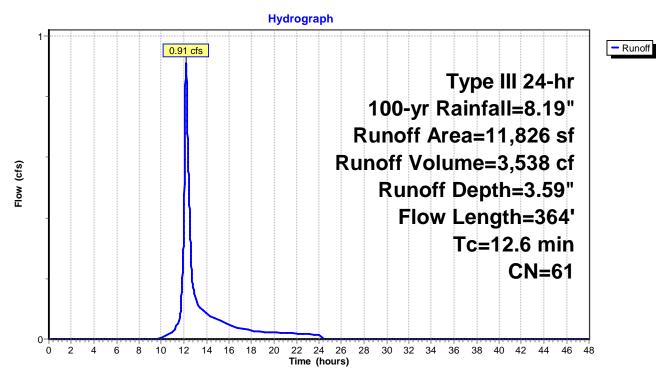
## Summary for Subcatchment CB-1B: CB-1B

Runoff = 0.91 cfs @ 12.18 hrs, Volume= 3,538 cf, Depth= 3.59"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 100-yr Rainfall=8.19"

_	Aı	rea (sf)	CN D	escription					
		11,826	61 1	61 1/4 acre lots, 38% imp, HSG A					
		7,332	6	2.00% Per	vious Area				
		4,494	3	8.00% lmp	ervious Are	ea			
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
-	9.7	34	0.0153	0.06		Sheet Flow,			
	2.9	330	0.0090	1.93		Grass: Bermuda n= 0.410 P2= 3.60" <b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps			
_	12.6	364	Total	•					

#### Subcatchment CB-1B: CB-1B



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## **Summary for Pond 2P: PR-CB-1**

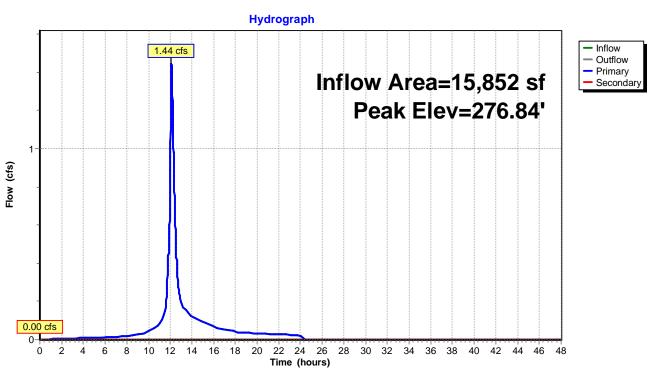
Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 276.84' @ 12.11 hrs Flood Elev= 280.40'

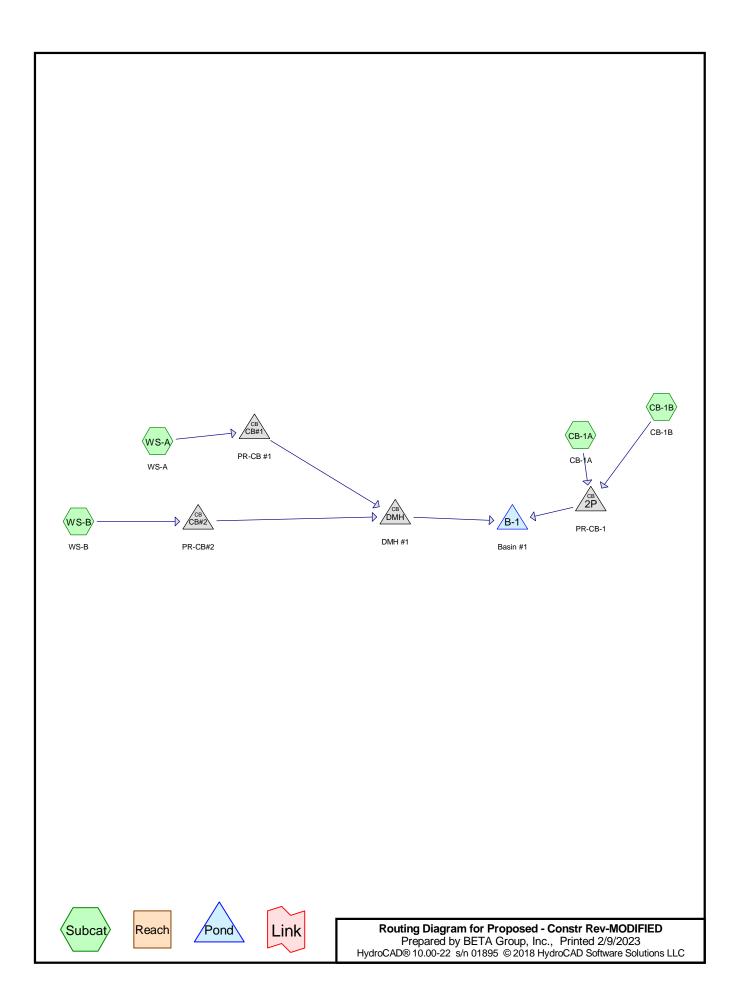
Device	Routing	Invert	Outlet Devices
#1	Secondary	280.40'	<b>24.0" x 24.0" Horiz. CB Grate</b> C= 0.600
	·		Limited to weir flow at low heads
#2	Primary	276.20'	12.0" Round Culvert
	•		L= 37.4' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 276.20' / 275.00' S= 0.0321 '/' Cc= 0.900
			n= 0.013 Flow Area= 0.79 sf

**Primary OutFlow** Max=1.44 cfs @ 12.11 hrs HW=276.84' (Free Discharge) **2=Culvert** (Inlet Controls 1.44 cfs @ 2.72 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=276.20' (Free Discharge) 1=CB Grate (Controls 0.00 cfs)

#### Pond 2P: PR-CB-1





# **Proposed - Constr Rev-MODIFIED**

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# **Area Listing (all nodes)**

Area	CN	Description
 (sq-ft)		(subcatchment-numbers)
8,317	61	1/4 acre lots, 38% imp, HSG A (CB-1B)
31,179	98	Paved roads w/curbs & sewers, HSG A (CB-1A, WS-A, WS-B)

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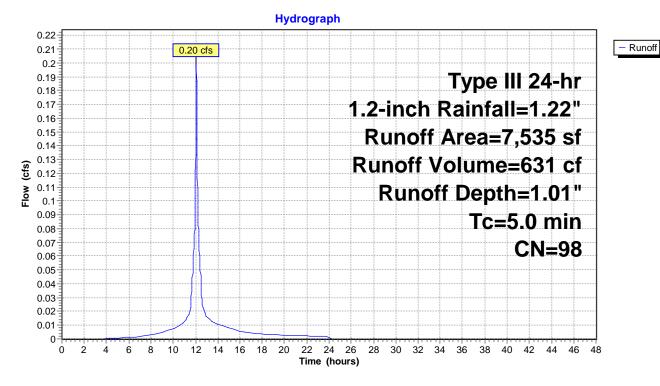
## Summary for Subcatchment CB-1A: CB-1A

Runoff = 0.20 cfs @ 12.07 hrs, Volume= 631 cf, Depth= 1.01"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 1.2-inch Rainfall=1.22"

	Α	rea (sf)	CN [	Description			
*		7,535	98 F	8 Paved roads w/curbs & sewers, HSG A			
		7,535	1	100.00% Impervious Area			
	Тс	- 3	Slope	•		Description	
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
	5.0					Direct Entry,	

#### Subcatchment CB-1A: CB-1A



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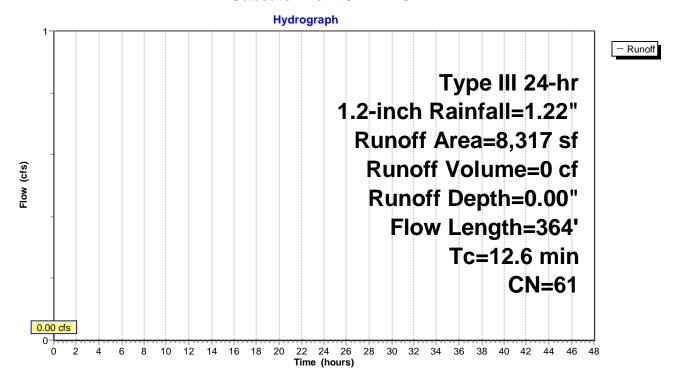
## Summary for Subcatchment CB-1B: CB-1B

Runoff = 0.00 cfs @ 0.00 hrs, Volume= 0 cf, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 1.2-inch Rainfall=1.22"

	Α	rea (sf)	CN D	escription					
		8,317	61 1	61 1/4 acre lots, 38% imp, HSG A					
		5,157	6	62.00% Pervious Area					
		3,160	3	38.00% Impervious Area					
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
_	9.7	34	0.0153	0.06		Sheet Flow,			
	2.9	330	0.0090	1.93		Grass: Bermuda n= 0.410 P2= 3.60" <b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps			
_	12 6	364	Total						

#### Subcatchment CB-1B: CB-1B



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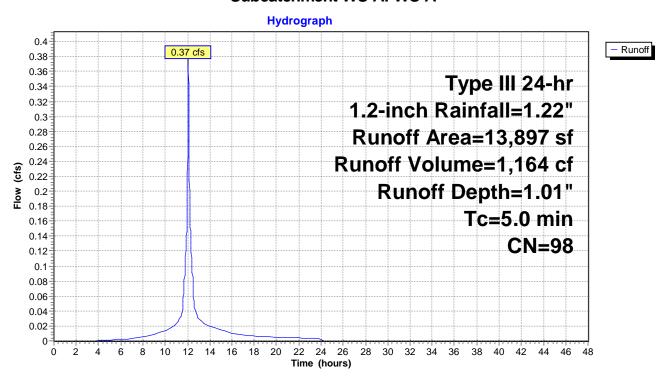
# Summary for Subcatchment WS-A: WS-A

Runoff = 0.37 cfs @ 12.07 hrs, Volume= 1,164 cf, Depth= 1.01"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 1.2-inch Rainfall=1.22"

Area (sf)	CN	Description				
13,897	98	98 Paved roads w/curbs & sewers, HSG A				
13,897		100.00% Impervious Area				
Tc Length (min) (feet)	Slop (ft/f	•	Capacity (cfs)	Description		
5.0				Direct Entry, Sheet Flow		

#### Subcatchment WS-A: WS-A



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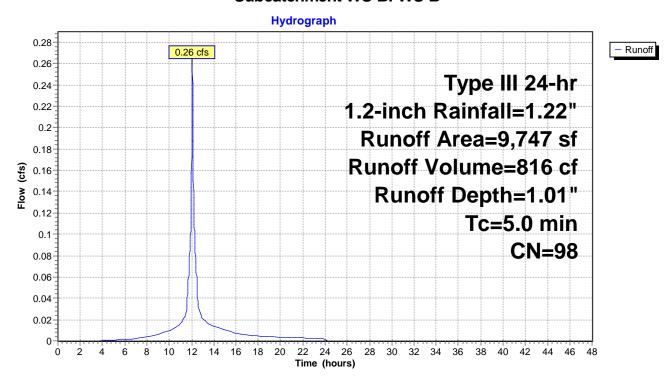
## Summary for Subcatchment WS-B: WS-B

Runoff = 0.26 cfs @ 12.07 hrs, Volume= 816 cf, Depth= 1.01"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 1.2-inch Rainfall=1.22"

A	rea (sf)	CN E	<b>Description</b>				
	9,747	98 F	98 Paved roads w/curbs & sewers, HSG A				
	9,747	1	100.00% Impervious Area				
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
5.0					Direct Entry, Sheet Flow		

#### Subcatchment WS-B: WS-B



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# **Summary for Pond 2P: PR-CB-1**

Inflow Area =	15,852 sf, 67.47% Impervious,	Inflow Depth = 0.48" for 1.2-inch event
Inflow =	0.20 cfs @ 12.07 hrs, Volume=	631 cf
Outflow =	0.20 cfs @ 12.07 hrs, Volume=	631 cf, Atten= 0%, Lag= 0.0 min
Primary =	0.18 cfs @ 12.06 hrs, Volume=	625 cf
Secondary =	0.02 cfs @ 12.08 hrs, Volume=	6 cf
Tertiary =	0.00 cfs @ 0.00 hrs, Volume=	0 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 276.43' @ 12.08 hrs

Flood Elev= 280.40'

Device	Routing	Invert	Outlet Devices
#1	Primary	276.20'	12.0" Round Culvert
	•		L= 155.0' RCP, groove end projecting, Ke= 0.200
			Inlet / Outlet Invert= 276.20' / 275.00' S= 0.0077 '/' Cc= 0.900
			n= 0.013, Flow Area= 0.79 sf
#2	Tertiary	280.40'	<b>24.0" x 24.0" Horiz. CB Grate</b> C= 0.600
			Limited to weir flow at low heads
#3	Secondary	276.20'	12.0" Round Culvert
			L= 37.4' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 276.20' / 275.00' S= 0.0321 '/' Cc= 0.900
			n= 0.013, Flow Area= 0.79 sf
#4	Device 3	276.42'	<b>4.0' long Sharp-Crested Rectangular Weir</b> 2 End Contraction(s)

**Primary OutFlow** Max=0.18 cfs @ 12.06 hrs HW=276.43' TW=275.48' (Dynamic Tailwater) **1=Culvert** (Outlet Controls 0.18 cfs @ 1.94 fps)

Secondary OutFlow Max=0.02 cfs @ 12.08 hrs HW=276.43' (Free Discharge)

3=Culvert (Passes 0.02 cfs of 0.23 cfs potential flow)

4=Sharp-Crested Rectangular Weir (Weir Controls 0.02 cfs @ 0.39 fps)

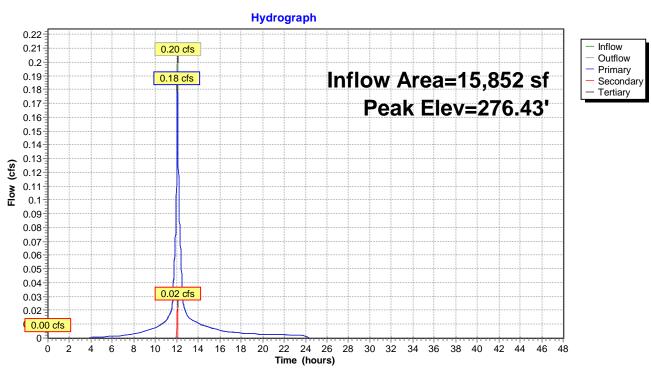
**Tertiary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=276.20' (Free Discharge) **2=CB Grate** (Controls 0.00 cfs)

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### Summary for Pond B-1: Basin #1

Inflow Area = 39,496 sf, 86.94% Impervious, Inflow Depth = 0.79" for 1.2-inch event
Inflow = 0.81 cfs @ 12.07 hrs, Volume= 2,606 cf
Outflow = 0.17 cfs @ 12.48 hrs, Volume= 2,606 cf
Oiscarded = 0.17 cfs @ 12.48 hrs, Volume= 2,606 cf
Primary = 0.00 cfs @ 0.00 hrs, Volume= 0 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 275.90' @ 12.48 hrs Surf.Area= 900 sf Storage= 671 cf Flood Elev= 285.00' Surf.Area= 2,737 sf Storage= 7,952 cf

Plug-Flow detention time= 24.0 min calculated for 2,605 cf (100% of inflow) Center-of-Mass det. time= 24.0 min (804.7 - 780.7)

Volume	Invert	Avail.Sto	rage Storage	e Description	
#1	275.00'	7,95	52 cf <b>Basin S</b>	Storage (Prismat	ic) Listed below (Recalc)
Elevatio	n Su	rf.Area	Inc.Store	Cum.Store	
(fee		(sq-ft)	(cubic-feet)	(cubic-feet)	
275.0	0	589	0	0	
276.0	0	934	762	762	
277.0	0	1,333	1,134	1,895	
278.0	0	1,777	1,555	3,450	
279.0	0	2,245	2,011	5,461	
280.0	0	2,737	2,491	7,952	
Device	Routing	Invert	Outlet Device	es	
#1	Discarded	275.00'	8.270 in/hr E	xfiltration over S	Surface area Phase-In= 0.01'
#2	Primary	279.50'	88.0' long x	5.0' breadth Bro	ad-Crested Rectangular Weir
	_		Head (feet)	0.20 0.40 0.60	0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00 3	.50 4.00 4.50 5	.00 5.50
			Coef. (Englis	sh) 2.34 2.50 2.	70 2.68 2.68 2.66 2.65 2.65 2.65 2.65
			2.67 2.66 2	.68 2.70 2.74 2	.79 2.88

**Discarded OutFlow** Max=0.17 cfs @ 12.48 hrs HW=275.90' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.17 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=275.00' (Free Discharge)

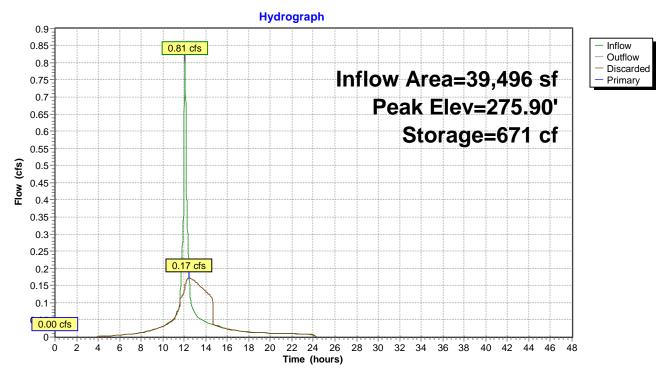
—2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Pond B-1: Basin #1



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Inflow

Outflow

Primary

Secondary

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### Summary for Pond CB#1: PR-CB #1

Inflow Area =	13,897 sf,100.00% Impervious,	Inflow Depth = 1.01" for 1.2-inch event
Inflow =	0.37 cfs @ 12.07 hrs, Volume=	1,164 cf
Outflow =	0.37 cfs @ 12.07 hrs, Volume=	1,164 cf, Atten= 0%, Lag= 0.0 min
Primary =	0.37 cfs @ 12.07 hrs, Volume=	1,164 cf
Secondary =	0.00 cfs @ 0.00 hrs, Volume=	0 cf

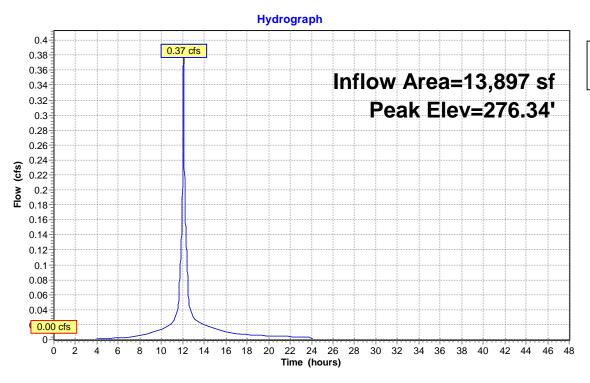
Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 276.34' @ 12.07 hrs Flood Elev= 278.90'

Device	Routing	Invert	Outlet Devices
#1	Primary	275.90'	12.0" Round RCP_Round 12"
	•		L= 15.0' RCP, groove end projecting, Ke= 0.200
			Inlet / Outlet Invert= 275.90' / 275.83' S= 0.0047 '/' Cc= 0.900
			n= 0.025 Corrugated metal, Flow Area= 0.79 sf
#2	Secondary	278.90'	<b>24.0" x 24.0" Horiz. CB Grate</b> C= 0.600
			Limited to weir flow at low heads

**Primary OutFlow** Max=0.37 cfs @ 12.07 hrs HW=276.34' TW=276.19' (Dynamic Tailwater) **1=RCP\_Round 12"** (Outlet Controls 0.37 cfs @ 1.61 fps)

**Secondary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=275.90' (Free Discharge) **2=CB Grate** (Controls 0.00 cfs)

#### Pond CB#1: PR-CB #1



- Inflow

Outflow

Primary

Secondary

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### **Summary for Pond CB#2: PR-CB#2**

Inflow Area =	9,747 sf,100.00% Impervious,	Inflow Depth = 1.01" for 1.2-inch event
Inflow =	0.26 cfs @ 12.07 hrs, Volume=	816 cf
Outflow =	0.26 cfs @ 12.07 hrs, Volume=	816 cf, Atten= 0%, Lag= 0.0 min
Primary =	0.26 cfs @ 12.07 hrs, Volume=	816 cf
Secondary =	0.00 cfs @ 0.00 hrs, Volume=	0 cf

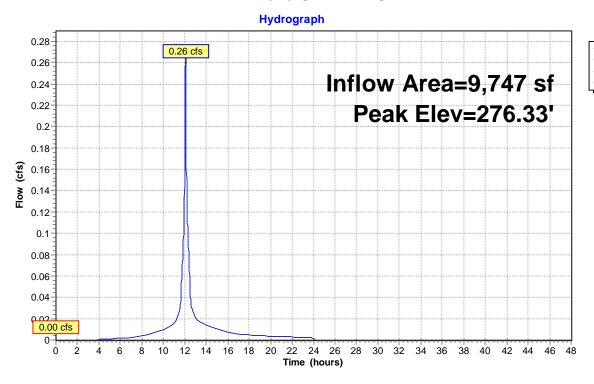
Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 276.33' @ 12.07 hrs Flood Elev= 278.90'

Device	Routing	Invert	Outlet Devices
#1	Primary	275.90'	12.0" Round RCP_Round 12"
	-		L= 25.0' CMP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 275.90' / 275.75' S= 0.0060 '/' Cc= 0.900
			n= 0.025 Corrugated metal, Flow Area= 0.79 sf
#2	Secondary	278.90'	<b>24.0" x 24.0" Horiz. CB Grate</b> C= 0.600

Primary OutFlow Max=0.26 cfs @ 12.07 hrs HW=276.33' TW=276.19' (Dynamic Tailwater) 1=RCP\_Round 12" (Outlet Controls 0.26 cfs @ 1.18 fps)

**Secondary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=275.90' (Free Discharge) **2=CB Grate** (Controls 0.00 cfs)

#### Pond CB#2: PR-CB#2



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### **Summary for Pond DMH: DMH #1**

Inflow Area = 23,644 sf,100.00% Impervious, Inflow Depth = 1.01" for 1.2-inch event

Inflow = 0.63 cfs @ 12.07 hrs, Volume= 1,981 cf

Outflow = 0.63 cfs @ 12.07 hrs, Volume= 1,981 cf, Atten= 0%, Lag= 0.0 min

Primary = 0.63 cfs @ 12.07 hrs, Volume= 1,981 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 276.19' @ 12.08 hrs

Flood Elev= 279.00'

Device Routing Invert Outlet Devices

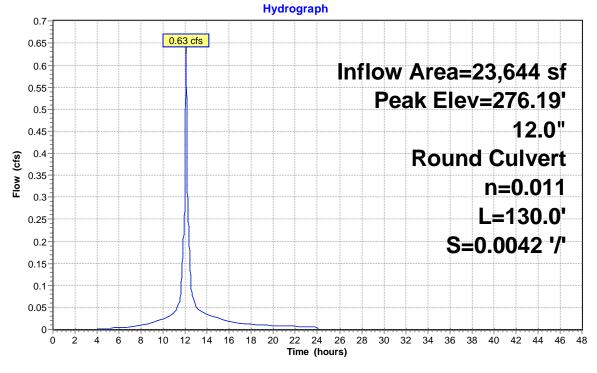
#1 Primary 275.75' 12.0" Round RCP Round 12"

L= 130.0' RCP, groove end projecting, Ke= 0.200

Inlet / Outlet Invert= 275.75' / 275.20' S= 0.0042 '/' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf

**Primary OutFlow** Max=0.63 cfs @ 12.07 hrs HW=276.19' TW=275.51' (Dynamic Tailwater) **1=RCP\_Round** 12" (Barrel Controls 0.63 cfs @ 2.76 fps)

#### Pond DMH: DMH #1





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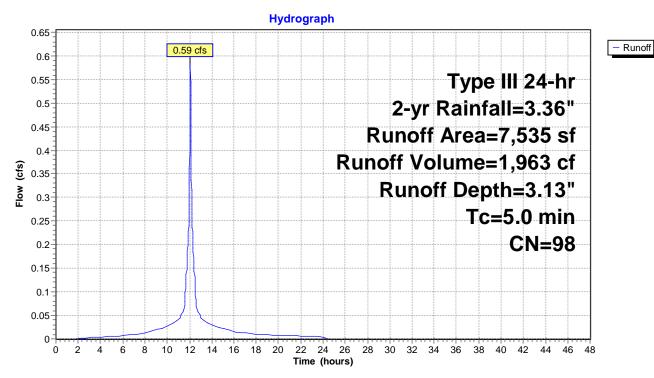
# Summary for Subcatchment CB-1A: CB-1A

Runoff = 0.59 cfs @ 12.07 hrs, Volume= 1,963 cf, Depth= 3.13"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 2-yr Rainfall=3.36"

	Α	rea (sf)	CN [	CN Description				
*	•	7,535	98 F	98 Paved roads w/curbs & sewers, HSG A				
		7,535	1	100.00% Impervious Area				
	Тс	Length	Slope	Velocity	Capacity	Description		
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
	5.0					Direct Entry,		

#### Subcatchment CB-1A: CB-1A



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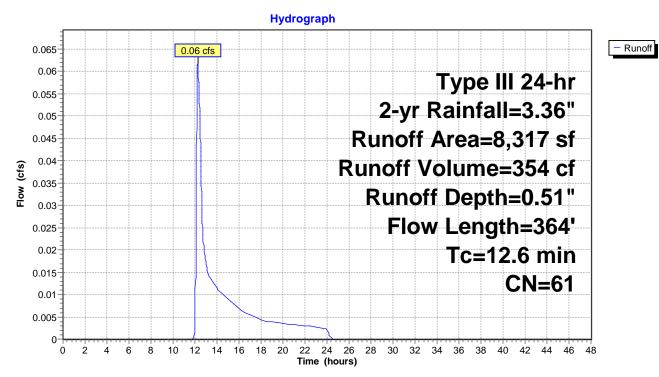
## Summary for Subcatchment CB-1B: CB-1B

Runoff = 0.06 cfs @ 12.23 hrs, Volume= 354 cf, Depth= 0.51"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 2-yr Rainfall=3.36"

_	Aı	rea (sf)	CN D	escription					
		8,317	61 1	61 1/4 acre lots, 38% imp, HSG A					
		5,157	6	2.00% Per	vious Area				
		3,160	3	8.00% lmp	ervious Ar	ea			
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
-	9.7	34	0.0153	0.06	, ,	Sheet Flow,			
	2.9	330	0.0090	1.93		Grass: Bermuda n= 0.410 P2= 3.60" <b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps			
	12.6	364	Total						

#### Subcatchment CB-1B: CB-1B



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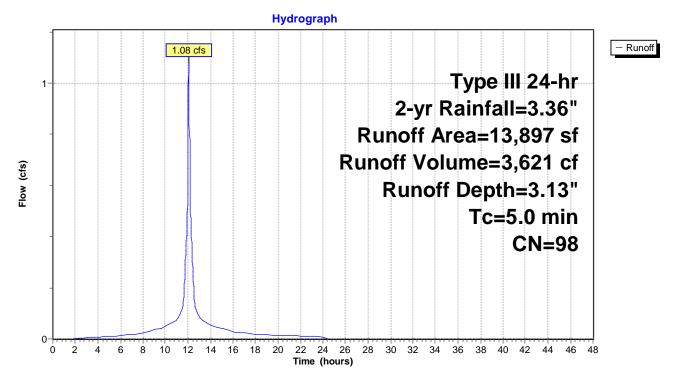
## Summary for Subcatchment WS-A: WS-A

Runoff = 1.08 cfs @ 12.07 hrs, Volume= 3,621 cf, Depth= 3.13"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 2-yr Rainfall=3.36"

Area (sf)	CN	CN Description			
13,897	98	98 Paved roads w/curbs & sewers, HSG A			
13,897		100.00% Im	pervious A	rea	
Tc Length (min) (feet)	Slop (ft/f	•	Capacity (cfs)	Description	
5.0				Direct Entry, Sheet Flow	

#### Subcatchment WS-A: WS-A



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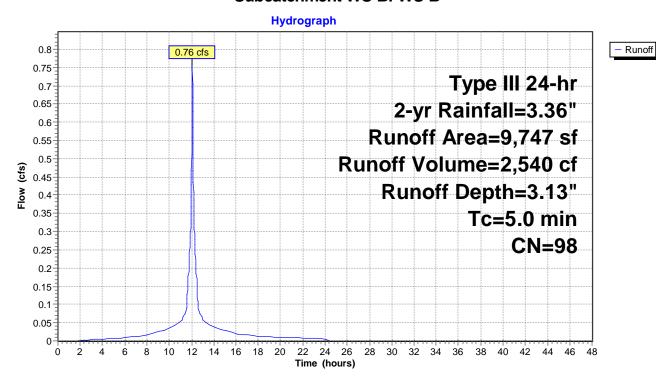
## Summary for Subcatchment WS-B: WS-B

Runoff = 0.76 cfs @ 12.07 hrs, Volume= 2,540 cf, Depth= 3.13"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 2-yr Rainfall=3.36"

_	Α	rea (sf)	CN [	CN Description			
		9,747	98 F	98 Paved roads w/curbs & sewers, HSG A			
		9,747	100.00% Impervious Area			ırea	
_	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
	5.0					Direct Entry, Sheet Flow	

#### Subcatchment WS-B: WS-B



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# Summary for Pond 2P: PR-CB-1

Inflow Area =	15,852 sf, 67.47% Impervious,	Inflow Depth = 1.75" for 2-yr event
Inflow =	0.61 cfs @ 12.07 hrs, Volume=	2,318 cf
Outflow =	0.61 cfs @ 12.07 hrs, Volume=	2,318 cf, Atten= 0%, Lag= 0.0 min
Primary =	0.15 cfs @ 11.81 hrs, Volume=	1,178 cf
Secondary =	0.61 cfs @ 12.07 hrs, Volume=	1,140 cf
Tertiary =	0.00 cfs @ 0.00 hrs, Volume=	0 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 276.59' @ 12.07 hrs

Flood Elev= 280.40'

Device	Routing	Invert	Outlet Devices
#1	Primary	276.20'	12.0" Round Culvert
	•		L= 155.0' RCP, groove end projecting, Ke= 0.200
			Inlet / Outlet Invert= 276.20' / 275.00' S= 0.0077 '/' Cc= 0.900
			n= 0.013, Flow Area= 0.79 sf
#2	Tertiary	280.40'	<b>24.0" x 24.0" Horiz. CB Grate</b> C= 0.600
	•		Limited to weir flow at low heads
#3	Secondary	276.20'	12.0" Round Culvert
	•		L= 37.4' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 276.20' / 275.00' S= 0.0321 '/' Cc= 0.900
			n= 0.013, Flow Area= 0.79 sf
#4	Device 3	276.42'	4.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=0.15 cfs @ 11.81 hrs HW=276.44' TW=275.79' (Dynamic Tailwater) 1=Culvert (Outlet Controls 0.15 cfs @ 1.62 fps)

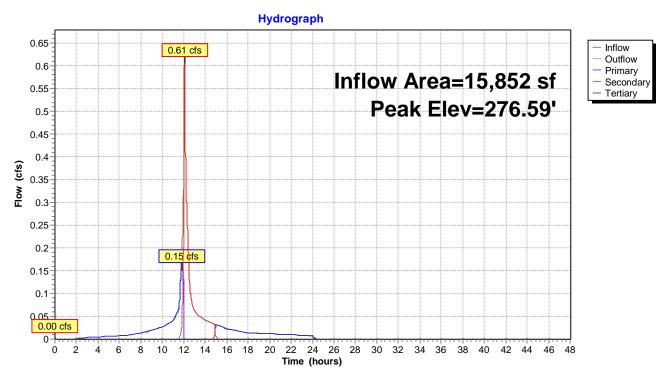
**Secondary OutFlow** Max=0.60 cfs @ 12.07 hrs HW=276.59' (Free Discharge) -3=Culvert (Inlet Controls 0.60 cfs @ 2.13 fps)

4=Sharp-Crested Rectangular Weir (Passes 0.60 cfs of 0.91 cfs potential flow)

**Tertiary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=276.20' (Free Discharge) **2=CB Grate** (Controls 0.00 cfs)

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### Pond 2P: PR-CB-1



Type III 24-hr 2-yr Rainfall=3.36" Printed 2/9/2023

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### **Summary for Pond B-1: Basin #1**

Inflow Area = 39,496 sf, 86.94% Impervious, Inflow Depth = 2.23" for 2-yr event

Inflow = 1.84 cfs @ 12.07 hrs, Volume= 7,339 cf

Outflow = 0.28 cfs @ 12.54 hrs, Volume= 7,339 cf, Atten= 85%, Lag= 28.1 min

Discarded = 0.00 cfs @ 0.00 hrs, Volume= 0 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 277.31' @ 12.54 hrs Surf.Area= 1,469 sf Storage= 2,324 cf Flood Elev= 285.00' Surf.Area= 2,737 sf Storage= 7,952 cf

Plug-Flow detention time= 62.4 min calculated for 7,338 cf (100% of inflow) Center-of-Mass det. time= 62.4 min (823.5 - 761.1)

<u>Volume</u>	Invert	Avail.Sto	rage Stora	ge Description	
#1	275.00'	7,95	52 cf <b>Basin</b>	Storage (Prismat	tic) Listed below (Recalc)
Elevatio	n Su	rf.Area	Inc.Store	Cum.Store	
(feet		(sq-ft)	(cubic-feet)	(cubic-feet)	
275.0	-	589	0	0	
276.0	0	934	762	762	
277.0	0	1,333	1,134	1,895	
278.0	0	1,777	1,555	3,450	
279.0	0	2,245	2,011	5,461	
280.0	0	2,737	2,491	7,952	
Device	Routing	Invert	Outlet Devi	ces	
#1	Discarded	275.00'	8.270 in/hr	Exfiltration over	Surface area Phase-In= 0.01'
#2	Primary	279.50'	88.0' long	x 5.0' breadth Bro	pad-Crested Rectangular Weir
	•		Head (feet)	0.20 0.40 0.60	0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00	3.50 4.00 4.50 5	5.00 5.50
			Coef. (Engl	lish) 2.34 2.50 2	.70 2.68 2.68 2.66 2.65 2.65 2.65 2.65
			2.67 2.66	2.68 2.70 2.74 2	2.79 2.88

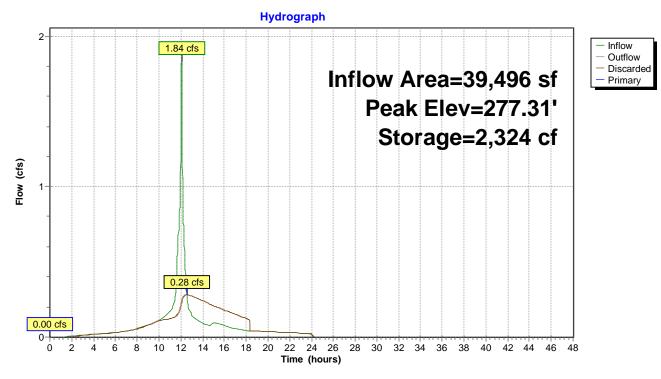
**Discarded OutFlow** Max=0.28 cfs @ 12.54 hrs HW=277.31' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.28 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=275.00' (Free Discharge)

—2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Pond B-1: Basin #1



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### Summary for Pond CB#1: PR-CB #1

Inflow Area = 13,897 sf,100.00% Impervious, Inflow Depth = 3.13" for 2-yr event

Inflow = 1.08 cfs @ 12.07 hrs, Volume= 3,621 cf

Outflow = 1.08 cfs @ 12.07 hrs, Volume= 3,621 cf, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3

Peak Elev= 277.32' @ 12.50 hrs

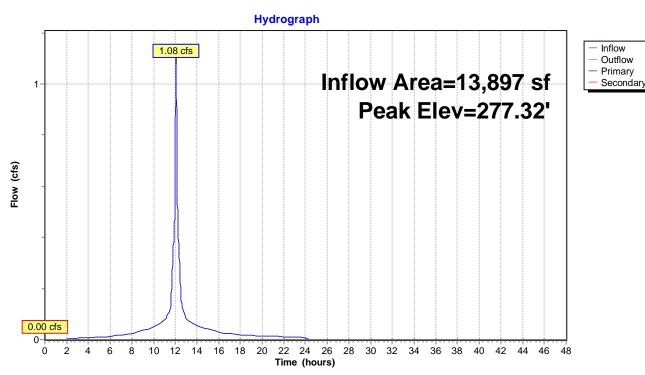
Flood Elev= 278.90'

Device	Routing	Invert	Outlet Devices
#1	Primary	275.90'	12.0" Round RCP_Round 12"
	•		L= 15.0' RCP, groove end projecting, Ke= 0.200
			Inlet / Outlet Invert= 275.90' / 275.83' S= 0.0047 '/' Cc= 0.900
			n= 0.025 Corrugated metal, Flow Area= 0.79 sf
#2	Secondary	278.90'	<b>24.0" x 24.0" Horiz. CB Grate</b> C= 0.600
	-		Limited to weir flow at low heads

**Primary OutFlow** Max=1.08 cfs @ 12.07 hrs HW=277.06' TW=276.97' (Dynamic Tailwater) **1=RCP\_Round** 12" (Outlet Controls 1.08 cfs @ 1.49 fps)

**Secondary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=275.90' (Free Discharge) **2=CB Grate** (Controls 0.00 cfs)

#### Pond CB#1: PR-CB #1



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Printed 2/9/2023 Page 23

- Inflow

Outflow

Primary

Secondary

### Summary for Pond CB#2: PR-CB#2

Inflow Area = 9,747 sf,100.00% Impervious, Inflow Depth = 3.13" for 2-yr event

Inflow = 0.76 cfs @ 12.07 hrs, Volume= 2,540 cf

Outflow = 0.76 cfs @ 12.07 hrs, Volume= 2,540 cf, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3

Peak Elev= 277.32' @ 12.50 hrs

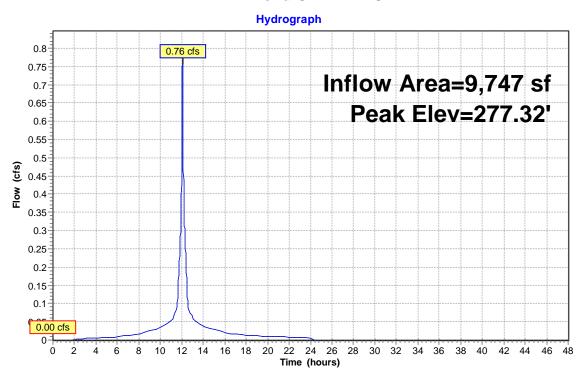
Flood Elev= 278.90'

Device	Routing	Invert	Outlet Devices
#1	Primary	275.90'	12.0" Round RCP_Round 12"
	-		L= 25.0' CMP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 275.90' / 275.75' S= 0.0060 '/' Cc= 0.900
			n= 0.025 Corrugated metal, Flow Area= 0.79 sf
#2	Secondary	278.90'	<b>24.0" x 24.0" Horiz. CB Grate</b> C= 0.600

**Primary OutFlow** Max=0.76 cfs @ 12.07 hrs HW=277.05' TW=276.97' (Dynamic Tailwater) **1=RCP\_Round 12"** (Outlet Controls 0.76 cfs @ 1.05 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=275.90' (Free Discharge) -2=CB Grate (Controls 0.00 cfs)

#### Pond CB#2: PR-CB#2



## **Proposed - Constr Rev-MODIFIED**

Type III 24-hr 2-yr Rainfall=3.36" Printed 2/9/2023

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### **Summary for Pond DMH: DMH #1**

Inflow Area = 23,644 sf,100.00% Impervious, Inflow Depth = 3.13" for 2-yr event

Inflow = 1.84 cfs @ 12.07 hrs, Volume= 6,161 cf

Outflow = 1.84 cfs @ 12.07 hrs, Volume= 6,161 cf, Atten= 0%, Lag= 0.0 min

Primary = 1.84 cfs @ 12.07 hrs, Volume= 6,161 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3

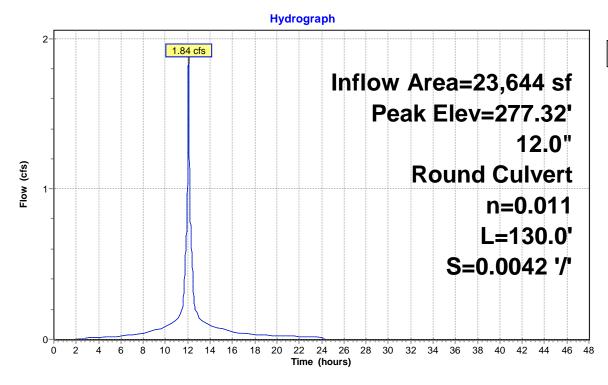
Peak Elev= 277.32' @ 12.51 hrs

Flood Elev= 279.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	275.75'	12.0" Round RCP_Round 12"
			L= 130.0' RCP, groove end projecting, Ke= 0.200
			Inlet / Outlet Invert= 275.75' / 275.20' S= 0.0042 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf

**Primary OutFlow** Max=1.84 cfs @ 12.07 hrs HW=276.97' TW=276.65' (Dynamic Tailwater) **1=RCP\_Round** 12" (Outlet Controls 1.84 cfs @ 2.43 fps)

#### Pond DMH: DMH #1





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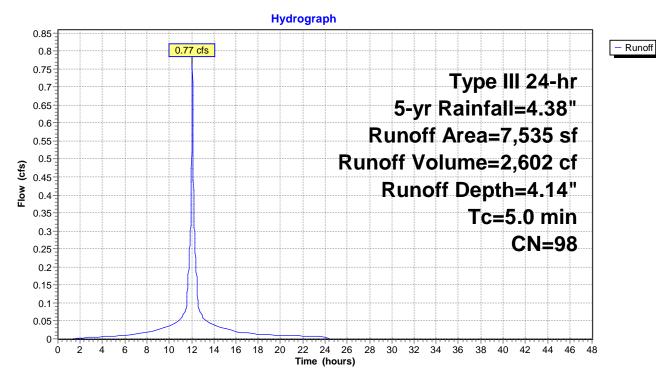
# Summary for Subcatchment CB-1A: CB-1A

Runoff = 0.77 cfs @ 12.07 hrs, Volume= 2,602 cf, Depth= 4.14"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 5-yr Rainfall=4.38"

	Α	rea (sf)	CN [	CN Description				
*	•	7,535	98 F	98 Paved roads w/curbs & sewers, HSG A				
		7,535	1	100.00% Impervious Area				
	Тс	Length	Slope	Velocity	Capacity	Description		
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
	5.0					Direct Entry,		

#### Subcatchment CB-1A: CB-1A



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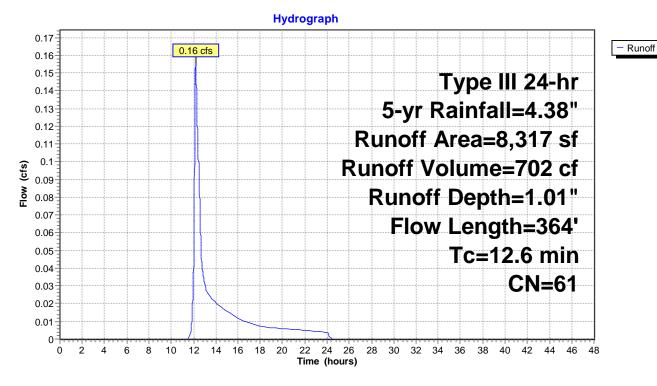
## Summary for Subcatchment CB-1B: CB-1B

Runoff = 0.16 cfs @ 12.20 hrs, Volume= 702 cf, Depth= 1.01"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 5-yr Rainfall=4.38"

_	Aı	rea (sf)	CN D	escription					
		8,317	61 1	61 1/4 acre lots, 38% imp, HSG A					
		5,157	6	62.00% Pervious Area					
		3,160	3	8.00% lmp	ervious Are	ea			
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
_	9.7	34	0.0153	0.06		Sheet Flow,			
	2.9	330	0.0090	1.93		Grass: Bermuda n= 0.410 P2= 3.60" <b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps			
_	12.6	364	Total	•					

#### Subcatchment CB-1B: CB-1B



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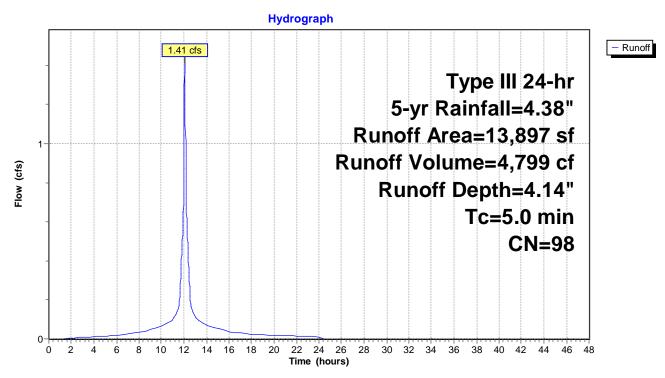
## Summary for Subcatchment WS-A: WS-A

Runoff = 1.41 cfs @ 12.07 hrs, Volume= 4,799 cf, Depth= 4.14"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 5-yr Rainfall=4.38"

Area (sf)	CN	I Description				
13,897	98	98 Paved roads w/curbs & sewers, HSG A				
13,897		100.00% Im	npervious A	rea		
Tc Length (min) (feet)	Slop (ft/f	•	Capacity (cfs)	Description		
5.0				Direct Entry, Sheet Flow		

#### Subcatchment WS-A: WS-A



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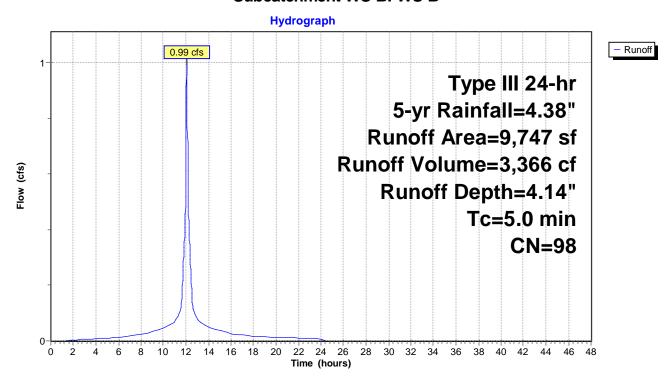
## Summary for Subcatchment WS-B: WS-B

Runoff = 0.99 cfs @ 12.07 hrs, Volume= 3,366 cf, Depth= 4.14"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 5-yr Rainfall=4.38"

_	Α	rea (sf)	CN [	N Description				
		9,747	98 F	98 Paved roads w/curbs & sewers, HSG A				
		9,747	100.00% Impervious Area					
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
Ī	5.0					Direct Entry, Sheet Flow		

#### Subcatchment WS-B: WS-B



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# Summary for Pond 2P: PR-CB-1

Inflow Area =	15,852 sf, 67.47% Impervious,	Inflow Depth = 2.50" for 5-yr event
Inflow =	0.85 cfs @ 12.08 hrs, Volume=	3,304 cf
Outflow =	0.85 cfs @ 12.08 hrs, Volume=	3,304 cf, Atten= 0%, Lag= 0.0 min
Primary =	0.14 cfs @ 11.72 hrs, Volume=	1,313 cf
Secondary =	0.85 cfs @ 12.08 hrs, Volume=	1,993 cf
Tertiary =	0.00 cfs @ 0.00 hrs, Volume=	0 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 276.67' @ 12.08 hrs

Flood Elev= 280.40'

Device	Routing	Invert	Outlet Devices
#1	Primary	276.20'	12.0" Round Culvert
	•		L= 155.0' RCP, groove end projecting, Ke= 0.200
			Inlet / Outlet Invert= 276.20' / 275.00' S= 0.0077 '/' Cc= 0.900
			n= 0.013, Flow Area= 0.79 sf
#2	Tertiary	280.40'	<b>24.0" x 24.0" Horiz. CB Grate</b> C= 0.600
			Limited to weir flow at low heads
#3	Secondary	276.20'	12.0" Round Culvert
			L= 37.4' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 276.20' / 275.00' S= 0.0321 '/' Cc= 0.900
			n= 0.013, Flow Area= 0.79 sf
#4	Device 3	276.42'	<b>4.0' long Sharp-Crested Rectangular Weir</b> 2 End Contraction(s)

**Primary OutFlow** Max=0.14 cfs @ 11.72 hrs HW=276.44' TW=275.97' (Dynamic Tailwater) **1=Culvert** (Outlet Controls 0.14 cfs @ 1.41 fps)

Secondary OutFlow Max=0.85 cfs @ 12.08 hrs HW=276.67' (Free Discharge)

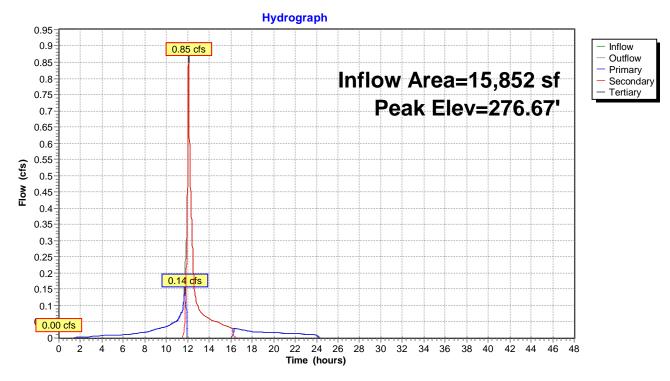
3=Culvert (Inlet Controls 0.85 cfs @ 2.34 fps)

4=Sharp-Crested Rectangular Weir (Passes 0.85 cfs of 1.62 cfs potential flow)

**Tertiary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=276.20' (Free Discharge) **2=CB Grate** (Controls 0.00 cfs)

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# Pond 2P: PR-CB-1



Type III 24-hr 5-yr Rainfall=4.38" Printed 2/9/2023

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### **Summary for Pond B-1: Basin #1**

Inflow Area = 39,496 sf, 86.94% Impervious, Inflow Depth = 2.88" for 5-yr event

Inflow = 2.41 cfs @ 12.07 hrs, Volume= 9,478 cf

Outflow = 0.33 cfs @ 12.56 hrs, Volume= 9,478 cf, Atten= 86%, Lag= 29.5 min

Discarded = 0.33 cfs @ 12.56 hrs, Volume= 9,478 cf

Primary = 0.00 cfs @ 0.00 hrs, Volume= 0 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 277.86' @ 12.56 hrs Surf.Area= 1,717 sf Storage= 3,214 cf Flood Elev= 285.00' Surf.Area= 2,737 sf Storage= 7,952 cf

Plug-Flow detention time= 79.2 min calculated for 9,476 cf (100% of inflow) Center-of-Mass det. time= 79.2 min (833.8 - 754.6)

<u>Volume</u>	Invert	Avail.Sto	rage Storage I	Description	
#1	275.00'	7,95	52 cf Basin St	orage (Prismat	ic) Listed below (Recalc)
Clayatia	C	rf Araa	Ina Ctora	Cum Store	
Elevation		rf.Area	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	
275.0	00	589	0	0	
276.0	00	934	762	762	
277.0	00	1,333	1,134	1,895	
278.0	00	1,777	1,555	3,450	
279.0	00	2,245	2,011	5,461	
280.0	00	2,737	2,491	7,952	
Device	Routing	Invert	Outlet Devices	3	
#1	Discarded	275.00'	8.270 in/hr Ex	filtration over \$	Surface area Phase-In= 0.01'
#2	Primary	279.50'	88.0' long x 5	.0' breadth Bro	pad-Crested Rectangular Weir
			Head (feet) 0.	20 0.40 0.60	0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00 3.5	0 4.00 4.50 5	.00 5.50
			Coef. (English	) 2.34 2.50 2.	.70 2.68 2.68 2.66 2.65 2.65 2.65 2.65
			` •	, 8 2.70 2.74 2	

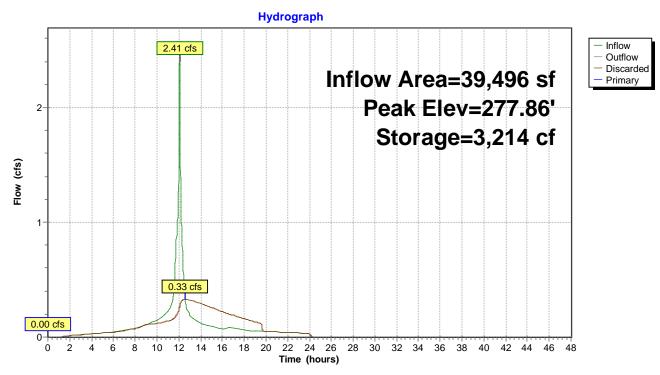
**Discarded OutFlow** Max=0.33 cfs @ 12.56 hrs HW=277.86' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.33 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=275.00' (Free Discharge)

—2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Pond B-1: Basin #1



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### Summary for Pond CB#1: PR-CB #1

Inflow Area = 13,897 sf,100.00% Impervious, Inflow Depth = 4.14" for 5-yr event

Inflow = 1.41 cfs @ 12.07 hrs, Volume= 4,799 cf

Outflow = 1.41 cfs @ 12.07 hrs, Volume= 4,799 cf, Atten= 0%, Lag= 0.0 min

Primary = 1.41 cfs @ 12.07 hrs, Volume= 4,799 cf

Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0 cf

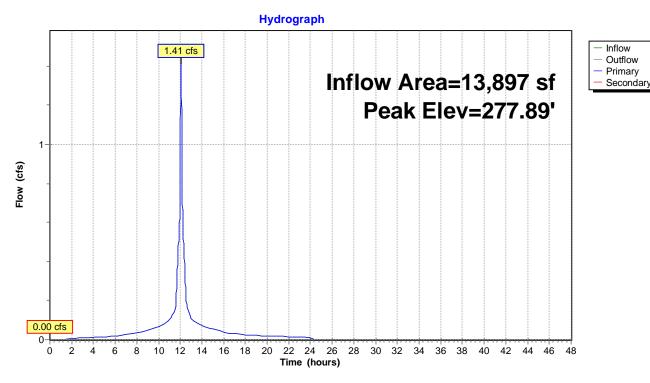
Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 277.89' @ 12.09 hrs Flood Elev= 278.90'

Device	Routing	Invert	Outlet Devices
#1	Primary	275.90'	12.0" Round RCP_Round 12"
	•		L= 15.0' RCP, groove end projecting, Ke= 0.200
			Inlet / Outlet Invert= 275.90' / 275.83' S= 0.0047 '/' Cc= 0.900
			n= 0.025 Corrugated metal, Flow Area= 0.79 sf
#2	Secondary	278.90'	<b>24.0" x 24.0" Horiz. CB Grate</b> C= 0.600
			Limited to weir flow at low heads

**Primary OutFlow** Max=1.41 cfs @ 12.07 hrs HW=277.83' TW=277.68' (Dynamic Tailwater) **1=RCP\_Round** 12" (Outlet Controls 1.41 cfs @ 1.80 fps)

**Secondary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=275.90' (Free Discharge) **2=CB Grate** (Controls 0.00 cfs)

#### Pond CB#1: PR-CB #1



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- Inflow

Outflow Primary

Secondary

# Summary for Pond CB#2: PR-CB#2

Inflow Area = 9,747 sf,100.00% Impervious, Inflow Depth = 4.14" for 5-yr event

Inflow = 0.99 cfs @ 12.07 hrs, Volume= 3,366 cf

Outflow = 0.99 cfs @ 12.07 hrs, Volume= 3,366 cf, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3

Peak Elev= 277.88' @ 12.50 hrs

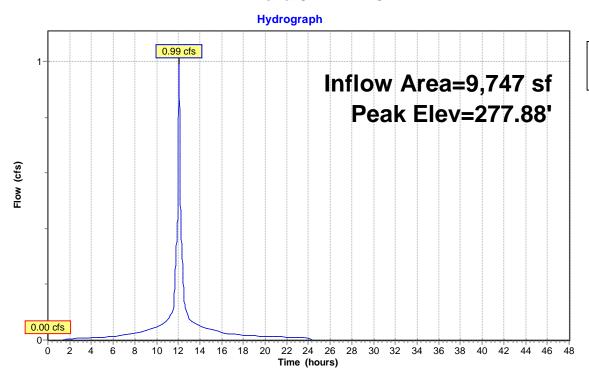
Flood Elev= 278.90'

Device	Routing	Invert	Outlet Devices	
#1	Primary	275.90'	12.0" Round RCP_Round 12"	
	•		L= 25.0' CMP, projecting, no headwall, Ke= 0.900	
			Inlet / Outlet Invert= 275.90' / 275.75' S= 0.0060 '/' Cc= 0.900	
			n= 0.025 Corrugated metal, Flow Area= 0.79 sf	
#2	Secondary	278.90'	<b>24.0" x 24.0" Horiz. CB Grate</b> C= 0.600	

**Primary OutFlow** Max=0.99 cfs @ 12.07 hrs HW=277.80' TW=277.68' (Dynamic Tailwater) **1=RCP\_Round 12"** (Outlet Controls 0.99 cfs @ 1.26 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=275.90' (Free Discharge)  $^{\bullet}$ 2=CB Grate (Controls 0.00 cfs)

#### Pond CB#2: PR-CB#2



## **Proposed - Constr Rev-MODIFIED**

Type III 24-hr 5-yr Rainfall=4.38" Printed 2/9/2023

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### **Summary for Pond DMH: DMH #1**

Inflow Area = 23,644 sf,100.00% Impervious, Inflow Depth = 4.14" for 5-yr event

Inflow = 2.41 cfs @ 12.07 hrs, Volume= 8,166 cf

Outflow = 2.41 cfs @ 12.07 hrs, Volume= 8,166 cf, Atten= 0%, Lag= 0.0 min

Primary = 2.41 cfs @ 12.07 hrs, Volume= 8,166 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3

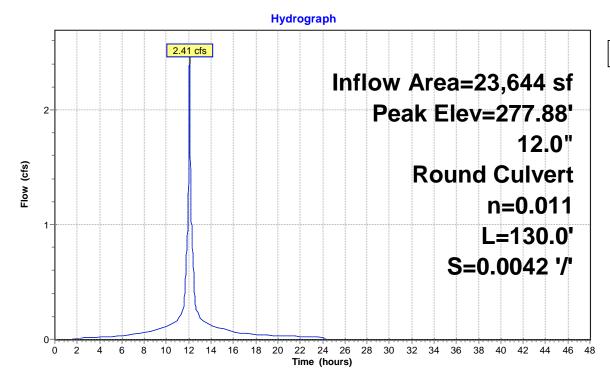
Peak Elev= 277.88' @ 12.52 hrs

Flood Elev= 279.00'

Device	Routing	Invert	Outlet Devices		
#1	Primary	275.75'	12.0" Round RCP_Round 12"		
	-		L= 130.0' RCP, groove end projecting, Ke= 0.200		
			Inlet / Outlet Invert= 275.75' / 275.20' S= 0.0042 '/' Cc= 0.900		
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf		

**Primary OutFlow** Max=2.41 cfs @ 12.07 hrs HW=277.68' TW=277.08' (Dynamic Tailwater) **1=RCP\_Round 12"** (Outlet Controls 2.41 cfs @ 3.06 fps)

#### Pond DMH: DMH #1





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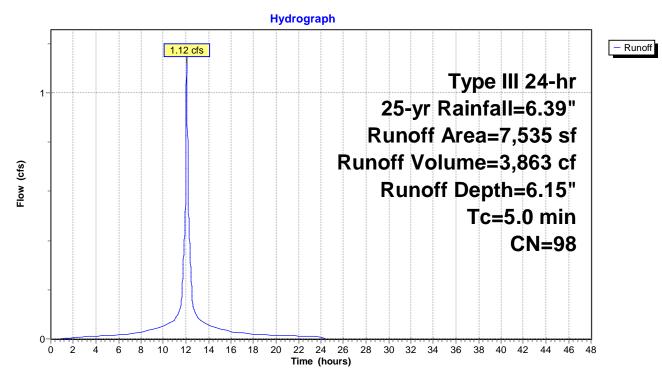
# Summary for Subcatchment CB-1A: CB-1A

Runoff = 1.12 cfs @ 12.07 hrs, Volume= 3,863 cf, Depth= 6.15"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 25-yr Rainfall=6.39"

	Α	rea (sf)	CN [	CN Description					
*		7,535	98 F	98 Paved roads w/curbs & sewers, HSG A					
		7,535	,	100.00% Impervious Area					
		Length		,	Capacity	Description			
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	5.0					Direct Entry,			

#### Subcatchment CB-1A: CB-1A



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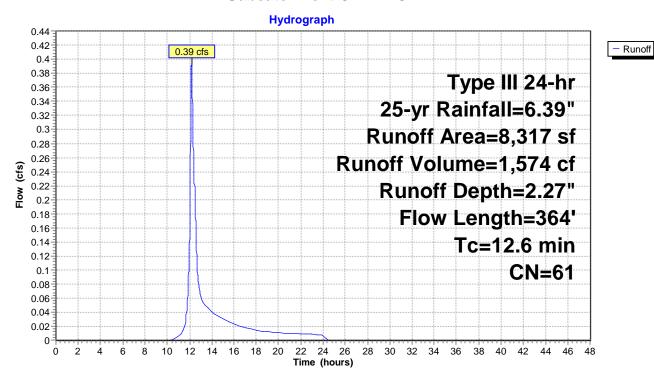
# Summary for Subcatchment CB-1B: CB-1B

Runoff = 0.39 cfs @ 12.19 hrs, Volume= 1,574 cf, Depth= 2.27"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 25-yr Rainfall=6.39"

	Aı	rea (sf)	CN Description							
		8,317	7 61 1/4 acre lots, 38% imp, HSG A							
_		5,157	6	62.00% Pervious Area						
		3,160	3	38.00% Impervious Area						
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
_	9.7	34	0.0153	0.06		Sheet Flow,				
	2.9	330	0.0090	1.93		Grass: Bermuda n= 0.410 P2= 3.60" <b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps				
_	12.6	364	Total				_			

### Subcatchment CB-1B: CB-1B



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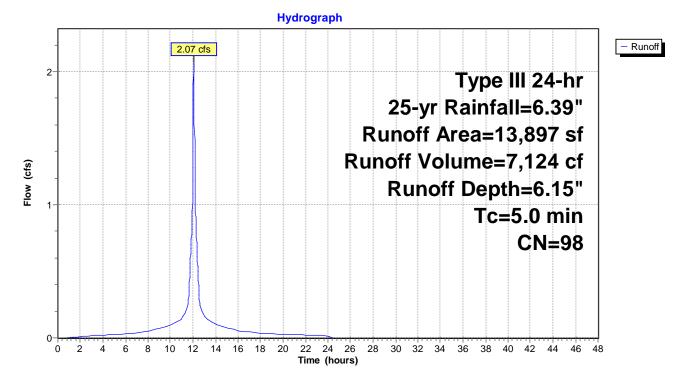
## Summary for Subcatchment WS-A: WS-A

Runoff = 2.07 cfs @ 12.07 hrs, Volume= 7,124 cf, Depth= 6.15"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 25-yr Rainfall=6.39"

	Area (sf)	CN	Description					
	13,897	98	Paved roads w/curbs & sewers, HSG A					
	13,897 100.00% Impervious Area							
T (min	c Length ) (feet		•	Capacity (cfs)	Description			
5.	)				Direct Entry, Sheet Flow			

### Subcatchment WS-A: WS-A



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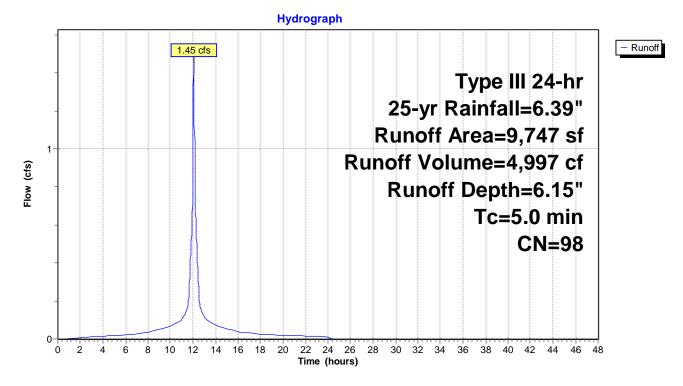
## Summary for Subcatchment WS-B: WS-B

Runoff = 1.45 cfs @ 12.07 hrs, Volume= 4,997 cf, Depth= 6.15"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 25-yr Rainfall=6.39"

	rea (sf)	CN I	Description					
	9,747	98	98 Paved roads w/curbs & sewers, HSG A					
	9,747		100.00% Impervious Area					
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
5.0					Direct Entry, Sheet Flow			

#### Subcatchment WS-B: WS-B



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# Summary for Pond 2P: PR-CB-1

Inflow Area =	15,852 sf, 67.47% Impervious,	Inflow Depth = 4.12" for 25-yr event
Inflow =	1.38 cfs @ 12.08 hrs, Volume=	5,436 cf
Outflow =	1.38 cfs @ 12.08 hrs, Volume=	5,436 cf, Atten= 0%, Lag= 0.0 min
Primary =	0.10 cfs @ 11.21 hrs, Volume=	1,531 cf
Secondary =	1.38 cfs @ 12.08 hrs, Volume=	3,906 cf
Tertiary =	0.00 cfs @ 0.00 hrs, Volume=	0 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 276.82' @ 12.08 hrs

Flood Elev= 280.40'

Device	Routing	Invert	Outlet Devices
#1	Primary	276.20'	12.0" Round Culvert
	•		L= 155.0' RCP, groove end projecting, Ke= 0.200
			Inlet / Outlet Invert= 276.20' / 275.00' S= 0.0077 '/' Cc= 0.900
			n= 0.013, Flow Area= 0.79 sf
#2	Tertiary	280.40'	<b>24.0" x 24.0" Horiz. CB Grate</b> C= 0.600
			Limited to weir flow at low heads
#3	Secondary	276.20'	12.0" Round Culvert
			L= 37.4' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 276.20' / 275.00' S= 0.0321 '/' Cc= 0.900
			n= 0.013, Flow Area= 0.79 sf
#4	Device 3	276.42'	<b>4.0' long Sharp-Crested Rectangular Weir</b> 2 End Contraction(s)

**Primary OutFlow** Max=0.10 cfs @ 11.21 hrs HW=276.42′ TW=276.07′ (Dynamic Tailwater) **1=Culvert** (Outlet Controls 0.10 cfs @ 1.15 fps)

Secondary OutFlow Max=1.38 cfs @ 12.08 hrs HW=276.82' (Free Discharge)

3=Culvert (Inlet Controls 1.38 cfs @ 2.68 fps)

4=Sharp-Crested Rectangular Weir (Passes 1.38 cfs of 3.26 cfs potential flow)

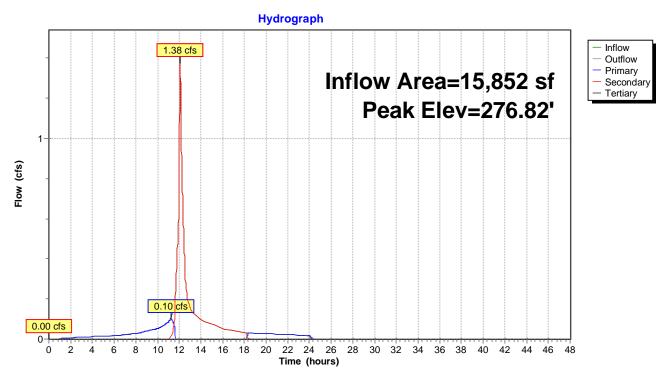
**Tertiary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=276.20' (Free Discharge) **2=CB Grate** (Controls 0.00 cfs)

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Pond 2P: PR-CB-1



Type III 24-hr 25-yr Rainfall=6.39" Printed 2/9/2023

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# **Summary for Pond B-1: Basin #1**

Inflow Area = 39,496 sf, 86.94% Impervious, Inflow Depth = 4.08" for 25-yr event

Inflow = 3.54 cfs @ 12.07 hrs, Volume= 13,437 cf

Outflow = 0.41 cfs @ 12.63 hrs, Volume= 13,437 cf, Atten= 89%, Lag= 33.7 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 278.73' @ 12.63 hrs Surf.Area= 2,119 sf Storage= 4,875 cf Flood Elev= 285.00' Surf.Area= 2,737 sf Storage= 7,952 cf

Plug-Flow detention time= 107.5 min calculated for 13,434 cf (100% of inflow)

Center-of-Mass det. time= 107.4 min (852.5 - 745.1)

Volume	Invert	Avail.Sto	rage Storage D	Description	
#1	275.00'	7,95	52 cf <b>Basin Sto</b>	orage (Prismat	cic) Listed below (Recalc)
	_				
Elevation	on Su	ırf.Area	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	
275.0	00	589	0	0	
276.0	00	934	762	762	
277.0	00	1,333	1,134	1,895	
278.0	00	1,777	1,555	3,450	
279.0	00	2,245	2,011	5,461	
280.0	00	2,737	2,491	7,952	
Device	Routing	Invert	Outlet Devices		
#1	Discarded	275.00'	8.270 in/hr Exf	iltration over	Surface area Phase-In= 0.01'
#2	Primary	279.50'	88.0' long x 5.	0' breadth Bro	pad-Crested Rectangular Weir
			Head (feet) 0.2	20 0.40 0.60	0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00 3.50	4.00 4.50 5	.00 5.50
			Coef. (English)	2.34 2.50 2.	.70 2.68 2.68 2.66 2.65 2.65 2.65 2.65
			2.67 2.66 2.68	3 2.70 2.74 2	.79 2.88

**Discarded OutFlow** Max=0.41 cfs @ 12.63 hrs HW=278.73' (Free Discharge) **1=Exfiltration** (Exfiltration Controls 0.41 cfs)

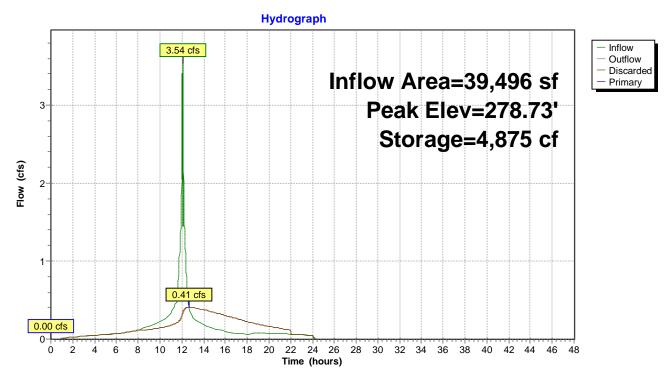
Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=275.00' (Free Discharge)

—2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Pond B-1: Basin #1



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## Summary for Pond CB#1: PR-CB #1

Inflow Area = 13,897 sf,100.00% Impervious, Inflow Depth = 6.15" for 25-yr event

Inflow = 2.07 cfs @ 12.07 hrs, Volume= 7,124 cf

Outflow = 2.07 cfs @ 12.07 hrs, Volume= 7,124 cf, Atten= 0%, Lag= 0.0 min

Primary = 2.08 cfs @ 12.07 hrs, Volume= 6,912 cf Secondary = 2.05 cfs @ 12.08 hrs, Volume= 391 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3

Peak Elev= 279.08' @ 12.08 hrs

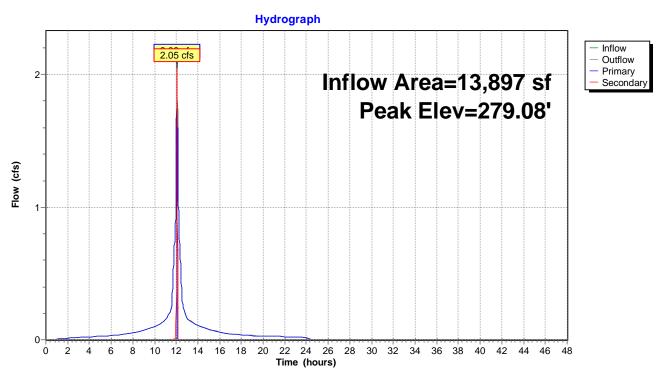
Flood Elev= 278.90'

Device	Routing	Invert	Outlet Devices
#1	Primary	275.90'	12.0" Round RCP_Round 12"
	•		L= 15.0' RCP, groove end projecting, Ke= 0.200
			Inlet / Outlet Invert= 275.90' / 275.83' S= 0.0047 '/' Cc= 0.900
			n= 0.025 Corrugated metal, Flow Area= 0.79 sf
#2	Secondary	278.90'	<b>24.0" x 24.0" Horiz. CB Grate</b> C= 0.600
	-		Limited to weir flow at low heads

**Primary OutFlow** Max=0.00 cfs @ 12.07 hrs HW=278.54' TW=279.01' (Dynamic Tailwater) **1=RCP\_Round 12"** (Controls 0.00 cfs)

Secondary OutFlow Max=1.55 cfs @ 12.08 hrs HW=279.05' (Free Discharge) —2=CB Grate (Weir Controls 1.55 cfs @ 1.27 fps)

### Pond CB#1: PR-CB #1



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## **Summary for Pond CB#2: PR-CB#2**

Inflow Area = 9,747 sf,100.00% Impervious, Inflow Depth = 6.15" for 25-yr event

Inflow = 1.45 cfs @ 12.07 hrs, Volume= 4,997 cf

Outflow = 1.45 cfs @ 12.07 hrs, Volume= 4,997 cf, Atten= 0%, Lag= 0.0 min

Primary = 1.45 cfs @ 12.07 hrs, Volume= 4,995 cf Secondary = 1.45 cfs @ 12.07 hrs, Volume= 370 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3

Peak Elev= 278.91' @ 12.06 hrs

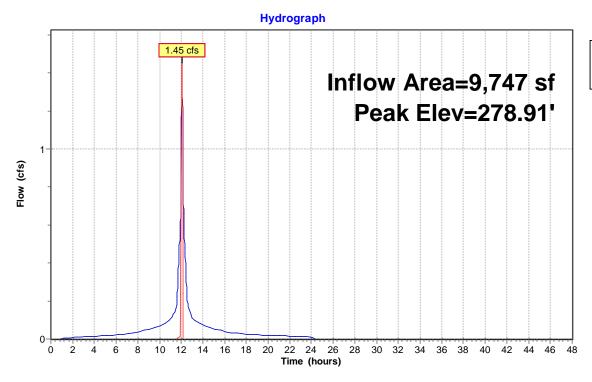
Flood Elev= 278.90'

Device	Routing	Invert	Outlet Devices	
#1	Primary	275.90'	12.0" Round RCP_Round 12"	
	-		L= 25.0' CMP, projecting, no headwall, Ke= 0.900	
			Inlet / Outlet Invert= 275.90' / 275.75' S= 0.0060 '/' Cc= 0.900	
			n= 0.025 Corrugated metal, Flow Area= 0.79 sf	
#2	Secondary	/ 278.90'	<b>24.0" x 24.0" Horiz. CB Grate</b> C= 0.600	

**Primary OutFlow** Max=0.00 cfs @ 12.07 hrs HW=278.43' TW=279.08' (Dynamic Tailwater) **1=RCP\_Round 12"** (Controls 0.00 cfs)

Secondary OutFlow Max= $0.00 \text{ cfs} \ @ 12.07 \text{ hrs} \ HW=278.43'$  (Free Discharge) -2=CB Grate (Controls 0.00 cfs)

#### Pond CB#2: PR-CB#2





### **Proposed - Constr Rev-MODIFIED**

Type III 24-hr 25-yr Rainfall=6.39" Printed 2/9/2023

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# **Summary for Pond DMH: DMH #1**

Inflow Area = 23,644 sf,100.00% Impervious, Inflow Depth = 6.04" for 25-yr event

Inflow = 3.54 cfs @ 12.07 hrs. Volume= 11.907 cf

Outflow = 3.54 cfs @ 12.07 hrs, Volume= 11,907 cf, Atten= 0%, Lag= 0.0 min

Primary = 3.54 cfs @ 12.07 hrs, Volume= 11,907 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3

Peak Elev= 279.08' @ 12.09 hrs Flood Elev= 279.00'

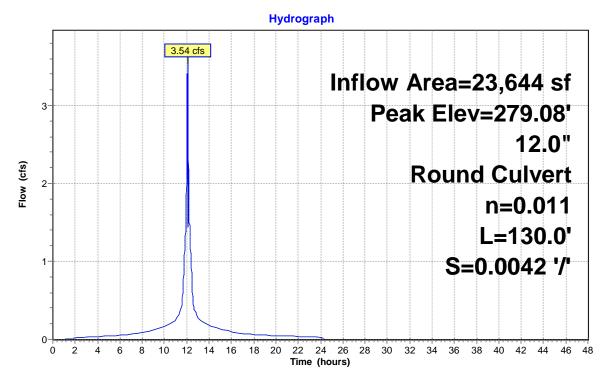
Device Routing Invert Outlet Devices

#1 Primary 275.75' **12.0" Round RCP\_Round 12"** 

L= 130.0' RCP, groove end projecting, Ke= 0.200 Inlet / Outlet Invert= 275.75' / 275.20' S= 0.0042 '/' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf

**Primary OutFlow** Max=3.40 cfs @ 12.07 hrs HW=279.01' TW=277.81' (Dynamic Tailwater) **1=RCP\_Round 12"** (Outlet Controls 3.40 cfs @ 4.33 fps)

#### Pond DMH: DMH #1





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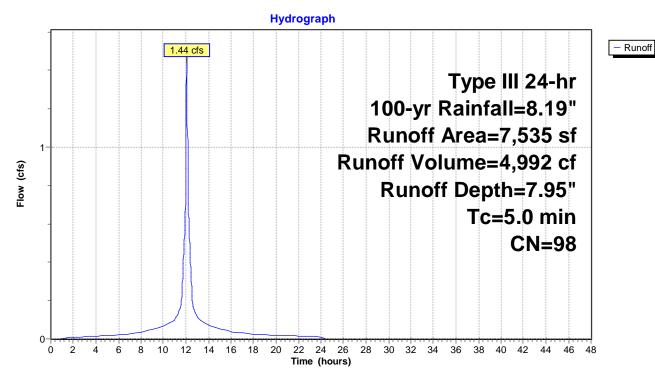
# Summary for Subcatchment CB-1A: CB-1A

Runoff = 1.44 cfs @ 12.07 hrs, Volume= 4,992 cf, Depth= 7.95"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 100-yr Rainfall=8.19"

	Α	rea (sf)	CN [	CN Description					
*		7,535	98 F	98 Paved roads w/curbs & sewers, HSG A					
		7,535	,	100.00% Impervious Area					
		Length		,	Capacity	Description			
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	5.0					Direct Entry,			

#### Subcatchment CB-1A: CB-1A



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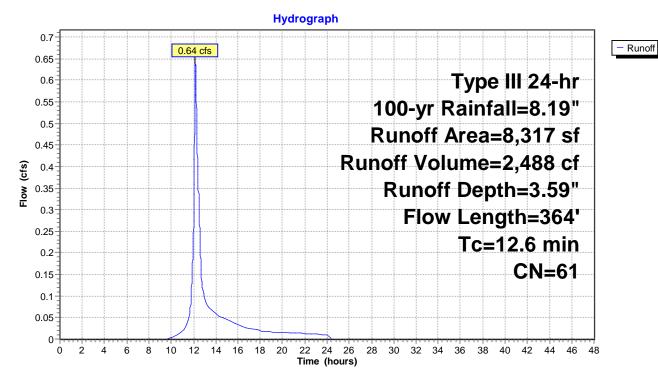
# Summary for Subcatchment CB-1B: CB-1B

Runoff = 0.64 cfs @ 12.18 hrs, Volume= 2,488 cf, Depth= 3.59"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 100-yr Rainfall=8.19"

	Α	rea (sf)	CN D	escription								
		8,317 61 1/4 acre lots, 38% imp, HSG A										
		5,157	6	62.00% Pervious Area								
		3,160	3	8.00% lmp	ervious Are	ea						
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description						
_	9.7	34	0.0153	0.06		Sheet Flow,						
	2.9	330	0.0090	1.93		Grass: Bermuda n= 0.410 P2= 3.60" <b>Shallow Concentrated Flow,</b> Paved Kv= 20.3 fps						
_	12 6	364	Total									

### Subcatchment CB-1B: CB-1B



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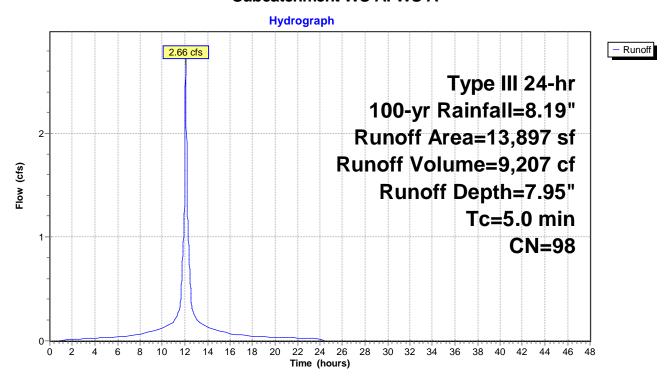
# Summary for Subcatchment WS-A: WS-A

Runoff 2.66 cfs @ 12.07 hrs, Volume= 9,207 cf, Depth= 7.95"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 100-yr Rainfall=8.19"

Area (sf)	CN	Description						
13,897	98	98 Paved roads w/curbs & sewers, HSG A						
13,897	13,897 100.00% Impervious Area							
Tc Length (min) (feet)	Slop (ft/f	•	Capacity (cfs)	Description				
5.0				Direct Entry, Sheet Flow				

### Subcatchment WS-A: WS-A



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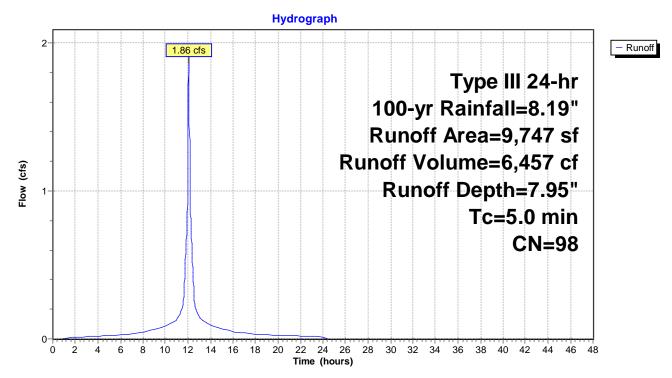
## Summary for Subcatchment WS-B: WS-B

Runoff = 1.86 cfs @ 12.07 hrs, Volume= 6,457 cf, Depth= 7.95"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs Type III 24-hr 100-yr Rainfall=8.19"

A	rea (sf)	CN [	Description						
	9,747	98 Paved roads w/curbs & sewers, HSG A							
	9,747	100.00% Impervious Area							
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
5.0					Direct Entry, Sheet Flow				

#### Subcatchment WS-B: WS-B



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# **Summary for Pond 2P: PR-CB-1**

Inflow Area =	15,852 sf, 67.47% Impervious,	Inflow Depth = 5.66" for 100-yr event
Inflow =	1.88 cfs @ 12.08 hrs, Volume=	7,480 cf
Outflow =	1.88 cfs @ 12.08 hrs, Volume=	7,480 cf, Atten= 0%, Lag= 0.0 min
Primary =	0.09 cfs @ 10.51 hrs, Volume=	1,658 cf
Secondary =	1.88 cfs @ 12.08 hrs, Volume=	5,822 cf
Tertiary =	0.00 cfs @ 0.00 hrs, Volume=	0 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 276.95' @ 12.08 hrs

Flood Elev= 280.40'

Device	Routing	Invert	Outlet Devices
#1	Primary	276.20'	12.0" Round Culvert
	•		L= 155.0' RCP, groove end projecting, Ke= 0.200
			Inlet / Outlet Invert= 276.20' / 275.00' S= 0.0077 '/' Cc= 0.900
			n= 0.013, Flow Area= 0.79 sf
#2	Tertiary	280.40'	<b>24.0" x 24.0" Horiz. CB Grate</b> C= 0.600
			Limited to weir flow at low heads
#3	Secondary	276.20'	12.0" Round Culvert
			L= 37.4' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 276.20' / 275.00' S= 0.0321 '/' Cc= 0.900
			n= 0.013, Flow Area= 0.79 sf
#4	Device 3	276.42'	<b>4.0' long Sharp-Crested Rectangular Weir</b> 2 End Contraction(s)

**Primary OutFlow** Max=0.09 cfs @ 10.51 hrs HW=276.42' TW=276.09' (Dynamic Tailwater) **1=Culvert** (Outlet Controls 0.09 cfs @ 1.10 fps)

Secondary OutFlow Max=1.87 cfs @ 12.08 hrs HW=276.95' (Free Discharge)

3=Culvert (Inlet Controls 1.87 cfs @ 2.95 fps)

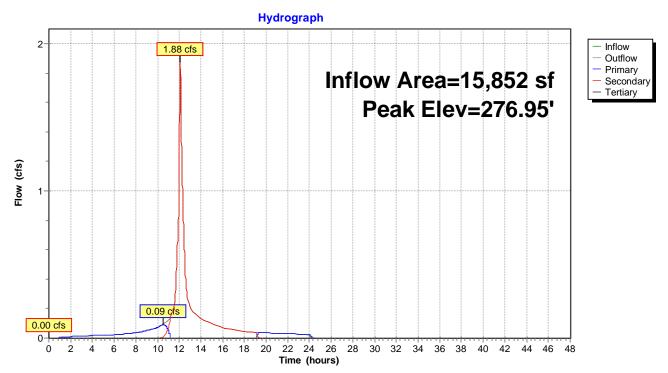
4=Sharp-Crested Rectangular Weir (Passes 1.87 cfs of 4.95 cfs potential flow)

**Tertiary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=276.20' (Free Discharge) **2=CB Grate** (Controls 0.00 cfs)

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# Pond 2P: PR-CB-1



Type III 24-hr 100-yr Rainfall=8.19" Printed 2/9/2023

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**Summary for Pond B-1: Basin #1** 

Inflow Area = 39,496 sf, 86.94% Impervious, Inflow Depth = 4.76" for 100-yr event

Inflow = 4.52 cfs @ 12.07 hrs, Volume= 15,673 cf

Outflow = 0.42 cfs @ 12.30 hrs, Volume= 15,673 cf, Atten= 91%, Lag= 13.9 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 278.94' @ 12.30 hrs Surf.Area= 2,218 sf Storage= 5,331 cf

Flood Elev= 285.00' Surf.Area= 2,737 sf Storage= 7,952 cf

Plug-Flow detention time= 116.8 min calculated for 15,669 cf (100% of inflow)

Center-of-Mass det. time= 116.8 min (856.6 - 739.8)

Volume	Invert	Avail.Sto	rage Storage	e Description					
#1	275.00'	7,95	2 cf Basin Storage (Prismatic) Listed below (Recalc)						
Elevatio		rf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)					
275.0	•	589	0	0					
276.0	00	934	762	762					
277.0	00	1,333	1,134	1,895					
278.0	00	1,777	1,555	3,450					
279.0	00	2,245	2,011	5,461					
280.0	00	2,737	2,491	7,952					
Device	Routing	Invert	Outlet Device	es					
#1	Discarded	275.00'	8.270 in/hr E	xfiltration over	Surface area Phase-In= 0.01'				
#2	Primary	279.50'	_		pad-Crested Rectangular Weir				
			` ,		0.80 1.00 1.20 1.40 1.60 1.80 2.00				
				.50 4.00 4.50 5					
			, ,	,	70 2.68 2.68 2.66 2.65 2.65 2.65 2.65				
			2.67 2.66 2.	.68 2.70 2.74 2	79 2.88				

**Discarded OutFlow** Max=0.42 cfs @ 12.30 hrs HW=278.94' (Free Discharge) —1=Exfiltration (Exfiltration Controls 0.42 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=275.00' (Free Discharge)

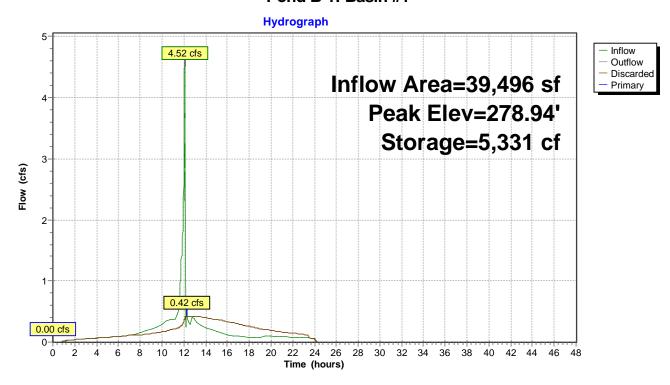
—2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Pond B-1: Basin #1



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# Summary for Pond CB#1: PR-CB #1

Inflow Area =	13,897 sf,100.00% Impervious,	Inflow Depth = 7.95" for 100-yr event
Inflow =	2.66 cfs @ 12.07 hrs, Volume=	9,207 cf
Outflow =	2.66 cfs @ 12.07 hrs, Volume=	9,207 cf, Atten= 0%, Lag= 0.0 min
Primary =	2.66 cfs @ 12.07 hrs, Volume=	8,497 cf
Secondary =	2.66 cfs @ 12.07 hrs, Volume=	1,993 cf

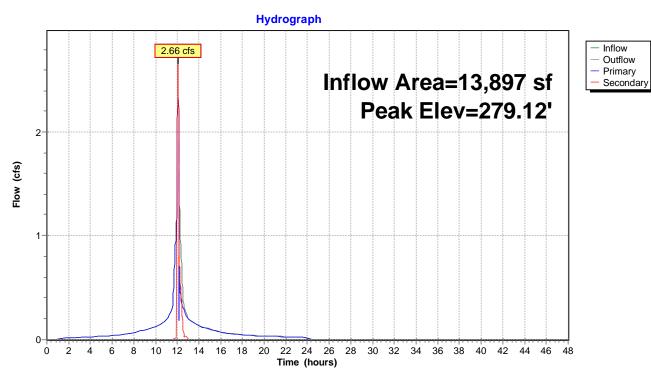
Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3 Peak Elev= 279.12' @ 12.07 hrs Flood Elev= 278.90'

Device	Routing	Invert	Outlet Devices
#1	Primary	275.90'	12.0" Round RCP_Round 12"
	•		L= 15.0' RCP, groove end projecting, Ke= 0.200
			Inlet / Outlet Invert= 275.90' / 275.83' S= 0.0047 '/' Cc= 0.900
			n= 0.025 Corrugated metal, Flow Area= 0.79 sf
#2	Secondary	278.90'	<b>24.0" x 24.0" Horiz. CB Grate</b> C= 0.600
	-		Limited to weir flow at low heads

**Primary OutFlow** Max=0.00 cfs @ 12.07 hrs HW=279.12' TW=280.53' (Dynamic Tailwater) **1=RCP\_Round** 12" (Controls 0.00 cfs)

Secondary OutFlow Max=2.66 cfs @ 12.07 hrs HW=279.12' (Free Discharge) —2=CB Grate (Weir Controls 2.66 cfs @ 1.53 fps)

### Pond CB#1: PR-CB #1



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- Inflow

Outflow Primary

Secondary

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## **Summary for Pond CB#2: PR-CB#2**

Inflow Area = 9,747 sf,100.00% Impervious, Inflow Depth = 7.95" for 100-yr event

Inflow = 1.86 cfs @ 12.07 hrs, Volume= 6,457 cf

Outflow = 1.86 cfs @ 12.07 hrs, Volume= 6,457 cf, Atten= 0%, Lag= 0.0 min

Primary = 1.86 cfs @ 12.07 hrs, Volume= 5,517 cf Secondary = 1.86 cfs @ 12.07 hrs, Volume= 2,019 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3

Peak Elev= 278.91' @ 12.07 hrs

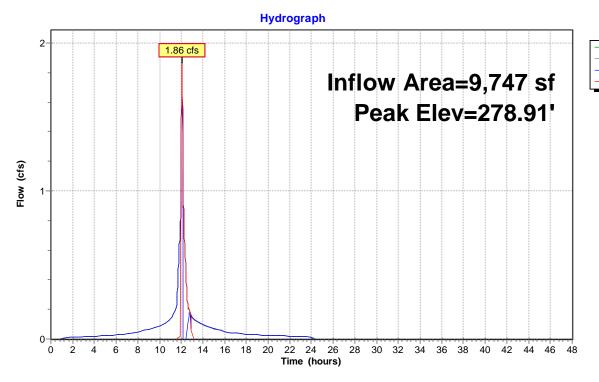
Flood Elev= 278.90'

Device	Routing	Invert	Outlet Devices
#1	Primary	275.90'	12.0" Round RCP_Round 12"
	-		L= 25.0' CMP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 275.90' / 275.75' S= 0.0060 '/' Cc= 0.900
			n= 0.025 Corrugated metal, Flow Area= 0.79 sf
#2	Secondary	/ 278.90'	<b>24.0" x 24.0" Horiz. CB Grate</b> C= 0.600

**Primary OutFlow** Max=0.00 cfs @ 12.07 hrs HW=278.91' TW=280.53' (Dynamic Tailwater) **1=RCP\_Round 12"** (Controls 0.00 cfs)

Secondary OutFlow Max=1.86 cfs @ 12.07 hrs HW=278.91' (Free Discharge) 2=CB Grate (Orifice Controls 1.86 cfs @ 0.47 fps)

#### Pond CB#2: PR-CB#2



## **Proposed - Constr Rev-MODIFIED**

Type III 24-hr 100-yr Rainfall=8.19" Printed 2/9/2023

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# **Summary for Pond DMH: DMH #1**

Inflow Area = 23,644 sf,100.00% Impervious, Inflow Depth = 7.11" for 100-yr event

Inflow = 4.52 cfs @ 12.07 hrs. Volume= 14.014 cf

Outflow = 4.52 cfs @ 12.07 hrs, Volume= 14,014 cf, Atten= 0%, Lag= 0.0 min

Primary = 4.52 cfs @ 12.07 hrs, Volume= 14,014 cf

Routing by Dyn-Stor-Ind method, Time Span= 0.00-48.00 hrs, dt= 0.01 hrs / 3

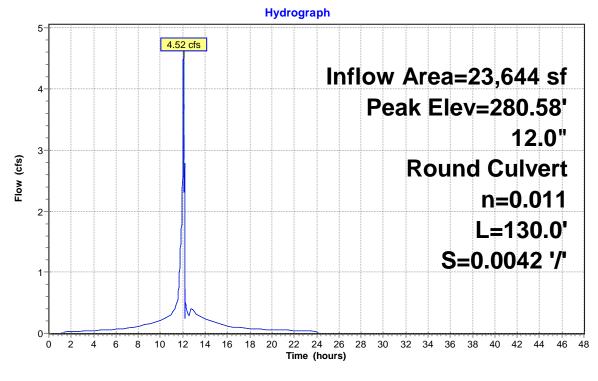
Peak Elev= 280.58' @ 12.08 hrs

Flood Elev= 279.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	275.75'	12.0" Round RCP_Round 12"
	-		L= 130.0' RCP, groove end projecting, Ke= 0.200
			Inlet / Outlet Invert= 275.75' / 275.20' S= 0.0042 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.79 sf

**Primary OutFlow** Max=4.52 cfs @ 12.07 hrs HW=280.53' TW=278.41' (Dynamic Tailwater) **1=RCP\_Round** 12" (Outlet Controls 4.52 cfs @ 5.76 fps)

### Pond DMH: DMH #1





```
Autodesk® Storm and Sanitary Analysis 2016 - Version 13.2.165 (Build 0)
Project Description
******
File Name ..... Grove_St_Ph2_r1-EX.SPF
******
Analysis Options
******
Flow Units ..... cfs
Subbasin Hydrograph Method. Rational
Time of Concentration..... SCS TR-55
Return Period..... 2 years
Link Routing Method ..... Kinematic Wave Storage Node Exfiltration. None
Starting Date ..... DEC-20-2022 00:00:00
Ending Date ..... DEC-21-2022 00:00:00
Report Time Step ...... 00:00:10
******
Element Count
Number of subbasins ..... 11
Number of nodes ..... 21
Number of links ..... 14
******
Subbasin Summary
******
Subbasin
                      Total
                       Area
TD
                       acres
                    0.36
0.33
Sub-CB-1
Sub-CB-10-11
                      1.61
0.69
Sub-CB-12-14
Sub-CB-15-17
                      0.95
Sub-CB-18-19
                       1.49
3.91
Sub-CB-20
Sub-CB-2-5
Sub-CB-6
                      0.14
Sub-CB-7
                       0.11
Sub-CB-8W
                       0.22
Sub-CB-9
                       0.15
*****
Node Summary
*****
                  Node
ID
CIT-8 JUNCTION 254.80 259.42 0.00 DH-10 JUNCTION 265.15 268.15 0.00 DH-13 JUNCTION 259.80 265.60 0.00 CINCTION 277.62 279.12 0.00
______
CIT-8
DH-10
DH-13
JUNCTION
DH-20
EX-18
JUNCTION
JUNCTION
JUNCTION
JUNCTION
JUNCTION
JUNCTION
JUNCTION
                                266.00 273.24 0.00
252.80 258.62 0.00
275.79 277.57 0.00
```

DP-1 DP-10 DP-13 DP-16 DP-18 DP-20 DP-5 DP-6 DP-7 Out-01		OUTFA	LL LL LL LL LL LL LL	264 259 252 264 274 248 246 252	5.00 4.78 9.60 2.66 4.36 4.20 8.00 6.50 2.60 1.22	276.00 265.78 260.60 252.66 265.86 275.70 248.00 246.50 253.60 281.50	0. 0. 0. 0. 0. 0. 0. 0.	00 00 00 00 00 00 00 00			
*********** Inlet Summ *****	ary										
Inlet		Inlet				Manufactur	er	I	nlet	Number	
Catchbasin			Ponded	Initia	al	Grate				_	
ID	D.		acturer		<b>a</b> 1	Part		L	ocation	of	
Invert	K.	im Ar	ea	Water	CTO	gging Number				Inlets	
Elevation	Eleva	ation		Elevation	n	Factor				1111000	
ft	ft	ft²		ft	9	8					
CB-1		FHWA	HEC-22	GENERIC		N/A		0:	n Grade	1	
278.10	281.2	22	_	278.10		0.00					
CB-18		FHWA	HEC-22	GENERIC		N/A		O:	n Sag	1	
269.61	273.7	72 10.	00	269.61		0.00					
EX-CB15		FHWA	HEC-22	GENERIC		N/A		O:	n Grade	1	
254.80	259.2		-	254.80		0.00					
EX-CB-16			HEC-22	GENERIC		N/A		O:	n Grade	1	
257.40	262.3	30	_	257.40		0.00					
********* Roadway an ******* Inlet ID	ıd Gutt	er Summar	У	Cross Slope		Roadway anning's oughness	Gutter Cross Slope ft/ft	Gutter Width ft	Depre	utter ssion in	
CB-1			0.0100	0.0200		0.0160	0.0620	2.00		2.00	
CB-18			-	0.0200		0.0160	0.0620	2.00		2.00	
EX-CB15			0.0100	0.0200		0.0160	0.0620	2.00		2.00	
EX-CB-16			0.0100	0.0200		0.0160	0.0620	2.00		2.00	
**************************************	ry										
Link ID		From Node		To Node		Element Type	1	Length ft	Slope %	Manning Roughnes	
CB-1_Overf		CB-1		Out-01		CHANNEL		241.8	0.2000	0.013	
CIT-9_Over	ilow	EX-CB-16		EX-CB15		CHANNEL		230.0	1.3478	0.013	
Link-17		EX-CB15		CIT-8		CONDUIT		8.9	0.2000	0.015	
Link-18	,	EX-CB15		DP-7		CHANNEL		220.5	2.9927	0.013	
Pipe - (21		CIT-8		EX-7		CONDUIT		196.9	1.0156	0.013	
Pipe - (22		EX-7		DP-7		CONDUIT		20.0	1.0000	0.013	
Pipe - (25		EX-CB-16		CIT-8		CONDUIT		219.0	1.1872	0.013	
Pipe - (33 Pipe - (44		DH-13 CB-18		DP-13 EX-18		CONDUIT		19.5 24.4	1.0000 2.4990	0.013	
Pipe - (44 Pipe - (45		EX-18		DP-18		CONDUIT CONDUIT		81.8	2.4990	0.013	
1150 (13	,	-41 10				00110011		01.0	2.0000	0.01	- 0

Pipe - (56) Pipe - (57) Pipe - (61) Pipe - (62)	DH-10 DH-20 CB-1 Structure		CONDUIT CONDUIT - (72)CONDUIT CONDUIT	55.! 79.8	6.1644 3 2.7583	0.0130 0.0150 0.0130 0.0130
********	*****					
Cross Section						
Link	Shape	Depth/	Width	No. of	Cross	Full Flow
Design ID		Diameter		Barrels	Sectional	Hydraulic
Flow					Area	Radius
Capacity		ft	ft		ft²	ft
cfs						
CB-1_Overflow 2.70	TRIANGULA	R 0.28	14.00	1	1.96	0.14
CIT-9_Overflow	TRIANGULA	R 0.28	14.00	1	1.96	0.14
7.01 Link-17	CIRCULAR	1.50	1.50	1	1.77	0.38
4.07 Link-18	TRIANGULA	R 0.28	14.00	1	1.96	0.14
10.44 Pipe - (21)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.59 Pipe - (22)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.56 Pipe - (25)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.88			1.00	1	0.79	0.25
Pipe - (33) 3.56	CIRCULAR	1.00				
Pipe - (44) 5.63	CIRCULAR	1.00	1.00	1	0.79	0.25
Pipe - (45) 14.86	CIRCULAR	1.50	1.50	1	1.77	0.38
Pipe - (56) 6.17	CIRCULAR	1.00	1.00	1	0.79	0.25
Pipe - (57) 22.60	CIRCULAR	1.50	1.50	1	1.77	0.38
Pipe - (61) 5.92	CIRCULAR	1.00	1.00	1	0.79	0.25
Pipe - (62) 3.56	CIRCULAR	1.00	1.00	1	0.79	0.25
**************************************	ry **					
Area:	_	010 0 0042	0 0076	0 0110		
0. 0. 0. 0. 0. 0.	0005 0.0 0170 0.0 0595 0.0 1312 0.1 2323 0.2 3604 0.3 4937 0.5 6269 0.6 7602 0.7	232 0.0305 715 0.0847 491 0.1682 561 0.2810 871 0.4137 203 0.5470 536 0.6802 868 0.8135	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668		
0.	8934 0.9	201 0.9467	0.9734	1.0000		

Hrad:					
Width:	0.0139 0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005	0.0278 0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995 0.9256	0.0418 0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.0557 0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.0696 0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754 1.0000
	0.0355 0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000	0.0711 0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000 1.0000	0.1066 0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000 1.0000	0.1422 0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000 1.0000	0.1777 0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000
Transect :	XS-L-Pipe -	(16)			
Hrad:	0.0005 0.0170 0.0595 0.1312 0.2323 0.3604 0.4937 0.6269 0.7602 0.8934	0.0019 0.0232 0.0715 0.1491 0.2561 0.3871 0.5203 0.6536 0.7868 0.9201	0.0043 0.0305 0.0847 0.1682 0.2810 0.4137 0.5470 0.6802 0.8135 0.9467	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401 0.9734	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668 1.0000
iii au	0.0139 0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005	0.0278 0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995 0.9256	0.0418 0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.0557 0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.0696 0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754
Width:	0.0355 0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000	0.0711 0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000	0.1066 0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000	0.1422 0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000	0.1777 0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000
Transect 2	XS-L-Pipe -	(18)			
Area:	0.0005 0.0170 0.0595 0.1312 0.2323 0.3604	0.0019 0.0232 0.0715 0.1491 0.2561 0.3871	0.0043 0.0305 0.0847 0.1682 0.2810 0.4137	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670

	0.4937 0.6269	0.5203 0.6536	0.5470 0.6802	0.5736 0.7069	0.6003 0.7335
	0.7602	0.7868	0.8135	0.8401	0.7333
	0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:					
	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835 0.1459	0.0963 0.1591	0.1080 0.1724	0.1202 0.1858	0.1329 0.1994
	0.2130	0.2267	0.2404	0.2542	0.2680
	0.2818	0.2957	0.3095	0.3238	0.3512
	0.3784	0.4055	0.4326	0.4595	0.4863
	0.5130 0.6448	0.5396 0.6708	0.5660 0.6968	0.5924 0.7226	0.6187 0.7483
	0.7740	0.7995	0.8249	0.8502	0.7403
	0.9005	0.9256	0.9505	0.9753	1.0000
Width:					
	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132 0.4283	0.2520 0.4724	0.2961 0.5164	0.3402 0.5605	0.3842
	0.6487	0.6927	0.7368	0.7809	0.8249
	0.8690	0.9131	0.9572	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000 1.0000	1.0000	1.0000 1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
Transect Area:	XS-L-Pipe -	(2)			
Area.	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312 0.2323	0.1491 0.2561	0.1682 0.2810	0.1884 0.3071	0.2098
	0.2323	0.3871	0.2810	0.4404	0.3336
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602 0.8934	0.7868 0.9201	0.8135 0.9467	0.8401 0.9734	0.8668
Hrad:	0.0934	0.9201	0.9467	0.9/34	1.0000
	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835	0.0963	0.1080	0.1202	0.1329
	0.1459	0.1591	0.1724	0.1858 0.2542	0.1994
	0.2130 0.2818	0.2267 0.2957	0.2404 0.3095	0.3238	0.2680 0.3512
	0.3784	0.4055	0.4326	0.4595	0.4863
	0.5130	0.5396	0.5660	0.5924	0.6187
	0.6448	0.6708	0.6968	0.7226	0.7483
	0.7740 0.9005	0.7995 0.9256	0.8249 0.9505	0.8502 0.9753	0.8754 1.0000
Width:	0.7003	0.7250	0.7505	0.7755	2.0000
	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132	0.2520	0.2961	0.3402	0.3842
	0.4283 0.6487	0.4724 0.6927	0.5164 0.7368	0.5605 0.7809	0.6046 0.8249
	0.8690	0.0327	0.9572	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000 1.0000	1.0000	1.0000 1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	XS-L-Pipe -	(24)			
Area:	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487

w	0.0595 0.1312 0.2323 0.3604 0.4937 0.6269 0.7602 0.8934	0.0715 0.1491 0.2561 0.3871 0.5203 0.6536 0.7868 0.9201	0.0847 0.1682 0.2810 0.4137 0.5470 0.6802 0.8135 0.9467	0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401 0.9734	0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668 1.0000
<pre>Hrad:</pre> <pre>Width:</pre>	0.0139 0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005	0.0278 0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995	0.0418 0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.0557 0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.0696 0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754
	0.0355 0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000	0.0711 0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000 1.0000	0.1066 0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000	0.1422 0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000	0.1777 0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000
Transect XS Area:	-L-Pipe -	(27)			
Hrad:	0.0005 0.0170 0.0595 0.1312 0.2323 0.3604 0.4937 0.6269 0.7602 0.8934	0.0019 0.0232 0.0715 0.1491 0.2561 0.3871 0.5203 0.6536 0.7868 0.9201	0.0043 0.0305 0.0847 0.1682 0.2810 0.4137 0.5470 0.6802 0.8135 0.9467	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401 0.9734	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668 1.0000
	0.0139 0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005	0.0278 0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995 0.9256	0.0418 0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.0557 0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.0696 0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754 1.0000
Width:	0.0355 0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000 1.0000	0.0711 0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000	0.1066 0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000	0.1422 0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000	0.1777 0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000

Transect :	XS-L-Pipe -	(28)			
Alea.	0.0005 0.0170 0.0595 0.1312 0.2323 0.3604 0.4937 0.6269 0.7602 0.8934	0.0019 0.0232 0.0715 0.1491 0.2561 0.3871 0.5203 0.6536 0.7868 0.9201	0.0043 0.0305 0.0847 0.1682 0.2810 0.4137 0.5470 0.6802 0.8135 0.9467	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401 0.9734	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668 1.0000
Hrad:	0.0551	0.5201	0.5107	0.5751	1.0000
	0.0139 0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005	0.0278 0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995 0.9256	0.0418 0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.0557 0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.0696 0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754 1.0000
Width:	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000	0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000 1.0000	0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000 1.0000	0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000	0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000 1.0000
	XS-L-Pipe -	(30)			
Area:	0.0005 0.0170 0.0595 0.1312 0.2323 0.3604 0.4937 0.6269 0.7602 0.8934	0.0019 0.0232 0.0715 0.1491 0.2561 0.3871 0.5203 0.6536 0.7868 0.9201	0.0043 0.0305 0.0847 0.1682 0.2810 0.4137 0.5470 0.6802 0.8135 0.9467	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401 0.9734	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668 1.0000
Hrad:					
Width:	0.0139 0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005	0.0278 0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995 0.9256	0.0418 0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.0557 0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.0696 0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754 1.0000
	0.0355 0.2132 0.4283 0.6487 0.8690 1.0000	0.0711 0.2520 0.4724 0.6927 0.9131 1.0000	0.1066 0.2961 0.5164 0.7368 0.9572 1.0000	0.1422 0.3402 0.5605 0.7809 1.0000 1.0000	0.1777 0.3842 0.6046 0.8249 1.0000 1.0000

1.0000	1.0000	1.0000	1.0000	1.0000
1.0000	1.0000	1.0000	1.0000	1.0000
1.0000	1.0000	1.0000	1.0000	1.0000
1.0000	1.0000	1.0000	1.0000	1.0000
Twomagat VC I Ding	(27)			
Transect XS-L-Pipe	- (37)			
Area:	0 0010	0 0040	0 0000	0 0110
0.0005	0.0019	0.0043	0.0076	0.0118
0.0170	0.0232	0.0305	0.0390	0.0487
0.0595	0.0715	0.0847	0.0990	0.1145
0.1312	0.1491	0.1682	0.1884	0.2098
0.2323	0.2561	0.2810	0.3071	0.3338
0.3604	0.3871	0.4137	0.4404	0.4670
0.4937	0.5203	0.5470	0.5736	0.6003
0.6269	0.6536	0.6802	0.7069	0.7335
0.7602	0.7868	0.8135	0.8401	0.8668
0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:				
0.0139	0.0278	0.0418	0.0557	0.0696
0.0835	0.0963	0.1080	0.1202	0.1329
0.1459	0.1591	0.1724	0.1858	0.1994
0.2130	0.2267	0.2404	0.2542	0.2680
0.2818	0.2957	0.3095	0.3238	0.3512
0.3784	0.4055	0.4326	0.4595	0.4863
0.5130	0.5396	0.5660	0.5924	0.6187
0.6448	0.6708	0.6968	0.7226	0.7483
0.7740	0.7995	0.8249	0.8502	0.8754
0.9005	0.9256	0.9505	0.9753	1.0000
Width:	0.5250	0.9505	0.5755	1.0000
0.0355	0.0711	0.1066	0.1422	0.1777
0.2132	0.2520	0.2961	0.3402	0.3842
0.4283	0.2320	0.5164	0.5605	0.6046
			0.7809	
0.6487	0.6927	0.7368		0.8249
0.8690	0.9131	0.9572	1.0000	1.0000
1.0000	1.0000	1.0000	1.0000	1.0000
1.0000	1.0000	1.0000	1.0000	1.0000
1.0000	1.0000	1.0000	1.0000	1.0000
1.0000	1.0000	1.0000	1.0000	1.0000
1.0000	1.0000	1.0000	1.0000	1.0000
Transect XS-L-Pipe	- (50)			
Area:				
0.0005	0.0019	0.0043	0.0076	0.0118
0.0170	0.0232	0.0305	0.0390	0.0487
0.0595	0.0715	0.0847	0.0990	0.1145
0.1312	0.1491	0.1682	0.1884	0.2098
0.2323	0.2561	0.2810	0.3071	0.3338
0.3604	0.3871	0.4137	0.4404	0.4670
0.4937	0.5203	0.5470	0.5736	0.6003
0.6269	0.6536	0.6802	0.7069	0.7335
0.7602	0.7868	0.8135	0.8401	0.8668
0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:				
0.0139	0.0278	0.0418	0.0557	0.0696
0.0835	0.0963	0.1080	0.1202	0.1329
0.1459	0.1591	0.1724	0.1858	0.1994
0.2130	0.2267	0.2404	0.2542	0.2680
0.2818	0.2957	0.3095	0.3238	0.3512
0.3784	0.4055	0.4326	0.4595	0.4863
0.5130	0.5396	0.5660	0.5924	0.6187
0.6448	0.6708	0.6968	0.7226	0.7483
0.7740	0.7995	0.8249	0.7220	0.7463
0.9005	0.7995	0.9505	0.8302	1.0000
Width:	0.3430	0.9303	0.9133	1.0000
0.0355	0 0711	0 1066	0.1422	0 1777
	0.0711	0.1066		0.1777
0.2132	0.2520	0.2961	0.3402	0.3842
0.4283	0.4724	0.5164	0.5605	0.6046

0.6487 0.8690 1.0000 1.0000 1.0000 1.0000	0.6927 0.9131 1.0000 1.0000 1.0000 1.0000	0.7368 0.9572 1.0000 1.0000 1.0000 1.0000	0.7809 1.0000 1.0000 1.0000 1.0000 1.0000	0.8249 1.0000 1.0000 1.0000 1.0000 1.0000
Transect XS-L-Pipe - Area:	(55)			
0.0005 0.0170 0.0595 0.1312 0.2323 0.3604 0.4937 0.6269 0.7602 0.8934	0.0019 0.0232 0.0715 0.1491 0.2561 0.3871 0.5203 0.6536 0.7868 0.9201	0.0043 0.0305 0.0847 0.1682 0.2810 0.4137 0.5470 0.6802 0.8135 0.9467	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401 0.9734	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668 1.0000
0.0139 0.0835 0.1459 0.2130	0.0278 0.0963 0.1591 0.2267	0.0418 0.1080 0.1724 0.2404	0.0557 0.1202 0.1858 0.2542	0.0696 0.1329 0.1994 0.2680
0.2818 0.3784 0.5130 0.6448 0.7740 0.9005	0.2957 0.4055 0.5396 0.6708 0.7995 0.9256	0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.2342 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.3512 0.4863 0.6187 0.7483 0.8754 1.0000
Width: 0.0355 0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000 1.0000 1.0000	0.0711 0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000	0.1066 0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000	0.1422 0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000 1.0000	0.1777 0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000
**************************************	inuity	Volume acre-ft	Depth inches	
Total Precipitation Continuity Error (%)		0.731 0.706	0.880	
**************************************	ity	Volume acre-ft	Volume Mgallons	
External Inflow External Outflow Initial Stored Volume Final Stored Volume Continuity Error (%)	e	0.000 0.215 0.000 0.000 -0.045	0.000 0.070 0.000 0.000	
**************************************	omputations	s Report		

Autodesk Storm and Sanitary Analysis

Subbasin Sub-CB-1			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.12 0.25 0.36	A (6%+) A (6%+)	0.79 0.29 0.45
Subbasin Sub-CB-10-11			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.17 0.16 0.33	A (6%+) A (6%+)	0.79 0.14 0.48
Subbasin Sub-CB-12-14			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.39 1.23 1.61	A (6%+) A (6%+)	0.79 0.14 0.30
Subbasin Sub-CB-15-17			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Streets, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.17 0.35 0.16 0.69	A (6%+) A (6%+) B (0-2%)	0.79 0.29 0.80 0.54
Subbasin Sub-CB-18-19			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.44 0.51 0.95	A (6%+) A (6%+)	0.79 0.29 0.52
Subbasin Sub-CB-20			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.45 1.05 1.49	A (6%+) A (6%+)	0.79 0.14 0.33
Subbasin Sub-CB-2-5			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.

Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.55 3.36 3.91	A (6%+) A (6%+)	0.79 0.14 0.23
Subbasin Sub-CB-6			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.09 0.05 0.14	A (2-6%) A (6%+)	0.77 0.29 0.59
Subbasin Sub-CB-7			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.08 0.03 0.11	A (0-2%) A (2-6%)	0.76 0.26 0.63
Subbasin Sub-CB-8W			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Meadow, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.16 0.06 0.22	A (2-6%) A (2-6%)	0.77 0.22 0.61
Subbasin Sub-CB-9			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.11 0.03 0.15	A (2-6%) A (2-6%)	0.77 0.26 0.65
**************************************			
Sheet Flow Equation			
$Tc = (0.007 * ((n * Lf)^0.8)) / ((P^0.5) * (S))$	Sf^0.4))		
Where:			
<pre>Tc = Time of Concentration (hrs) n = Manning's Roughness Lf = Flow Length (ft) P = 2 yr, 24 hr Rainfall (inches) Sf = Slope (ft/ft)</pre>			
Shallow Concentrated Flow Equation			
<pre>V = 16.1345 * (Sf^0.5) (unpaved surface)</pre>			

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V = 20.3282 * (Sf^0.5) (paved surface)
          V = 15.0 * (Sf^0.5) (grassed waterway surface)
          V = 10.0 * (Sf^0.5) (nearly bare & untilled surface)
            = 9.0 * (Sf^0.5) (cultivated straight rows surface)
          V = 7.0 * (Sf^0.5) (short grass pasture surface)
          V = 5.0 * (Sf^0.5) \text{ (woodland surface)}
          V = 2.5 * (Sf^0.5) (forest w/heavy litter surface)
          Tc = (Lf / V) / (3600 sec/hr)
          Where:
          Tc = Time of Concentration (hrs)
          Lf = Flow Length (ft)
          V = Velocity (ft/sec)
          Sf = Slope (ft/ft)
 Channel Flow Equation
          V = (1.49 * (R^{(2/3)}) * (Sf^{0.5})) / n
          R = Aq / Wp
          Tc = (Lf / V) / (3600 sec/hr)
          Where:
          Tc = Time of Concentration (hrs)
          Lf = Flow Length (ft)
          R = Hydraulic Radius (ft)
          Aq = Flow Area (ft<sup>2</sup>)
          Wp = Wetted Perimeter (ft)
          V = Velocity (ft/sec)
          Sf = Slope (ft/ft)
         n = Manning's Roughness
 Subbasin Sub-CB-1
 Sheet Flow Computations
                                                 Subarea A
                                                                     Subarea B
                                                                                          Subarea
         Manning's Roughness:
                                                      0.40
                                                                           0.00
0.00
          Flow Length (ft):
                                                     33.69
                                                                           0.00
0.00
         Slope (%):
                                                      1.60
                                                                           0.00
0.00
          2 yr, 24 hr Rainfall (in):
                                                                           0.00
                                                      3.60
0.00
                                                      0.06
                                                                           0.00
          Velocity (ft/sec):
0.00
          Computed Flow Time (minutes):
                                                      9.26
                                                                           0.00
0.00
 Shallow Concentrated Flow Computations
                                                                     Subarea B
                                                 Subarea A
                                                                                          Subarea
                                                                           0.00
          Flow Length (ft):
                                                    329.84
0.00
          Slope (%):
                                                      0.77
                                                                           0.00
0.00
         Surface Type:
                                                     Paved
                                                                         Paved
Paved
                                                                          0.00
         Velocity (ft/sec):
                                                     1.79
```

С

C

0.00		2 00	0.00	
0.00	Computed Flow Time (minutes):	3.08	0.00	
======				========
	Total TOC (minutes):	12.34		
======		:========:	===========	========
	in Sub-CB-10-11 			
	Flow Computations			
		Subarea A	Subarea B	Subarea
C	Manning's Roughness:	0.40	0.00	
0.00	Flow Length (ft):	82.40	0.00	
0.00	Slope (%):	22.88	0.00	
0.00	2 yr, 24 hr Rainfall (in):	3.60	0.00	
0.00	Velocity (ft/sec):	0.21	0.00	
0.00	Computed Flow Time (minutes):	6.54	0.00	
	w Concentrated Flow Computations			
		Subarea A	Subarea B	Subarea
С	Flow Length (ft):	332.66	0.00	
0.00	Slope (%):	2.02	0.00	
0.00	Surface Type:	Paved	Paved	
Paved	Velocity (ft/sec):	2.89	0.00	
0.00	Computed Flow Time (minutes):	1.92	0.00	
0.00				
======	Total TOC (minutes):	8.46	==========	========
======		:========:		========
	in Sub-CB-12-14			
sneet :	Flow Computations	Gulana a	Quihace a D	G 1
С	Manning La Doughnasa	Subarea A	Subarea B	Subarea
0.00	Manning's Roughness:	0.40	0.00	
0.00	Flow Length (ft):	222.41	0.00	
0.00	Slope (%):	10.60	0.00	

0.00	2 yr, 24 hr Rainfall (in):	3.60	0.00	
0.00	Velocity (ft/sec):	0.19	0.00	
0.00	Computed Flow Time (minutes):	19.69	0.00	
0.00				
	w Concentrated Flow Computations			
С		Subarea A	Subarea B	Subarea
0.00	Flow Length (ft):	430.84	0.00	
0.00	Slope (%):	3.53	0.00	
Paved	Surface Type:	Paved	Paved	
0.00	Velocity (ft/sec):	3.82	0.00	
0.00	Computed Flow Time (minutes):	1.88	0.00	
	Total TOC (minutes):	21.57		
======			=======================================	
Subbas	in Sub-CB-15-17			
	User-Defined TOC override (minutes):	5.00		
	in Sub-CB-18-19			
	User-Defined TOC override (minutes):	5.00		
	in Sub-CB-20			
Sheet	Flow Computations			
G		Subarea A	Subarea B	Subarea
C	Manning's Roughness:	0.40	0.00	
0.00	Flow Length (ft):	227.22	0.00	
0.00	Slope (%):	7.48	0.00	
0.00	2 yr, 24 hr Rainfall (in):	3.60	0.00	
0.00	Velocity (ft/sec):	0.16	0.00	
0.00	Computed Flow Time (minutes):	23.04	0.00	
0.00				
	w Concentrated Flow Computations			
С		Subarea A	Subarea B	Subarea
Ü	Flow Length (ft):	193.35	0.00	

0.00	Slope (%):	2.77	0.00	
0.00	Surface Type:	Paved	Paved	
Paved	Velocity (ft/sec):	3.38	0.00	
0.00	-			
0.00	Computed Flow Time (minutes):	0.95	0.00	
======	Total TOC (minutes):	======================================		
	iotal ioc (minutes).			
Subbasi	n Sub-CB-2-5			
	low Computations			
		Subarea A	Subarea B	Subarea
С	Manning's Roughness:	0.40	0.00	
0.00	Flow Length (ft):	526.06	0.00	
0.00	Slope (%):	1.65	0.00	
0.00	2 yr, 24 hr Rainfall (in):	3.60	0.00	
0.00	Velocity (ft/sec):	0.11	0.00	
0.00	Computed Flow Time (minutes):	82.52	0.00	
	Concentrated Flow Computations			
		Subarea A	Subarea B	Subarea
C	Flow Length (ft):	591.37	0.00	
0.00	Slope (%):	2.70	0.00	
0.00	Surface Type:	Unpaved	Paved	
Paved	Velocity (ft/sec):	2.65	0.00	
0.00	Computed Flow Time (minutes):	3.72	0.00	
0.00				
=======	Total TOC (minutes):	86.24		
======				
	n Sub-CB-6			
	User-Defined TOC override (minutes):	5.00		
	.n Sub-CB-7			

\_\_\_\_\_

User-Defined TOC override (minutes): 5.00

Subbasin Sub-CB-8W

User-Defined TOC override (minutes): 5.00

Subbasin Sub-CB-9

User-Defined TOC override (minutes): 5.00

Subbasin ID	Accumulated Precip in	Rainfall Intensity in/hr	Total Runoff in	Peak Runoff cfs	Weighted Runoff Coeff	Conc days	Time of entration hh:mm:ss
Sub-CB-1	0.60	2.92	0.27	0.48	0.450	0	00:12:20
Sub-CB-10-11	0.51	3.57	0.24	0.56	0.480	0	00:08:27
Sub-CB-12-14	0.77	2.16	0.23	1.04	0.300	0	00:21:34
Sub-CB-15-17	0.39	4.72	0.21	1.76	0.540	0	00:05:00
Sub-CB-18-19	0.39	4.72	0.20	2.33	0.520	0	00:05:00
Sub-CB-20	0.81	2.03	0.27	1.00	0.330	0	00:23:59
Sub-CB-2-5	1.29	0.90	0.30	0.81	0.230	0	01:26:14
Sub-CB-6	0.39	4.72	0.23	0.40	0.590	0	00:05:00
Sub-CB-7	0.39	4.72	0.25	0.32	0.630	0	00:05:00
Sub-CB-8W	0.39	4.72	0.24	0.63	0.610	0	00:05:00
Sub-CB-9	0.39	4.72	0.26	0.45	0.650	0	00:05:00

Node ID	Average Depth Attained	Maximum Depth Attained	Maximum HGL Attained		of Max urrence	Total Flooded Volume	Total Time Flooded	Retention Time
	ft	ft	ft	days	hh:mm	acre-in	minutes	hh:mm:ss
CIT-8	0.00	0.36	255.16	0	00:05	0	0	0:00:00
DH-10	0.00	0.20	265.35	0	00:08	0	0	0:00:00
DH-13	0.01	0.37	260.17	0	00:21	0	0	0:00:00
DH-20	0.00	0.21	277.83	0	00:24	0	0	0:00:00
EX-18	3.00	3.45	269.45	0	00:05	0	0	0:00:00
EX-7	0.00	0.36	253.16	0	00:06	0	0	0:00:00
Structure - (7	2) 0.11	0.30	276.09	0	00:12	0	0	0:00:00
DP-1	0.00	0.24	275.24	0	00:12	0	0	0:00:00
DP-10	0.00	0.20	264.98	0	00:08	0	0	0:00:00
DP-13	0.01	0.37	259.97	0	00:21	0	0	0:00:00
DP-16	0.00	0.00	252.66	0	00:00	0	0	0:00:00
DP-18	0.01	0.40	264.76	0	00:05	0	0	0:00:00
DP-20	0.00	0.21	274.41	0	00:24	0	0	0:00:00
DP-5	0.00	0.00	248.00	0	00:00	0	0	0:00:00
DP-6	0.00	0.00	246.50	0	00:00	0	0	0:00:00
DP-7	0.00	0.36	252.96	0	00:06	0	0	0:00:00
Out-01	0.00	0.04	281.26	0	00:18	0	0	0:00:00

Node ID	Element Type	Maximum Lateral	Peak Inflow	Peak	Time of Inflow	Maxim	um Time ng F	of Peak Flooding
		Inflow cfs	cfs					
 CIT-8	JUNCTION		1.00					
DH-10	JUNCTION	0.56	0.56	0	00:08	0.		
DH-13	JUNCTION	1 04	0.56 1.04 1.00 2.32	0	00:00	0.		
DH-20	JUNCTION	1.01	1 00	0	00.21	0.		
EX-18		0.00	2.00	0	00.24	0.		
	JUNCTION	0.00	2.32	0	00.05	0.		
EX-7	JUNCTION	0.00	0.97	0	00.00	0.		
Structure - (72)		0.00	0.45	0	00.12	0.		
DP-1	OUTFALL	0.00	0.45	0	00:12	0.		
DP-10	OUTFALL	0.00	0.97 0.45 0.45 0.56	Û	00:08	0.		
DP-13	OUTFALL	0.00	1.04	0	00:21	0.		
DP-16	OUTFALL	1.76	1.76	0	00:05	0.		
DP-18	OUTFALL	0.00	1.04 1.76 2.30 1.00	0	00:05	0.		
DP-20	OUTFALL	0.00	1.00	0	00:24	0.		
DP-5	OUTFALL	0.81	0.81	0	01:26	0.		
DP-6	OUTFALL	0.81 0.40 0.32 0.00	0.40	0	00:05	0.		
DP-7	OUTFALL	0.32	1.24	0	00:05	0.		
Out-01	OUTFALL	0.00	0.02	0	00:18	0.	00	
**************************************	сy							
*****	* *							
******								
******								
******								
******								
**************************************	Max Gutter Spread during Peak Flow	Max Gut Water I du Peak I	ter Elev ring Flow	Max G Water c Peak	Sutter Depth Suring	T M Occu	ime of aximum Depth rrence	
**************************************	Max Gutter Spread during Peak Flow ft	Max Gut Water I du Peak I	tter Elev ring Flow ft	Max G Water c Peak	Gutter Depth during Flow ft	T M Occu days	ime of aximum Depth rrence hh:mm	
**************************************	Max Gutter Spread during Peak Flow	Max Gut Water I du Peak I	tter Elev ring Flow ft	Max G Water c Peak	Gutter Depth during Flow ft	T M Occu days	ime of aximum Depth rrence hh:mm	
**************************************	Max Gutter Spread during Peak Flow ft 4.02 9.44 0.79	Max Gut Water I du Peak I	tter Elev ring Flow ft	Max G Water c Peak	Gutter Depth during Flow ft	T M Occu days	ime of aximum Depth rrence hh:mm	
**************************************	Max Gutter Spread during Peak Flow ft 4.02 9.44	Max Gut Water I du Peak I28: 27: 25:	tter Elev ring Flow ft	Max G Water c Peak	Gutter Depth during Flow ft	T M Occu	ime of aximum Depth rrence hh:mm	
**************************************	Max Gutter Spread during Peak Flow ft 4.02 9.44 0.79 3.88	Max Gut Water I du Peak I	tter Elev ring Flow ft	Max G Water c Peak	Gutter Depth during Flow ft	T M Occu days	ime of aximum Depth rrence hh:mm	
**************************************	Max Gutter Spread during Peak Flow ft 4.02 9.44 0.79 3.88	Max Gut Water I du Peak I	tter Elev ring Flow ft	Max G Water c Peak	Gutter Depth during Flow ft	T M Occu days	ime of aximum Depth rrence hh:mm	
**************************************	Max Gutter Spread during Peak Flow ft 4.02 9.44 0.79 3.88	Max Gut Water I du Peak I	tter Elev ring Flow ft	Max G Water c Peak	Gutter Depth during Flow ft	T M Occu days	ime of aximum Depth rrence hh:mm	
**************************************	Max Gutter Spread during Peak Flow ft 4.02 9.44 0.79 3.88	Max Gut Water I du Peak I	tter Elev ring Flow ft	Max G Water c Peak	Gutter Depth during Flow ft	T M Occu days	ime of aximum Depth rrence hh:mm	
**************************************	Max Gutter Spread during Peak Flow ft 4.02 9.44 0.79 3.88	Max Gui Water I dui Peak I 28: 27: 25: 26:	tter Elev ring Flow ft 	Max G Water c Peak	Gutter Depth during Flow ft 0.16 0.29 0.05 0.16	Occu days  0 0 0	ime of aximum Depth rrence hh:mm 00:12 00:05 00:08 00:05	
**************************************	Max Gutter Spread during Peak Flow ft 4.02 9.44 0.79 3.88	Max Gui Water I dui Peak I 28: 27: 25: 26:	tter Elev ring Flow ft 	Max G Water c Peak	Gutter Depth during Flow ft 0.16 0.29 0.05 0.16	Occu days  0 0 0	ime of aximum Depth rrence hh:mm 00:12 00:05 00:08 00:05	
**************************************	Max Gutter Spread during Peak Flow ft  4.02 9.44 0.79 3.88	Max Gui Water I dui Peak I 28: 27: 25: 26:	ter Elev ring Flow ft 1.38 4.01 9.25 2.46	Max G Water G Peak	Gutter Depth during Flow ft 0.16 0.29 0.05 0.16	Occu days  0 0 0	ime of aximum Depth rrence hh:mm 00:12 00:05 00:05	
**************************************	Max Gutter Spread during Peak Flow ft  4.02 9.44 0.79 3.88	Max Gui Water I dun Peak I 28: 27/ 25: 26:	Eter Elev ring Flow ft 1.38 4.01 9.25 2.46	Max G Water C Peak	Gutter Depth during Flow ft 0.16 0.29 0.05 0.16	Occu days 0 0 0 0 0	ime of aximum Depth rrence hh: mm 00:12 00:05 00:08 00:05	Total
**************************************	Max Gutter Spread during Peak Flow ft  4.02 9.44 0.79 3.88	Max Gui Water I dui Peak I 28: 27: 25: 26: Peak	Eter Elev ring Flow ft 	Max G Water C Peak 	Sutter Depth Suring Flow ft 0.16 0.29 0.05 0.16	Occudays Occudays O O O O O O O O O O O O O O O O O O O	ime of aximum Depth rrence hh:mm 00:12 00:05 00:08 00:05	Total  Flooding
**************************************	Max Gutter Spread during Peak Flow ft  4.02 9.44 0.79 3.88	Max Gui Water I dui Peak I 28: 27: 25: 26: Peak	Eter Elev ring Flow ft 1.38 4.01 9.25 2.46	Max G Water C Peak 	Sutter Depth Suring Flow ft 0.16 0.29 0.05 0.16	Occudays Occudays O O O O O O O O O O O O O O O O O O O	ime of aximum Depth rrence hh: mm 00:12 00:05 00:08 00:05	Total  Flooding
**************************************	Max Gutter Spread during Peak Flow ft  4.02 9.44 0.79 3.88	Max Gui Water I dui Peak I 28: 27: 25: 26: Peak	Eter Elev ring Flow ft 1.38 4.01 9.25 2.46  Fintercep by In	Max G Water  Peak  Peak  Peak  Peak  Peak	Sutter Depth during Flow ft 0.16 0.29 0.05 0.16	Occudays Occudays O O O O O O O O O O O O O O O O O O O	ime of aximum Depth rrence hh:mm 00:12 00:05 00:08 00:05	Total

_						
CB-1 0	0.48	0.48	0.46	0.02	95.36	0.000
CB-18	2.33	2.33	-	-	-	0.000
EX-CB15	0.02	0.00	0.02	0.00	100.00	0.000
EX-CB-16	0.45	0.45	0.43	0.02	96.00	0.000

Outfall Node ID	Flow Frequency (%)	Average Flow cfs	Peak Inflow cfs
DP-1 DP-10 DP-13 DP-16 DP-18	1.89 1.19 3.00 0.69 0.87	0.20 0.28 0.52 0.88 0.92	0.45 0.56 1.04 1.76 2.30
DP-20 DP-5 DP-6 DP-7 Out-01	3.37 11.95 0.69 1.88 2.53	0.92 0.49 0.40 0.20 0.26 0.01	1.00 0.81 0.40 1.24 0.02
System	2.81	4.17	6.56

Link ID		Element	Т	ime of	Maximum	Length	Peak Flow	Design	Ratio of
Ratio of	То	tal Reported							
			Pea	k Flow	Velocity	Factor	during	Flow	Maximum
Maximum	Ti	me Condition	_						<i>i</i> = 1
T] Gb			Occu	rrence	Attained		Analysis	Capacity	/Design
Flow Surcharg	jea		darra	hh·mm	ft/sec		cfs	cfs	Flow
Depth minu	1+60		uays	1111 • 111111	It/sec		CIS	CIS	FIOW
Depen mino	iccs	•							
CB-1_Overflo	w	CHANNEL	0	00:18	1.53	1.00	0.02	2.70	0.01
0.15	0	Calculated							
CIT-9_Overfl		CHANNEL	0	00:08	3.14	1.00	0.02	7.01	0.00
0.10	0	Calculated							
Link-17		CONDUIT	0	00:08	0.56	1.00	0.02	4.07	0.00
0.05	0	Calculated	_						
Link-18		CHANNEL	0	00:12	0.00	1.00	0.00	10.44	0.00
0.03	0	Calculated	0	00.06	2 00	1 00	0.05	2 50	0 05
Pipe - (21)	0	CONDUIT	0	00:06	3.99	1.00	0.97	3.59	0.27
0.35	U	Calculated CONDUIT	0	00:06	3.87	1.00	0.97	3.56	0.27
Pipe - (22) 0.36	0	Conduit	U	00.06	3.87	1.00	0.97	3.50	0.27
Pipe - (25)	U	Calculated	0	00:05	6.24	1.00	0.41	3.88	0.10
0.22	Ο	Calculated	U	00.00	0.21	1.00	0.41	3.00	0.10
0.22	0	carcaracca							

Pipe - (33) 0.37	0	CONDUIT Calculated	0	00:21	3.94	1.00	1.04	3.56	0.29
Pipe - (44)		CONDUIT	0	00:05	6.84	1.00	2.32	5.63	0.41
0.45 Pipe - (45)	0	Calculated CONDUIT	0	00:05	6.15	1.00	2.30	14.86	0.15
0.27	0	Calculated							
Pipe - (56)		CONDUIT	0	00:08	4.88	1.00	0.56	6.17	0.09
0.20	0	Calculated							
Pipe - (57)		CONDUIT	0	00:24	6.46	1.00	1.00	22.60	0.04
0.14	0	Calculated							
Pipe - (61)		CONDUIT	0	00:12	5.10	1.00	0.45	5.92	0.08
0.19	0	Calculated							
Pipe - (62)		CONDUIT	0	00:12	3.13	1.00	0.45	3.56	0.13
0.24	0	Calculated							

All links are stable.

WARNING 108: Surcharge elevation defined for Junction EX-18 is below junction maximum elevation. Assumed surcharge elevation equal to maximum elevation.

WARNING 139 : Ponded area defined for on sag Inlet CB-18 is zero. Assumed ponded area equal to 10 ft $^2$  (0.929 m $^2$ ).

WARNING 138 : Initial water surface elevation defined for Inlet EX-CB15 is below catchbasin invert elevation.

Assumed initial water surface elevation equal to catchbasin inlet invert

elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB-1\_Overflow

is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CIT-9\_Overflow is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 117: Conduit outlet invert elevation defined for Conduit CB-1\_Overflow is below downstream node invert elevation.

Assumed conduit outlet invert elevation equal to downstream node invert

elevation.

WARNING 004 : Minimum elevation drop used for Conduit CB-1\_Overflow.

WARNING 005 : Minimum slope used for Conduit CB-1\_Overflow.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CIT-9\_Overflow is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet EX-CB15.

WARNING 116: Conduit inlet invert elevation defined for Conduit Link-17 is below upstream node invert elevation.

Assumed conduit inlet invert elevation equal to upstream node invert elevation.

WARNING 004: Minimum elevation drop used for Conduit Link-17.

WARNING 005 : Minimum slope used for Conduit Link-17.

Analysis began on: Tue Jan 31 10:57:26 2023 Analysis ended on: Tue Jan 31 10:57:27 2023

Total elapsed time: 00:00:01

```
Autodesk® Storm and Sanitary Analysis 2016 - Version 13.2.165 (Build 0)
Project Description
******
File Name ..... Grove_St_Ph2_r1-EX.SPF
******
Analysis Options
******
Flow Units ..... cfs
Subbasin Hydrograph Method. Rational
Time of Concentration..... SCS TR-55
Return Period...... 10 years
Link Routing Method ..... Kinematic Wave Storage Node Exfiltration. None
Starting Date ..... DEC-20-2022 00:00:00
Ending Date ..... DEC-21-2022 00:00:00
Report Time Step ...... 00:00:10
******
Element Count
Number of subbasins ..... 11
Number of nodes ..... 21
Number of links ..... 14
******
Subbasin Summary
******
Subbasin
                      Total
                       Area
TD
                       acres
                    0.36
0.33
Sub-CB-1
Sub-CB-10-11
                      1.61
0.69
Sub-CB-12-14
Sub-CB-15-17
                      0.95
Sub-CB-18-19
                       1.49
3.91
Sub-CB-20
Sub-CB-2-5
Sub-CB-6
                      0.14
Sub-CB-7
                       0.11
Sub-CB-8W
                       0.22
Sub-CB-9
                       0.15
*****
Node Summary
*****
                  Node
ID
CIT-8 JUNCTION 254.80 259.42 0.00 DH-10 JUNCTION 265.15 268.15 0.00 DH-13 JUNCTION 259.80 265.60 0.00 TUNCTION 277.62 279.12 0.00
______
CIT-8
DH-10
DH-13
JUNCTION
DH-20
EX-18
JUNCTION
JUNCTION
JUNCTION
JUNCTION
JUNCTION
JUNCTION
JUNCTION
                                266.00 273.24 0.00
252.80 258.62 0.00
275.79 277.57 0.00
```

DP-1 DP-10 DP-13 DP-16 DP-18 DP-20 DP-5 DP-6 DP-7 Out-01		OUTFA	LL LL LL LL LL LL LL	264 259 252 264 274 248 246 252	5.00 4.78 9.60 2.66 4.36 4.20 8.00 6.50 2.60 1.22	276.00 265.78 260.60 252.66 265.86 275.70 248.00 246.50 253.60 281.50	0. 0. 0. 0. 0. 0. 0. 0.	00 00 00 00 00 00 00 00			
*********** Inlet Summ *****	ary										
Inlet		Inlet				Manufactur	er	I	nlet	Number	
Catchbasin			Ponded	Initia	al	Grate				_	
ID	D.		acturer		<b>a</b> 1	Part		L	ocation	of	
Invert	K.	im Ar	ea	Water	CTO	gging Number				Inlets	
Elevation	Eleva	ation		Elevation	n	Factor				1111000	
ft	ft	ft²		ft	9	8					
CB-1		FHWA	HEC-22	GENERIC		N/A		0:	n Grade	1	
278.10	281.2	22	_	278.10		0.00					
CB-18		FHWA	HEC-22	GENERIC		N/A		O:	n Sag	1	
269.61	273.7	72 10.	00	269.61		0.00					
EX-CB15		FHWA	HEC-22	GENERIC		N/A		O:	n Grade	1	
254.80	259.2		-	254.80		0.00					
EX-CB-16			HEC-22	GENERIC		N/A		O:	n Grade	1	
257.40	262.3	30	_	257.40		0.00					
********* Roadway an ******* Inlet ID	ıd Gutt	er Summar	У	Cross Slope		Roadway anning's oughness	Gutter Cross Slope ft/ft	Gutter Width ft	Depre	utter ssion in	
CB-1			0.0100	0.0200		0.0160	0.0620	2.00		2.00	
CB-18			-	0.0200		0.0160	0.0620	2.00		2.00	
EX-CB15			0.0100	0.0200		0.0160	0.0620	2.00		2.00	
EX-CB-16			0.0100	0.0200		0.0160	0.0620	2.00		2.00	
**************************************	ry										
Link ID		From Node		To Node		Element Type	1	Length ft	Slope %	Manning Roughnes	
CB-1_Overf		CB-1		Out-01		CHANNEL		241.8	0.2000	0.013	
CIT-9_Over	ilow	EX-CB-16		EX-CB15		CHANNEL		230.0	1.3478	0.013	
Link-17		EX-CB15		CIT-8		CONDUIT		8.9	0.2000	0.015	
Link-18	,	EX-CB15		DP-7		CHANNEL		220.5	2.9927	0.013	
Pipe - (21		CIT-8		EX-7		CONDUIT		196.9	1.0156	0.013	
Pipe - (22		EX-7		DP-7		CONDUIT		20.0	1.0000	0.013	
Pipe - (25		EX-CB-16		CIT-8		CONDUIT		219.0	1.1872	0.013	
Pipe - (33 Pipe - (44		DH-13 CB-18		DP-13 EX-18		CONDUIT		19.5 24.4	1.0000 2.4990	0.013	
Pipe - (44 Pipe - (45		EX-18		DP-18		CONDUIT CONDUIT		81.8	2.4990	0.013	
1150 (13	,	-41 10				00110011		01.0	2.0000	0.01	- 0

Pipe - (56) Pipe - (57) Pipe - (61) Pipe - (62)	DH-10 DH-20 CB-1 Structure		CONDUIT CONDUIT - (72)CONDUIT CONDUIT	55.! 79.8	6.1644 3 2.7583	0.0130 0.0150 0.0130 0.0130
********	*****					
Cross Section						
Link	Shape	Depth/	Width	No. of	Cross	Full Flow
Design ID		Diameter		Barrels	Sectional	Hydraulic
Flow					Area	Radius
Capacity		ft	ft		ft²	ft
cfs						
CB-1_Overflow 2.70	TRIANGULA	R 0.28	14.00	1	1.96	0.14
CIT-9_Overflow	TRIANGULA	R 0.28	14.00	1	1.96	0.14
7.01 Link-17	CIRCULAR	1.50	1.50	1	1.77	0.38
4.07 Link-18	TRIANGULA	R 0.28	14.00	1	1.96	0.14
10.44 Pipe - (21)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.59 Pipe - (22)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.56 Pipe - (25)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.88			1.00	1	0.79	0.25
Pipe - (33) 3.56	CIRCULAR	1.00				
Pipe - (44) 5.63	CIRCULAR	1.00	1.00	1	0.79	0.25
Pipe - (45) 14.86	CIRCULAR	1.50	1.50	1	1.77	0.38
Pipe - (56) 6.17	CIRCULAR	1.00	1.00	1	0.79	0.25
Pipe - (57) 22.60	CIRCULAR	1.50	1.50	1	1.77	0.38
Pipe - (61) 5.92	CIRCULAR	1.00	1.00	1	0.79	0.25
Pipe - (62) 3.56	CIRCULAR	1.00	1.00	1	0.79	0.25
**************************************	ry **					
Area:	_	010 0 0042	0 0076	0 0110		
0. 0. 0. 0. 0. 0.	0005 0.0 0170 0.0 0595 0.0 1312 0.1 2323 0.2 3604 0.3 4937 0.5 6269 0.6 7602 0.7	232 0.0305 715 0.0847 491 0.1682 561 0.2810 871 0.4137 203 0.5470 536 0.6802 868 0.8135	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668		
0.	8934 0.9	201 0.9467	0.9734	1.0000		

Hrad:					
Width:	0.0139 0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005	0.0278 0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995 0.9256	0.0418 0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.0557 0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.0696 0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754 1.0000
	0.0355 0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000	0.0711 0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000 1.0000	0.1066 0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000 1.0000	0.1422 0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000 1.0000	0.1777 0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000
Transect :	XS-L-Pipe -	(16)			
Hrad:	0.0005 0.0170 0.0595 0.1312 0.2323 0.3604 0.4937 0.6269 0.7602 0.8934	0.0019 0.0232 0.0715 0.1491 0.2561 0.3871 0.5203 0.6536 0.7868 0.9201	0.0043 0.0305 0.0847 0.1682 0.2810 0.4137 0.5470 0.6802 0.8135 0.9467	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401 0.9734	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668 1.0000
iii au	0.0139 0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005	0.0278 0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995 0.9256	0.0418 0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.0557 0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.0696 0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754
Width:	0.0355 0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000	0.0711 0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000	0.1066 0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000	0.1422 0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000	0.1777 0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000
Transect 2	XS-L-Pipe -	(18)			
Area:	0.0005 0.0170 0.0595 0.1312 0.2323 0.3604	0.0019 0.0232 0.0715 0.1491 0.2561 0.3871	0.0043 0.0305 0.0847 0.1682 0.2810 0.4137	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670

	0.4937 0.6269	0.5203 0.6536	0.5470 0.6802	0.5736 0.7069	0.6003 0.7335
	0.7602	0.7868	0.8135	0.8401	0.7333
	0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:					
	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835 0.1459	0.0963 0.1591	0.1080 0.1724	0.1202 0.1858	0.1329 0.1994
	0.2130	0.2267	0.2404	0.2542	0.2680
	0.2818	0.2957	0.3095	0.3238	0.3512
	0.3784	0.4055	0.4326	0.4595	0.4863
	0.5130 0.6448	0.5396 0.6708	0.5660 0.6968	0.5924 0.7226	0.6187 0.7483
	0.7740	0.7995	0.8249	0.8502	0.7403
	0.9005	0.9256	0.9505	0.9753	1.0000
Width:					
	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132 0.4283	0.2520 0.4724	0.2961 0.5164	0.3402 0.5605	0.3842
	0.6487	0.6927	0.7368	0.7809	0.8249
	0.8690	0.9131	0.9572	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000 1.0000	1.0000	1.0000 1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
Transect Area:	XS-L-Pipe -	(2)			
AI Ca.	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312 0.2323	0.1491 0.2561	0.1682 0.2810	0.1884 0.3071	0.2098
	0.2323	0.3871	0.2810	0.4404	0.3336
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602 0.8934	0.7868 0.9201	0.8135 0.9467	0.8401 0.9734	0.8668
Hrad:	0.0934	0.9201	0.9467	0.9/34	1.0000
	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835	0.0963	0.1080	0.1202	0.1329
	0.1459	0.1591	0.1724	0.1858 0.2542	0.1994
	0.2130 0.2818	0.2267 0.2957	0.2404 0.3095	0.3238	0.2680 0.3512
	0.3784	0.4055	0.4326	0.4595	0.4863
	0.5130	0.5396	0.5660	0.5924	0.6187
	0.6448	0.6708	0.6968	0.7226	0.7483
	0.7740 0.9005	0.7995 0.9256	0.8249 0.9505	0.8502 0.9753	0.8754 1.0000
Width:	0.7003	0.7250	0.7505	0.7755	2.0000
	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132	0.2520	0.2961	0.3402	0.3842
	0.4283 0.6487	0.4724 0.6927	0.5164 0.7368	0.5605 0.7809	0.6046 0.8249
	0.8690	0.9131	0.9572	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000 1.0000	1.0000	1.0000 1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	XS-L-Pipe -	(24)			
Area:	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487

w	0.0595 0.1312 0.2323 0.3604 0.4937 0.6269 0.7602 0.8934	0.0715 0.1491 0.2561 0.3871 0.5203 0.6536 0.7868 0.9201	0.0847 0.1682 0.2810 0.4137 0.5470 0.6802 0.8135 0.9467	0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401 0.9734	0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668 1.0000
<pre>Hrad:</pre> <pre>Width:</pre>	0.0139 0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005	0.0278 0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995	0.0418 0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.0557 0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.0696 0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754
	0.0355 0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000	0.0711 0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000 1.0000	0.1066 0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000	0.1422 0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000 1.0000	0.1777 0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000
Transect XS Area:	-L-Pipe -	(27)			
Hrad:	0.0005 0.0170 0.0595 0.1312 0.2323 0.3604 0.4937 0.6269 0.7602 0.8934	0.0019 0.0232 0.0715 0.1491 0.2561 0.3871 0.5203 0.6536 0.7868 0.9201	0.0043 0.0305 0.0847 0.1682 0.2810 0.4137 0.5470 0.6802 0.8135 0.9467	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401 0.9734	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668 1.0000
	0.0139 0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005	0.0278 0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995 0.9256	0.0418 0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.0557 0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.0696 0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754 1.0000
Width:	0.0355 0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000 1.0000	0.0711 0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000	0.1066 0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000	0.1422 0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000	0.1777 0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000

Transect :	XS-L-Pipe -	(28)			
Alea	0.0005 0.0170 0.0595 0.1312 0.2323 0.3604 0.4937 0.6269 0.7602 0.8934	0.0019 0.0232 0.0715 0.1491 0.2561 0.3871 0.5203 0.6536 0.7868 0.9201	0.0043 0.0305 0.0847 0.1682 0.2810 0.4137 0.5470 0.6802 0.8135 0.9467	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401 0.9734	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668 1.0000
Hrad:	0.0551	0.5201	0.5107	0.5751	1.0000
	0.0139 0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005	0.0278 0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995 0.9256	0.0418 0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.0557 0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.0696 0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754 1.0000
Width:	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000	0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000 1.0000	0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000 1.0000	0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000	0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000 1.0000
	XS-L-Pipe -	(30)			
Area:	0.0005 0.0170 0.0595 0.1312 0.2323 0.3604 0.4937 0.6269 0.7602 0.8934	0.0019 0.0232 0.0715 0.1491 0.2561 0.3871 0.5203 0.6536 0.7868 0.9201	0.0043 0.0305 0.0847 0.1682 0.2810 0.4137 0.5470 0.6802 0.8135 0.9467	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401 0.9734	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668 1.0000
Hrad:					
Width:	0.0139 0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005	0.0278 0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995 0.9256	0.0418 0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.0557 0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.0696 0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754 1.0000
	0.0355 0.2132 0.4283 0.6487 0.8690 1.0000	0.0711 0.2520 0.4724 0.6927 0.9131 1.0000	0.1066 0.2961 0.5164 0.7368 0.9572 1.0000	0.1422 0.3402 0.5605 0.7809 1.0000 1.0000	0.1777 0.3842 0.6046 0.8249 1.0000 1.0000

1.000	1.0000	1.0000	1.0000	1.0000
1.0000		1.0000	1.0000	1.0000
1.0000		1.0000	1.0000	1.0000
1.0000	1.0000	1.0000	1.0000	1.0000
Twomacat VC I Din	. (27)			
Transect XS-L-Pipe	= - (3/)			
Area:	- 0.0010	0 0040	0 0000	0 0110
0.000!		0.0043	0.0076	0.0118
0.0170		0.0305	0.0390	0.0487
0.059		0.0847	0.0990	0.1145
0.131		0.1682	0.1884	0.2098
0.2323		0.2810	0.3071	0.3338
0.360		0.4137	0.4404	0.4670
0.493		0.5470	0.5736	0.6003
0.6269	0.6536	0.6802	0.7069	0.7335
0.760	2 0.7868	0.8135	0.8401	0.8668
0.893	4 0.9201	0.9467	0.9734	1.0000
Hrad:				
0.0139	9 0.0278	0.0418	0.0557	0.0696
0.083	0.0963	0.1080	0.1202	0.1329
0.1459	0.1591	0.1724	0.1858	0.1994
0.213	0.2267	0.2404	0.2542	0.2680
0.2818	0.2957	0.3095	0.3238	0.3512
0.378		0.4326	0.4595	0.4863
0.513		0.5660	0.5924	0.6187
0.644		0.6968	0.7226	0.7483
0.774		0.8249	0.8502	0.8754
0.900!		0.9505	0.9753	1.0000
Width:	0.5250	0.5505	0.5755	1.0000
0.035	0.0711	0.1066	0.1422	0.1777
0.033		0.2961	0.3402	0.3842
0.4283		0.5164	0.5605	0.6046
			0.7809	
0.648		0.7368		0.8249
0.8690		0.9572	1.0000	1.0000
1.0000		1.0000	1.0000	1.0000
1.0000		1.0000	1.0000	1.0000
1.0000		1.0000	1.0000	1.0000
1.0000		1.0000	1.0000	1.0000
1.0000	1.0000	1.0000	1.0000	1.0000
Transect XS-L-Pipe	e - (50)			
Area:				
0.000!	5 0.0019	0.0043	0.0076	0.0118
0.0170	0.0232	0.0305	0.0390	0.0487
0.059	5 0.0715	0.0847	0.0990	0.1145
0.131	2 0.1491	0.1682	0.1884	0.2098
0.232	3 0.2561	0.2810	0.3071	0.3338
0.360	4 0.3871	0.4137	0.4404	0.4670
0.493	7 0.5203	0.5470	0.5736	0.6003
0.6269	0.6536	0.6802	0.7069	0.7335
0.760	2 0.7868	0.8135	0.8401	0.8668
0.893	4 0.9201	0.9467	0.9734	1.0000
Hrad:				
0.013	0.0278	0.0418	0.0557	0.0696
0.083		0.1080	0.1202	0.1329
0.1459		0.1724	0.1858	0.1994
0.213		0.2404	0.2542	0.2680
0.2818		0.3095	0.3238	0.3512
0.378		0.4326	0.4595	0.4863
0.576		0.4320	0.5924	0.4003
0.6448		0.6968	0.7226	0.7483
0.774		0.8249	0.8502	0.8754
0.900!	0.9256	0.9505	0.9753	1.0000
Width:	- 0 0511	0 1000	0 1400	0 1000
0.035		0.1066	0.1422	0.1777
0.213		0.2961	0.3402	0.3842
0.4283	3 0.4724	0.5164	0.5605	0.6046

0.6487 0.8690 1.0000 1.0000 1.0000 1.0000	0.6927 0.9131 1.0000 1.0000 1.0000 1.0000	0.7368 0.9572 1.0000 1.0000 1.0000 1.0000	0.7809 1.0000 1.0000 1.0000 1.0000 1.0000	0.8249 1.0000 1.0000 1.0000 1.0000 1.0000
Transect XS-L-Pipe	- (55)			
Area:  0.0005 0.0170 0.0595 0.1312 0.2323 0.3604 0.4937 0.6269 0.7602 0.8934 Hrad:	0.0019 0.0232 0.0715 0.1491 0.2561 0.3871 0.5203 0.6536 0.7868 0.9201	0.0043 0.0305 0.0847 0.1682 0.2810 0.4137 0.5470 0.6802 0.8135 0.9467	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401 0.9734	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668 1.0000
0.0139 0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005	0.0278 0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995	0.0418 0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.0557 0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.0696 0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754
0.0355 0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000	0.0711 0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000 1.0000	0.1066 0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000	0.1422 0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000 1.0000	0.1777 0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000
**************************************	tinuity ******	Volume acre-ft  1.116	Depth inches1.344	
Continuity Error (%	)	0.706		
**************************************	****** uity *****	Volume acre-ft	Volume Mgallons	
External Inflow External Outflow Initial Stored Volume Final Stored Volume Continuity Error (%	me	0.000 0.328 0.000 0.000 -0.044	0.000 0.107 0.000 0.000	
**************************************	Computation	s Report		

Subbasin Sub-CB-1			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.12 0.25 0.36	A (6%+) A (6%+)	0.79 0.29 0.45
Subbasin Sub-CB-10-11			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.17 0.16 0.33	A (6%+) A (6%+)	0.79 0.14 0.48
Subbasin Sub-CB-12-14			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.39 1.23 1.61	A (6%+) A (6%+)	0.79 0.14 0.30
Subbasin Sub-CB-15-17			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Streets, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.17 0.35 0.16 0.69	A (6%+) A (6%+) B (0-2%)	0.79 0.29 0.80 0.54
Subbasin Sub-CB-18-19			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.44 0.51 0.95	A (6%+) A (6%+)	0.79 0.29 0.52
Subbasin Sub-CB-20			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.45 1.05 1.49	A (6%+) A (6%+)	0.79 0.14 0.33
Subbasin Sub-CB-2-5			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.

Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.55 3.36 3.91	A (6%+) A (6%+)	0.79 0.14 0.23
Subbasin Sub-CB-6			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.09 0.05 0.14	A (2-6%) A (6%+)	0.77 0.29 0.59
Subbasin Sub-CB-7			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.08 0.03 0.11	A (0-2%) A (2-6%)	0.76 0.26 0.63
Subbasin Sub-CB-8W			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Meadow, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.16 0.06 0.22	A (2-6%) A (2-6%)	0.77 0.22 0.61
Subbasin Sub-CB-9			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.11 0.03 0.15	A (2-6%) A (2-6%)	0.77 0.26 0.65
**************************************			
Sheet Flow Equation			
$Tc = (0.007 * ((n * Lf)^0.8)) / ((P^0.5) * (S))$	Sf^0.4))		
Where:			
<pre>Tc = Time of Concentration (hrs) n = Manning's Roughness Lf = Flow Length (ft) P = 2 yr, 24 hr Rainfall (inches) Sf = Slope (ft/ft)</pre>			
Shallow Concentrated Flow Equation			
<pre>V = 16.1345 * (Sf^0.5) (unpaved surface)</pre>			

```
V = 20.3282 * (Sf^0.5) (paved surface)
          V = 15.0 * (Sf^0.5) (grassed waterway surface)
          V = 10.0 * (Sf^0.5) (nearly bare & untilled surface)
            = 9.0 * (Sf^0.5) (cultivated straight rows surface)
          V = 7.0 * (Sf^0.5) (short grass pasture surface)
          V = 5.0 * (Sf^0.5) \text{ (woodland surface)}
          V = 2.5 * (Sf^0.5) (forest w/heavy litter surface)
          Tc = (Lf / V) / (3600 sec/hr)
          Where:
          Tc = Time of Concentration (hrs)
          Lf = Flow Length (ft)
          V = Velocity (ft/sec)
          Sf = Slope (ft/ft)
 Channel Flow Equation
          V = (1.49 * (R^{(2/3)}) * (Sf^{0.5})) / n
          R = Aq / Wp
          Tc = (Lf / V) / (3600 sec/hr)
          Where:
          Tc = Time of Concentration (hrs)
          Lf = Flow Length (ft)
          R = Hydraulic Radius (ft)
          Aq = Flow Area (ft<sup>2</sup>)
          Wp = Wetted Perimeter (ft)
          V = Velocity (ft/sec)
          Sf = Slope (ft/ft)
         n = Manning's Roughness
 Subbasin Sub-CB-1
 Sheet Flow Computations
                                                 Subarea A
                                                                     Subarea B
                                                                                          Subarea
         Manning's Roughness:
                                                      0.40
                                                                           0.00
0.00
          Flow Length (ft):
                                                     33.69
                                                                           0.00
0.00
         Slope (%):
                                                      1.60
                                                                           0.00
0.00
          2 yr, 24 hr Rainfall (in):
                                                                           0.00
                                                      3.60
0.00
                                                      0.06
                                                                           0.00
          Velocity (ft/sec):
0.00
          Computed Flow Time (minutes):
                                                      9.26
                                                                           0.00
0.00
 Shallow Concentrated Flow Computations
                                                                     Subarea B
                                                 Subarea A
                                                                                          Subarea
                                                                           0.00
          Flow Length (ft):
                                                    329.84
0.00
          Slope (%):
                                                      0.77
                                                                           0.00
0.00
         Surface Type:
                                                     Paved
                                                                         Paved
Paved
                                                                          0.00
         Velocity (ft/sec):
                                                     1.79
```

С

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0.00		2 00	0.00	
0.00	Computed Flow Time (minutes):	3.08	0.00	
======				========
	Total TOC (minutes):	12.34		
======		:========:	===========	========
	in Sub-CB-10-11 			
	Flow Computations			
		Subarea A	Subarea B	Subarea
C	Manning's Roughness:	0.40	0.00	
0.00	Flow Length (ft):	82.40	0.00	
0.00	Slope (%):	22.88	0.00	
0.00	2 yr, 24 hr Rainfall (in):	3.60	0.00	
0.00	Velocity (ft/sec):	0.21	0.00	
0.00	Computed Flow Time (minutes):	6.54	0.00	
	w Concentrated Flow Computations			
		Subarea A	Subarea B	Subarea
С	Flow Length (ft):	332.66	0.00	
0.00	Slope (%):	2.02	0.00	
0.00	Surface Type:	Paved	Paved	
Paved	Velocity (ft/sec):	2.89	0.00	
0.00	Computed Flow Time (minutes):	1.92	0.00	
0.00				
======	Total TOC (minutes):	8.46	==========	========
======		:========:		========
	in Sub-CB-12-14			
sneet :	Flow Computations	Gulana a	Quihace a D	G 1
С	Manning La Doughnasa	Subarea A	Subarea B	Subarea
0.00	Manning's Roughness:	0.40	0.00	
0.00	Flow Length (ft):	222.41	0.00	
0.00	Slope (%):	10.60	0.00	

0.00	2 yr, 24 hr Rainfall (in):	3.60	0.00	
0.00	Velocity (ft/sec):	0.19	0.00	
0.00	Computed Flow Time (minutes):	19.69	0.00	
0.00				
	w Concentrated Flow Computations			
С		Subarea A	Subarea B	Subarea
0.00	Flow Length (ft):	430.84	0.00	
0.00	Slope (%):	3.53	0.00	
Paved	Surface Type:	Paved	Paved	
0.00	Velocity (ft/sec):	3.82	0.00	
0.00	Computed Flow Time (minutes):	1.88	0.00	
	Total TOC (minutes):	21.57		
======			=======================================	
Subbas	in Sub-CB-15-17			
	User-Defined TOC override (minutes):	5.00		
	in Sub-CB-18-19			
	User-Defined TOC override (minutes):	5.00		
	in Sub-CB-20			
Sheet	Flow Computations			
		Subarea A	Subarea B	Subarea
C	Manning's Roughness:	0.40	0.00	
0.00	Flow Length (ft):	227.22	0.00	
0.00	Slope (%):	7.48	0.00	
0.00	2 yr, 24 hr Rainfall (in):	3.60	0.00	
0.00	Velocity (ft/sec):	0.16	0.00	
0.00	Computed Flow Time (minutes):	23.04	0.00	
0.00				
	w Concentrated Flow Computations			
С		Subarea A	Subarea B	Subarea
Ü	Flow Length (ft):	193.35	0.00	

0.00	Slope (%):	2.77	0.00	
0.00	Surface Type:	Paved	Paved	
Paved	Velocity (ft/sec):	3.38	0.00	
0.00	-			
0.00	Computed Flow Time (minutes):	0.95	0.00	
======	Total TOC (minutes):	======================================		
	iotal ioc (minutes).			
Subbasi	n Sub-CB-2-5			
	low Computations			
		Subarea A	Subarea B	Subarea
С	Manning's Roughness:	0.40	0.00	
0.00	Flow Length (ft):	526.06	0.00	
0.00	Slope (%):	1.65	0.00	
0.00	2 yr, 24 hr Rainfall (in):	3.60	0.00	
0.00	Velocity (ft/sec):	0.11	0.00	
0.00	Computed Flow Time (minutes):	82.52	0.00	
	Concentrated Flow Computations			
		Subarea A	Subarea B	Subarea
C	Flow Length (ft):	591.37	0.00	
0.00	Slope (%):	2.70	0.00	
0.00	Surface Type:	Unpaved	Paved	
Paved	Velocity (ft/sec):	2.65	0.00	
0.00	Computed Flow Time (minutes):	3.72	0.00	
0.00				
=======	Total TOC (minutes):	86.24		
======				
	n Sub-CB-6			
	User-Defined TOC override (minutes):	5.00		
	.n Sub-CB-7			

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User-Defined TOC override (minutes): 5.00

Subbasin Sub-CB-8W

User-Defined TOC override (minutes): 5.00

Subbasin Sub-CB-9

User-Defined TOC override (minutes): 5.00

Subbasin ID	Accumulated Precip in	Rainfall Intensity in/hr	Total Runoff in	Peak Runoff cfs	Weighted Runoff Coeff	Conc days	Time of entration hh:mm:ss
Sub-CB-1	0.91	4.45	0.41	0.73	0.450	0	00:12:20
Sub-CB-10-11	0.77	5.44	0.37	0.85	0.480	0	00:08:27
Sub-CB-12-14	1.18	3.28	0.35	1.59	0.300	0	00:21:34
Sub-CB-15-17	0.60	7.21	0.32	2.69	0.540	0	00:05:00
Sub-CB-18-19	0.60	7.21	0.31	3.55	0.520	0	00:05:00
Sub-CB-20	1.24	3.10	0.41	1.53	0.330	0	00:23:59
Sub-CB-2-5	1.97	1.37	0.45	1.23	0.230	0	01:26:14
Sub-CB-6	0.60	7.21	0.35	0.61	0.590	0	00:05:00
Sub-CB-7	0.60	7.21	0.38	0.49	0.630	0	00:05:00
Sub-CB-8W	0.60	7.21	0.37	0.97	0.610	0	00:05:00
Sub-CB-9	0.60	7.21	0.39	0.69	0.650	0	00:05:00
Sub-CB-15-17 Sub-CB-18-19 Sub-CB-20 Sub-CB-2-5 Sub-CB-6 Sub-CB-7 Sub-CB-8W	0.60 0.60 1.24 1.97 0.60 0.60	7.21 7.21 3.10 1.37 7.21 7.21	0.32 0.31 0.41 0.45 0.35 0.38	2.69 3.55 1.53 1.23 0.61 0.49	0.540 0.520 0.330 0.230 0.590 0.630 0.610	0 0 0 0 0	00:05:00 00:05:00 00:23:59 01:26:14 00:05:00 00:05:00 00:05:00

Node ID	Average Depth Attained	Maximum Depth Attained	Maximum HGL Attained		of Max rrence	Total Flooded Volume	Total Time Flooded	Retention Time
	ft	ft	ft	days	hh:mm	acre-in	minutes	hh:mm:ss
CIT-8	0.00	0.45	255.25	0	00:05	0	0	0:00:00
DH-10	0.00	0.25	265.40	0	00:08	0	0	0:00:00
DH-13	0.01	0.47	260.26	0	00:21	0	0	0:00:00
DH-20	0.01	0.27	277.89	0	00:24	0	0	0:00:00
EX-18	3.00	3.58	269.58	0	00:05	0	0	0:00:00
EX-7	0.00	0.45	253.25	0	00:05	0	0	0:00:00
Structure - (7	72) 0.11	0.33	276.12	0	00:12	0	0	0:00:00
DP-1	0.00	0.29	275.29	0	00:12	0	0	0:00:00
DP-10	0.00	0.25	265.03	0	00:08	0	0	0:00:00
DP-13	0.01	0.47	260.07	0	00:21	0	0	0:00:00
DP-16	0.00	0.00	252.66	0	00:00	0	0	0:00:00
DP-18	0.01	0.50	264.86	0	00:05	0	0	0:00:00
DP-20	0.01	0.26	274.46	0	00:24	0	0	0:00:00
DP-5	0.00	0.00	248.00	0	00:00	0	0	0:00:00
DP-6	0.00	0.00	246.50	0	00:00	0	0	0:00:00
DP-7	0.00	0.45	253.05	0	00:06	0	0	0:00:00
Out-01	0.00	0.07	281.29	0	00:16	0	0	0:00:00

Node ID	Element Type	Inflow cfs	cfs	Occu days	rrence hh:mm	Overfl c	ow Oco fs day:	currence s hh:mm
CIT-8	JUNCTION							
DH-10	JUNCTION	0.85	1.51	0	00:08	0.		
DH-13	JUNCTION	1.59	1.59	0	00:21	0.		
DH-20	JUNCTION	1 53	1.59 1.53 3.54 1.47	0	00.21	0.		
EX-18	JUNCTION	1.55	2 5/	0	00.24	0.		
EX-7	JUNCTION	0.00	1 47	0	00:05	0.		
	JUNCTION	0.00	0.47	0	00.03	0.		
Structure - (72) DP-1	OUTFALL	0.00	0.04	0	00.12	0.		
		0.00	0.04	0	00.12	0.		
DP-10	OUTFALL	0.00	0.64 0.64 0.85 1.59	0	00.08			
DP-13	OUTFALL	0.00	1.59	0	00:21	0.		
DP-16	OUTFALL	2.69	2.69	0	00:05	0.		
DP-18	OUTFALL	0.00	3.51	U	00:05	0.		
DP-20	OUTFALL	0.00	2.69 3.51 1.52 1.23	0	00:24	0.		
DP-5	OUTFALL	1.23	1.23	0	01:26	0.	00	
DP-6	OUTFALL	0.61 0.49 0.00	0.61	0	00:05	0.	00	
DP-7	OUTFALL	0.49	1.89	0	00:05	0.	00	
Out-01	OUTFALL	0.00	0.06	0	00:16	0.	00	
**************************************								
Inlet Depth Summar:	Max Gutter Spread during Peak Flow ft	Max Gut Water I du Peak I	ter Elev ring Flow ft	Max G Water d Peak	Sutter Depth Suring Flow ft	T M Occu days	ime of aximum Depth rrence hh:mm	
Inlet Depth Summar: ***************  Inlet ID	Max Gutter Spread during Peak Flow ft	Max Gut Water I du Peak I	ter Elev ring Flow ft	Max G Water d Peak	Sutter Depth Suring Flow ft	T M Occu days	ime of aximum Depth rrence hh:mm	
Inlet Depth Summar: **************  Inlet ID  CB-1	Max Gutter Spread during Peak Flow ft	Max Gut Water I du Peak I	ter Elev ring Flow ft	Max G Water d Peak	Sutter Depth Suring Flow ft	T M Occu days	ime of aximum Depth rrence hh:mm	
Inlet Depth Summar: **************  Inlet ID  CB-1 CB-18	Max Gutter Spread during Peak Flow ft 5.20 12.89	Max Gut Water I du Peak I	tter Elev ring Flow ft	Max G Water d Peak	dutter Depth luring Flow ft	T M Occu days	ime of aximum Depth rrence hh:mm	
Inlet Depth Summar: **************  Inlet ID  CB-1 CB-18 EX-CB15	Max Gutter Spread during Peak Flow ft  5.20 12.89 1.16 5.05	Max Gut Water I du Peak I	ter Elev ring Flow ft	Max G Water d Peak	Sutter Depth Suring Flow ft	T M Occu days	ime of aximum Depth rrence hh:mm	
Inlet Depth Summar:  ****************  Inlet ID  CB-1 CB-18 EX-CB15 EX-CB-16  ***********************************	Max Gutter Spread during Peak Flow ft 5.20 12.89 1.16 5.05	Max Gut Water I du Peak I	tter Elevering Flow ft 1.41 4.08 9.27 2.49	Max G Water d Peak	Sutter Depth Suring Flow ft 0.19 0.36 0.07 0.19	Occu days Occu 0 0 0	ime of aximum Depth rrence hh:mm 00:12 00:05 00:06 00:05	 t Tota
Inlet Depth Summar: ************************************	Max Gutter Spread during Peak Flow ft  5.20 12.89 1.16 5.05	Max Gut Water I du Peak I  283 274 259 262	Elevering Flow ft 1.41 4.08 9.27 2.49	Max G Water d Peak	Sutter Depth Suring Flow ft 0.19 0.36 0.07 0.19	Occudays 000000000000000000000000000000000000	ime of aximum Depth rrence hh:mm 00:12 00:05 00:06 00:05	
Inlet Depth Summar:  ********************  Inlet ID  CB-1 CB-18 EX-CB15 EX-CB-16  ****************** Inlet Flow Summary  ***********************  Inlet flow Summary	Max Gutter Spread during Peak Flow ft  5.20 12.89 1.16 5.05	Max Gut Water I du Peak I  283 274 255 262	Elevering Flow ft 1.41 4.08 9.27 2.49	Max G Water d Peak	Pee	Occudays Occudays O O O O O O O O O O O O O O O O O O O	ime of aximum Depth rrence hh: mm 00:12 00:05 00:06 00:05	y Flooding
Inlet Depth Summar:  **************************  Inlet ID  CB-1 CB-18 EX-CB-16  *************************  Inlet Flow Summary  ***********************************	Max Gutter Spread during Peak Flow ft  5.20 12.89 1.16 5.05	Max Gut Water I du Peak I  283 274 255 262	Elevering Flow ft 1.41 4.08 9.27 2.49  Flow Flow Flow Flow Flow Flow Flow Flo	Max G Water d Peak	Pepsassi	Occudays Occudos Occud	ime of aximum Depth rrence hh: mm 00:12 00:05 00:06 00:05	y Flooding

_						
CB-1 0	0.73	0.73	0.65	0.08	89.27	0.000
CB-18	3.55	3.55	-	-	-	0.000
EX-CB15	0.05	0.00	0.05	0.00	100.00	0.000
0 EX-CB-16	0.69	0.69	0.62	0.07	90.11	0.000

Outfall Node ID	Flow Frequency (%)	Average Flow cfs	Peak Inflow cfs
DP-1 DP-10 DP-13 DP-16 DP-18 DP-20 DP-5 DP-6 DP-7 Out-01	1.91 1.19 3.01 0.69 0.87 3.38 11.96 0.69 1.94 2.76	0.30 0.42 0.79 1.35 1.40 0.75 0.62 0.30 0.38 0.02	0.64 0.85 1.59 2.69 3.51 1.52 1.23 0.61 1.89
System	2.84	6.33	10.06

Link ID		Element	Т	ime of	Maximum	Length	Peak Flow	Design	Ratio of
Ratio of	То	tal Reported							
			Pea	k Flow	Velocity	Factor	during	Flow	Maximum
Maximum	Ti	me Condition							
-1 1	,		0ccu	rrence	Attained		Analysis	Capacity	/Design
Flow Surcharg	rea		4	la la •	£		cfs	cfs	ml
Depth minu	+00		days	11111 • 111111	ft/sec		CIS	CIS	Flow
Depth minu	ices								
CB-1_Overflo	w	CHANNEL	0	00:16	1.74	1.00	0.06	2.70	0.02
0.23	0	Calculated							
CIT-9_Overfl		CHANNEL	0	00:06	3.57	1.00	0.05	7.01	0.01
0.15	0	Calculated							
Link-17		CONDUIT	0	00:06	0.77	1.00	0.05	4.07	0.01
0.08	0	Calculated							
Link-18	^	CHANNEL	0	00:11	0.63	1.00	0.00	10.44	0.00
0.04 Pipe - (21)	U	Calculated CONDUIT	0	00:05	4.44	1.00	1.47	3.59	0.41
0.44	Λ	Calculated	U	00.05	4.44	1.00	1.4/	3.59	0.41
Pipe - (22)	U	CONDUIT	0	00:06	4.32	1.00	1.47	3.56	0.41
0.45	0	Calculated	U	00.00	1.52	1.00	1.17	3.30	0.11
Pipe - (25)	,	CONDUIT	0	00:05	6.78	1.00	0.59	3.88	0.15
0.26	0	Calculated							

Pipe - (33)		CONDUIT	0	00:21	4.41	1.00	1.59	3.56	0.45
0.47	0	Calculated							
Pipe - (44)		CONDUIT	0	00:05	7.59	1.00	3.54	5.63	0.63
0.57	0	Calculated							
Pipe - (45)		CONDUIT	0	00:05	6.92	1.00	3.51	14.86	0.24
0.33	0	Calculated							
Pipe - (56)		CONDUIT	0	00:08	5.52	1.00	0.85	6.17	0.14
0.25	0	Calculated							
Pipe - (57)		CONDUIT	0	00:24	7.25	1.00	1.52	22.60	0.07
0.18	0	Calculated							
Pipe - (61)		CONDUIT	0	00:12	5.59	1.00	0.64	5.92	0.11
0.22	0	Calculated							
Pipe - (62)		CONDUIT	0	00:12	3.44	1.00	0.64	3.56	0.18
0.29	0	Calculated							

All links are stable.

WARNING 108 : Surcharge elevation defined for Junction EX-18 is below junction maximum elevation. Assumed surcharge elevation equal to maximum elevation.

WARNING 139 : Ponded area defined for on sag Inlet CB-18 is zero. Assumed ponded area equal to 10 ft $^2$  (0.929 m $^2$ ).

WARNING 138 : Initial water surface elevation defined for Inlet EX-CB15 is below catchbasin invert elevation.

Assumed initial water surface elevation equal to catchbasin inlet invert

elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB-1\_Overflow is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CIT-9\_Overflow is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 117: Conduit outlet invert elevation defined for Conduit CB-1\_Overflow is below downstream node invert elevation.

Assumed conduit outlet invert elevation equal to downstream node invert

elevation.

WARNING 004 : Minimum elevation drop used for Conduit CB-1\_Overflow.

WARNING 005 : Minimum slope used for Conduit CB-1\_Overflow.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CIT-9\_Overflow is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet EX-CB15.

WARNING 116: Conduit inlet invert elevation defined for Conduit Link-17 is below upstream node invert elevation.

Assumed conduit inlet invert elevation equal to upstream node invert elevation.

WARNING 004: Minimum elevation drop used for Conduit Link-17.

WARNING 005 : Minimum slope used for Conduit Link-17.

Analysis began on: Tue Jan 31 11:03:17 2023 Analysis ended on: Tue Jan 31 11:03:18 2023

Total elapsed time: 00:00:01

```
Autodesk® Storm and Sanitary Analysis 2016 - Version 13.2.165 (Build 0)
Project Description
******
File Name ..... Grove_St_Ph2_r1-EX.SPF
******
Analysis Options
******
Flow Units ..... cfs
Subbasin Hydrograph Method. Rational
Time of Concentration..... SCS TR-55
Return Period...... 25 years
Link Routing Method ..... Kinematic Wave Storage Node Exfiltration. None
Starting Date ..... DEC-20-2022 00:00:00
Ending Date ..... DEC-21-2022 00:00:00
Report Time Step ...... 00:00:10
******
Element Count
Number of subbasins ..... 11
Number of nodes ..... 21
Number of links ..... 14
******
Subbasin Summary
******
Subbasin
                      Total
                       Area
TD
                       acres
                    0.36
0.33
Sub-CB-1
Sub-CB-10-11
                      1.61
0.69
Sub-CB-12-14
Sub-CB-15-17
                      0.95
Sub-CB-18-19
                       1.49
3.91
Sub-CB-20
Sub-CB-2-5
Sub-CB-6
                      0.14
Sub-CB-7
                       0.11
Sub-CB-8W
                       0.22
Sub-CB-9
                       0.15
*****
Node Summary
*****
                  Node
ID
CIT-8 JUNCTION 254.80 259.42 0.00 DH-10 JUNCTION 265.15 268.15 0.00 DH-13 JUNCTION 259.80 265.60 0.00 TUNCTION 277.62 279.12 0.00
______
CIT-8
DH-10
DH-13
JUNCTION
DH-20
EX-18
JUNCTION
JUNCTION
JUNCTION
JUNCTION
JUNCTION
JUNCTION
JUNCTION
                                266.00 273.24 0.00
252.80 258.62 0.00
275.79 277.57 0.00
```

DP-1 DP-10 DP-13 DP-16 DP-18 DP-20 DP-5 DP-6 DP-7 Out-01		OUTFA	LL LL LL LL LL LL LL	264 259 252 264 274 248 246 252	5.00 4.78 9.60 2.66 4.36 4.20 8.00 6.50 2.60 1.22	276.00 265.78 260.60 252.66 265.86 275.70 248.00 246.50 253.60 281.50	0. 0. 0. 0. 0. 0. 0. 0.	00 00 00 00 00 00 00 00			
*********** Inlet Summ *****	ary										
Inlet		Inlet				Manufactur	er	I	nlet	Number	
Catchbasin			Ponded	Initia	al	Grate				_	
ID	D.		acturer		<b>a</b> 1	Part		L	ocation	of	
Invert	K.	im Ar	ea	Water	CTO	gging Number				Inlets	
Elevation	Eleva	ation		Elevation	n	Factor				1111000	
ft	ft	ft²		ft	9	8					
CB-1		FHWA	HEC-22	GENERIC		N/A		0:	n Grade	1	
278.10	281.2	22	_	278.10		0.00					
CB-18		FHWA	HEC-22	GENERIC		N/A		O:	n Sag	1	
269.61	273.7	72 10.	00	269.61		0.00					
EX-CB15		FHWA	HEC-22	GENERIC		N/A		O:	n Grade	1	
254.80	259.2		-	254.80		0.00					
EX-CB-16			HEC-22	GENERIC		N/A		O:	n Grade	1	
257.40	262.3	30	_	257.40		0.00					
********* Roadway an ******* Inlet ID	ıd Gutt	er Summar	У	Cross Slope		Roadway anning's oughness	Gutter Cross Slope ft/ft	Gutter Width ft	Depre	utter ssion in	
CB-1			0.0100	0.0200		0.0160	0.0620	2.00		2.00	
CB-18			-	0.0200		0.0160	0.0620	2.00		2.00	
EX-CB15			0.0100	0.0200		0.0160	0.0620	2.00		2.00	
EX-CB-16			0.0100	0.0200		0.0160	0.0620	2.00		2.00	
**************************************	ry										
Link ID		From Node		To Node		Element Type	1	Length ft	Slope %	Manning Roughnes	
CB-1_Overf		CB-1		Out-01		CHANNEL		241.8	0.2000	0.013	
CIT-9_Over	ilow	EX-CB-16		EX-CB15		CHANNEL		230.0	1.3478	0.013	
Link-17		EX-CB15		CIT-8		CONDUIT		8.9	0.2000	0.015	
Link-18	,	EX-CB15		DP-7		CHANNEL		220.5	2.9927	0.013	
Pipe - (21		CIT-8		EX-7		CONDUIT		196.9	1.0156	0.013	
Pipe - (22		EX-7		DP-7		CONDUIT		20.0	1.0000	0.013	
Pipe - (25		EX-CB-16		CIT-8		CONDUIT		219.0	1.1872	0.013	
Pipe - (33 Pipe - (44		DH-13 CB-18		DP-13 EX-18		CONDUIT		19.5 24.4	1.0000 2.4990	0.013	
Pipe - (44 Pipe - (45		EX-18		DP-18		CONDUIT CONDUIT		81.8	2.4990	0.013	
1150 (13	,	-41 10				00110011		01.0	2.0000	0.01	- 0

Pipe - (56) Pipe - (57) Pipe - (61) Pipe - (62)	DH-10 DH-20 CB-1 Structure		CONDUIT CONDUIT - (72)CONDUIT CONDUIT	55.! 79.8	6.1644 3 2.7583	0.0130 0.0150 0.0130 0.0130			
********	*****								
Cross Section									
Link	Shape	Depth/	Width	No. of	Cross	Full Flow			
Design ID		Diameter		Barrels	Sectional	Hydraulic			
Flow					Area	Radius			
Capacity		ft	ft		ft²	ft			
cfs									
CB-1_Overflow 2.70	TRIANGULA	R 0.28	14.00	1	1.96	0.14			
CIT-9_Overflow	TRIANGULA	R 0.28	14.00	1	1.96	0.14			
7.01 Link-17	CIRCULAR	1.50	1.50	1	1.77	0.38			
4.07 Link-18	TRIANGULA	R 0.28	14.00	1	1.96	0.14			
10.44 Pipe - (21)	CIRCULAR	1.00	1.00	1	0.79	0.25			
3.59 Pipe - (22)	CIRCULAR	1.00	1.00	1	0.79	0.25			
3.56 Pipe - (25)	CIRCULAR	1.00	1.00	1	0.79	0.25			
3.88			1.00	1	0.79	0.25			
Pipe - (33) 3.56	CIRCULAR	1.00							
Pipe - (44) 5.63	CIRCULAR	1.00	1.00	1	0.79	0.25			
Pipe - (45) 14.86	CIRCULAR	1.50	1.50	1	1.77	0.38			
Pipe - (56) 6.17	CIRCULAR	1.00	1.00	1	0.79	0.25			
Pipe - (57) 22.60	CIRCULAR	1.50	1.50	1	1.77	0.38			
Pipe - (61) 5.92	CIRCULAR	1.00	1.00	1	0.79	0.25			
Pipe - (62) 3.56	CIRCULAR	1.00	1.00	1	0.79	0.25			
3.56  *********  Transect Summary  ***********  Transect XS-L-Pipe - (13)									
Area:	_	010 0 0042	0 0076	0 0110					
0. 0. 0. 0. 0. 0.	0005 0.0 0170 0.0 0595 0.0 1312 0.1 2323 0.2 3604 0.3 4937 0.5 6269 0.6 7602 0.7	232 0.0305 715 0.0847 491 0.1682 561 0.2810 871 0.4137 203 0.5470 536 0.6802 868 0.8135	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668					
0.	8934 0.9	201 0.9467	0.9734	1.0000					

Hrad:					
Width:	0.0139 0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005	0.0278 0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995 0.9256	0.0418 0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.0557 0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.0696 0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754 1.0000
	0.0355 0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000	0.0711 0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000 1.0000	0.1066 0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000 1.0000	0.1422 0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000 1.0000	0.1777 0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000
Transect :	XS-L-Pipe -	(16)			
Hrad:	0.0005 0.0170 0.0595 0.1312 0.2323 0.3604 0.4937 0.6269 0.7602 0.8934	0.0019 0.0232 0.0715 0.1491 0.2561 0.3871 0.5203 0.6536 0.7868 0.9201	0.0043 0.0305 0.0847 0.1682 0.2810 0.4137 0.5470 0.6802 0.8135 0.9467	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401 0.9734	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668 1.0000
iii au	0.0139 0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005	0.0278 0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995 0.9256	0.0418 0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.0557 0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.0696 0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754
Width:	0.0355 0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000	0.0711 0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000	0.1066 0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000	0.1422 0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000	0.1777 0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000
Transect 2	XS-L-Pipe -	(18)			
Area:	0.0005 0.0170 0.0595 0.1312 0.2323 0.3604	0.0019 0.0232 0.0715 0.1491 0.2561 0.3871	0.0043 0.0305 0.0847 0.1682 0.2810 0.4137	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670

	0.4937 0.6269	0.5203 0.6536	0.5470 0.6802	0.5736 0.7069	0.6003 0.7335
	0.7602	0.7868	0.8135	0.8401	0.7333
	0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:					
	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835 0.1459	0.0963 0.1591	0.1080 0.1724	0.1202 0.1858	0.1329 0.1994
	0.2130	0.2267	0.2404	0.2542	0.2680
	0.2818	0.2957	0.3095	0.3238	0.3512
	0.3784	0.4055	0.4326	0.4595	0.4863
	0.5130 0.6448	0.5396 0.6708	0.5660 0.6968	0.5924 0.7226	0.6187 0.7483
	0.7740	0.7995	0.8249	0.8502	0.7403
	0.9005	0.9256	0.9505	0.9753	1.0000
Width:					
	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132 0.4283	0.2520 0.4724	0.2961 0.5164	0.3402 0.5605	0.3842
	0.6487	0.6927	0.7368	0.7809	0.8249
	0.8690	0.9131	0.9572	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000 1.0000	1.0000	1.0000 1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
Transect Area:	XS-L-Pipe -	(2)			
AI Ca.	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312 0.2323	0.1491 0.2561	0.1682 0.2810	0.1884 0.3071	0.2098
	0.2323	0.3871	0.2810	0.4404	0.3336
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602 0.8934	0.7868 0.9201	0.8135 0.9467	0.8401 0.9734	0.8668
Hrad:	0.0934	0.9201	0.9467	0.9/34	1.0000
	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835	0.0963	0.1080	0.1202	0.1329
	0.1459	0.1591	0.1724	0.1858 0.2542	0.1994
	0.2130 0.2818	0.2267 0.2957	0.2404 0.3095	0.3238	0.2680 0.3512
	0.3784	0.4055	0.4326	0.4595	0.4863
	0.5130	0.5396	0.5660	0.5924	0.6187
	0.6448	0.6708	0.6968	0.7226	0.7483
	0.7740 0.9005	0.7995 0.9256	0.8249 0.9505	0.8502 0.9753	0.8754 1.0000
Width:	0.7003	0.7250	0.7505	0.7755	2.0000
	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132	0.2520	0.2961	0.3402	0.3842
	0.4283 0.6487	0.4724 0.6927	0.5164 0.7368	0.5605 0.7809	0.6046 0.8249
	0.8690	0.9131	0.9572	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000 1.0000	1.0000	1.0000 1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	XS-L-Pipe -	(24)			
Area:	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487

w	0.0595 0.1312 0.2323 0.3604 0.4937 0.6269 0.7602 0.8934	0.0715 0.1491 0.2561 0.3871 0.5203 0.6536 0.7868 0.9201	0.0847 0.1682 0.2810 0.4137 0.5470 0.6802 0.8135 0.9467	0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401 0.9734	0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668 1.0000
<pre>Hrad:</pre> <pre>Width:</pre>	0.0139 0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005	0.0278 0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995	0.0418 0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.0557 0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.0696 0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754
	0.0355 0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000	0.0711 0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000 1.0000	0.1066 0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000	0.1422 0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000 1.0000	0.1777 0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000
Transect XS Area:	-L-Pipe -	(27)			
Hrad:	0.0005 0.0170 0.0595 0.1312 0.2323 0.3604 0.4937 0.6269 0.7602 0.8934	0.0019 0.0232 0.0715 0.1491 0.2561 0.3871 0.5203 0.6536 0.7868 0.9201	0.0043 0.0305 0.0847 0.1682 0.2810 0.4137 0.5470 0.6802 0.8135 0.9467	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401 0.9734	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668 1.0000
	0.0139 0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005	0.0278 0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995 0.9256	0.0418 0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.0557 0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.0696 0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754 1.0000
Width:	0.0355 0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000 1.0000	0.0711 0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000	0.1066 0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000	0.1422 0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000	0.1777 0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000

Transect :	XS-L-Pipe -	(28)			
Alea	0.0005 0.0170 0.0595 0.1312 0.2323 0.3604 0.4937 0.6269 0.7602 0.8934	0.0019 0.0232 0.0715 0.1491 0.2561 0.3871 0.5203 0.6536 0.7868 0.9201	0.0043 0.0305 0.0847 0.1682 0.2810 0.4137 0.5470 0.6802 0.8135 0.9467	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401 0.9734	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668 1.0000
Hrad:	0.0551	0.5201	0.5107	0.5751	1.0000
	0.0139 0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005	0.0278 0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995 0.9256	0.0418 0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.0557 0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.0696 0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754 1.0000
Width:	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000	0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000 1.0000	0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000 1.0000	0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000	0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000 1.0000
	XS-L-Pipe -	(30)			
Area:	0.0005 0.0170 0.0595 0.1312 0.2323 0.3604 0.4937 0.6269 0.7602 0.8934	0.0019 0.0232 0.0715 0.1491 0.2561 0.3871 0.5203 0.6536 0.7868 0.9201	0.0043 0.0305 0.0847 0.1682 0.2810 0.4137 0.5470 0.6802 0.8135 0.9467	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401 0.9734	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668 1.0000
Hrad:					
Width:	0.0139 0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005	0.0278 0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995 0.9256	0.0418 0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.0557 0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.0696 0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754 1.0000
	0.0355 0.2132 0.4283 0.6487 0.8690 1.0000	0.0711 0.2520 0.4724 0.6927 0.9131 1.0000	0.1066 0.2961 0.5164 0.7368 0.9572 1.0000	0.1422 0.3402 0.5605 0.7809 1.0000 1.0000	0.1777 0.3842 0.6046 0.8249 1.0000 1.0000

1.0000	1.0000	1.0000	1.0000	1.0000
1.0000	1.0000	1.0000	1.0000	1.0000
1.0000	1.0000	1.0000	1.0000	1.0000
1.0000	1.0000	1.0000	1.0000	1.0000
Twomagat VC I Ding	(27)			
Transect XS-L-Pipe	- (37)			
Area:	0 0010	0 0040	0 0000	0 0110
0.0005	0.0019	0.0043	0.0076	0.0118
0.0170	0.0232	0.0305	0.0390	0.0487
0.0595	0.0715	0.0847	0.0990	0.1145
0.1312	0.1491	0.1682	0.1884	0.2098
0.2323	0.2561	0.2810	0.3071	0.3338
0.3604	0.3871	0.4137	0.4404	0.4670
0.4937	0.5203	0.5470	0.5736	0.6003
0.6269	0.6536	0.6802	0.7069	0.7335
0.7602	0.7868	0.8135	0.8401	0.8668
0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:				
0.0139	0.0278	0.0418	0.0557	0.0696
0.0835	0.0963	0.1080	0.1202	0.1329
0.1459	0.1591	0.1724	0.1858	0.1994
0.2130	0.2267	0.2404	0.2542	0.2680
0.2818	0.2957	0.3095	0.3238	0.3512
0.3784	0.4055	0.4326	0.4595	0.4863
0.5130	0.5396	0.5660	0.5924	0.6187
0.6448	0.6708	0.6968	0.7226	0.7483
0.7740	0.7995	0.8249	0.8502	0.8754
0.9005	0.9256	0.9505	0.9753	1.0000
Width:	0.5250	0.9505	0.5755	1.0000
0.0355	0.0711	0.1066	0.1422	0.1777
0.2132	0.2520	0.2961	0.3402	0.3842
0.4283	0.2320	0.5164	0.5605	0.6046
			0.7809	
0.6487	0.6927	0.7368		0.8249
0.8690	0.9131	0.9572	1.0000	1.0000
1.0000	1.0000	1.0000	1.0000	1.0000
1.0000	1.0000	1.0000	1.0000	1.0000
1.0000	1.0000	1.0000	1.0000	1.0000
1.0000	1.0000	1.0000	1.0000	1.0000
1.0000	1.0000	1.0000	1.0000	1.0000
Transect XS-L-Pipe	- (50)			
Area:				
0.0005	0.0019	0.0043	0.0076	0.0118
0.0170	0.0232	0.0305	0.0390	0.0487
0.0595	0.0715	0.0847	0.0990	0.1145
0.1312	0.1491	0.1682	0.1884	0.2098
0.2323	0.2561	0.2810	0.3071	0.3338
0.3604	0.3871	0.4137	0.4404	0.4670
0.4937	0.5203	0.5470	0.5736	0.6003
0.6269	0.6536	0.6802	0.7069	0.7335
0.7602	0.7868	0.8135	0.8401	0.8668
0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:				
0.0139	0.0278	0.0418	0.0557	0.0696
0.0835	0.0963	0.1080	0.1202	0.1329
0.1459	0.1591	0.1724	0.1858	0.1994
0.2130	0.2267	0.2404	0.2542	0.2680
0.2818	0.2957	0.3095	0.3238	0.3512
0.3784	0.4055	0.4326	0.4595	0.4863
0.5130	0.5396	0.5660	0.5924	0.6187
0.6448	0.6708	0.6968	0.7226	0.7483
0.7740	0.7995	0.8249	0.7220	0.7463
0.9005	0.7995	0.9505	0.8302	1.0000
Width:	0.9430	0.9303	0.9133	1.0000
0.0355	0 0711	0 1066	0.1422	0 1777
	0.0711	0.1066		0.1777
0.2132	0.2520	0.2961	0.3402	0.3842
0.4283	0.4724	0.5164	0.5605	0.6046

	0.6487 0.8690 1.0000 1.0000 1.0000 1.0000	0.6927 0.9131 1.0000 1.0000 1.0000 1.0000	0.7368 0.9572 1.0000 1.0000 1.0000 1.0000	0.7809 1.0000 1.0000 1.0000 1.0000 1.0000	0.8249 1.0000 1.0000 1.0000 1.0000 1.0000		
Transect XS-	L-Pipe - (	55)					
	0.0005 0.0170 0.0595 0.1312 0.2323 0.3604 0.4937 0.6269 0.7602 0.8934	0.0019 0.0232 0.0715 0.1491 0.2561 0.3871 0.5203 0.6536 0.7868 0.9201	0.0043 0.0305 0.0847 0.1682 0.2810 0.4137 0.5470 0.6802 0.8135 0.9467	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401 0.9734	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668 1.0000		
	0.0139 0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005	0.0278 0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995 0.9256	0.0418 0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.0557 0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.0696 0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754 1.0000		
	0.0355 0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000 1.0000	0.0711 0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000 1.0000	0.1066 0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000	0.1422 0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000	0.1777 0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000		
**************************************		Volume acre-ft	Depth inches				
********* Total Precipitation Continuity Error (%)		1.354 0.706	1.630				
**************************************		Volume acre-ft	Volume Mgallons				
External Inflow  External Outflow  Initial Stored Volume  Final Stored Volume  Continuity Error (%)		0.000 0.398 0.000 0.000 -0.043	0.000 0.130 0.000 0.000				
**************************************							

Autodesk Storm and Sanitary Analysis

Subbasin Sub-CB-1			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.12 0.25 0.36	A (6%+) A (6%+)	0.79 0.29 0.45
Subbasin Sub-CB-10-11			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.17 0.16 0.33	A (6%+) A (6%+)	0.79 0.14 0.48
Subbasin Sub-CB-12-14			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.39 1.23 1.61	A (6%+) A (6%+)	0.79 0.14 0.30
Subbasin Sub-CB-15-17			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Streets, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.17 0.35 0.16 0.69	A (6%+) A (6%+) B (0-2%)	0.79 0.29 0.80 0.54
Subbasin Sub-CB-18-19			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.44 0.51 0.95	A (6%+) A (6%+)	0.79 0.29 0.52
Subbasin Sub-CB-20			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.45 1.05 1.49	A (6%+) A (6%+)	0.79 0.14 0.33
Subbasin Sub-CB-2-5			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.

Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.55 3.36 3.91	A (6%+) A (6%+)	0.79 0.14 0.23
Subbasin Sub-CB-6			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.09 0.05 0.14	A (2-6%) A (6%+)	0.77 0.29 0.59
Subbasin Sub-CB-7			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.08 0.03 0.11	A (0-2%) A (2-6%)	0.76 0.26 0.63
Subbasin Sub-CB-8W			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Meadow, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.16 0.06 0.22	A (2-6%) A (2-6%)	0.77 0.22 0.61
Subbasin Sub-CB-9			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.11 0.03 0.15	A (2-6%) A (2-6%)	0.77 0.26 0.65
**************************************			
Sheet Flow Equation			
$Tc = (0.007 * ((n * Lf)^0.8)) / ((P^0.5) * (S))$	Sf^0.4))		
Where:			
<pre>Tc = Time of Concentration (hrs) n = Manning's Roughness Lf = Flow Length (ft) P = 2 yr, 24 hr Rainfall (inches) Sf = Slope (ft/ft)</pre>			
Shallow Concentrated Flow Equation			
<pre>V = 16.1345 * (Sf^0.5) (unpaved surface)</pre>			

```
V = 20.3282 * (Sf^0.5) (paved surface)
          V = 15.0 * (Sf^0.5) (grassed waterway surface)
          V = 10.0 * (Sf^0.5) (nearly bare & untilled surface)
            = 9.0 * (Sf^0.5) (cultivated straight rows surface)
          V = 7.0 * (Sf^0.5) (short grass pasture surface)
          V = 5.0 * (Sf^0.5) \text{ (woodland surface)}
          V = 2.5 * (Sf^0.5) (forest w/heavy litter surface)
          Tc = (Lf / V) / (3600 sec/hr)
          Where:
          Tc = Time of Concentration (hrs)
          Lf = Flow Length (ft)
          V = Velocity (ft/sec)
          Sf = Slope (ft/ft)
 Channel Flow Equation
          V = (1.49 * (R^{(2/3)}) * (Sf^{0.5})) / n
          R = Aq / Wp
          Tc = (Lf / V) / (3600 sec/hr)
          Where:
          Tc = Time of Concentration (hrs)
          Lf = Flow Length (ft)
          R = Hydraulic Radius (ft)
          Aq = Flow Area (ft<sup>2</sup>)
          Wp = Wetted Perimeter (ft)
          V = Velocity (ft/sec)
          Sf = Slope (ft/ft)
         n = Manning's Roughness
 Subbasin Sub-CB-1
 Sheet Flow Computations
                                                 Subarea A
                                                                     Subarea B
                                                                                          Subarea
         Manning's Roughness:
                                                      0.40
                                                                           0.00
0.00
          Flow Length (ft):
                                                     33.69
                                                                           0.00
0.00
         Slope (%):
                                                      1.60
                                                                           0.00
0.00
          2 yr, 24 hr Rainfall (in):
                                                                           0.00
                                                      3.60
0.00
                                                      0.06
                                                                           0.00
          Velocity (ft/sec):
0.00
          Computed Flow Time (minutes):
                                                      9.26
                                                                           0.00
0.00
 Shallow Concentrated Flow Computations
                                                                     Subarea B
                                                 Subarea A
                                                                                          Subarea
                                                                           0.00
          Flow Length (ft):
                                                    329.84
0.00
          Slope (%):
                                                      0.77
                                                                           0.00
0.00
         Surface Type:
                                                     Paved
                                                                         Paved
Paved
                                                                          0.00
         Velocity (ft/sec):
                                                     1.79
```

С

C

0.00	Computed Flow Time (minutes):	2 00	0.00	
0.00	Computed Flow Time (minutes):	3.08	0.00	
======				========
	Total TOC (minutes):	12.34		
======		:========:	===========	========
	in Sub-CB-10-11 			
	Flow Computations			
		Subarea A	Subarea B	Subarea
C	Manning's Roughness:	0.40	0.00	
0.00	Flow Length (ft):	82.40	0.00	
0.00	Slope (%):	22.88	0.00	
0.00	2 yr, 24 hr Rainfall (in):	3.60	0.00	
0.00	Velocity (ft/sec):	0.21	0.00	
0.00	Computed Flow Time (minutes):	6.54	0.00	
	w Concentrated Flow Computations			
		Subarea A	Subarea B	Subarea
С	Flow Length (ft):	332.66	0.00	
0.00	Slope (%):	2.02	0.00	
0.00	Surface Type:	Paved	Paved	
Paved	Velocity (ft/sec):	2.89	0.00	
0.00	Computed Flow Time (minutes):	1.92	0.00	
0.00				
======	Total TOC (minutes):	8.46	==========	========
======		:========:		========
	in Sub-CB-12-14			
sneet :	Flow Computations	Gulana a	Quihace a D	G 1
С	Manning La Doughnasa	Subarea A	Subarea B	Subarea
0.00	Manning's Roughness:	0.40	0.00	
0.00	Flow Length (ft):	222.41	0.00	
0.00	Slope (%):	10.60	0.00	

0.00	2 yr, 24 hr Rainfall (in):	3.60	0.00	
0.00	Velocity (ft/sec):	0.19	0.00	
0.00	Computed Flow Time (minutes):	19.69	0.00	
0.00				
	w Concentrated Flow Computations			
С		Subarea A	Subarea B	Subarea
0.00	Flow Length (ft):	430.84	0.00	
0.00	Slope (%):	3.53	0.00	
Paved	Surface Type:	Paved	Paved	
0.00	Velocity (ft/sec):	3.82	0.00	
0.00	Computed Flow Time (minutes):	1.88	0.00	
	Total TOC (minutes):	21.57		
======			=======================================	
Subbas	in Sub-CB-15-17			
	User-Defined TOC override (minutes):	5.00		
	in Sub-CB-18-19			
	User-Defined TOC override (minutes):	5.00		
	in Sub-CB-20			
Sheet	Flow Computations			
		Subarea A	Subarea B	Subarea
C	Manning's Roughness:	0.40	0.00	
0.00	Flow Length (ft):	227.22	0.00	
0.00	Slope (%):	7.48	0.00	
0.00	2 yr, 24 hr Rainfall (in):	3.60	0.00	
0.00	Velocity (ft/sec):	0.16	0.00	
0.00	Computed Flow Time (minutes):	23.04	0.00	
0.00				
	w Concentrated Flow Computations			
С		Subarea A	Subarea B	Subarea
Ü	Flow Length (ft):	193.35	0.00	

0.00	Slope (%):	2.77	0.00	
0.00	Surface Type:	Paved	Paved	
Paved	Velocity (ft/sec):	3.38	0.00	
0.00	-			
0.00	Computed Flow Time (minutes):	0.95	0.00	
======	Total TOC (minutes):	======================================		
	iotal ioc (minutes).			
Subbasi	n Sub-CB-2-5			
	low Computations			
		Subarea A	Subarea B	Subarea
С	Manning's Roughness:	0.40	0.00	
0.00	Flow Length (ft):	526.06	0.00	
0.00	Slope (%):	1.65	0.00	
0.00	2 yr, 24 hr Rainfall (in):	3.60	0.00	
0.00	Velocity (ft/sec):	0.11	0.00	
0.00	Computed Flow Time (minutes):	82.52	0.00	
	Concentrated Flow Computations			
		Subarea A	Subarea B	Subarea
C	Flow Length (ft):	591.37	0.00	
0.00	Slope (%):	2.70	0.00	
0.00	Surface Type:	Unpaved	Paved	
Paved	Velocity (ft/sec):	2.65	0.00	
0.00	Computed Flow Time (minutes):	3.72	0.00	
0.00				
=======	Total TOC (minutes):	86.24		
======				
	n Sub-CB-6			
	User-Defined TOC override (minutes):	5.00		
	.n Sub-CB-7			

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User-Defined TOC override (minutes): 5.00

Subbasin Sub-CB-8W

User-Defined TOC override (minutes): 5.00

Subbasin Sub-CB-9

User-Defined TOC override (minutes): 5.00

Subbasin ID	Accumulated Precip in	Rainfall Intensity in/hr	Total Runoff in	Peak Runoff cfs	Weighted Runoff Coeff	Conc days	Time of entration hh:mm:ss
Sub-CB-1 Sub-CB-10-11 Sub-CB-12-14 Sub-CB-15-17 Sub-CB-18-19 Sub-CB-20 Sub-CB-2-5	1.11 0.94 1.43 0.73 0.73 1.50 2.39	5.40 6.60 3.98 8.75 8.75 3.75	0.50 0.45 0.43 0.39 0.38 0.50	0.88 1.03 1.93 3.26 4.31 1.85	0.450 0.480 0.300 0.540 0.520 0.330	0 0 0 0 0	00:12:20 00:08:27 00:21:34 00:05:00 00:05:00 00:23:59 01:26:14
Sub-CB-2-3 Sub-CB-6 Sub-CB-7 Sub-CB-8W Sub-CB-9	0.73 0.73 0.73 0.73	8.75 8.75 8.75 8.75	0.43 0.46 0.44 0.47	0.74 0.60 1.18 0.84	0.590 0.630 0.610 0.650	0 0 0 0	00:05:00 00:05:00 00:05:00 00:05:00

Node ID	Average Depth Attained	Maximum Depth Attained	Maximum HGL Attained		ne of Max To ccurrence Floo Vol		Total Time Flooded	Retention Time	
	ft	ft	ft	days	hh:mm	acre-in	minutes	hh:mm:ss	
CIT-8	0.00	0.50	255.30	0	00:05	0	0	0:00:00	
DH-10	0.00	0.28	265.43	0	00:08	0	0	0:00:00	
DH-13	0.01	0.52	260.32	0	00:21	0	0	0:00:00	
DH-20	0.01	0.29	277.91	0	00:24	0	0	0:00:00	
EX-18	3.00	3.65	269.65	0	00:05	0	0	0:00:00	
EX-7	0.00	0.50	253.30	0	00:05	0	0	0:00:00	
Structure - (7	2) 0.11	0.35	276.14	0	00:12	0	0	0:00:00	
DP-1	0.00	0.31	275.31	0	00:12	0	0	0:00:00	
DP-10	0.00	0.28	265.05	0	00:08	0	0	0:00:00	
DP-13	0.01	0.52	260.12	0	00:21	0	0	0:00:00	
DP-16	0.00	0.00	252.66	0	00:00	0	0	0:00:00	
DP-18	0.01	0.55	264.91	0	00:05	0	0	0:00:00	
DP-20	0.01	0.29	274.49	0	00:24	0	0	0:00:00	
DP-5	0.00	0.00	248.00	0	00:00	0	0	0:00:00	
DP-6	0.00	0.00	246.50	0	00:00	0	0	0:00:00	
DP-7	0.00	0.50	253.10	0	00:06	0	0	0:00:00	
Out-01	0.00	0.08	281.30	0	00:16	0	0	0:00:00	

Node ID	Element Type	IIILIOW	cfs	days	hh:mm	C	fs days	s hh:mm
CIT-8	JUNCTION		1.82	0	00:05	0.	00	
DH-10	JUNCTION	1.03	1.03	0	00:08	0.	00	
DH-13	JUNCTION	1.93	1.93	0	00:21	0.	00	
DH-20	JUNCTION	1.85	1.85	0	00:24	0.	00	
EX-18	JUNCTION	0.00	4.30	0	00:05	0.	00	
EX-7	TITATOTTOTT	0.00	1.78	0	00:05	0.	00	
Structure - (72)	JUNCTION	0.00	0.75	0	00:12	0.	00	
Structure - (72) DP-1 DP-10	OUTFALL	0.00	1.78 0.75 0.75 1.03	0	00:12	0.	00	
DP-10	00111111	0.00	1.03	0	00:08	0.	00	
DP-13	OUTFALL OUTFALL	0.00	1.92	0	00:21	0.	00	
DP-16	OUTFALL	3.26	3.26	0	00:05	0.	00	
DP-18	OUTFALL	0.00	1.92 3.26 4.27 1.85	0	00:05	0.		
DP-20		0.00	1.85	0	00:24	0.		
DP-5	OUTFALL	1.50	1.50	0	01:26	0.		
DP-6	OUTFALL OUTFALL OUTFALL OUTFALL	0.74	0.74	0	00:05	0.		
DP-7	OUTFALL	0.60	2.28	0	00:05	0.		
Out-01	OUTFALL	0.00	0.10	U	00.10	0.	00	
**************************************								
Inlet Depth Summar	Y  *  Max Gutter Spread during Peak Flow ft	Max Gu Water du Peak	tter Elev ring Flow ft	Max G Water d Peak	Sutter Depth Suring Flow ft	T M Occu days	ime of aximum Depth rrence hh:mm	
Inlet Depth Summar	Y  *  Max Gutter Spread during Peak Flow ft	Max Gu Water du Peak	tter Elev ring Flow ft	Max G Water d Peak	Sutter Depth luring Flow ft	T M Occu days	ime of aximum Depth rrence hh:mm	
Inlet Depth Summary ***************  Inlet ID  CB-1	Y  *  Max Gutter Spread during Peak Flow ft	Max Gu Water du Peak	tter Elev ring Flow ft	Max G Water d Peak	Sutter Depth luring Flow ft	T M Occu days	ime of aximum Depth rrence hh:mm	
Inlet Depth Summar: *************** Inlet ID CB-1 CB-18 EX-CB15	Y  *  Max Gutter Spread during Peak Flow ft	Max Gu Water du Peak	tter Elev ring Flow ft	Max G Water d Peak	Jutter Depth Juring Flow ft 0.20 0.40 0.09	T M Occu days 0 0	ime of aximum Depth rrence hh:mm 00:12 00:05 00:07	
Inlet Depth Summar: ***************  Inlet ID  CB-1 CB-18 EX-CB15	Y  *  Max Gutter Spread during Peak Flow ft	Max Gu Water : du Peak :	tter Elev ring Flow ft	Max G Water d Peak	Jutter Depth Juring Flow ft 0.20 0.40 0.09	T M Occu days	ime of aximum Depth rrence hh:mm 00:12 00:05 00:07	
Inlet Depth Summar: ***************  Inlet ID  CB-1 CB-18 EX-CB15 EX-CB-16	Y  *  Max Gutter Spread during Peak Flow ft	Max Gu Water du Peak	tter Elev ring Flow ft	Max G Water d Peak	Jutter Depth Juring Flow ft 0.20 0.40 0.09	T M Occu days 0 0	ime of aximum Depth rrence hh:mm 00:12 00:05 00:07	
Inlet Depth Summar: **************  Inlet ID	Max Gutter Spread during Peak Flow ft  5.78 14.81 1.41 5.62	Max Gu Water du Peak	tter Elev ring Flow ft	Max G Water d Peak	Jutter Depth Juring Flow ft 0.20 0.40 0.09	T M Occu days 0 0	ime of aximum Depth rrence hh:mm 00:12 00:05 00:07	
Inlet Depth Summary ****************  Inlet ID  CB-1 CB-18 EX-CB15 EX-CB-16  ***************** Inlet Flow Summary *****************  Inlet	Max Gutter Spread during Peak Flow ft  5.78 14.81 1.41 5.62	Max Gu Water du Peak	tter Elev ring Flow ft 	Max G Water G Peak	Sutter Depth luring Flow ft 0.20 0.40 0.09 0.20	T M Occu days 0 0	ime of aximum Depth rrence hh:mm 00:12 00:05 00:07 00:05	
Inlet Depth Summary ************************************	Max Gutter Spread during Peak Flow ft  5.78 14.81 1.41 5.62	Max Gu Water: du Peak: 28 27 25 26	tter Elev ring Flow ft 1.42 4.12 9.29 2.50	Max G Water d Peak	Sutter Depth Suring Flow Ft 0.20 0.40 0.09 0.20	Occudays Occu Occudays Occudays Occudays Occudays Occudays Occudays	ime of aximum Depth rrence hh:mm 00:12 00:05 00:07 00:05	Total
Inlet Depth Summary ****************  Inlet ID  CB-1 CB-18 EX-CB15 EX-CB-16  ***************** Inlet Flow Summary *****************  Inlet tital	Max Gutter Spread during Peak Flow ft  5.78 14.81 1.41 5.62	Max Gu Water: du: Peak: 28 27 25 26 Peak Lateral	tter Elev ring Flow ft 1.42 4.12 9.29 2.50	Max G Water G Peak	Sutter Depth Suring Flow ft 0.20 0.40 0.09 0.20	Occudays Occudays O O O O O O O O O O O O O O O O O O O	ime of aximum Depth rrence hh:mm 00:12 00:05 00:07 00:05	y Flooding

_						
CB-1 0	0.88	0.88	0.76	0.12	86.02	0.000
CB-18	4.31	4.31	-	_	-	0.000
EX-CB15	0.08	0.00	0.08	0.00	100.00	0.000
0 EX-CB-16	0.84	0.84	0.73	0.11	86.91	0.000

Outfall Node ID	Flow	Average	Peak
	Frequency	Flow	Inflow
	(%)	cfs	cfs
DP-1 DP-10 DP-13 DP-16 DP-18 DP-20 DP-5 DP-6 DP-7 Out-01	1.92	0.36	0.75
	1.19	0.51	1.03
	3.01	0.96	1.92
	0.69	1.63	3.26
	0.88	1.70	4.27
	3.39	0.91	1.85
	11.96	0.75	1.50
	0.69	0.37	0.74
	1.97	0.45	2.28
	2.79	0.03	0.10
System	2.85	7.66	12.21

Link ID		Element	Т	ime of	Maximum	Length	Peak Flow	Design	Ratio of
Ratio of	То	tal Reported Type	Doo	le Elou	Wologitu	Engton	during	Flow	Maximum
Maximum	Ti	me Condition	Pea	K FIOW	velocity	ractor	during	FIOW	MaxIllulli
			Occu	rrence	Attained		Analysis	Capacity	/Design
Flow Surcharg	jed		darra	hh:mm	ft/sec		cfs	cfs	Flow
Depth minu	ıtes		uays	1111•111111	IC/Sec		CIS	CIS	FIOW
-									
CB-1_Overflo	w	CHANNEL	0	00:16	1.85	1.00	0.10	2.70	0.04
0.28	0	Calculated							
CIT-9_Overfl	.OW	CHANNEL	0	00:07	3.83	1.00	0.08	7.01	0.01
0.18	0	Calculated							
Link-17		CONDUIT	0	00:07	0.91	1.00	0.08	4.07	0.02
0.10	0	Calculated							
Link-18		CHANNEL	0	00:10	0.99	1.00	0.00	10.44	0.00
0.04	0	Calculated							
Pipe - (21)		CONDUIT	0	00:05	4.66	1.00	1.78	3.59	0.49
0.50	0	Calculated							
Pipe - (22)		CONDUIT	0	00:06	4.53	1.00	1.78	3.56	0.50
0.50	0	Calculated							
Pipe - (25)		CONDUIT	0	00:05	7.08	1.00	0.69	3.88	0.18
0.28	0	Calculated							

_	CONDUIT	0	00:21	4.63	1.00	1.92	3.56	0.54
0			00.05	F 00	1 00	4 20	F 63	0 86
	CONDULT	0	00:05	7.92	1.00	4.30	5.63	0.76
0	Calculated							
	CONDUIT	0	00:05	7.31	1.00	4.27	14.86	0.29
0	Calculated							
	CONDUIT	0	00:08	5.83	1.00	1.03	6.17	0.17
0	Calculated							
	CONDUIT	0	00:24	7.72	1.00	1.85	22.60	0.08
0	Calculated							
	CONDUIT	0	00:12	5.84	1.00	0.75	5.92	0.13
0	Calculated							
	CONDUIT	0	00:12	3.61	1.00	0.75	3.56	0.21
0	Calculated							
	0 0 0	O Calculated CONDUIT Calculated	O Calculated CONDUIT O Calculated	O Calculated	O Calculated	O Calculated	O Calculated CONDUIT O 00:05 7.92 1.00 4.30  Calculated CONDUIT O 00:05 7.31 1.00 4.27  Calculated CONDUIT O 00:08 5.83 1.00 1.03  Calculated CONDUIT O 00:24 7.72 1.00 1.85  Calculated CONDUIT O 00:12 5.84 1.00 0.75  Calculated CONDUIT O 00:12 3.61 1.00 0.75	O Calculated CONDUIT O 00:05 7.92 1.00 4.30 5.63  O Calculated CONDUIT O 00:05 7.31 1.00 4.27 14.86  O Calculated CONDUIT O 00:08 5.83 1.00 1.03 6.17  O Calculated CONDUIT O 00:24 7.72 1.00 1.85 22.60  O Calculated CONDUIT O 00:12 5.84 1.00 0.75 5.92  O Calculated CONDUIT O 00:12 3.61 1.00 0.75 3.56

All links are stable.

WARNING 108: Surcharge elevation defined for Junction EX-18 is below junction maximum elevation. Assumed surcharge elevation equal to maximum elevation.

WARNING 139 : Ponded area defined for on sag Inlet CB-18 is zero. Assumed ponded area equal to 10 ft $^2$  (0.929 m $^2$ ).

WARNING 138 : Initial water surface elevation defined for Inlet EX-CB15 is below catchbasin invert elevation.

Assumed initial water surface elevation equal to catchbasin inlet invert

elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB-1\_Overflow

is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CIT-9\_Overflow is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 117: Conduit outlet invert elevation defined for Conduit CB-1\_Overflow is below downstream node invert elevation.

Assumed conduit outlet invert elevation equal to downstream node invert

elevation.

WARNING 004 : Minimum elevation drop used for Conduit CB-1\_Overflow.

WARNING 005 : Minimum slope used for Conduit CB-1\_Overflow.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CIT-9\_Overflow is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet EX-CB15.

WARNING 116: Conduit inlet invert elevation defined for Conduit Link-17 is below upstream node invert elevation.

Assumed conduit inlet invert elevation equal to upstream node invert elevation.

WARNING 004: Minimum elevation drop used for Conduit Link-17.

WARNING 005 : Minimum slope used for Conduit Link-17.

Analysis began on: Tue Jan 31 11:03:56 2023 Analysis ended on: Tue Jan 31 11:03:58 2023

Total elapsed time: 00:00:02

```
Autodesk® Storm and Sanitary Analysis 2016 - Version 13.2.165 (Build 0)
Project Description
******
File Name ..... Grove_St_Ph2_r1-EX.SPF
******
Analysis Options
******
Flow Units ..... cfs
Subbasin Hydrograph Method. Rational
Time of Concentration..... SCS TR-55
Return Period..... 100 years
Link Routing Method ..... Kinematic Wave Storage Node Exfiltration. None
Starting Date ..... DEC-20-2022 00:00:00
Ending Date ..... DEC-21-2022 00:00:00
Report Time Step ...... 00:00:10
******
Element Count
Number of subbasins ..... 11
Number of nodes ..... 21
Number of links ..... 14
******
Subbasin Summary
******
Subbasin
                     Total
                       Area
TD
                      acres
                    0.36
0.33
Sub-CB-1
Sub-CB-10-11
                     1.61
0.69
Sub-CB-12-14
Sub-CB-15-17
                      0.95
Sub-CB-18-19
                      1.49
3.91
Sub-CB-20
Sub-CB-2-5
Sub-CB-6
                      0.14
Sub-CB-7
                       0.11
Sub-CB-8W
                       0.22
Sub-CB-9
                       0.15
*****
Node Summary
*****
                  Node
ID
CIT-8 JUNCTION 254.80 259.42 0.00 DH-10 JUNCTION 265.15 268.15 0.00 DH-13 JUNCTION 259.80 265.60 0.00 TUNCTION 277.62 279.12 0.00
______
DH-13 JUNCTION
DH-20 JUNCTION
EX-18 JUNCTION
EX-7 JUNCTION
Structure - (72) JUNCTION
                                266.00 273.24 0.00
252.80 258.62 0.00
275.79 277.57 0.00
```

DP-1 DP-10 DP-13 DP-16 DP-18 DP-20 DP-5 DP-6 DP-7 Out-01		OUTFA	LL LL LL LL LL LL LL	264 259 252 264 274 248 246 252	5.00 4.78 9.60 2.66 4.36 4.20 8.00 6.50 2.60 1.22	276.00 265.78 260.60 252.66 265.86 275.70 248.00 246.50 253.60 281.50	0. 0. 0. 0. 0. 0. 0. 0.	00 00 00 00 00 00 00 00			
*********** Inlet Summ *****	ary										
Inlet		Inlet				Manufactur	er	I	nlet	Number	
Catchbasin			Ponded	Initia	al	Grate				_	
ID	D.		acturer		<b>a</b> 1	Part		L	ocation	of	
Invert	K.	im Ar	ea	Water	CTO	gging Number				Inlets	
Elevation	Eleva	ation		Elevation	n	Factor				1111000	
ft	ft	ft²		ft	9	8					
CB-1		FHWA	HEC-22	GENERIC		N/A		0:	n Grade	1	
278.10	281.2	22	_	278.10		0.00					
CB-18		FHWA	HEC-22	GENERIC		N/A		O:	n Sag	1	
269.61	273.7	72 10.	00	269.61		0.00					
EX-CB15		FHWA	HEC-22	GENERIC		N/A		O:	n Grade	1	
254.80	259.2		-	254.80		0.00					
EX-CB-16			HEC-22	GENERIC		N/A		O:	n Grade	1	
257.40	262.3	30	-	257.40		0.00					
********* Roadway an ******* Inlet ID	ıd Gutt	er Summar	У	Cross Slope		Roadway anning's oughness	Gutter Cross Slope ft/ft	Gutter Width ft	Depre	utter ssion in	
CB-1			0.0100	0.0200		0.0160	0.0620	2.00		2.00	
CB-18			-	0.0200		0.0160	0.0620	2.00		2.00	
EX-CB15			0.0100	0.0200		0.0160	0.0620	2.00		2.00	
EX-CB-16			0.0100	0.0200		0.0160	0.0620	2.00		2.00	
**************************************	ry										
Link ID		From Node		To Node		Element Type	1	Length ft	Slope %	Manning Roughnes	
CB-1_Overf		CB-1		Out-01		CHANNEL		241.8	0.2000	0.013	
CIT-9_Over	ilow	EX-CB-16		EX-CB15		CHANNEL		230.0	1.3478	0.013	
Link-17		EX-CB15		CIT-8		CONDUIT		8.9	0.2000	0.015	
Link-18	,	EX-CB15		DP-7		CHANNEL		220.5	2.9927	0.013	
Pipe - (21		CIT-8		EX-7		CONDUIT		196.9	1.0156	0.013	
Pipe - (22		EX-7		DP-7		CONDUIT		20.0	1.0000	0.013	
Pipe - (25		EX-CB-16		CIT-8		CONDUIT		219.0	1.1872	0.013	
Pipe - (33 Pipe - (44		DH-13 CB-18		DP-13 EX-18		CONDUIT		19.5 24.4	1.0000 2.4990	0.013	
Pipe - (44 Pipe - (45		EX-18		DP-18		CONDUIT CONDUIT		81.8	2.4990	0.013	
1150 (13	,	-41 10				00110011		01.0	2.0000	0.01	- 0

Pipe - (56) Pipe - (57) Pipe - (61) Pipe - (62)	DH-10 DH-20 CB-1 Structure		CONDUIT CONDUIT - (72)CONDUIT CONDUIT	55.! 79.8	6.1644 3 2.7583	0.0130 0.0150 0.0130 0.0130
********	*****					
Cross Section						
Link	Shape	Depth/	Width	No. of	Cross	Full Flow
Design ID		Diameter		Barrels	Sectional	Hydraulic
Flow					Area	Radius
Capacity		ft	ft		ft²	ft
cfs						
CB-1_Overflow 2.70	TRIANGULA	R 0.28	14.00	1	1.96	0.14
CIT-9_Overflow	TRIANGULA	R 0.28	14.00	1	1.96	0.14
7.01 Link-17	CIRCULAR	1.50	1.50	1	1.77	0.38
4.07 Link-18	TRIANGULA	R 0.28	14.00	1	1.96	0.14
10.44 Pipe - (21)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.59 Pipe - (22)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.56 Pipe - (25)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.88			1.00	1	0.79	0.25
Pipe - (33) 3.56	CIRCULAR	1.00				
Pipe - (44) 5.63	CIRCULAR	1.00	1.00	1	0.79	0.25
Pipe - (45) 14.86	CIRCULAR	1.50	1.50	1	1.77	0.38
Pipe - (56) 6.17	CIRCULAR	1.00	1.00	1	0.79	0.25
Pipe - (57) 22.60	CIRCULAR	1.50	1.50	1	1.77	0.38
Pipe - (61) 5.92	CIRCULAR	1.00	1.00	1	0.79	0.25
Pipe - (62) 3.56	CIRCULAR	1.00	1.00	1	0.79	0.25
********** Transect Summary ************ Transect XS-L-Pipe - (13)						
Area:	_	010 0 0042	0 0076	0 0110		
0. 0. 0. 0. 0. 0.	0005 0.0 0170 0.0 0595 0.0 1312 0.1 2323 0.2 3604 0.3 4937 0.5 6269 0.6 7602 0.7	232 0.0305 715 0.0847 491 0.1682 561 0.2810 871 0.4137 203 0.5470 536 0.6802 868 0.8135	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668		
0.	8934 0.9	201 0.9467	0.9734	1.0000		

Hrad:					
Width:	0.0139 0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005	0.0278 0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995 0.9256	0.0418 0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.0557 0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.0696 0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754 1.0000
	0.0355 0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000	0.0711 0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000 1.0000	0.1066 0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000 1.0000	0.1422 0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000 1.0000	0.1777 0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000
Transect :	XS-L-Pipe -	(16)			
Hrad:	0.0005 0.0170 0.0595 0.1312 0.2323 0.3604 0.4937 0.6269 0.7602 0.8934	0.0019 0.0232 0.0715 0.1491 0.2561 0.3871 0.5203 0.6536 0.7868 0.9201	0.0043 0.0305 0.0847 0.1682 0.2810 0.4137 0.5470 0.6802 0.8135 0.9467	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401 0.9734	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668 1.0000
iii au	0.0139 0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005	0.0278 0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995 0.9256	0.0418 0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.0557 0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.0696 0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754
Width:	0.0355 0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000	0.0711 0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000	0.1066 0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000	0.1422 0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000	0.1777 0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000
Transect 2	XS-L-Pipe -	(18)			
Area:	0.0005 0.0170 0.0595 0.1312 0.2323 0.3604	0.0019 0.0232 0.0715 0.1491 0.2561 0.3871	0.0043 0.0305 0.0847 0.1682 0.2810 0.4137	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670

	0.4937 0.6269	0.5203 0.6536	0.5470 0.6802	0.5736 0.7069	0.6003 0.7335
	0.7602	0.7868	0.8135	0.8401	0.7333
	0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:					
	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835 0.1459	0.0963 0.1591	0.1080 0.1724	0.1202 0.1858	0.1329 0.1994
	0.2130	0.2267	0.2404	0.2542	0.2680
	0.2818	0.2957	0.3095	0.3238	0.3512
	0.3784	0.4055	0.4326	0.4595	0.4863
	0.5130 0.6448	0.5396 0.6708	0.5660 0.6968	0.5924 0.7226	0.6187 0.7483
	0.7740	0.7995	0.8249	0.8502	0.7403
	0.9005	0.9256	0.9505	0.9753	1.0000
Width:					
	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132 0.4283	0.2520 0.4724	0.2961 0.5164	0.3402 0.5605	0.3842
	0.6487	0.6927	0.7368	0.7809	0.8249
	0.8690	0.9131	0.9572	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000 1.0000	1.0000	1.0000 1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
Transect Area:	XS-L-Pipe -	(2)			
AI Ca.	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312 0.2323	0.1491 0.2561	0.1682 0.2810	0.1884 0.3071	0.2098
	0.2323	0.3871	0.2810	0.4404	0.3336
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602 0.8934	0.7868 0.9201	0.8135 0.9467	0.8401 0.9734	0.8668
Hrad:	0.0934	0.9201	0.9467	0.9/34	1.0000
	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835	0.0963	0.1080	0.1202	0.1329
	0.1459	0.1591	0.1724	0.1858 0.2542	0.1994
	0.2130 0.2818	0.2267 0.2957	0.2404 0.3095	0.3238	0.2680 0.3512
	0.3784	0.4055	0.4326	0.4595	0.4863
	0.5130	0.5396	0.5660	0.5924	0.6187
	0.6448	0.6708	0.6968	0.7226	0.7483
	0.7740 0.9005	0.7995 0.9256	0.8249 0.9505	0.8502 0.9753	0.8754 1.0000
Width:	0.7003	0.7250	0.7505	0.7755	2.0000
	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132	0.2520	0.2961	0.3402	0.3842
	0.4283 0.6487	0.4724 0.6927	0.5164 0.7368	0.5605 0.7809	0.6046 0.8249
	0.8690	0.9131	0.9572	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000 1.0000	1.0000	1.0000 1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	XS-L-Pipe -	(24)			
Area:	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487

w	0.0595 0.1312 0.2323 0.3604 0.4937 0.6269 0.7602 0.8934	0.0715 0.1491 0.2561 0.3871 0.5203 0.6536 0.7868 0.9201	0.0847 0.1682 0.2810 0.4137 0.5470 0.6802 0.8135 0.9467	0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401 0.9734	0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668 1.0000
<pre>Hrad:</pre> <pre>Width:</pre>	0.0139 0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005	0.0278 0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995	0.0418 0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.0557 0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.0696 0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754
	0.0355 0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000	0.0711 0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000 1.0000	0.1066 0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000	0.1422 0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000 1.0000	0.1777 0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000
Transect XS Area:	-L-Pipe -	(27)			
Hrad:	0.0005 0.0170 0.0595 0.1312 0.2323 0.3604 0.4937 0.6269 0.7602 0.8934	0.0019 0.0232 0.0715 0.1491 0.2561 0.3871 0.5203 0.6536 0.7868 0.9201	0.0043 0.0305 0.0847 0.1682 0.2810 0.4137 0.5470 0.6802 0.8135 0.9467	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401 0.9734	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668 1.0000
	0.0139 0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005	0.0278 0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995 0.9256	0.0418 0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.0557 0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.0696 0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754 1.0000
Width:	0.0355 0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000 1.0000	0.0711 0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000	0.1066 0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000	0.1422 0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000	0.1777 0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000

Transect :	XS-L-Pipe -	(28)			
Alea.	0.0005 0.0170 0.0595 0.1312 0.2323 0.3604 0.4937 0.6269 0.7602 0.8934	0.0019 0.0232 0.0715 0.1491 0.2561 0.3871 0.5203 0.6536 0.7868 0.9201	0.0043 0.0305 0.0847 0.1682 0.2810 0.4137 0.5470 0.6802 0.8135 0.9467	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401 0.9734	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668 1.0000
Hrad:	0.0551	0.5201	0.5107	0.5751	1.0000
	0.0139 0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005	0.0278 0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995 0.9256	0.0418 0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.0557 0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.0696 0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754 1.0000
Width:	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000	0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000 1.0000	0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000 1.0000	0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000	0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000 1.0000
	XS-L-Pipe -	(30)			
Area:	0.0005 0.0170 0.0595 0.1312 0.2323 0.3604 0.4937 0.6269 0.7602 0.8934	0.0019 0.0232 0.0715 0.1491 0.2561 0.3871 0.5203 0.6536 0.7868 0.9201	0.0043 0.0305 0.0847 0.1682 0.2810 0.4137 0.5470 0.6802 0.8135 0.9467	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401 0.9734	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668 1.0000
Hrad:					
Width:	0.0139 0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005	0.0278 0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995 0.9256	0.0418 0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.0557 0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.0696 0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754 1.0000
	0.0355 0.2132 0.4283 0.6487 0.8690 1.0000	0.0711 0.2520 0.4724 0.6927 0.9131 1.0000	0.1066 0.2961 0.5164 0.7368 0.9572 1.0000	0.1422 0.3402 0.5605 0.7809 1.0000 1.0000	0.1777 0.3842 0.6046 0.8249 1.0000 1.0000

1.000	1.0000	1.0000	1.0000	1.0000
1.0000		1.0000	1.0000	1.0000
1.0000		1.0000	1.0000	1.0000
1.0000	1.0000	1.0000	1.0000	1.0000
Twomacat VC I Din	. (27)			
Transect XS-L-Pipe	= - (3/)			
Area:	- 0.0010	0 0040	0 0000	0 0110
0.000!		0.0043	0.0076	0.0118
0.0170		0.0305	0.0390	0.0487
0.059		0.0847	0.0990	0.1145
0.131		0.1682	0.1884	0.2098
0.2323		0.2810	0.3071	0.3338
0.360		0.4137	0.4404	0.4670
0.493		0.5470	0.5736	0.6003
0.6269	0.6536	0.6802	0.7069	0.7335
0.760	2 0.7868	0.8135	0.8401	0.8668
0.893	4 0.9201	0.9467	0.9734	1.0000
Hrad:				
0.0139	9 0.0278	0.0418	0.0557	0.0696
0.083	0.0963	0.1080	0.1202	0.1329
0.1459	0.1591	0.1724	0.1858	0.1994
0.213	0.2267	0.2404	0.2542	0.2680
0.2818	0.2957	0.3095	0.3238	0.3512
0.378		0.4326	0.4595	0.4863
0.513		0.5660	0.5924	0.6187
0.644		0.6968	0.7226	0.7483
0.774		0.8249	0.8502	0.8754
0.900!		0.9505	0.9753	1.0000
Width:	0.5250	0.5505	0.5755	1.0000
0.035	0.0711	0.1066	0.1422	0.1777
0.033		0.2961	0.3402	0.3842
0.4283		0.5164	0.5605	0.6046
			0.7809	
0.648		0.7368		0.8249
0.8690		0.9572	1.0000	1.0000
1.0000		1.0000	1.0000	1.0000
1.0000		1.0000	1.0000	1.0000
1.0000		1.0000	1.0000	1.0000
1.0000		1.0000	1.0000	1.0000
1.0000	1.0000	1.0000	1.0000	1.0000
Transect XS-L-Pipe	e - (50)			
Area:				
0.000!	5 0.0019	0.0043	0.0076	0.0118
0.0170	0.0232	0.0305	0.0390	0.0487
0.059	5 0.0715	0.0847	0.0990	0.1145
0.131	2 0.1491	0.1682	0.1884	0.2098
0.232	3 0.2561	0.2810	0.3071	0.3338
0.360	4 0.3871	0.4137	0.4404	0.4670
0.493	7 0.5203	0.5470	0.5736	0.6003
0.6269	0.6536	0.6802	0.7069	0.7335
0.760	2 0.7868	0.8135	0.8401	0.8668
0.893	4 0.9201	0.9467	0.9734	1.0000
Hrad:				
0.013	0.0278	0.0418	0.0557	0.0696
0.083		0.1080	0.1202	0.1329
0.1459		0.1724	0.1858	0.1994
0.213		0.2404	0.2542	0.2680
0.2818		0.3095	0.3238	0.3512
0.378		0.4326	0.4595	0.4863
0.576		0.4320	0.5924	0.4003
0.6448		0.6968	0.7226	0.7483
0.774		0.8249	0.8502	0.8754
0.900!	0.9256	0.9505	0.9753	1.0000
Width:	- 0 0511	0 1000	0 1400	0 1000
0.035		0.1066	0.1422	0.1777
0.213		0.2961	0.3402	0.3842
0.4283	3 0.4724	0.5164	0.5605	0.6046

	0.6487 0.8690 1.0000 1.0000 1.0000 1.0000	0.6927 0.9131 1.0000 1.0000 1.0000 1.0000	0.7368 0.9572 1.0000 1.0000 1.0000 1.0000	0.7809 1.0000 1.0000 1.0000 1.0000 1.0000	0.8249 1.0000 1.0000 1.0000 1.0000 1.0000
	KS-L-Pipe -	(55)			
Area:	0.0005 0.0170 0.0595 0.1312 0.2323 0.3604 0.4937 0.6269 0.7602 0.8934	0.0019 0.0232 0.0715 0.1491 0.2561 0.3871 0.5203 0.6536 0.7868 0.9201	0.0043 0.0305 0.0847 0.1682 0.2810 0.4137 0.5470 0.6802 0.8135 0.9467	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401 0.9734	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668 1.0000
	0.0139 0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005	0.0278 0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995 0.9256	0.0418 0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.0557 0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.0696 0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754 1.0000
Width:	0.0355 0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000 1.0000	0.0711 0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000	0.1066 0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000	0.1422 0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000	0.1777 0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000
******	******	****	Volume	Depth	
	ntity Conti		acre-ft	inches	
	cipitation . Error (%)		1.719 0.706	2.070	
Flow Routi	************ .ng Continui	.ty	Volume acre-ft	Volume Mgallons	
External I External C Initial St Final Stor	Inflow Outflow Cored Volume red Volume . red Frror (%)	2	0.000 0.505 0.000 0.000 -0.042	0.000 0.165 0.000 0.000	
Runoff Coe	************ efficient Co	mputations	s Report		

Autodesk Storm and Sanitary Analysis

Subbasin Sub-CB-1			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.12 0.25 0.36	A (6%+) A (6%+)	0.79 0.29 0.45
Subbasin Sub-CB-10-11			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.17 0.16 0.33	A (6%+) A (6%+)	0.79 0.14 0.48
Subbasin Sub-CB-12-14			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.39 1.23 1.61	A (6%+) A (6%+)	0.79 0.14 0.30
Subbasin Sub-CB-15-17			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Streets, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.17 0.35 0.16 0.69	A (6%+) A (6%+) B (0-2%)	0.79 0.29 0.80 0.54
Subbasin Sub-CB-18-19			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.44 0.51 0.95	A (6%+) A (6%+)	0.79 0.29 0.52
Subbasin Sub-CB-20			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.45 1.05 1.49	A (6%+) A (6%+)	0.79 0.14 0.33
Subbasin Sub-CB-2-5			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.

Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.55 3.36 3.91	A (6%+) A (6%+)	0.79 0.14 0.23
Subbasin Sub-CB-6			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.09 0.05 0.14	A (2-6%) A (6%+)	0.77 0.29 0.59
Subbasin Sub-CB-7			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.08 0.03 0.11	A (0-2%) A (2-6%)	0.76 0.26 0.63
Subbasin Sub-CB-8W			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Meadow, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.16 0.06 0.22	A (2-6%) A (2-6%)	0.77 0.22 0.61
Subbasin Sub-CB-9			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.11 0.03 0.15	A (2-6%) A (2-6%)	0.77 0.26 0.65
**************************************			
Sheet Flow Equation			
$Tc = (0.007 * ((n * Lf)^0.8)) / ((P^0.5) * (S))$	Sf^0.4))		
Where:			
<pre>Tc = Time of Concentration (hrs) n = Manning's Roughness Lf = Flow Length (ft) P = 2 yr, 24 hr Rainfall (inches) Sf = Slope (ft/ft)</pre>			
Shallow Concentrated Flow Equation			
<pre>V = 16.1345 * (Sf^0.5) (unpaved surface)</pre>			

```
V = 20.3282 * (Sf^0.5) (paved surface)
          V = 15.0 * (Sf^0.5) (grassed waterway surface)
          V = 10.0 * (Sf^0.5) (nearly bare & untilled surface)
            = 9.0 * (Sf^0.5) (cultivated straight rows surface)
          V = 7.0 * (Sf^0.5) (short grass pasture surface)
          V = 5.0 * (Sf^0.5) \text{ (woodland surface)}
          V = 2.5 * (Sf^0.5) (forest w/heavy litter surface)
          Tc = (Lf / V) / (3600 sec/hr)
          Where:
          Tc = Time of Concentration (hrs)
          Lf = Flow Length (ft)
          V = Velocity (ft/sec)
          Sf = Slope (ft/ft)
 Channel Flow Equation
          V = (1.49 * (R^{(2/3)}) * (Sf^{0.5})) / n
          R = Aq / Wp
          Tc = (Lf / V) / (3600 sec/hr)
          Where:
          Tc = Time of Concentration (hrs)
          Lf = Flow Length (ft)
          R = Hydraulic Radius (ft)
          Aq = Flow Area (ft<sup>2</sup>)
          Wp = Wetted Perimeter (ft)
          V = Velocity (ft/sec)
          Sf = Slope (ft/ft)
         n = Manning's Roughness
 Subbasin Sub-CB-1
 Sheet Flow Computations
                                                 Subarea A
                                                                     Subarea B
                                                                                          Subarea
         Manning's Roughness:
                                                      0.40
                                                                           0.00
0.00
          Flow Length (ft):
                                                     33.69
                                                                           0.00
0.00
         Slope (%):
                                                      1.60
                                                                           0.00
0.00
          2 yr, 24 hr Rainfall (in):
                                                                           0.00
                                                      3.60
0.00
                                                      0.06
                                                                           0.00
          Velocity (ft/sec):
0.00
          Computed Flow Time (minutes):
                                                      9.26
                                                                           0.00
0.00
 Shallow Concentrated Flow Computations
                                                                     Subarea B
                                                 Subarea A
                                                                                          Subarea
                                                                           0.00
          Flow Length (ft):
                                                    329.84
0.00
          Slope (%):
                                                      0.77
                                                                           0.00
0.00
         Surface Type:
                                                     Paved
                                                                         Paved
Paved
                                                                          0.00
         Velocity (ft/sec):
                                                     1.79
```

С

C

0.00		2 00	0.00	
0.00	Computed Flow Time (minutes):	3.08	0.00	
======				========
	Total TOC (minutes):	12.34		
======		:========:	===========	========
	in Sub-CB-10-11 			
	Flow Computations			
		Subarea A	Subarea B	Subarea
C	Manning's Roughness:	0.40	0.00	
0.00	Flow Length (ft):	82.40	0.00	
0.00	Slope (%):	22.88	0.00	
0.00	2 yr, 24 hr Rainfall (in):	3.60	0.00	
0.00	Velocity (ft/sec):	0.21	0.00	
0.00	Computed Flow Time (minutes):	6.54	0.00	
	w Concentrated Flow Computations			
		Subarea A	Subarea B	Subarea
С	Flow Length (ft):	332.66	0.00	
0.00	Slope (%):	2.02	0.00	
0.00	Surface Type:	Paved	Paved	
Paved	Velocity (ft/sec):	2.89	0.00	
0.00	Computed Flow Time (minutes):	1.92	0.00	
0.00				
======	Total TOC (minutes):	8.46	==========	========
======		:========:		========
	in Sub-CB-12-14			
sneet :	Flow Computations	Gulana a	Quihace a D	G 1
С	Manning La Doughnasa	Subarea A	Subarea B	Subarea
0.00	Manning's Roughness:	0.40	0.00	
0.00	Flow Length (ft):	222.41	0.00	
0.00	Slope (%):	10.60	0.00	

0.00	2 yr, 24 hr Rainfall (in):	3.60	0.00	
0.00	Velocity (ft/sec):	0.19	0.00	
0.00	Computed Flow Time (minutes):	19.69	0.00	
0.00				
	w Concentrated Flow Computations			
С		Subarea A	Subarea B	Subarea
0.00	Flow Length (ft):	430.84	0.00	
0.00	Slope (%):	3.53	0.00	
Paved	Surface Type:	Paved	Paved	
0.00	Velocity (ft/sec):	3.82	0.00	
0.00	Computed Flow Time (minutes):	1.88	0.00	
	Total TOC (minutes):	21.57		
======			=======================================	
Subbas	in Sub-CB-15-17			
	User-Defined TOC override (minutes):	5.00		
	in Sub-CB-18-19			
	User-Defined TOC override (minutes):	5.00		
	in Sub-CB-20			
Sheet	Flow Computations			
		Subarea A	Subarea B	Subarea
C	Manning's Roughness:	0.40	0.00	
0.00	Flow Length (ft):	227.22	0.00	
0.00	Slope (%):	7.48	0.00	
0.00	2 yr, 24 hr Rainfall (in):	3.60	0.00	
0.00	Velocity (ft/sec):	0.16	0.00	
0.00	Computed Flow Time (minutes):	23.04	0.00	
0.00				
	w Concentrated Flow Computations			
С		Subarea A	Subarea B	Subarea
Ü	Flow Length (ft):	193.35	0.00	

0.00	Slope (%):	2.77	0.00	
0.00	Surface Type:	Paved	Paved	
Paved	Velocity (ft/sec):	3.38	0.00	
0.00	-			
0.00	Computed Flow Time (minutes):	0.95	0.00	
======	Total TOC (minutes):	======================================		
	iotal ioc (minutes).			
Subbasi	n Sub-CB-2-5			
	low Computations			
		Subarea A	Subarea B	Subarea
С	Manning's Roughness:	0.40	0.00	
0.00	Flow Length (ft):	526.06	0.00	
0.00	Slope (%):	1.65	0.00	
0.00	2 yr, 24 hr Rainfall (in):	3.60	0.00	
0.00	Velocity (ft/sec):	0.11	0.00	
0.00	Computed Flow Time (minutes):	82.52	0.00	
	Concentrated Flow Computations			
		Subarea A	Subarea B	Subarea
C	Flow Length (ft):	591.37	0.00	
0.00	Slope (%):	2.70	0.00	
0.00	Surface Type:	Unpaved	Paved	
Paved	Velocity (ft/sec):	2.65	0.00	
0.00	Computed Flow Time (minutes):	3.72	0.00	
0.00				
=======	Total TOC (minutes):	86.24		
======				
	n Sub-CB-6			
	User-Defined TOC override (minutes):	5.00		
	.n Sub-CB-7			

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User-Defined TOC override (minutes): 5.00

Subbasin Sub-CB-8W

User-Defined TOC override (minutes): 5.00

Subbasin Sub-CB-9

User-Defined TOC override (minutes): 5.00

Subbasin ID	Accumulated Precip in	Rainfall Intensity in/hr	Total Runoff in	Peak Runoff cfs	Weighted Runoff Coeff	Conc days	Time of entration
Sub-CB-1	1.41	6.86	0.63	1.12	0.450	0	00:12:20
Sub-CB-10-11	1.19	8.39	0.57	1.31	0.480	0	00:08:27
Sub-CB-12-14	1.82	5.07	0.54	2.45	0.300	0	00:21:34
Sub-CB-15-17	0.93	11.10	0.50	4.14	0.540	0	00:05:00
Sub-CB-18-19	0.93	11.10	0.48	5.47	0.520	0 0 0	00:05:00
Sub-CB-20	1.91	4.78	0.63	2.36	0.330		00:23:59
Sub-CB-2-5	3.03	2.11	0.70	1.90	0.230		01:26:14
Sub-CB-6	0.93	11.10	0.55	0.93	0.590		00:05:00
Sub-CB-7	0.93	11.10	0.58	0.76	0.630	0	00:05:00
Sub-CB-8W	0.93	11.10	0.56	1.49	0.610	0	00:05:00
Sub-CB-9	0.93	11.10	0.60	1.06	0.650	0	00:05:00

Node ID	Average Depth Attained	Maximum Depth Attained	Maximum HGL Attained		of Max urrence	Total Flooded Volume	Total Time Flooded	Retention Time
	ft	ft	ft	days	hh:mm	acre-in	minutes	hh:mm:ss
CIT-8	0.00	0.58	255.38	0	00:05	0	0	0:00:00
DH-10	0.00	0.31	265.46	0	00:08	0	0	0:00:00
DH-13	0.01	0.61	260.41	0	00:21	0	0	0:00:00
DH-20	0.01	0.33	277.95	0	00:24	0	0	0:00:00
EX-18	3.00	3.79	269.79	0	00:05	0	0	0:00:00
EX-7	0.00	0.58	253.38	0	00:05	0	0	0:00:00
Structure - (7	2) 0.11	0.38	276.17	0	00:12	0	0	0:00:00
DP-1	0.00	0.34	275.34	0	00:12	0	0	0:00:00
DP-10	0.00	0.31	265.09	0	00:08	0	0	0:00:00
DP-13	0.01	0.61	260.21	0	00:21	0	0	0:00:00
DP-16	0.00	0.00	252.66	0	00:00	0	0	0:00:00
DP-18	0.01	0.63	264.99	0	00:05	0	0	0:00:00
DP-20	0.01	0.33	274.53	0	00:24	0	0	0:00:00
DP-5	0.00	0.00	248.00	0	00:00	0	0	0:00:00
DP-6	0.00	0.00	246.50	0	00:00	0	0	0:00:00
DP-7	0.00	0.58	253.18	0	00:06	0	0	0:00:00
Out-01	0.00	0.10	281.32	0	00:16	0	0	0:00:00

Node	Element	Maximum Lateral	Peak	D. T	ime of	Maxim	um Time o	of Peak
ID	T'ype	Lateral	Inilow	Реак	TULTOM	F.Toodi:	ng Fl	Looding
		Inflow						
		CIS	CIS	uays 		C	fs days 	
CIT-8	JUNCTION	1.49	2.31	0	00:05	0.		
DH-10	JUNCTION	1.31	1.31	0	00:08	0.	00	
DH-13	JUNCTION	2.45	2.45	0	00:21	0.	00	
DH-20	JUNCTION	2.36	2.36	0	00:24	0.	00	
EX-18	JUNCTION	0.00	1.31 2.45 2.36 5.45	0	00:05	0.	00	
EX-7	JUNCTION						00	
Structure - (72)	JUNCTION	0.00	0.91	0	00:12	0.	00	
DP-1	OUTFALL	0.00	0.91 0.91 1.31	0	00:12	0.	00	
DP-10	OUTFALL	0.00	1.31	0	00:08	0.	00	
DP-13	OUTFALL	0.00	2.45	0	00:21	0.	00	
DP-16	OUTFALL	4.14	4.14	0	00:05	0.	00	
DP-18	OUTFALL	0.00	2.45 4.14 5.41 2.35	0	00:05	0.	00	
DP-20	OUTFALL	0.00	2.35	0	00:24	0.	00	
DP-5	OUTFALL	1.90	1.90	0	01:26	0.	00	
DP-6	OUTFALL	0.93	0.93	0	00:05	0.	00	
DP-7	OUTFALL	0.76	2.92	0	00:05	0.		
Out-01	OUTFALL	1.90 0.93 0.76 0.00	0.16	0	00:16	0.	00	
******	L .L							
Inlet Depth Summan	- <u>Y</u> * *							
Iniet Depth Summai	- Y * *							
Iniet Depth Summa:	* * 							
******	* * 							
******	* * 							
**************************************	* * 							
**************************************	Max Gutter Spread during Peak Flow	Max Gut Water I du Peak I	ter Elev ring Flow	Max G Water c Peak	Sutter Depth Luring Flow	T M Occu	ime of aximum Depth rrence	
**************************************	Max Gutter Spread during Peak Flow	Max Gut Water I du Peak I	ter Elev ring Flow	Max G Water c Peak	Sutter Depth Luring Flow	T M Occu	ime of aximum Depth rrence	
**************************************	Max Gutter Spread during Peak Flow ft	Max Gut Water I du Peak I	tter Elev ring Flow ft	Max G Water c Peak	Sutter Depth Suring Flow ft	T M Occu days	ime of aximum Depth rrence hh:mm	
**************************************	Max Gutter Spread during Peak Flow ft	Max Gut Water I du Peak I	tter Elev ring Flow ft	Max G Water c Peak	Sutter Depth Suring Flow ft	T M Occu days	ime of aximum Depth rrence hh:mm	
**************************************	Max Gutter Spread during Peak Flow ft 6.53 17.55	Max Gut Water I du Peak I	tter Elev ring Flow ft	Max G Water c Peak	Sutter Depth Suring Flow ft	T M Occu days	ime of aximum Depth rrence hh:mm	
**************************************	Max Gutter Spread during Peak Flow ft  6.53 17.55 1.68	Max Gut Water I du Peak I	tter Elev ring Flow ft	Max G Water c Peak	Sutter Depth Suring Flow ft	T M Occu days	ime of aximum Depth rrence hh:mm	
**************************************	Max Gutter Spread during Peak Flow ft 6.53 17.55	Max Gut Water I du Peak I	tter Elev ring Flow ft	Max G Water c Peak	Sutter Depth Suring Flow ft	T M Occu	ime of aximum Depth rrence hh:mm	
**************************************	Max Gutter Spread during Peak Flow ft  6.53 17.55 1.68 6.36	Max Gut Water I du Peak I	tter Elev ring Flow ft	Max G Water c Peak	Sutter Depth Suring Flow ft	T M Occu days	ime of aximum Depth rrence hh:mm	
**************************************	Max Gutter Spread during Peak Flow ft  6.53 17.55 1.68 6.36	Max Gut Water I du Peak I	tter Elev ring Flow ft	Max G Water c Peak	Sutter Depth Suring Flow ft	T M Occu days	ime of aximum Depth rrence hh:mm	
**************************************	Max Gutter Spread during Peak Flow ft	Max Gut Water I du Peak I	tter Elev ring Flow ft	Max G Water c Peak	Sutter Depth Suring Flow ft	T M Occu days	ime of aximum Depth rrence hh:mm	
**************************************	Max Gutter Spread during Peak Flow ft	Max Gut Water I du Peak I	tter Elev ring Flow ft	Max G Water c Peak	Sutter Depth Suring Flow ft	T M Occu days	ime of aximum Depth rrence hh:mm	
**************************************	Max Gutter Spread during Peak Flow ft	Max Gut Water I du Peak I	tter Elev ring Flow ft	Max G Water c Peak	Sutter Depth Suring Flow ft	T M Occu days	ime of aximum Depth rrence hh:mm	
**************************************	Max Gutter Spread during Peak Flow ft  6.53 17.55 1.68 6.36	Max Gut Water I du Peak I285 277 259	tter Elev ring Flow ft 	Max G Water c Peak	Sutter Depth Suring Flow ft 0.21 0.46 0.10 0.21	Occudays 0 0 0	ime of aximum Depth rrence hh:mm 00:12 00:05 00:06 00:05	
**************************************	Max Gutter Spread during Peak Flow ft  6.53 17.55 1.68 6.36	Max Gut Water I du Peak I  283 274 255 262	ter Elev ring Flow ft 1.43 4.18 9.30 2.51	Max G Water G Peak	Sutter Depth Suring Flow ft 0.21 0.46 0.10 0.21	Occudays Occudos	ime of aximum Depth rrence hh:mm 00:12 00:05 00:06 00:05	
**************************************	Max Gutter Spread during Peak Flow ft  6.53 17.55 1.68 6.36	Max Gut Water I du Peak I285 277 259	ter Elev ring Flow ft 1.43 4.18 9.30 2.51	Max G Water G Peak	Sutter Depth Suring Flow ft 0.21 0.46 0.10 0.21	Occudays 0 0 0	ime of aximum Depth rrence hh:mm 00:12 00:05 00:06 00:05	
**************************************	Max Gutter Spread during Peak Flow ft  6.53 17.55 1.68 6.36	Max Gut Water I du Peak I  28: 274 259 262	Eter Elev ring Flow ft 1.43 4.18 9.30 2.51	Max G Water C Peak	Sutter Depth Suring Flow ft 0.21 0.46 0.10 0.21	T M Occu days0 0 0 0	ime of aximum Depth rrence hh:mm 00:12 00:05 00:06 00:05	Total
**************************************	Max Gutter Spread during Peak Flow ft  6.53 17.55 1.68 6.36	Max Gut Water I du Peak I  28: 274 259 262	Eter Elev ring Flow ft 1.43 4.18 9.30 2.51	Max G Water C Peak	Sutter Depth Suring Flow ft 0.21 0.46 0.10 0.21	T M Occu days0 0 0 0	ime of aximum Depth rrence hh:mm 00:12 00:05 00:06 00:05	Total
**************************************	Max Gutter Spread during Peak Flow ft  6.53 17.55 1.68 6.36	Max Gut Water I du Peak I  283 274 255 262	Eter Elev ring Flow ft 1.43 4.18 9.30 2.51	Max G Water C Peak	Sutter Depth Suring Flow ft 0.21 0.46 0.10 0.21	T M Occu days0 0 0 0	ime of aximum Depth rrence hh:mm 00:12 00:05 00:06 00:05	Total
**************************************	Max Gutter Spread during Peak Flow ft  6.53 17.55 1.68 6.36	Max Gut Water I du Peak I  28: 27/ 25: 262  Peak  Lateral	Eter Elev ring Flow ft 1.43 4.18 9.30 2.51	Max G Water Peak	Sutter Depth luring Flow ft 0.21 0.46 0.10 0.21	Occudays Occudays O O O O O O O O O O  Expression of the control o	ime of aximum Depth rrence hh:mm 00:12 00:05 00:06 00:05	Total
**************************************	Max Gutter Spread during Peak Flow ft  6.53 17.55 1.68 6.36	Max Gut Water I du Peak I  28: 27/ 25: 262  Peak  Lateral	Eter Elevering Flow ft 1.43 4.18 9.30 2.51	Max G Water  Peak  Peak  Peak  Peak  Peak	Pepsassi	Occudays Occudos O O O O O O O O O O O O O O O O O O O	ime of aximum Depth rrence hh:mm 00:12 00:05 00:06 00:05	Total
**************************************	Max Gutter Spread during Peak Flow ft  6.53 17.55 1.68 6.36	Max Gut Water I du Peak I  283 274 255 262  Peak  Lateral Flow	Eter Elev ring Flow ft 1.43 4.18 9.30 2.51  F Intercep by In	Max G Water  Peak  Peak  Peak  Peak  Peak  Peak  Peak  Peak	Pepsassi	Occudays Occudos O O O O O O O O O O O O O O O O O O O	ime of aximum Depth rrence hh:mm 00:12 00:05 00:06 00:05	Total
**************************************	Max Gutter Spread during Peak Flow ft  6.53 17.55 1.68 6.36	Max Gut Water I du Peak I  28: 27/ 25: 262  Peak  Lateral	Eter Elev ring Flow ft 1.43 4.18 9.30 2.51  F Intercep by In	Max G Water  Peak  Peak  Peak  Peak  Peak	Pepsassi	Occudays Occudays Occudays Occudays Occudate Occ	ime of aximum Depth rrence hh:mm 00:12 00:05 00:06 00:05	Total

_						
CB-1 0	1.12	1.12	0.92	0.21	81.74	0.000
CB-18	5.47	5.47	-	_	-	0.000
EX-CB15	0.14	0.00	0.14	0.00	100.00	0.000
0 EX-CB-16	1.06	1.06	0.88	0.18	82.70	0.000

Outfall Node ID	Flow Frequency (%)	Average Flow cfs	Peak Inflow cfs
DP-1 DP-10 DP-13 DP-16 DP-18 DP-20 DP-5 DP-6	1.93 1.19 3.01 0.69 0.88 3.39 11.96 0.69	0.44 0.65 1.21 2.07 2.15 1.16 0.95 0.47	0.91 1.31 2.45 4.14 5.41 2.35 1.90
DP-7 Out-01	2.00 2.83	0.57 0.04	2.92
System	2.86	9.71	15.51

Link ID		Element	Т	ime of	Maximum	Length	Peak Flow	Design	Ratio of
Ratio of	То	tal Reported							
			Pea	k Flow	Velocity	Factor	during	Flow	Maximum
Maximum	Ti	me Condition							
-1 1	,		0ccu	rrence	Attained		Analysis	Capacity	/Design
Flow Surcharg	jed		4	la la •	£		cfs	cfs	ml
Depth minu	+ 0 0		days	11111 • 111111	ft/sec		CIS	CIS	Flow
Depth mind	ices								
CB-1_Overflo	w	CHANNEL	0	00:16	2.01	1.00	0.16	2.70	0.06
0.34	0	Calculated							
CIT-9_Overfl	.OW	CHANNEL	0	00:06	4.18	1.00	0.14	7.01	0.02
0.22	0	Calculated							
Link-17		CONDUIT	0	00:07	1.05	1.00	0.13	4.07	0.03
0.12	0	Calculated							
Link-18		CHANNEL	0	00:09	1.16	1.00	0.01	10.44	0.00
0.06	0	Calculated		00.05	4 0 4	1 00	0.05	2 50	0 60
Pipe - (21)	0	CONDUIT	0	00:05	4.94	1.00	2.27	3.59	0.63
0.58	U	Calculated CONDUIT	0	00:06	4.81	1.00	2.27	3.56	0.64
Pipe - (22) 0.58	Λ	Calculated	U	00.00	4.01	1.00	2.21	3.30	0.04
Pipe - (25)	U	CONDUIT	0	00:05	7.46	1.00	0.85	3.88	0.22
0.32	0	Calculated	0	30.03	7.10	1.00	0.05	3.00	0.22
0.52	0	carcaracca							

Pipe - (33)		CONDUIT	0	00:21	4	1.89	1.00	2.45	3.56	0.69
0.61	0	Calculated								
Pipe - (44)		CONDUIT	0	00:05	Ω	3.20	1.00	5.45	5.63	0.97
- '	_		U	00.03	Ü	0.20	1.00	J. <del>1</del> J	5.05	0.97
0.79	0	Calculated								
Pipe - (45)		CONDUIT	0	00:05	7	7.79	1.00	5.41	14.86	0.36
0.42	0	Calculated								
Pipe - (56)		CONDUIT	0	00:08	6	5.24	1.00	1.31	6.17	0.21
0.31	Ω	Calculated								
	•		^	00.01			1 00	0 25	22 62	0 10
Pipe - (57)		CONDUIT	U	00:24	8	3.28	1.00	2.35	22.60	0.10
0.22	0	Calculated								
Pipe - (61)		CONDUIT	0	00:12	6	5.17	1.00	0.91	5.92	0.15
0.26	0	Calculated								
Pipe - (62)		CONDUIT	0	00:12	3	3.80	1.00	0.91	3.56	0.25
- '	_		ŭ	00 12				0.,,_	3.30	0.25
0.34	0	Calculated								

All links are stable.

WARNING 108 : Surcharge elevation defined for Junction EX-18 is below junction maximum elevation. Assumed surcharge elevation equal to maximum elevation.

WARNING 139 : Ponded area defined for on sag Inlet CB-18 is zero. Assumed ponded area equal to 10 ft $^2$  (0.929 m $^2$ ).

WARNING 138 : Initial water surface elevation defined for Inlet EX-CB15 is below catchbasin invert elevation.

Assumed initial water surface elevation equal to catchbasin inlet invert

elevation.
WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB-1\_Overflow

is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CIT-9\_Overflow is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 117: Conduit outlet invert elevation defined for Conduit CB-1\_Overflow is below downstream node invert elevation.

Assumed conduit outlet invert elevation equal to downstream node invert

elevation.

WARNING 004 : Minimum elevation drop used for Conduit CB-1\_Overflow.

WARNING 005 : Minimum slope used for Conduit CB-1\_Overflow.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CIT-9\_Overflow is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet EX-CB15.

WARNING 116: Conduit inlet invert elevation defined for Conduit Link-17 is below upstream node invert elevation.

Assumed conduit inlet invert elevation equal to upstream node invert elevation.

WARNING 004: Minimum elevation drop used for Conduit Link-17.

WARNING 005 : Minimum slope used for Conduit Link-17.

Analysis began on: Tue Jan 31 11:04:37 2023 Analysis ended on: Tue Jan 31 11:04:39 2023

Total elapsed time: 00:00:02

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Autodesk® Storm and Sanitary Analysis 2016 - Version 13.2.165 (Build 0)
Project Description
******
File Name ..... Grove_St_Ph2_r1-PR.SPF
******
Analysis Options
******
Flow Units ..... cfs
Subbasin Hydrograph Method. Rational
Time of Concentration..... SCS TR-55
Return Period..... 2 years
Link Routing Method ...... Kinematic Wave Storage Node Exfiltration. None
Starting Date ..... DEC-20-2022 00:00:00
Ending Date ..... DEC-21-2022 00:00:00 Report Time Step ..... 00:00:10
******
Element Count
Number of subbasins ..... 17
Number of nodes ..... 50
Number of links ..... 52
******
Subbasin Summary
******
Subbasin
                      Total
                        Area
TD
                       acres
Sub-CB-1
                    0.36
0.13
0.20
1.28
0.34
0.40
0.29
Sub-CB-10
Sub-CB-11
Sub-CB-12
Sub-CB-13-14
Sub-CB-15-16
Sub-CB-17
Sub-CB-18-19
                      0.95
Sub-CB-2
                        0.40
                        1.49
Sub-CB-20
Sub-CB-3
                        2.84
Sub-CB-4
                        0.34
                       0.33
Sub-CB-5
Sub-CB-6
                        0.14
Sub-CB-7
                        0.11
Sub-CB-8W
                        0.22
Sub-CB-9
                        0.15
*****
Node Summary
                  Element Invert Maximum Ponded External Type Elevation Elev. Area Inflow ft ft ft
Node
TD
```

257.54 259.20 0.00

JUNCTION

CB-8E

CIT-8 CIT-9 DH-10 DH-13		JUNCTION JUNCTION JUNCTION JUNCTION		259.42 40 262.67 L5 268.15 30 265.60	0.00 0.00 0.00 0.00		
DH-20		JUNCTION		52 280.21	0.00		
DH-6		JUNCTION	246.	95 255.72	0.00		
DMH-10		JUNCTION		32 267.86	0.00		
DMH-11		JUNCTION		75 272.24	0.00		
DMH-12		JUNCTION		70 271.08	0.00		
DMH-13		JUNCTION	262.	77 265.40 55 280.22	0.00		
DMH-20		JUNCTION	277.	55 280.22	0.00		
DMH-3		JUNCTION	262.	24 265.34 35 255.95	0.00		
DMH-4N		JUNCTION			0.00		
DMH-4S		JUNCTION	257.	13 262.56	0.00		
DMH-6		JUNCTION		257.58	0.00		
DMH-7		JUNCTION		10 258.76	0.00		
EX-18		JUNCTION		273.24	0.00		
EX-7	(72)	JUNCTION		30 258.62	0.00		
Structure STU-16	- (/2)	JUNCTION JUNCTION	273.	79 277.57 70 255.49	0.00		
STU-5		JUNCTION	248	53 251 88	0.00		
DP-1		OUTFALL	275	251.88 276.00	0.00		
DP-10		OUTFALL		78 265.78	0.00		
DP-13		OUTFALL		260.60	0.00		
DP-16		OUTFALL		56 253.66	0.00		
DP-18		OUTFALL			0.00		
DP-20		OUTFALL	274.	36 265.86 20 275.70	0.00		
DP-5		OUTFALL	248.	00 249.00	0.00		
DP-6		OUTFALL	246.	249.00 247.50	0.00		
DP-7		OUTFALL	252.	50 253.60	0.00		
OFFSITE1		OUTFALL	281.	22 281.50	0.00		
OFFSITE-1		OUTFALL	267.	58 268.43	0.00		
*********  Inlet Summ  *******  Inlet  Catchbasin	nary :***	Inlet	Initial	Manufacturer Grate		Inlet	Number
Inlet Summ *******  Inlet  Catchbasin	nary :***	Let Ponded		Grate			
Inlet Summ ******* Inlet	nary **** Inl	let Ponded Manufacture	<u> </u>	Grate Part		Inlet Location	Number of
Inlet Summ ******* Inlet Catchbasin ID	nary **** Inl	Let Ponded	<u> </u>	Grate Part			
Inlet Summ ******* Inlet Catchbasin ID	nary **** Inl Rim	let Ponded Manufacture: Area	<u> </u>	Grate Part Logging Number			of
Inlet Summ ******* Inlet Catchbasin ID Invert Elevation	nary *** Inl Rim Elevatio	let Ponded Manufacture Area on	Water C	Grate Part Logging Number Factor			of
Inlet Summ ******* Inlet Catchbasin ID Invert Elevation	nary **** Inl Rim	let Ponded Manufacture Area on	. Water C	Grate Part Logging Number			of
Inlet Summ ******* Inlet Catchbasin ID Invert Elevation	nary *** Inl Rim Elevatio	let Ponded Manufacture Area on	Water C	Grate Part Logging Number Factor			of
Inlet Summ  *******  Inlet Catchbasin  ID Invert  Elevation  ft	nary ***  Inl Rim Elevation	let Ponded Manufacturen Area on ft²	Water C Elevation ft	Grate Part Logging Number Factor			of
Inlet Summ  *******  Inlet Catchbasin  ID Invert  Elevation  ft	nary ***  Inl Rim Elevation	let Ponded Manufacturer Area on ft²	Water C Elevation ft	Grate Part Logging Number Factor		Location	of Inlets
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft	nary ****  Inl Rim Elevation	let Ponded Manufacturer Area on ft² FHWA HEC-22	Water C Elevation ft GENERIC	Grate Part Logging Number Factor %			of
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10	Rim Elevation ft 281.22	let Ponded Manufacturer Area on ft² FHWA HEC-22	Water C Elevation ft  GENERIC 278.10	Grate Part Logging Number Factor  % N/A 0.00		Location On Grade	of Inlets
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10 CB-10	Rim Elevation ft 281.22	let Ponded Manufactures Area on ft² FHWA HEC-22 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC	Grate Part logging Number Factor  % N/A 0.00 N/A		Location	of Inlets
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10	Rim Elevation ft 281.22	Let Ponded Manufactures Area on ft² FHWA HEC-22 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44	Grate Part Logging Number Factor  % N/A 0.00		Location On Grade	of Inlets
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft	Rim Elevation ft 281.22	let Ponded Manufactures Area on ft² FHWA HEC-22 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44	Grate Part logging Number Factor  % N/A 0.00 N/A 0.00		Location On Grade On Grade	of Inlets  1
Inlet Summ ******* Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10 CB-10 265.44 CB-11	Inl Rim Elevation ft 281.22 267.69 272.10	Let Ponded Manufactures Area on ft² FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22	Water C. Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10	Grate Part Logging Number Factor		Location On Grade On Grade	of Inlets  1 1 1
Inlet Summ  ******* Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10 CB-10 265.44 CB-11 269.10	Inl Rim Elevation ft 281.22 267.69	let Ponded Manufacturer Area on ft² FHWA HEC-22 FHWA HEC-22 FHWA HEC-22	Water C. Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10	Grate Part Logging Number Factor		Location  On Grade  On Grade  On Grade	of Inlets  1 1 1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10 CB-10 265.44 CB-11 269.10 CB-12	Elevation ft 281.22 267.69 272.10 271.07	let Ponded Manufacturer Area on ft² FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 269.10 GENERIC 268.07	Grate Part Logging Number Factor  % N/A 0.00 N/A 0.00 N/A 0.00 N/A 0.00 N/A		Location  On Grade  On Grade  On Grade	of Inlets  1 1 1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft	Inl Rim Elevation ft 281.22 267.69 272.10	let Ponded Manufacturen Area on ft² FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 269.10 GENERIC 268.07	Grate Part Logging Number Factor  % N/A 0.00 N/A 0.00 N/A 0.00 N/A 0.00 N/A 0.00		On Grade On Grade On Grade On Grade	of Inlets  1 1 1
Inlet Summ ******* Inlet Catchbasin ID Invert Elevation ft	Rim Elevation ft 281.22 267.69 272.10 271.07	Let Ponded Manufactures Area  on  ft²  FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 10.00 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 268.07 GENERIC 268.07 GENERIC 262.90 GENERIC	Grate Part Logging Number Factor  % N/A 0.00 N/A		On Grade On Grade On Grade On Grade	of Inlets  1 1 1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10 CB-10 265.44 CB-11 269.10 CB-12 268.07 CB-13 262.90 CB-16 252.93	Elevation ft 281.22 267.69 272.10 271.07	Let Ponded Manufactures Area on ft² FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 10.00 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 268.07 GENERIC 262.90 GENERIC 252.93	Grate Part Logging Number Factor		On Grade On Grade On Grade On Grade On Grade On Sag On Sag	of Inlets  1 1 1 1 1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10 CB-10 265.44 CB-11 269.10 CB-12 268.07 CB-13 262.90 CB-16 252.93 CB-17	Rim Elevation ft  281.22 267.69 272.10 271.07 264.85 254.93	Let Ponded Manufactures Area on ft² FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 10.00 FHWA HEC-22 10.00 FHWA HEC-22	Water C. Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 268.07 GENERIC 262.90 GENERIC 252.93 GENERIC	Grate Part Logging Number Factor		On Grade On Grade On Grade On Grade On Grade	of Inlets  1 1 1 1 1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft	Rim Elevation ft 281.22 267.69 272.10 271.07	Let Ponded Manufactures Area  on  ft²  FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 10.00 FHWA HEC-22 10.00 FHWA HEC-22	Water C. Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 268.07 GENERIC 268.07 GENERIC 252.93 GENERIC 260.16	Grate Part Logging Number Factor  % N/A 0.00 N/A		On Grade On Grade On Grade On Grade On Sag On Sag On Grade	of Inlets  1 1 1 1 1 1 1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft	Elevation ft 281.22 267.69 272.10 271.07 264.85 254.93 265.49	Let Ponded Manufactures Area  on  ft²  FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 10.00 FHWA HEC-22 10.00 FHWA HEC-22 10.00 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 269.10 GENERIC 262.90 GENERIC 252.93 GENERIC 260.16 GENERIC	Grate Part Logging Number Factor  % N/A 0.00 N/A		On Grade On Grade On Grade On Grade On Grade On Sag On Sag	of Inlets  1 1 1 1 1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft	Rim Elevation ft  281.22 267.69 272.10 271.07 264.85 254.93	Let Ponded Manufactures Area  on  ft²  FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 10.00 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 268.07 GENERIC 262.90 GENERIC 252.93 GENERIC 250.16 GENERIC 260.16 GENERIC 269.61	Grate Part Logging Number Factor		On Grade On Grade On Grade On Grade On Sag On Sag On Grade On Sag	of Inlets  1 1 1 1 1 1 1 1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft	Elevation ft 281.22 267.69 272.10 271.07 264.85 254.93 265.49	Let Ponded Manufactures Area  on  ft²  FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 10.00 FHWA HEC-22 10.00 FHWA HEC-22 10.00 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 268.07 GENERIC 262.90 GENERIC 252.93 GENERIC 250.16 GENERIC 260.16 GENERIC 269.61	Grate Part Logging Number Factor  % N/A 0.00 N/A		On Grade On Grade On Grade On Grade On Sag On Sag On Grade	of Inlets  1 1 1 1 1 1 1 1

CB-20		FHWA	HEC-22	GENERIC	N/A		Or	ı Sag	1	
278.18	279.	67 10.	00	278.18	0.00					
CB-3			HEC-22	GENERIC	N/A		Or	n Grade	1	
262.89	265.	39	-	262.89	0.00					
CB-4		FHWA	HEC-22	GENERIC	N/A		Or	n Grade	1	
254.18	255.	93	-	254.18	0.00					
CB-5		FHWA	HEC-22	GENERIC	N/A		Or	n Sag	1	
249.44	251.	18 10.	00	249.44	0.00					
CB-6		FHWA	HEC-22	GENERIC	N/A		Or	n Grade	1	
252.35	255.	35	-	252.35	0.00					
CB-7		FHWA	HEC-22	GENERIC	N/A		Or	ı Grade	1	
255.41	258.	41	-	255.41	0.00					
CB-8W		FHWA	HEC-22	GENERIC	N/A		Or	ı Grade	1	
257.08	260.	08	-	257.08	0.00					
CB-9		FHWA	HEC-22	GENERIC	N/A		Or	ı Grade	1	
259.82	262.	82	-	259.82	0.00					
*****	*****	*****	*							
		ter Summar								
				Doodsso	Dood	C11++0	C11++ 0	_	111++02	
Inlet ID			Roadwa: tudina		_	Gutter Cross	Gutter Width		utter ssion	
ID		rongr	Slope		_	Slope	WIGCII	рерге	SSIOII	
			ft/f		Rougilliess	ft/ft	ft		in	
			IL/I	L IL/IL					111	
CB-1			0.010	0 0.0200	0.0160	0.0620	2.00		2.00	
CB-10			0.020		0.0130	0.0620	2.00		0.00	
CB-11			0.020		0.0130	0.0620	2.00		0.00	
CB-11			0.020		0.0130	0.0620	2.00		0.00	
CB-12				- 0.0500	0.0130	0.0620	2.00		0.00	
CB-15				- 0.0500	0.0130	0.0620	2.00		0.00	
CB-17			0.010		0.0160	0.0620	2.00		2.00	
CB-17			0.010		0.0160	0.0620	2.00		2.00	
			0 020	- 0.0200						
CB-2			0.020		0.0130	0.0620	2.00		0.00	
CB-20			0 000	- 0.0500	0.0130	0.0620	2.00		0.00	
CB-3			0.020		0.0130	0.0620	2.00		0.00	
CB-4			0.020		0.0130	0.0620	2.00		0.00	
CB-5				- 0.0500	0.0130	0.0620	2.00		0.00	
CB-6			0.020		0.0130	0.0620	2.00		0.00	
CB-7			0.020			0.0620	2.00		0.00	
CB-8W			0.010		0.0130	0.0620	2.00		2.00	
CB-9			0.020	0.0500	0.0130	0.0620	2.00		0.00	
*****	***									
Link Sum										
Link		From Node		To Node	Element	т	onath	Clana	Manning's	~
ID		FIOIII NOGE	:	10 Node	Element Type	L	ength ft	Slope %	Roughnes	
								·•		_
CB-1_Ove	rflow	CB-1		OFFSITE1	CHANNEL		241.8	0.2000	0.013	0
CB10-9_G		CB-10		CB-9	CHANNEL		254.5	1.9133	0.013	
CB11-10_		CB-11		CB-10	CHANNEL		254.5	1.7326	0.013	
CB12-13		CB-12		CB-13	CHANNEL		254.5	2.4437	0.013	
CB17-16_		CB-17		CB-16	CHANNEL		254.5	4.1501	0.013	
CB2-3 Gu		CB-2		CB-3	CHANNEL		241.8	4.7276	0.013	
CB2-3_Gu CB3-4 Gu		CB-3		CB-4	CHANNEL		254.5	3.7167	0.013	
CB4-5_Gu		CB-4		CB-5	CHANNEL		254.5	1.8662	0.013	
CB6-5_Gu		CB-4 CB-6		CB-5	CHANNEL		254.5	1.6383	0.013	
_									0.013	
CB7-6_Gu		CB-7		CB-6	CHANNEL		254.5	1.2022		
CB8-7_Gu		CB-8W		CB-7	CHANNEL		254.5	0.6561	0.013	
CB9-8_Gu		CB-9		CB-8W	CHANNEL		254.5	1.0765	0.013	
L-Pipe -		CB-20		OFFSITE-1	CHANNEL		546.0	2.1967	0.013	
Pipe - (		DMH-6		DH-6	CONDUIT		13.3	3.0144	0.013	
Pipe - (	13)	CB-6		DMH-6	CONDUIT		12.5	0.7995	0.013	0

Pipe - (14)	CB-5	STU-5	CONDUIT	28.8	2.4635	0.0130
Pipe - (16)	CB-3	DMH-3	CONDUIT	11.9	4.6382	0.0130
Pipe - (18)	CB-7	DMH-7	CONDUIT	20.7	1.0000	0.0130
<u> </u>						
Pipe - (19)	DMH-7	EX-7	CONDUIT	6.9	1.4505	0.0130
Pipe - (2)	CB-2	DMH-3	CONDUIT	246.6	4.6555	0.0130
Pipe - (20)	CB-8E	CIT-8	CONDUIT	7.6	0.6131	0.0130
Pipe - (21)	CIT-8	EX-7	CONDUIT	196.9	1.0156	0.0130
Pipe - (22)	EX-7	DP-7	CONDUIT	20.0	1.0000	0.0130
Pipe - (23)	CB-8W	CIT-8	CONDUIT	20.5	3.2241	0.0130
Pipe - (24)	CB-9	CIT-9	CONDUIT	16.5	0.9092	0.0130
Pipe - (25)	CIT-9	CIT-8	CONDUIT	219.0	1.1872	0.0130
Pipe - (26)	DMH-10	DH-10	CONDUIT	14.0	0.5000	0.0130
Pipe - (27)	CB-10	DMH-10	CONDUIT	4.2	0.5000	0.0130
Pipe - (28)	CB-11	DMH-11	CONDUIT	4.9	5.1092	0.0130
Pipe - (29)	DMH-11	DH-10	CONDUIT	190.5	1.8369	0.0130
Pipe - (3)	DMH-4S	DMH-4N	CONDUIT	131.6	3.1757	0.0130
Pipe - (30)	CB-12	DMH-12	CONDUIT	3.6	1.0000	0.0130
Pipe - (31)	DMH-12	DH-13	CONDUIT	217.3	2.4045	0.0130
Pipe - (33)	DH-13	DP-13	CONDUIT	19.5	1.0000	0.0130
Pipe - (34)	CB-13	DMH-13	CONDUIT	5.9	0.5098	0.0130
Pipe - (35)	DMH-13	DH-13	CONDUIT	19.9	1.0989	0.0130
Pipe - (4)	DMH-4N	STU-5	CONDUIT	263.5	1.5634	0.0130
Pipe - (40)	CB-17	STU-16	CONDUIT	220.1	3.2621	0.0130
				4.1	1.0000	
Pipe - (41)	STU-16	DP-16	CONDUIT			0.0130
Pipe - (43)	CB-16	STU-16	CONDUIT	7.3	1.7930	0.0130
Pipe - (44)	CB-18	EX-18	CONDUIT	24.4	2.4990	0.0130
Pipe - (45)	EX-18	DP-18	CONDUIT	81.8	2.0000	0.0130
Pipe - (5)	STU-5	DP-5	CONDUIT	16.3	3.8608	0.0130
Pipe - (50)	CB-20	DMH-20	CONDUIT	6.5	8.1871	0.0130
Pipe - (51)	DMH-20	DH-20	CONDUIT	5.7	8.1142	0.0130
Pipe - (54)	DH-6	DP-6	CONDUIT	8.5	5.3000	0.0130
Pipe - (55)	CB-4	DMH-4N	CONDUIT	10.6	11.5699	0.0130
Pipe - (56)	DH-10	DP-10	CONDUIT	12.4	3.0000	0.0130
Pipe - (57)	DH-20	DP-20	CONDUIT	55.5	6.1646	0.0130
Pipe - (61)	CB-1	Structure -	(72)CONDUIT	79.8	2.7583	0.0130
Pipe - (62)	<u></u>					
FIDE - (07)	Structure -	(72)DP-1	CONDUIT	79.0	1.0000	0.0130
Pipe - (62) Pipe - (7)	Structure - DMH-3	(72)DP-1 DMH-4S	CONDUIT CONDUIT	79.0 124.6	1.0000 4.0212	0.0130 0.0130
Pipe - (7)	DMH-3					
	DMH-3					
Pipe - (7)  ***********************************	DMH-3 ***** ummary					
Pipe - (7)	DMH-3 ***** ummary					
Pipe - (7)  ***********************************	DMH-3 ***** ummary					
Pipe - (7)  ******************  Cross Section S  ***********************************	DMH-3  ***** ummary *****	DMH-4S	CONDUIT	124.6	4.0212	0.0130
Pipe - (7)  *************  Cross Section S  *************  Link	DMH-3  ***** ummary *****	DMH-4S	CONDUIT	124.6	4.0212	0.0130
Pipe - (7)  *************  Cross Section S  ***********  Link  Design	DMH-3  ***** ummary *****	DMH-4S Depth/	CONDUIT	124.6 No. of	4.0212 Cross	0.0130
Pipe - (7)  *********  Cross Section S  ********  Link  Design  ID	DMH-3  ***** ummary *****	DMH-4S Depth/	CONDUIT	124.6 No. of	4.0212 Cross	0.0130
Pipe - (7)  *********  Cross Section S  ********  Link  Design  ID	DMH-3  ***** ummary *****	DMH-4S Depth/	CONDUIT	124.6 No. of	4.0212 Cross Sectional	0.0130  Full Flow  Hydraulic
Pipe - (7)  *********  Cross Section S  *********  Link  Design  ID  Flow	DMH-3  ***** ummary *****	DMH-4S Depth/	CONDUIT	124.6 No. of	4.0212 Cross Sectional	0.0130  Full Flow  Hydraulic
Pipe - (7)  *********  Cross Section S  *********  Link  Design  ID  Flow	DMH-3  ***** ummary *****	DMH-4S  Depth/ Diameter	CONDUIT Width	124.6 No. of	4.0212  Cross Sectional Area	0.0130  Full Flow  Hydraulic  Radius
Pipe - (7)  **********  Cross Section S  *******  Link  Design  ID  Flow  Capacity	DMH-3  ***** ummary *****	DMH-4S  Depth/ Diameter	CONDUIT Width	124.6 No. of	4.0212  Cross Sectional Area	0.0130  Full Flow  Hydraulic  Radius
Pipe - (7)  ***********  Cross Section S  *******  Link  Design  ID  Flow  Capacity  cfs	DMH-3  *****  ummary  *****  Shape	DMH-4S  Depth/ Diameter	CONDUIT Width ft	No. of	4.0212  Cross Sectional  Area  ft²	0.0130  Full Flow  Hydraulic  Radius  ft
Pipe - (7)  **********  Cross Section S  *******  Link  Design  ID  Flow  Capacity  cfs	DMH-3  *****  ummary  *****  Shape	DMH-4S  Depth/ Diameter  ft	CONDUIT  Width  ft	No. of Barrels	4.0212  Cross Sectional  Area  ft²	0.0130  Full Flow  Hydraulic  Radius  ft
Pipe - (7)  ***********  Cross Section S *******  Link  Design  ID  Flow  Capacity  cfs   CB-1_Overflow	DMH-3  *****  ummary  *****  Shape	DMH-4S  Depth/ Diameter  ft	CONDUIT Width ft	No. of	4.0212  Cross Sectional  Area  ft²	0.0130  Full Flow  Hydraulic  Radius  ft
Pipe - (7)  ***********  Cross Section S *******  Link  Design ID  Flow  Capacity  cfs   CB-1_Overflow 2.70	DMH-3  ***** ummary  ***** Shape  TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28	CONDUIT  Width  ft  14.00	No. of Barrels	Cross Sectional Area ft²	0.0130  Full Flow Hydraulic Radius ft
Pipe - (7)  ***********  Cross Section S  *******  Link  Design  ID  Flow  Capacity  cfs   CB-1_Overflow  2.70  CB10-9_Gutter	DMH-3  ***** ummary  ***** Shape  TRIANGULAR	DMH-4S  Depth/ Diameter  ft	CONDUIT  Width  ft	No. of Barrels	4.0212  Cross Sectional  Area  ft²	0.0130  Full Flow  Hydraulic  Radius  ft
Pipe - (7)  ************* Cross Section S ******** Link Design ID Flow Capacity cfs CB-1_Overflow 2.70 CB10-9_Gutter 8.35	DMH-3  ***** ummary ***** Shape  TRIANGULAR TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28 0.28	CONDUIT  Width  ft  14.00  14.00	No. of Barrels	Cross Sectional Area ft²  1.96 1.96	0.0130  Full Flow Hydraulic Radius ft  0.14 0.14
Pipe - (7)  ************* Cross Section S ******** Link Design ID Flow Capacity cfs  CB-1_Overflow 2.70 CB10-9_Gutter 8.35 CB11-10_Gutter	TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28	CONDUIT  Width  ft  14.00	No. of Barrels	Cross Sectional Area ft²	0.0130  Full Flow Hydraulic Radius ft
Pipe - (7)  ************* Cross Section S ******** Link Design ID Flow Capacity cfs  CB-1_Overflow 2.70 CB10-9_Gutter 8.35 CB11-10_Gutter 7.95	DMH-3  ***** ummary ***** Shape  TRIANGULAR TRIANGULAR TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28  0.28  0.28	CONDUIT  Width  ft  14.00 14.00 14.00	No. of Barrels  1 1 1	Cross Sectional Area ft²  1.96 1.96	0.0130  Full Flow Hydraulic Radius ft  0.14 0.14 0.14
Pipe - (7)  ************  Cross Section S *******  Link  Design  ID  Flow  Capacity  cfs   CB-1_Overflow  2.70  CB10-9_Gutter  8.35  CB11-10_Gutter  7.95  CB12-13_Gutter	DMH-3  ***** ummary ***** Shape  TRIANGULAR TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28 0.28	CONDUIT  Width  ft  14.00  14.00	No. of Barrels	Cross Sectional Area ft²  1.96 1.96	0.0130  Full Flow Hydraulic Radius ft  0.14 0.14
Pipe - (7)  ***********  Cross Section S *******  Link  Design ID  Flow  Capacity  cfs   CB-1_Overflow  2.70  CB10-9_Gutter  8.35  CB11-10_Gutter  7.95  CB12-13_Gutter  9.44	*****  wmmary  ***** Shape  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28 0.28 0.28 0.28	ft  14.00 14.00 14.00 14.00	No. of Barrels  1 1 1 1	4.0212  Cross Sectional Area ft²  1.96 1.96 1.96 1.96	Full Flow Hydraulic Radius ft  0.14 0.14 0.14 0.14
Pipe - (7)  ************  Cross Section S *******  Link  Design ID Flow  Capacity  cfs   CB-1_Overflow  2.70  CB10-9_Gutter  7.95  CB12-13_Gutter  9.44  CB17-16_Gutter	DMH-3  ***** ummary ***** Shape  TRIANGULAR TRIANGULAR TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28  0.28  0.28	CONDUIT  Width  ft  14.00 14.00 14.00	No. of Barrels  1 1 1	Cross Sectional Area ft²  1.96 1.96	0.0130  Full Flow Hydraulic Radius ft  0.14 0.14 0.14
Pipe - (7)  **************  Cross Section S  ********  Link  Design  ID  Flow  Capacity  cfs   CB-1_Overflow  2.70  CB10-9_Gutter  8.35  CB11-10_Gutter  7.95  CB12-13_Gutter  9.44  CB17-16_Gutter  12.30	*****  wmmary  ***** Shape  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28 0.28 0.28 0.28 0.28	ft  14.00 14.00 14.00 14.00 14.00	No. of Barrels  1 1 1 1 1	4.0212  Cross Sectional Area ft²  1.96 1.96 1.96 1.96 1.96	0.0130  Full Flow Hydraulic Radius ft  0.14 0.14 0.14 0.14 0.14
Pipe - (7)  ************** Cross Section S ********* Link Design ID Flow  Capacity cfs  CB-1_Overflow 2.70 CB10-9_Gutter 8.35 CB11-10_Gutter 7.95 CB12-13_Gutter 9.44 CB17-16_Gutter 12.30 CB2-3_Gutter	*****  wmmary  ***** Shape  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28 0.28 0.28 0.28	ft  14.00 14.00 14.00 14.00	No. of Barrels  1 1 1 1	4.0212  Cross Sectional Area ft²  1.96 1.96 1.96 1.96	Full Flow Hydraulic Radius ft  0.14 0.14 0.14 0.14
Pipe - (7)  *************  Cross Section S  ********  Link  Design  ID  Flow  Capacity  cfs   CB-1_Overflow  2.70  CB10-9_Gutter  8.35  CB11-10_Gutter  7.95  CB12-13_Gutter  9.44  CB17-16_Gutter  12.30  CB2-3_Gutter  13.13	DMH-3  ***** ummary ***** Shape  TRIANGULAR TRIANGULAR TRIANGULAR TRIANGULAR TRIANGULAR TRIANGULAR TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28 0.28 0.28 0.28 0.28 0.28 0.28	ft  14.00 14.00 14.00 14.00 14.00 14.00	124.6  No. of Barrels  1 1 1 1 1 1	4.0212  Cross Sectional Area ft²  1.96 1.96 1.96 1.96 1.96 1.96	0.0130  Full Flow Hydraulic Radius ft  0.14 0.14 0.14 0.14 0.14 0.14
Pipe - (7)  ************** Cross Section S ********* Link Design ID Flow  Capacity cfs  CB-1_Overflow 2.70 CB10-9_Gutter 8.35 CB11-10_Gutter 7.95 CB12-13_Gutter 9.44 CB17-16_Gutter 12.30 CB2-3_Gutter	*****  wmmary  ***** Shape  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28 0.28 0.28 0.28 0.28	ft  14.00 14.00 14.00 14.00 14.00	No. of Barrels  1 1 1 1 1	4.0212  Cross Sectional Area ft²  1.96 1.96 1.96 1.96 1.96	0.0130  Full Flow Hydraulic Radius ft  0.14 0.14 0.14 0.14 0.14

11 (4						
11.64 CB4-5_Gutter	TRIANGULAR	0.28	14.00	1	1.96	0.14
8.25 CB6-5_Gutter	TRIANGULAR	0.28	14.00	1	1.96	0.14
7.73 CB7-6_Gutter	TRIANGULAR	0.28	14.00	1	1.96	0.14
6.62 CB8-7_Gutter	TRIANGULAR	0.28	14.00	1	1.96	0.14
4.89 CB9-8_Gutter	TRIANGULAR	0.28	14.00	1	1.96	0.14
6.26 L-Pipe - (50)	IRREGULAR	0.75	6.80	1	3.82	0.50
41.01 Pipe - (12)	CIRCULAR	1.00	1.00	1	0.79	0.25
6.19 Pipe - (13)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.19 Pipe - (14)	CIRCULAR	1.00	1.00	1	0.79	0.25
5.59 Pipe - (16)	CIRCULAR	1.00	1.00	1	0.79	0.25
7.67 Pipe - (18)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.56 Pipe - (19)	CIRCULAR	1.00	1.00	1	0.79	0.25
4.29 Pipe - (2)	CIRCULAR	1.00	1.00	1	0.79	0.25
7.69 Pipe - (20)	CIRCULAR	1.00	1.00	1	0.79	0.25
2.79 Pipe - (21)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.59 Pipe - (22)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.56 Pipe - (23)	CIRCULAR	1.00	1.00	1	0.79	0.25
6.40 Pipe - (24)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.40 Pipe - (25)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.88 Pipe - (26)	CIRCULAR	1.00	1.00	1	0.79	0.25
2.52 Pipe - (27)	CIRCULAR	1.00	1.00	1	0.79	0.25
2.52 Pipe - (28)	CIRCULAR	1.00	1.00	1	0.79	0.25
8.05 Pipe - (29)	CIRCULAR	1.00	1.00	1	0.79	0.25
4.83 Pipe - (3)	CIRCULAR	1.00	1.00	1	0.79	0.25
6.35 Pipe - (30)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.56 Pipe - (31)	CIRCULAR	1.00	1.00	1	0.79	0.25
5.52 Pipe - (33)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.56 Pipe - (34)	CIRCULAR	1.00	1.00	1	0.79	0.25
2.54 Pipe - (35)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.73 Pipe - (4)	CIRCULAR	1.00	1.00	1	0.79	0.25
4.45 Pipe - (40)	CIRCULAR	1.00	1.00	1	0.79	0.25
6.43 Pipe - (41)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.56 Pipe - (43)	CIRCULAR	1.00	1.00	1	0.79	0.25

4 55								
4.77 Pipe - (44)	CIRC	ULAR	1.00	1.00		1	0.79	0.25
5.63 Pipe - (45)	CIRC	ULAR	1.50	1.50		1	1.77	0.38
14.86 Pipe - (5)	CIRC	ULAR	1.00	1.00		1	0.79	0.25
7.00 Pipe - (50)	CIRC	ULAR	1.50	1.50		1	1.77	0.38
30.06 Pipe - (51)	CIRC	ULAR	1.00	1.00		1	0.79	0.25
10.15 Pipe - (54)	CIRC	ULAR	1.00	1.00		1	0.79	0.25
8.20 Pipe - (55)	CIRC	ULAR	1.00	1.00		1	0.79	0.25
12.12 Pipe - (56)	CIRC	ULAR	1.00	1.00		1	0.79	0.25
6.17 Pipe - (57)	CIRC	ULAR	1.50	1.50		1	1.77	0.38
26.08 Pipe - (61)	CIRC	ULAR	1.00	1.00		1	0.79	0.25
5.92 Pipe - (62)	CIRC	ULAR	1.00	1.00		1	0.79	0.25
3.56 Pipe - (7)	CIRC	ULAR	1.00	1.00		1	0.79	0.25
7.14								
*******								
Transect Su								
Transect XS	G-L-Pipe -	(13)						
Area:	0 0005	0 0010	0.0042	0 0076	0 0110			
	0.0005 0.0170	0.0019 0.0232	0.0043 0.0305	0.0076 0.0390	0.0118 0.0487			
	0.0595	0.0715	0.0847	0.0990	0.1145			
	0.1312	0.1491	0.1682	0.1884	0.2098			
	0.2323 0.3604	0.2561 0.3871	0.2810 0.4137	0.3071 0.4404	0.3338 0.4670			
	0.4937	0.5203	0.5470	0.5736	0.6003			
	0.6269	0.6536	0.6802	0.7069	0.7335			
	0.7602 0.8934	0.7868 0.9201	0.8135 0.9467	0.8401 0.9734	0.8668 1.0000			
Hrad:	0.0551	0.5201	0.5107	0.5751	1.0000			
	0.0139	0.0278	0.0418	0.0557	0.0696			
	0.0835 0.1459	0.0963 0.1591	0.1080 0.1724	0.1202 0.1858	0.1329 0.1994			
	0.2130	0.2267	0.2404	0.2542	0.2680			
	0.2818	0.2957	0.3095	0.3238	0.3512			
	0.3784 0.5130	0.4055 0.5396	0.4326 0.5660	0.4595 0.5924	0.4863 0.6187			
	0.6448	0.6708	0.6968	0.7226	0.7483			
	0.7740	0.7995	0.8249	0.8502	0.8754			
Width:	0.9005	0.9256	0.9505	0.9753	1.0000			
wideli.	0.0355	0.0711	0.1066	0.1422	0.1777			
	0.2132	0.2520	0.2961	0.3402	0.3842			
	0.4283 0.6487	0.4724 0.6927	0.5164 0.7368	0.5605 0.7809	0.6046 0.8249			
	0.8690	0.9131	0.9572	1.0000	1.0000			
	1.0000	1.0000	1.0000	1.0000	1.0000			
	1.0000	1.0000	1.0000	1.0000	1.0000			
	1.0000	1.0000	1.0000 1.0000	1.0000 1.0000	1.0000			
	1.0000	1.0000	1.0000	1.0000	1.0000			

Transect XS	-L-Pipe -	(16)			
Area:					
	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312 0.2323	0.1491 0.2561	0.1682 0.2810	0.1884 0.3071	0.2098
	0.2323	0.3871	0.4137	0.4404	0.3336
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868	0.8135	0.8401	0.8668
	0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:					
	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835	0.0963	0.1080	0.1202	0.1329
	0.1459 0.2130	0.1591 0.2267	0.1724 0.2404	0.1858 0.2542	0.1994
	0.2130	0.2957	0.3095	0.3238	0.3512
	0.3784	0.4055	0.4326	0.4595	0.4863
	0.5130	0.5396	0.5660	0.5924	0.6187
	0.6448	0.6708	0.6968	0.7226	0.7483
	0.7740	0.7995	0.8249	0.8502	0.8754
	0.9005	0.9256	0.9505	0.9753	1.0000
Width:					
	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132 0.4283	0.2520 0.4724	0.2961 0.5164	0.3402 0.5605	0.3842
	0.4203	0.6927	0.7368	0.7809	0.8249
	0.8690	0.9131	0.9572	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
Transect XS	-L-Pipe -	(18)			
Area:					
	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312 0.2323	0.1491 0.2561	0.1682 0.2810	0.1884 0.3071	0.2098
	0.2323	0.2301	0.4137	0.4404	0.4670
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868	0.8135	0.8401	0.8668
	0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:	0 0120	0 0070	0 0410	0.0557	0.0606
	0.0139 0.0835	0.0278 0.0963	0.0418 0.1080	0.0557 0.1202	0.0696 0.1329
	0.0833	0.0903	0.1724	0.1858	0.1323
	0.2130	0.2267	0.2404	0.2542	0.2680
	0.2818	0.2957	0.3095	0.3238	0.3512
	0.3784	0.4055	0.4326	0.4595	0.4863
	0.5130	0.5396	0.5660	0.5924	0.6187
	0.6448	0.6708	0.6968	0.7226	0.7483
	0.7740	0.7995	0.8249	0.8502	0.8754
Width:	0.9005	0.9256	0.9505	0.9753	1.0000
WIGCII.	0.0355	0.0711	0.1066	0.1422	0.1777
	0.0333	0.2520	0.2961	0.3402	0.3842
	0.4283	0.4724	0.5164	0.5605	0.6046
	0.6487	0.6927	0.7368	0.7809	0.8249
	0.8690	0.9131	0.9572	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000

:	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
Transect XS-	L-Pipe -	(2)			
Area:					
	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312	0.1491	0.1682	0.1884	0.2098
	0.2323 0.3604	0.2561 0.3871	0.2810 0.4137	0.3071 0.4404	0.3336
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868	0.8135	0.8401	0.8668
	0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:		***			
	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835	0.0963	0.1080	0.1202	0.1329
	0.1459	0.1591	0.1724	0.1858	0.1994
	0.2130	0.2267	0.2404	0.2542	0.2680
1	0.2818	0.2957	0.3095	0.3238	0.3512
	0.3784	0.4055	0.4326	0.4595	0.4863
	0.5130	0.5396	0.5660	0.5924	0.6187
	0.6448	0.6708	0.6968	0.7226	0.7483
	0.7740	0.7995	0.8249	0.8502	0.8754
	0.9005	0.9256	0.9505	0.9753	1.0000
Width:	0.0355	0 0711	0 1066	0 1422	0 1777
	0.2132	0.0711 0.2520	0.1066 0.2961	0.1422 0.3402	0.1777 0.3842
	0.4283	0.2320	0.5164	0.5605	0.6046
	0.6487	0.6927	0.7368	0.7809	0.8249
	0.8690	0.9131	0.9572	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
:	1.0000	1.0000	1.0000	1.0000	1.0000
Transect XS-1	L-Pipe -	(24)			
	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312	0.1491	0.1682	0.1884	0.2098
1	0.2323	0.2561	0.2810	0.3071	0.3338
	0.3604	0.3871	0.4137	0.4404	0.4670
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868	0.8135	0.8401	0.8668
Hrad:	0.8934	0.9201	0.9467	0.9734	1.0000
	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835	0.0278	0.1080	0.1202	0.1329
	0.1459	0.1591	0.1724	0.1858	0.1994
	0.2130	0.2267	0.2404	0.2542	0.2680
	0.2818	0.2957	0.3095	0.3238	0.3512
	0.3784	0.4055	0.4326	0.4595	0.4863
	0.5130	0.5396	0.5660	0.5924	0.6187
	0.6448	0.6708	0.6968	0.7226	0.7483
	0.7740	0.7995	0.8249	0.8502	0.8754
	0.9005	0.9256	0.9505	0.9753	1.0000
Width:					
	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132	0.2520	0.2961	0.3402	0.3842
	0.4283	0.4724	0.5164	0.5605	0.6046

	0.6487 0.8690 1.0000 1.0000 1.0000 1.0000	0.6927 0.9131 1.0000 1.0000 1.0000 1.0000	0.7368 0.9572 1.0000 1.0000 1.0000 1.0000	0.7809 1.0000 1.0000 1.0000 1.0000 1.0000	0.8249 1.0000 1.0000 1.0000 1.0000 1.0000
Transect XS	G-L-Pipe -	(27)			
Hrad:	0.0005 0.0170 0.0595 0.1312 0.2323 0.3604 0.4937 0.6269 0.7602 0.8934	0.0019 0.0232 0.0715 0.1491 0.2561 0.3871 0.5203 0.6536 0.7868 0.9201	0.0043 0.0305 0.0847 0.1682 0.2810 0.4137 0.5470 0.6802 0.8135 0.9467	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401 0.9734	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668 1.0000
iii au•	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740	0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995 0.9256	0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754 1.0000
Width:	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000	0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000 1.0000	0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000	0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000 1.0000	0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000
Transect XS	G-L-Pipe -	(28)			
	0.0005 0.0170 0.0595 0.1312 0.2323 0.3604 0.4937 0.6269 0.7602 0.8934	0.0019 0.0232 0.0715 0.1491 0.2561 0.3871 0.5203 0.6536 0.7868 0.9201	0.0043 0.0305 0.0847 0.1682 0.2810 0.4137 0.5470 0.6802 0.8135 0.9467	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401 0.9734	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668 1.0000
Hrad:	0.0139 0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005	0.0278 0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995 0.9256	0.0418 0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.0557 0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.0696 0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754 1.0000

Width:	0.0355 0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000	0.0711 0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000	0.1066 0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000	0.1422 0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000 1.0000	0.1777 0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000
Transect XX	S-L-Pipe -	(30)			
	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312	0.1491	0.1682	0.1884	0.2098
	0.2323	0.2561	0.2810	0.3071	0.3338
	0.3604	0.3871	0.4137	0.4404	0.4670
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868	0.8135	0.8401	0.8668
	0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:	0.0139	0.0278	0.0418	0.0557	0.0696
Width:	0.0835	0.0963	0.1080	0.1202	0.1329
	0.1459	0.1591	0.1724	0.1858	0.1994
	0.2130	0.2267	0.2404	0.2542	0.2680
	0.2818	0.2957	0.3095	0.3238	0.3512
	0.3784	0.4055	0.4326	0.4595	0.4863
	0.5130	0.5396	0.5660	0.5924	0.6187
	0.6448	0.6708	0.6968	0.7226	0.7483
	0.7740	0.7995	0.8249	0.8502	0.8754
	0.9005	0.9256	0.9505	0.9753	1.0000
Width:	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132	0.2520	0.2961	0.3402	0.3842
	0.4283	0.4724	0.5164	0.5605	0.6046
	0.6487	0.6927	0.7368	0.7809	0.8249
	0.8690	0.9131	0.9572	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
Transect XS	S-L-Pipe -	(37)			
Area:	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312	0.1491	0.1682	0.1884	0.2098
	0.2323	0.2561	0.2810	0.3071	0.3338
	0.3604	0.3871	0.4137	0.4404	0.4670
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868	0.8135	0.8401	0.8668
	0.8934	0.9201	0.9467	0.9734	1.0000
	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835	0.0963	0.1080	0.1202	0.1329
	0.1459	0.1591	0.1724	0.1858	0.1994
	0.2130	0.2267	0.2404	0.2542	0.2680
	0.2818	0.2957	0.3095	0.3238	0.3512
	0.3784	0.4055	0.4326	0.4595	0.4863

	0.5130	0.5396	0.5660	0.5924	0.6187
	0.6448	0.6708	0.6968	0.7226	0.7483
	0.7740	0.7995	0.8249	0.8502	0.8754
ratalele e	0.9005	0.9256	0.9505	0.9753	1.0000
Width:	0.0355	0.0711	0.1066	0.1422	0.1777
	0.0333	0.2520	0.2961	0.3402	0.3842
	0.4283	0.4724	0.5164	0.5605	0.6046
	0.6487	0.6927	0.7368	0.7809	0.8249
	0.8690	0.9131	0.9572	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
Transect XS	-L-Pipe -	(50)			
Area:	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0003	0.0019	0.0305	0.0390	0.0118
	0.0595	0.0232	0.0847	0.0990	0.1145
	0.1312	0.1491	0.1682	0.1884	0.2098
	0.2323	0.2561	0.2810	0.3071	0.3338
	0.3604	0.3871	0.4137	0.4404	0.4670
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868	0.8135	0.8401	0.8668
	0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:					
	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835	0.0963	0.1080	0.1202	0.1329
	0.1459	0.1591	0.1724	0.1858	0.1994
	0.2130	0.2267	0.2404	0.2542	0.2680
	0.2818	0.2957	0.3095	0.3238	0.3512
	0.3784 0.5130	0.4055 0.5396	0.4326 0.5660	0.4595 0.5924	0.4863 0.6187
	0.6448	0.5390	0.6968	0.7226	0.7483
	0.7740	0.0708	0.8249	0.8502	0.8754
	0.9005	0.7555	0.9505	0.9753	1.0000
Width:	0.5005	0.5250	0.,,,,	0.7733	1.0000
	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132	0.2520	0.2961	0.3402	0.3842
	0.4283	0.4724	0.5164	0.5605	0.6046
	0.6487	0.6927	0.7368	0.7809	0.8249
	0.8690	0.9131	0.9572	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000 1.0000	1.0000	1.0000 1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
Transect XS	-L-Pipe -	(55)			
Area:	-	•			
	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312	0.1491	0.1682	0.1884	0.2098
	0.2323	0.2561	0.2810	0.3071	0.3338
	0.3604	0.3871	0.4137	0.4404	0.4670
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269 0.7602	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868 0.9201	0.8135 0.9467	0.8401 0.9734	0.8668 1.0000
Hrad:	0.0001	0.7201	0.7107	0.7/34	1.0000
	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835	0.0963	0.1080	0.1202	0.1329

Width:	0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005 0.0355 0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000	0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995 0.9256 0.0711 0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000	0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505 0.1066 0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000	0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753 0.1422 0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754 1.0000 0.1777 0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000		
*****	*****	****	Volume	Depth			
	uantity Cont:		acre-ft	inches			
	ecipitation ty Error (%)		0.596 0.682	0.718			
*****	* * * * * * * * * * * * *	****	Volume	Volume			
	ting Continu		acre-ft	Mgallons			
External Initial S Final Sto	Inflow Outflow Stored Volume ored Volume ty Error (%)	 e	0.000 0.248 0.000 0.000 -0.812	0.000 0.081 0.000 0.000			
Runoff Co	exxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxxx	omputations	Report				
					Area	Soil	Runoff
Soil/Suri	face Descript	tion 			(acres)	Group	Coeff.
Resident	25 years or ial Lot Size e Area & Weig	1 Acre, 25		reater	0.17 0.19 0.36	A (6%+) A (6%+)	0.79 0.29 0.53
Subbasin	Sub-CB-10	_					
Soil/Suri	face Descrip	tion			Area (acres)	Soil Group	Runoff Coeff.
Resident	25 years or ial Lot Size e Area & Weig	1 Acre, 25	_	reater	0.12 0.01 0.13	A (6%+) A (6%+)	0.79 0.29 0.75
Subbasin	Sub-CB-11	_					
		_			Area	Soil	Runoff

Soil/Surface Description	(acres)	Group	Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.11 0.09 0.20	A (6%+) A (6%+)	0.79 0.14 0.50
Subbasin Sub-CB-12			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.23 1.05 1.28	A (6%+) A (6%+)	0.79 0.14 0.26
Subbasin Sub-CB-13-14			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.25 0.09 0.34	A (6%+) A (6%+)	0.79 0.14 0.61
Subbasin Sub-CB-15-16			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Streets, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.19 0.05 0.16 0.40	A (6%+) A (6%+) B (0-2%)	0.79 0.29 0.80 0.73
Subbasin Sub-CB-17			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.15 0.13 0.29	A (6%+) A (6%+)	0.79 0.29 0.56
Subbasin Sub-CB-18-19			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.47 0.47 0.95	A (6%+) A (6%+)	0.79 0.29 0.54
Subbasin Sub-CB-2			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.17 0.23 0.40	A (6%+) A (6%+)	0.79 0.29 0.50

Subbasin Sub-CB-20			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.49 1.00 1.49	A (6%+) A (6%+)	0.79 0.14 0.35
Subbasin Sub-CB-3			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.14 2.69 2.84	A (6%+) A (6%+)	0.79 0.14 0.17
Subbasin Sub-CB-4			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.15 0.19 0.34	A (6%+) A (6%+)	0.79 0.14 0.43
Subbasin Sub-CB-5			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Soil/Surface Description	(acres)  0.32 0.01	Group  A (6%+)	Coeff. 0.79 0.14
Soil/Surface Description	(acres)  0.32 0.01	Group  A (6%+)	Coeff. 0.79 0.14
Soil/Surface Description	0.32 0.01 0.33	Group  A (6%+) A (6%+)  Soil	Coeff. 0.79 0.14 0.78
Soil/Surface Description  Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.  Subbasin Sub-CB-6  Soil/Surface Description  Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater	0.32 0.01 0.33 Area (acres)	Group  A (6%+) A (6%+)  Soil Group  A (2-6%)	Coeff.  0.79  0.14  0.78  Runoff Coeff.  0.77
Soil/Surface Description  Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.  Subbasin Sub-CB-6  Soil/Surface Description  Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.  Subbasin Sub-CB-7  Subbasin Sub-CB-7  Soil/Surface Description	0.32 0.01 0.33 Area (acres)	Group  A (6%+) A (6%+)  Soil Group  A (2-6%)	Coeff.  0.79  0.14  0.78  Runoff Coeff.  0.77
Soil/Surface Description  Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.32 0.01 0.33 Area (acres) 	Group  A (6%+) A (6%+)  Soil Group  A (2-6%) A (6%+)	Coeff.  0.79 0.14 0.78  Runoff Coeff.  0.77 0.29 0.76
Soil/Surface Description Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.  Subbasin Sub-CB-6 Soil/Surface Description Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.  Subbasin Sub-CB-7 Subbasin Sub-CB-7 Subbasin Sub-CB-7 Soil/Surface Description Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater	Area (acres)  0.32 0.01 0.33  Area (acres)  0.14 0.00 0.14  Area (acres)  0.10 0.01	Group  A (6%+)  A (6%+)  Soil Group  A (2-6%) A (6%+)  Soil Group  A (0-2%)	Coeff.  0.79 0.14 0.78  Runoff Coeff.  0.77 0.29 0.76  Runoff Coeff.  0.76 0.26

```
0.17 A (2-6%) 0.77
0.05 A (2-6%) 0.22
0.22 0.64
Streets, 25 years or greater
Meadow, 25 years or greater
Composite Area & Weighted Runoff Coeff.
                                                       0.22
Subbasin Sub-CB-9
______
                                                             Soil Runoff
Group Coeff
                                                      Area
Soil/Surface Description
                                                    (acres)
______
                                                    0.15 A (2-6%) 0.77
0.00 A (2-6%) 0.26
0.15 0.76
Streets, 25 years or greater
Residential Lot Size 1 Acre, 25 years or greater
Composite Area & Weighted Runoff Coeff.
SCS TR-55 Time of Concentration Computations Report
Sheet Flow Equation
       Tc = (0.007 * ((n * Lf)^0.8)) / ((P^0.5) * (Sf^0.4))
       Where:
       Tc = Time of Concentration (hrs)
       n = Manning's Roughness
       Lf = Flow Length (ft)
       P = 2 yr, 24 hr Rainfall (inches)
       Sf = Slope (ft/ft)
Shallow Concentrated Flow Equation
       V = 16.1345 * (Sf^0.5) (unpaved surface)

V = 20.3282 * (Sf^0.5) (paved surface)
       V = 15.0 * (Sf^0.5) (grassed waterway surface)
         = 10.0 * (Sf^0.5) (nearly bare & untilled surface)
       V = 9.0 * (Sf^0.5) (cultivated straight rows surface)
       V = 7.0 * (Sf^0.5) (short grass pasture surface)
         = 5.0 * (Sf^0.5) (woodland surface)
       V = 2.5 * (Sf^0.5) (forest w/heavy litter surface)
       Tc = (Lf / V) / (3600 sec/hr)
       Where:
       Tc = Time of Concentration (hrs)
       Lf = Flow Length (ft)
       V = Velocity (ft/sec)
       Sf = Slope (ft/ft)
Channel Flow Equation
       V = (1.49 * (R^{(2/3)}) * (Sf^{0.5})) / n
       R = Aq / Wp
       Tc = (Lf / V) / (3600 sec/hr)
       Where:
       Tc = Time of Concentration (hrs)
       Lf = Flow Length (ft)
       R = Hydraulic Radius (ft)
       Aq = Flow Area (ft<sup>2</sup>)
```

Wp = Wetted Perimeter (ft) V = Velocity (ft/sec) Sf = Slope (ft/ft)n = Manning's Roughness Subbasin Sub-CB-1 \_\_\_\_\_\_ Sheet Flow Computations Subarea A Subarea B Subarea С Manning's Roughness: 0.40 0.00 0.00 Flow Length (ft): 33.69 0.00 0.00 Slope (%): 0.00 1.60 0.00 2 yr, 24 hr Rainfall (in): 3.60 0.00 0.00 Velocity (ft/sec): 0.00 0.06 0.00 0.00 Computed Flow Time (minutes): 9.26 0.00 Shallow Concentrated Flow Computations Subarea A Subarea B Subarea С Flow Length (ft): 0.00 329.84 0.00 Slope (%): 0.77 0.00 0.00 Surface Type: Paved Paved Paved Velocity (ft/sec): 1.79 0.00 0.00 Computed Flow Time (minutes): 3.08 0.00 0.00 \_\_\_\_\_\_ Total TOC (minutes): 12.34 \_\_\_\_\_\_ Subbasin Sub-CB-10 User-Defined TOC override (minutes): 5.00 Subbasin Sub-CB-11 Sheet Flow Computations Subarea A Subarea B Subarea С Manning's Roughness: 0.40 0.00 0.00

73.91

24.40

0.00

0.00

Slope (%):

0.00

Flow Length (ft):

0 00				
0.00	2 yr, 24 hr Rainfall (in):	3.60	0.00	
0.00	Velocity (ft/sec):	0.21	0.00	
0.00	Computed Flow Time (minutes):	5.85	0.00	
0.00				
	ow Concentrated Flow Computations			
С		Subarea A	Subarea B	Subarea
0.00	Flow Length (ft):	147.74	0.00	
0.00	Slope (%):	2.17	0.00	
Paved	Surface Type:	Paved	Paved	
0.00	Velocity (ft/sec):	2.99	0.00	
0.00	Computed Flow Time (minutes):	0.82	0.00	
		:==========	=======================================	=========
	Total TOC (minutes):	6.67		
======		=======================================	=======================================	========
	Flow Computations	Qulbarra 3	Quibaura D	Colorado
		Subarea A	Subarea B	Subarea
	Manning's Roughness:	0.40	0.00	Subarea
С	Manning's Roughness: Flow Length (ft):	0.40	0.00	Subarea
C 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):	0.40 222.44 10.60	0.00 0.00 0.00	Subarea
C 0.00 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):	0.40 222.44 10.60 3.60	0.00 0.00 0.00 0.00	Subarea
C 0.00 0.00 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):	0.40 222.44 10.60	0.00 0.00 0.00	Subarea
C 0.00 0.00 0.00 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):	0.40 222.44 10.60 3.60	0.00 0.00 0.00 0.00	Subarea
C 0.00 0.00 0.00 0.00 0.00 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):  Velocity (ft/sec):	0.40 222.44 10.60 3.60 0.19	0.00 0.00 0.00 0.00	Subarea
C 0.00 0.00 0.00 0.00 0.00 0.00 Shallo	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):  Velocity (ft/sec):  Computed Flow Time (minutes):	0.40 222.44 10.60 3.60 0.19	0.00 0.00 0.00 0.00	Subarea
C 0.00 0.00 0.00 0.00 0.00 Shall C	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):  Velocity (ft/sec):  Computed Flow Time (minutes):  ow Concentrated Flow Computations	0.40 222.44 10.60 3.60 0.19 19.70	0.00 0.00 0.00 0.00 0.00	
C 0.00 0.00 0.00 0.00 0.00 Shall C 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):  Velocity (ft/sec):  Computed Flow Time (minutes):  ow Concentrated Flow Computations	0.40 222.44 10.60 3.60 0.19 19.70	0.00 0.00 0.00 0.00 0.00 0.00	
C 0.00 0.00 0.00 0.00 Shall C 0.00 0.00 0.00 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):  Velocity (ft/sec):  Computed Flow Time (minutes):  ow Concentrated Flow Computations  Flow Length (ft):	0.40 222.44 10.60 3.60 0.19 19.70 Subarea A 185.02	0.00 0.00 0.00 0.00 0.00 0.00 Subarea B	
C 0.00 0.00 0.00 0.00 0.00 C 0.00 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):  Velocity (ft/sec):  Computed Flow Time (minutes):  ow Concentrated Flow Computations  Flow Length (ft):  Slope (%):	0.40 222.44 10.60 3.60 0.19 19.70 Subarea A 185.02 4.77	0.00 0.00 0.00 0.00 0.00 0.00 Subarea B 0.00	
C 0.00 0.00 0.00 0.00 0.00 C 0.00 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):  Velocity (ft/sec):  Computed Flow Time (minutes):  ow Concentrated Flow Computations  Flow Length (ft):  Slope (%):  Surface Type:	0.40 222.44 10.60 3.60 0.19 19.70  Subarea A 185.02 4.77 Paved	0.00 0.00 0.00 0.00 0.00 0.00 Subarea B 0.00 0.00	
C 0.00 0.00 0.00 0.00 0.00 C 0.00 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):  Velocity (ft/sec):  Computed Flow Time (minutes):  ow Concentrated Flow Computations  Flow Length (ft):  Slope (%):  Surface Type:  Velocity (ft/sec):	0.40 222.44 10.60 3.60 0.19 19.70 Subarea A 185.02 4.77 Paved 4.44	0.00 0.00 0.00 0.00 0.00 0.00 Subarea B 0.00 0.00 Paved 0.00	

	Total TOC (minutes):	20.39		
======		=======================================	=======================================	========
	in Sub-CB-13-14			
	Flow Computations			
C		Subarea A	Subarea B	Subarea
0.00	Manning's Roughness:	0.40	0.00	
0.00	Flow Length (ft):	80.13	0.00	
0.00	Slope (%):	24.40	0.00	
0.00	2 yr, 24 hr Rainfall (in):	3.60	0.00	
0.00	Velocity (ft/sec):	0.21	0.00	
0.00	Computed Flow Time (minutes):	6.23	0.00	
	w Concentrated Flow Computations			
		Subarea A	Subarea B	Subarea
C	Flow Length (ft):	174.35	0.00	
0.00	Slope (%):	2.45	0.00	
0.00	Surface Type:	Paved	Paved	
Paved	Velocity (ft/sec):	3.18	0.00	
0.00	Computed Flow Time (minutes):	0.91	0.00	
		.========	=======================================	:=======
	Total TOC (minutes):	7.15		
======		=======================================	===========	========
Subbas	in Sub-CB-15-16			
	User-Defined TOC override (minutes):	5.00		
Subbas	in Sub-CB-17			
	User-Defined TOC override (minutes):	5.00		
	in Sub-CB-18-19			
	User-Defined TOC override (minutes):	5.00		

## Subbasin Sub-CB-2

User-Defined TOC override (minutes): 5.00

Subbasin Sub-CB-20

Sheet Flow Computations

		Subarea A	Subarea B	Subarea
C	Manning's Roughness:	0.40	0.00	
0.00	Flow Length (ft):	227.22	0.00	
0.00	Slope (%):	7.48	0.00	
0.00	2 yr, 24 hr Rainfall (in):	3.60	0.00	
0.00	Velocity (ft/sec):	0.16	0.00	
0.00	Computed Flow Time (minutes):	23.04	0.00	
0.00				
Shallo	w Concentrated Flow Computations			
	<del>-</del>	Subarea A	Subarea B	Subarea
C	Flow Length (ft):	Subarea A	Subarea B	Subarea
C 0.00	Flow Length (ft): Slope (%):			Subarea
C 0.00 0.00	J , ,	193.35	0.00	Subarea
C 0.00 0.00 Paved	Slope (%):	193.35 2.77	0.00	Subarea
C 0.00 0.00 Paved 0.00	Slope (%): Surface Type:	193.35 2.77 Paved	0.00 0.00 Paved	Subarea
C 0.00 0.00 Paved	Slope (%): Surface Type: Velocity (ft/sec):	193.35 2.77 Paved 3.38	0.00 0.00 Paved 0.00	Subarea

\_\_\_\_\_\_

Subbasin Sub-CB-3

Sheet Flow Computations

a		Subarea A	Subarea B	Subarea
C	Manning's Roughness:	0.40	0.00	
0.00	Flow Length (ft):	492.34	0.00	
0.00	Slope (%):	3.89	0.00	
0.00	2 yr, 24 hr Rainfall (in):	3.60	0.00	
0.00	Velocity (ft/sec):	0.15	0.00	
0.00	Computed Flow Time (minutes):	55.54	0.00	

	Concentrated Flow	_			
			Subarea A		Suba
00	Flow Length (ft):		70.73	0.00	
00	Slope (%):		4.87	0.00	
ved	Surface Type:		Unpaved	Paved	
0.0	Velocity (ft/sec)	:	3.56	0.00	
00	Computed Flow Tim	e (minutes):	0.33	0.00	
				===========	
	Total TOC (minute		55.87		
Subbasin	Sub-CB-4				
	User-Defined TOC	override (minutes	): 5.00		
	 1 Sub-CB-5				
	User-Defined TOC	override (minutes	): 5.00		
Subbasin	 1 Sub-CB-6				
	User-Defined TOC	override (minutes	): 5.00		
	 n Sub-CB-7				
	User-Defined TOC	override (minutes	5.00		
Subbasin	n Sub-CB-8W				
	User-Defined TOC	override (minutes	): 5.00		
Subbasin	Sub-CB-9				
	User-Defined TOC	override (minutes	): 5.00		
Subbasin	*****************  Runoff Summary  ***************				
 Subbasin ID	a Accumulate Preci	d Rainfall	Total Pea Runoff Runof	k Weighted f Runoff Cor	Time of accentration

	in	in/hr	in	cfs	Coeff	days	hh:mm:ss
Sub-CB-1	0.60	2.92	0.32	0.56	0.530	0	00:12:20
Sub-CB-10	0.39	4.72	0.29	0.45	0.750	0	00:05:00
Sub-CB-11	0.45	4.05	0.22	0.40	0.500	0	00:06:40
Sub-CB-12	0.75	2.22	0.20	0.74	0.260	0	00:20:23
Sub-CB-13-14	0.47	3.90	0.28	0.80	0.610	0	00:07:09
Sub-CB-15-16	0.39	4.72	0.29	1.39	0.730	0	00:05:00
Sub-CB-17	0.39	4.72	0.22	0.75	0.560	0	00:05:00
Sub-CB-18-19	0.39	4.72	0.21	2.42	0.540	0	00:05:00
Sub-CB-2	0.39	4.72	0.20	0.95	0.500	0	00:05:00
Sub-CB-20	0.81	2.03	0.28	1.06	0.350	0	00:23:59
Sub-CB-3	1.11	1.19	0.19	0.58	0.170	0	00:55:52
Sub-CB-4	0.39	4.72	0.17	0.70	0.430	0	00:05:00
Sub-CB-5	0.39	4.72	0.31	1.21	0.780	0	00:05:00
Sub-CB-6	0.39	4.72	0.30	0.51	0.760	0	00:05:00
Sub-CB-7	0.39	4.72	0.28	0.37	0.720	0	00:05:00
Sub-CB-8W	0.39	4.72	0.25	0.67	0.640	0	00:05:00
Sub-CB-9	0.39	4.72	0.30	0.53	0.760	0	00:05:00

\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*
Node Depth Summary
\*\*\*\*\*\*\*\*\*\*\*\*\*\*

Node ID	Average Depth Attained ft	Maximum Depth Attained ft	Maximum HGL Attained ft		of Max urrence	Total Flooded Volume acre-in	Total Time Flooded minutes	Retention Time
CB-8E	0.00	0.00	257.54	0	00:00	0	0	0:00:00
CIT-8	2.69	2.69	257.49	0	00:00	0	0	0:00:00
CIT-9	2.27	2.53	259.93	0	00:05	0	0	0:00:00
DH-10	0.10	0.39	265.54	0	00:05	0	0	0:00:00
DH-13	2.76	3.07	262.87	0	00:07	0	0	0:00:00
DH-20	0.01	0.31	277.93	0	00:24	0	0	0:00:00
DH-6	0.05	0.24	247.19	0	00:05	0	0	0:00:00
DMH-10	0.10	0.39	265.71	0	00:05	0	0	0:00:00
DMH-11	0.10	0.25	269.00	0	00:06	0	0	0:00:00
DMH-12	0.34	0.64	268.34	0	00:20	0	0	0:00:00
DMH-13	0.10	0.49	263.26	0	00:07	0	0	0:00:00
DMH-20	0.44	0.74	278.39	0	00:24	0	0	0:00:00
DMH-3	0.11	0.33	262.57	0	00:05	0	0	0:00:00
DMH-4N	0.11	0.40	253.25	0	00:05	0	0	0:00:00
DMH-4S	0.11	0.35	257.48	0	00:05	0	0	0:00:00
DMH-6	4.85	5.12	252.52	0	00:05	0	0	0:00:00
DMH-7	1.10	1.32	255.42	0	00:05	0	0	0:00:00
EX-18	3.00	3.46	269.46	0	00:05	0	0	0:00:00
EX-7	1.20	1.40	254.20	0	00:05	0	0	0:00:00
Structure - (72	0.11	0.31	276.10	0	00:12	0	0	0:00:00
STU-16	0.28	0.54	253.24	0	00:05	0	0	0:00:00
STU-5	0.11	0.50	249.13	0	00:06	0	0	0:00:00
DP-1	0.00	0.26	275.26	0	00:12	0	0	0:00:00
DP-10	0.00	0.23	265.01	0	00:05	0	0	0:00:00
DP-13	0.01	0.37	259.97	0	00:07	0	0	0:00:00
DP-16	0.00	0.54	253.20	0	00:05	0	0	0:00:00
DP-18	0.01	0.41	264.77	0	00:05	0	0	0:00:00
DP-20	0.01	0.29	274.49	0	00:24	0	0	0:00:00
DP-5	0.01	0.41	248.41	0	00:06	0	0	0:00:00
DP-6	0.00	0.17	246.67	0	00:05	0	0	0:00:00
DP-7	0.00	0.43	253.03	0	00:06	0	0	0:00:00
OFFSITE1	0.00	0.05	281.27	0	00:17	0	0	0:00:00
OFFSITE-1	0.00	0.17	267.85	0	00:25	0	0	0:00:00

Node							
ID	Type	Lateral	Inflow	Peak	Inflow	Flooding	Flooding
		Inflow		0ccu	rrence	Overflow	Occurrence days hh:mm
		cfs	cfs	days	hh:mm	cfs	days hh:mm
CB-8E	JUNCTION	0.00					
CIT-8	JUNCTION		1.05		00:05		
CIT-9	JUNCTION	0.00	0.50	0	00:05	0.00	
DH-10	JUNCTION	0.00	0.71	0	00:05	0.00	
DH-13	JUNCTION	0.00	1.04	0	00:07	0.00	
DH-20	JUNCTION JUNCTION JUNCTION	0.00	2.13	0	00:24	0.00	
DH-6	JUNCTION	0.00	0.51	0	00:05	0.00	
DMH-10	JUNCTION	0.00	0.45	0	00:05	0.00	
DMH-11	JUNCTION	0.00	0.40	0	00:06	0.00	
DMH-12	JUNCTION	0.00	0.72	0	00:20	0.00	
DMH-13	JUNCTION	0.00	0.80	0	00:07	0.00	
DMH-20	JUNCTION	0.00	2.13	0	00:24	0.00	
DMH-3	JUNCTION	0.00	0.95	0	00:05	0.00	
DMH-4N	JUNCTION	() ()()	1.52	0	00:05	0.00	
DMH-4S	JUNCTION		0.95	0		0.00	
DMH-6	JUNCTION	0.00	0.51	0	00:05	0.00	
DMH-7	JUNCTION	0.00	0.37	0	00:05	0.00	
EX-18	JUNCTION	0.00	2.41	0	00:05	0.00	
EX-7	JUNCTION	0.00	1.35	0	00:06	0.00	
Structure - (72)	JUNCTION	0.00	0.52	0	00:12	0.00	
STU-16	JUNCTION JUNCTION OUTFALL	0.00	2.03	0	00:05	0.00	
STU-5	JUNCTION	0.00	2.47	0	00:06	0.00	
DP-1	OUTFALL	0.00	0.52	0	00:12	0.00	
DP-10	OUTFALL	0.00	0.71	0	00:05	0.00	
DP-13	OUTFALL	0.00	1.03	0	00:07	0.00	
DP-16	OUTFALL	0.00	2.03	0	00:05	0.00	
DP-18	OUTFALL	0.00	2.39	0	00:05	0.00	
DP-20	OUTFALL	0.00	2.12	0	00:24	0.00	
DP-5	OUTFALL	0.00	2.47	0	00:06	0.00	
DP-6	OUTFALL	0.00	0.51	0	00:05	0.00	
DP-7	OUTFALL		1.35	0	00:06	0.00	
OFFSITE1	OUTFALL	0.00		0		0.00	
OFFSITE-1	OUTFALL	0.00	0.69	0	00:25	0.00	

Inlet ID	Max Gutter Spread during Peak Flow ft	Max Gutter Water Elev during Peak Flow ft	Max Gutter Water Depth during Peak Flow ft	M	ime of aximum Depth arrence hh:mm
CB-1	4.47	281.39	0.17	0	00:12
CB-10	2.18	267.82	0.13	0	00:05
CB-11	2.07	272.23	0.13	0	00:06
CB-12	2.72	271.23	0.16	0	00:20
CB-13	3.27	264.98	0.13	0	00:07
CB-16	4.43	255.11	0.18	0	00:05
CB-17	5.30	265.68	0.19	0	00:05
CB-18	9.71	274.02	0.30	0	00:05
CB-2	3.03	277.00	0.18	0	00:05

CB-20	3.26	279.80	0.13	0	00:00
CB-3	2.44	265.54	0.15	0	00:56
CB-4	2.65	256.09	0.16	0	00:05
CB-5	4.06	251.35	0.17	0	00:05
CB-6	2.31	255.49	0.14	0	00:05
CB-7	1.99	258.53	0.12	0	00:05
CB-8W	4.37	260.25	0.17	0	00:05
CB-9	2.35	262.96	0.14	0	00:05

- Inlet	Peak	Peak	Peak	Peak	Inlet	Total
Total ID Time	Flow	Lateral	Flow	Flow	Efficiency	Flooding
		Flow	Intercepted	Bypassing	during	
Flooded	cfs	cfs		Inlet cfs	Peak Flow %	acre-in
minutes						
-						
CB-1 0	0.56	0.56	0.52	0.04	93.21	0.000
CB-10	0.45	0.45	0.45	0.00	99.92	0.000
CB-11	0.40	0.40	0.40	0.00	99.99	0.000
CB-12	0.74	0.74	0.72	0.01	98.05	0.000
CB-13	0.80	0.80	-	-	-	0.000
CB-16	1.42	1.39	_	-	-	0.000
CB-17	0.75	0.75	0.67	0.09	88.70	0.000
CB-18	2.42	2.42	-	-	_	0.000
CB-2	0.95	0.95	0.91	0.04	95.99	0.000
CB-20	1.06	1.06	-	-	_	0.000
CB-3	0.58	0.58	0.57	0.00	99.34	0.000
CB-4	0.70	0.70	0.69	0.01	98.42	0.000
CB-5	1.21	1.21	-	_	_	0.000
CB-6	0.51	0.51	0.51	0.00	99.70	0.000
0 CB-7	0.37	0.37	0.37	0.00	100.00	0.000
0 CB-8W	0.67	0.67	0.62	0.05	93.01	0.000
0 CB-9 0	0.53	0.53	0.50	0.03	94.98	0.000

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## Outfall Loading Summary

Outfall Node ID	Flow Frequency (%)	Average Flow cfs	Peak Inflow cfs
DP-1 DP-10 DP-13 DP-16 DP-18 DP-20 DP-5 DP-6 DP-7 OFFSITE1	1.90 1.33 3.25 1.27 0.87 3.39 8.50 0.73 2.26 2.61	0.24 0.26 0.44 0.59 0.96 1.05 0.38 0.24 0.24	0.52 0.71 1.03 2.03 2.39 2.12 2.47 0.51 1.35 0.02
System	2.78	4.67	10.74

Link ID	Element	Т	ime of	Maximum	Length	Peak Flow	Design	Ratio of
Ratio of To	tal Reported			1.				1
Maximum Ti	Type .me Condition	Pea	k Flow	Velocity	Factor	during	Flow	Maximum
Maxillulli II	.me condition	Occii	rrence	Attained		Analweie	Capacity	/Design
Flow Surcharged		occu	I I CIICC	Accarnea		Analysis	capacity	/ Design
		days	hh:mm	ft/sec		cfs	cfs	Flow
Depth minutes	\$							
CB-1 Overflow	CHANNEL	0	00:17	1.59	1.00	0.02	2.70	0.01
0.17 0	Calculated							
CB10-9_Gutter	CHANNEL	0	00:10	0.00	1.00	0.00	8.35	0.00
0.03 0	Calculated							
CB11-10_Gutter		0	00:13	0.00	1.00	0.00	7.95	0.00
	Calculated							
CB12-13_Gutter		0	00:23	1.81	1.00	0.02	9.44	0.00
	Calculated	0	00:06	5.27	1 00	0 07	12.30	0 01
	CHANNEL Calculated	0	00.06	5.47	1.00	0.07	12.30	0.01
CB2-3 Gutter		0	00:06	3.39	1.00	0.03	13.13	0.00
0.10 0		O	00.00	3.37	1.00	0.03	13.13	0.00
CB3-4 Gutter		0	00:58	1.29	1.00	0.01	11.64	0.00
0.06 0								
CB4-5_Gutter	CHANNEL	0	00:06	1.77	1.00	0.01	8.25	0.00
0.07 0	Calculated							
_	CHANNEL	0	00:10	0.00	1.00	0.00	7.73	0.00
0.03 0								
	CHANNEL	0	00:10	0.00	1.00	0.00	6.62	0.00
	Calculated		00.00	1 (4	1 00	0.00	4 00	0 01
CB8-7_Gutter 0.14 0		0	00:06	1.64	1.00	0.03	4.89	0.01
0.14 0 CB9-8_Gutter		0	00:10	2.41	1.00	0.02	6.26	0.00
0.10 0		U	00.10	2.41	1.00	0.02	0.20	0.00
L-Pipe - (50)		0	00:25	7.62	1.00	0.69	41.01	0.02
(50)		-				05		

0.22	0	Calculated							
Pipe - (12)	U	CONDUIT	0	00:05	4.76	1.00	0.51	6.19	0.08
0.19	0	Calculated							
Pipe - (13) 0.27	0	CONDUIT Calculated	0	00:05	2.97	1.00	0.51	3.19	0.16
Pipe - (14)	U	CONDUIT	0	00:05	5.70	1.00	1.21	5.59	0.22
0.32	0	Calculated							
Pipe - (16) 0.18	0	CONDUIT Calculated	0	00:56	5.73	1.00	0.57	7.67	0.07
Pipe - (18)	U	CONDUIT	0	00:05	2.93	1.00	0.37	3.56	0.10
0.22	0	Calculated							
Pipe - (19) 0.20	0	CONDUIT Calculated	0	00:05	3.34	1.00	0.37	4.29	0.09
Pipe - (2)	U	CONDUIT	0	00:05	11.06	1.00	0.88	7.69	0.11
0.23	0	Calculated							
Pipe - (20) 0.00	0	CONDUIT Calculated	0	00:00	0.00	1.00	0.00	2.79	0.00
Pipe - (21)		CONDUIT	0	00:06	4.06	1.00	1.03	3.59	0.29
0.36	0	Calculated CONDUIT	0	00:06	4.23	1.00	1.35	3.56	0.38
Pipe - (22) 0.43	0	Calculated	U	00.06	4.23	1.00	1.35	3.50	0.36
Pipe - (23)		CONDUIT	0	00:05	5.15	1.00	0.61	6.40	0.10
0.21 Pipe - (24)	0	Calculated CONDUIT	0	00:05	3.10	1.00	0.50	3.40	0.15
0.26	0	Calculated	O	00.03	3.10	1.00	0.30	3.10	0.15
Pipe - (25)	^	CONDUIT	0	00:05	4.58	1.00	0.48	3.88	0.12
0.24 Pipe - (26)	0	Calculated CONDUIT	0	00:05	2.43	1.00	0.45	2.52	0.18
0.29	0	Calculated							
Pipe - (27) 0.29	0	CONDUIT Calculated	0	00:05	2.42	1.00	0.45	2.52	0.18
Pipe - (28)	U	CONDUIT	0	00:06	5.35	1.00	0.40	8.05	0.05
0.15	0	Calculated							
Pipe - (29) 0.19	0	CONDUIT Calculated	0	00:07	5.37	1.00	0.39	4.83	0.08
Pipe - (3)	Ü	CONDUIT	0	00:06	5.86	1.00	0.94	6.35	0.15
0.26	0	Calculated	0	00.20	2 55	1 00	0.70	2 56	0 20
Pipe - (30) 0.30	0	CONDUIT Calculated	U	00:20	3.55	1.00	0.72	3.56	0.20
Pipe - (31)		CONDUIT	0	00:20	5.20	1.00	0.71	5.52	0.13
0.24 Pipe - (33)	0	Calculated CONDUIT	0	00:07	3.93	1.00	1.03	3.56	0.29
0.37	0	Calculated	Ü	00-07	3.75	1.00	1.03	3.30	0.25
Pipe - (34)	0	CONDUIT	0	00:07	2.87	1.00	0.80	2.54	0.31
0.39 Pipe - (35)	0	Calculated CONDUIT	0	00:07	3.79	1.00	0.80	3.73	0.21
0.31	0	Calculated							
Pipe - (4) 0.40	0	CONDUIT Calculated	0	00:06	5.26	1.00	1.50	4.45	0.34
Pipe - (40)	Ü	CONDUIT	0	00:05	9.18	1.00	0.64	6.43	0.10
0.21	0	Calculated	0	00.05	4 60	1 00	0.00	2 56	0 55
Pipe - (41) 0.54	0	CONDUIT Calculated	0	00:05	4.68	1.00	2.03	3.56	0.57
Pipe - (43)		CONDUIT	0	00:05	5.30	1.00	1.42	4.77	0.30
0.37 Pipe - (44)	0	Calculated CONDUIT	0	00:05	6.91	1.00	2.41	5.63	0.43
0.46	0	Calculated	U	00.03	0.91	1.00	2.41	5.03	0.43
Pipe - (45)		CONDUIT	0	00:05	6.22	1.00	2.39	14.86	0.16
0.27 Pipe - (5)	0	Calculated CONDUIT	0	00:06	8.14	1.00	2.47	7.00	0.35
0.41	0	Calculated	3	00700					
Pipe - (50)	0	CONDUIT	0	00:24	9.84	1.00	2.13	30.06	0.07
0.18 Pipe - (51)	0	Calculated CONDUIT	0	00:24	10.22	1.00	2.13	10.15	0.21
0.31	0	Calculated							
Pipe - (54)		CONDUIT	0	00:05	5.79	1.00	0.51	8.20	0.06

0.17	0	Calculated							
Pipe - (55)		CONDUIT	0	00:05	8.32	1.00	0.68	12.12	0.06
0.16	0	Calculated							
Pipe - (56)		CONDUIT	0	00:05	5.23	1.00	0.71	6.17	0.12
0.23	0	Calculated							
Pipe - (57)		CONDUIT	0	00:24	8.90	1.00	2.12	26.08	0.08
0.19	0	Calculated							
Pipe - (61)		CONDUIT	0	00:12	5.28	1.00	0.52	5.92	0.09
0.20	0	Calculated							
Pipe - (62)		CONDUIT	0	00:12	3.24	1.00	0.52	3.56	0.14
0.26	0	Calculated							
Pipe - (7)		CONDUIT	0	00:05	6.36	1.00	0.95	7.14	0.13
0.25	Λ	Calgulated							

All links are stable.

WARNING 108: Surcharge elevation defined for Junction EX-18 is below junction maximum elevation. Assumed surcharge elevation equal to maximum elevation.

WARNING 139 : Ponded area defined for on sag Inlet CB-18 is zero. Assumed ponded area equal to 10 ft $^2$  (0.929 m $^2$ ).

WARNING 138: Initial water surface elevation defined for Inlet CB-20 is below catchbasin invert elevation.

Assumed initial water surface elevation equal to catchbasin inlet invert

elevation.

WARNING 138: Initial water surface elevation defined for Inlet CB-4 is below catchbasin invert elevation.

Assumed initial water surface elevation equal to catchbasin inlet invert

elevation.

WARNING 138: Initial water surface elevation defined for Inlet CB-5 is below catchbasin invert elevation.

Assumed initial water surface elevation equal to catchbasin inlet invert

elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB-1\_Overflow is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB10-9\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB11-10\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB12-13\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB17-16\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB2-3\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB3-4\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB4-5\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB6-5\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB7-6\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB8-7\_Gutter is below the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB9-8\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 117 : Conduit outlet invert elevation defined for Conduit CB-1\_Overflow is below downstream node invert elevation.

Assumed conduit outlet invert elevation equal to downstream node invert

elevation.

WARNING 004 : Minimum elevation drop used for Conduit CB-1\_Overflow.

WARNING 005: Minimum slope used for Conduit CB-1\_Overflow.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB10-9\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-9.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB11-10\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-10.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB12-13\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-13.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB17-16\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-16.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB2-3\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-3.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB3-4\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-4.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB4-5\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-5.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB6-5\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-5.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB7-6\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-6.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB8-7\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-7.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB9-8\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-8W.

WARNING 116 : Conduit inlet invert elevation defined for Conduit Pipe - (14) is below upstream node invert elevation.

Assumed conduit inlet invert elevation equal to upstream node invert elevation. WARNING 116: Conduit inlet invert elevation defined for Conduit Pipe - (50) is below upstream node invert elevation.

Assumed conduit inlet invert elevation equal to upstream node invert elevation. WARNING 116: Conduit inlet invert elevation defined for Conduit Pipe - (55) is below upstream node invert elevation.

Assumed conduit inlet invert elevation equal to upstream node invert elevation.

Analysis began on: Tue Jan 31 11:09:22 2023 Analysis ended on: Tue Jan 31 11:09:24 2023

Total elapsed time: 00:00:02

```
Autodesk® Storm and Sanitary Analysis 2016 - Version 13.2.165 (Build 0)
Project Description
******
File Name ..... Grove_St_Ph2_r1-PR.SPF
******
Analysis Options
******
Flow Units ..... cfs
Subbasin Hydrograph Method. Rational
Time of Concentration..... SCS TR-55
Return Period...... 10 years
Link Routing Method ...... Kinematic Wave Storage Node Exfiltration. None
Starting Date ..... DEC-20-2022 00:00:00
Ending Date ..... DEC-21-2022 00:00:00 Report Time Step ..... 00:00:10
******
Element Count
Number of subbasins ..... 17
Number of nodes ..... 50
Number of links ..... 52
******
Subbasin Summary
******
Subbasin
                      Total
                        Area
TD
                       acres
Sub-CB-1
                    0.36
0.13
0.20
1.28
0.34
0.40
0.29
Sub-CB-10
Sub-CB-11
Sub-CB-12
Sub-CB-12
Sub-CB-13-14
Sub-CB-15-16
Sub-CB-17
Sub-CB-18-19
                       0.95
Sub-CB-2
                        0.40
                        1.49
Sub-CB-20
Sub-CB-3
                        2.84
Sub-CB-4
                        0.34
                        0.33
Sub-CB-5
Sub-CB-6
                        0.14
Sub-CB-7
                        0.11
Sub-CB-8W
                        0.22
Sub-CB-9
                        0.15
*****
Node Summary
                  Element Invert Maximum Ponded External Type Elevation Elev. Area Inflow ft ft ft
Node
TD
```

257.54 259.20 0.00

JUNCTION

CB-8E

CIT-8 CIT-9 DH-10 DH-13		JUNCTION JUNCTION JUNCTION JUNCTION		259.42 40 262.67 L5 268.15 30 265.60	0.00 0.00 0.00 0.00		
DH-20		JUNCTION		52 280.21	0.00		
DH-6		JUNCTION	246.	95 255.72	0.00		
DMH-10		JUNCTION		32 267.86	0.00		
DMH-11		JUNCTION		75 272.24	0.00		
DMH-12		JUNCTION		70 271.08	0.00		
DMH-13		JUNCTION	262.	77 265.40 55 280.22	0.00		
DMH-20		JUNCTION	277.	55 280.22	0.00		
DMH-3		JUNCTION	262.	24 265.34 35 255.95	0.00		
DMH-4N		JUNCTION			0.00		
DMH-4S		JUNCTION	257.	13 262.56	0.00		
DMH-6		JUNCTION		257.58	0.00		
DMH-7		JUNCTION		10 258.76	0.00		
EX-18		JUNCTION		273.24	0.00		
EX-7	(72)	JUNCTION		30 258.62	0.00		
Structure STU-16	- (72)	JUNCTION JUNCTION	273.	79 277.57 70 255.49	0.00		
STU-5		JUNCTION	248	53 251 88	0.00		
DP-1		OUTFALL	275	251.88 276.00	0.00		
DP-10		OUTFALL		78 265.78	0.00		
DP-13		OUTFALL		260.60	0.00		
DP-16		OUTFALL		56 253.66	0.00		
DP-18		OUTFALL			0.00		
DP-20		OUTFALL	274.	36 265.86 20 275.70	0.00		
DP-5		OUTFALL	248.	00 249.00	0.00		
DP-6		OUTFALL	246.	249.00 247.50	0.00		
DP-7		OUTFALL	252.	50 253.60	0.00		
OFFSITE1		OUTFALL	281.	22 281.50	0.00		
OFFSITE-1		OUTFALL	267.	58 268.43	0.00		
*********  Inlet Summ  *******  Inlet  Catchbasin	nary :***	Inlet	Initial	Manufacturer Grate		Inlet	Number
Inlet Summ *******  Inlet  Catchbasin	nary :***	Let Ponded		Grate			
Inlet Summ ******* Inlet	nary **** Inl	let Ponded Manufacture	<u> </u>	Grate Part		Inlet Location	Number of
Inlet Summ ******* Inlet Catchbasin ID	nary **** Inl	Let Ponded	<u> </u>	Grate Part			
Inlet Summ ******* Inlet Catchbasin ID	nary **** Inl Rim	let Ponded Manufacture: Area	<u> </u>	Grate Part Logging Number			of
Inlet Summ ******* Inlet Catchbasin ID Invert Elevation	nary *** Inl Rim Elevatio	let Ponded Manufacture Area on	Water C	Grate Part Logging Number Factor			of
Inlet Summ ******* Inlet Catchbasin ID Invert Elevation	nary **** Inl Rim	let Ponded Manufacture Area on	. Water C	Grate Part Logging Number			of
Inlet Summ ******* Inlet Catchbasin ID Invert Elevation	nary *** Inl Rim Elevatio	let Ponded Manufacture Area on	Water C	Grate Part Logging Number Factor			of
Inlet Summ  *******  Inlet Catchbasin  ID Invert  Elevation  ft	nary ***  Inl Rim Elevation	let Ponded Manufacturen Area on ft²	Water C Elevation ft	Grate Part Logging Number Factor			of
Inlet Summ  *******  Inlet Catchbasin  ID Invert  Elevation  ft	nary ***  Inl Rim Elevation	let Ponded Manufacturer Area on ft²	Water C Elevation ft	Grate Part Logging Number Factor		Location	of Inlets
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft	Rim Elevation	let Ponded Manufacturer Area on ft² FHWA HEC-22	Water C Elevation ft GENERIC	Grate Part Logging Number Factor %			of
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10	Rim Elevation ft 281.22	let Ponded Manufacturer Area on ft² FHWA HEC-22	Water C Elevation ft  GENERIC 278.10	Grate Part Logging Number Factor  % N/A 0.00		Location On Grade	of Inlets
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10 CB-10	Rim Elevation ft 281.22	let Ponded Manufactures Area on ft² FHWA HEC-22 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC	Grate Part logging Number Factor  % N/A 0.00 N/A		Location	of Inlets
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10	Rim Elevation ft 281.22	Let Ponded Manufactures Area on ft² FHWA HEC-22 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44	Grate Part Logging Number Factor  % N/A 0.00		Location On Grade	of Inlets
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10 CB-10 265.44	Rim Elevation ft 281.22	let Ponded Manufactures Area on ft² FHWA HEC-22 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44	Grate Part logging Number Factor  % N/A 0.00 N/A 0.00		Location  On Grade  On Grade	of Inlets  1
Inlet Summ  ******* Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10 CB-10 265.44 CB-11	Inl Rim Elevation ft 281.22 267.69 272.10	Let Ponded Manufactures Area on ft² FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22	Water C. Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10	Grate Part Logging Number Factor		Location  On Grade  On Grade	of Inlets  1 1 1
Inlet Summ  ******* Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10 CB-10 265.44 CB-11 269.10	Inl Rim Elevation ft 281.22 267.69	let Ponded Manufacturer Area on ft² FHWA HEC-22 FHWA HEC-22 FHWA HEC-22	Water C. Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10	Grate Part Logging Number Factor		Location  On Grade  On Grade  On Grade	of Inlets  1 1 1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10 CB-10 265.44 CB-11 269.10 CB-12	Elevation ft 281.22 267.69 272.10 271.07	let Ponded Manufacturer Area on ft² FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 269.10 GENERIC 268.07	Grate Part Logging Number Factor  % N/A 0.00 N/A 0.00 N/A 0.00 N/A		Location  On Grade  On Grade  On Grade	of Inlets  1 1 1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft	Inl Rim Elevation ft 281.22 267.69 272.10	let Ponded Manufacturen Area on ft² FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 269.10 GENERIC 268.07	Grate Part Logging Number Factor  % N/A 0.00 N/A 0.00 N/A 0.00 N/A 0.00 N/A 0.00		On Grade On Grade On Grade On Grade	of Inlets  1 1 1
Inlet Summ ******* Inlet Catchbasin ID Invert Elevation ft	Rim Elevation ft 281.22 267.69 272.10 271.07	Let Ponded Manufactures Area  on  ft²  FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 10.00 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 268.07 GENERIC 268.07 GENERIC 262.90 GENERIC	Grate Part Logging Number Factor  % N/A 0.00 N/A		On Grade On Grade On Grade On Grade	of Inlets  1 1 1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10 CB-10 265.44 CB-11 269.10 CB-12 268.07 CB-13 262.90 CB-16 252.93	Elevation ft 281.22 267.69 272.10 271.07	Let Ponded Manufactures Area on ft² FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 10.00 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 268.07 GENERIC 262.90 GENERIC 252.93	Grate Part Logging Number Factor		On Grade On Grade On Grade On Grade On Grade On Sag On Sag	of Inlets  1 1 1 1 1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft	Rim Elevation ft  281.22 267.69 272.10 271.07 264.85 254.93	Let Ponded Manufactures Area on ft² FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 10.00 FHWA HEC-22 10.00 FHWA HEC-22	Water C. Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 268.07 GENERIC 262.90 GENERIC 252.93 GENERIC	Grate Part Logging Number Factor		On Grade On Grade On Grade On Grade On Grade	of Inlets  1 1 1 1 1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft	Rim Elevation ft 281.22 267.69 272.10 271.07	Let Ponded Manufactures Area  on  ft²  FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 10.00 FHWA HEC-22 10.00 FHWA HEC-22	Water C. Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 268.07 GENERIC 268.07 GENERIC 252.93 GENERIC 260.16	Grate Part Logging Number Factor  % N/A 0.00 N/A		On Grade On Grade On Grade On Grade On Sag On Sag On Grade	of Inlets  1 1 1 1 1 1 1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft	Elevation ft 281.22 267.69 272.10 271.07 264.85 254.93 265.49	Let Ponded Manufactures Area  on  ft²  FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 10.00 FHWA HEC-22 10.00 FHWA HEC-22 10.00 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 269.10 GENERIC 262.90 GENERIC 252.93 GENERIC 260.16 GENERIC	Grate Part Logging Number Factor  % N/A 0.00 N/A		On Grade On Grade On Grade On Grade On Grade On Sag On Sag	of Inlets  1 1 1 1 1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft	Rim Elevation ft  281.22 267.69 272.10 271.07 264.85 254.93	Let Ponded Manufactures Area  on  ft²  FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 10.00 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 268.07 GENERIC 262.90 GENERIC 252.93 GENERIC 250.16 GENERIC 260.16 GENERIC 269.61	Grate Part Logging Number Factor		On Grade On Grade On Grade On Grade On Sag On Sag On Grade On Sag	of Inlets  1 1 1 1 1 1 1 1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft	Elevation ft 281.22 267.69 272.10 271.07 264.85 254.93 265.49	Let Ponded Manufactures Area  on  ft²  FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 10.00 FHWA HEC-22 10.00 FHWA HEC-22 10.00 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 268.07 GENERIC 262.90 GENERIC 252.93 GENERIC 250.16 GENERIC 260.16 GENERIC 269.61	Grate Part Logging Number Factor  % N/A 0.00 N/A		On Grade On Grade On Grade On Grade On Sag On Sag On Grade	of Inlets  1 1 1 1 1 1 1 1

CB-20		FHWA	HEC-22	GENERIC	N/A		Or	ı Sag	1	
278.18	279.	67 10.	00	278.18	0.00					
CB-3			HEC-22	GENERIC	N/A		Or	n Grade	1	
262.89	265.	39	-	262.89	0.00					
CB-4		FHWA	HEC-22	GENERIC	N/A		Or	n Grade	1	
254.18	255.	93	-	254.18	0.00					
CB-5		FHWA	HEC-22	GENERIC	N/A		Or	n Sag	1	
249.44	251.	18 10.	00	249.44	0.00					
CB-6		FHWA	HEC-22	GENERIC	N/A		Or	n Grade	1	
252.35	255.	35	-	252.35	0.00					
CB-7		FHWA	HEC-22	GENERIC	N/A		Or	ı Grade	1	
255.41	258.	41	-	255.41	0.00					
CB-8W		FHWA	HEC-22	GENERIC	N/A		Or	ı Grade	1	
257.08	260.	08	-	257.08	0.00					
CB-9		FHWA	HEC-22	GENERIC	N/A		Or	ı Grade	1	
259.82	262.	82	-	259.82	0.00					
*****	*****	*****	*							
		ter Summar								
				Doodsso	Dood	C11++0	C11++ 0	_	111++02	
Inlet ID			Roadwa: tudina		_	Gutter Cross	Gutter Width		utter ssion	
ID		rongr	Slope		_	Slope	WIGCII	рерге	SSIOII	
			ft/f		Rougilliess	ft/ft	ft		in	
			IL/I	L IL/IL					111	
CB-1			0.010	0 0.0200	0.0160	0.0620	2.00		2.00	
CB-10			0.020		0.0130	0.0620	2.00		0.00	
CB-11			0.020		0.0130	0.0620	2.00		0.00	
CB-11			0.020		0.0130	0.0620	2.00		0.00	
CB-12				- 0.0500	0.0130	0.0620	2.00		0.00	
CB-15				- 0.0500	0.0130	0.0620	2.00		0.00	
CB-17			0.010		0.0160	0.0620	2.00		2.00	
CB-17			0.010		0.0160	0.0620	2.00		2.00	
			0 020	- 0.0200						
CB-2			0.020		0.0130	0.0620	2.00		0.00	
CB-20			0 000	- 0.0500	0.0130	0.0620	2.00		0.00	
CB-3			0.020		0.0130	0.0620	2.00		0.00	
CB-4			0.020		0.0130	0.0620	2.00		0.00	
CB-5				- 0.0500	0.0130	0.0620	2.00		0.00	
CB-6			0.020		0.0130	0.0620	2.00		0.00	
CB-7			0.020			0.0620	2.00		0.00	
CB-8W			0.010		0.0130	0.0620	2.00		2.00	
CB-9			0.020	0.0500	0.0130	0.0620	2.00		0.00	
*****	***									
Link Sum										
Link		From Node		To Node	Element	т.	onath	Clana	Manning's	~
ID		FIOIII NOGE	:	10 Node	Element Type	ь	ength ft	Slope %	Roughnes	
								·•		_
CB-1_Ove	rflow	CB-1		OFFSITE1	CHANNEL		241.8	0.2000	0.013	0
CB10-9_G		CB-10		CB-9	CHANNEL		254.5	1.9133	0.013	
CB11-10_		CB-11		CB-10	CHANNEL		254.5	1.7326	0.013	
CB12-13		CB-12		CB-13	CHANNEL		254.5	2.4437	0.013	
CB17-16_		CB-17		CB-16	CHANNEL		254.5	4.1501	0.013	
CB2-3 Gu		CB-2		CB-3	CHANNEL		241.8	4.7276	0.013	
CB2-3_Gu CB3-4 Gu		CB-3		CB-4	CHANNEL		254.5	3.7167	0.013	
CB4-5_Gu		CB-4		CB-5	CHANNEL		254.5	1.8662	0.013	
CB6-5_Gu		CB-4 CB-6		CB-5	CHANNEL		254.5	1.6383	0.013	
_									0.013	
CB7-6_Gu		CB-7		CB-6	CHANNEL		254.5	1.2022		
CB8-7_Gu		CB-8W		CB-7	CHANNEL		254.5	0.6561	0.013	
CB9-8_Gu		CB-9		CB-8W	CHANNEL		254.5	1.0765	0.013	
L-Pipe -		CB-20		OFFSITE-1	CHANNEL		546.0	2.1967	0.013	
Pipe - (		DMH-6		DH-6	CONDUIT		13.3	3.0144	0.013	
Pipe - (	13)	CB-6		DMH-6	CONDUIT		12.5	0.7995	0.013	0

Pipe - (14)	CB-5	STU-5	CONDUIT	28.8	2.4635	0.0130
Pipe - (16)	CB-3	DMH-3	CONDUIT	11.9	4.6382	0.0130
Pipe - (18)	CB-7	DMH-7	CONDUIT	20.7	1.0000	0.0130
<u> </u>						
Pipe - (19)	DMH-7	EX-7	CONDUIT	6.9	1.4505	0.0130
Pipe - (2)	CB-2	DMH-3	CONDUIT	246.6	4.6555	0.0130
Pipe - (20)	CB-8E	CIT-8	CONDUIT	7.6	0.6131	0.0130
Pipe - (21)	CIT-8	EX-7	CONDUIT	196.9	1.0156	0.0130
Pipe - (22)	EX-7	DP-7	CONDUIT	20.0	1.0000	0.0130
Pipe - (23)	CB-8W	CIT-8	CONDUIT	20.5	3.2241	0.0130
Pipe - (24)	CB-9	CIT-9	CONDUIT	16.5	0.9092	0.0130
Pipe - (25)	CIT-9	CIT-8	CONDUIT	219.0	1.1872	0.0130
Pipe - (26)	DMH-10	DH-10	CONDUIT	14.0	0.5000	0.0130
Pipe - (27)	CB-10	DMH-10	CONDUIT	4.2	0.5000	0.0130
Pipe - (28)	CB-11	DMH-11	CONDUIT	4.9	5.1092	0.0130
Pipe - (29)	DMH-11	DH-10	CONDUIT	190.5	1.8369	0.0130
Pipe - (3)	DMH-4S	DMH-4N	CONDUIT	131.6	3.1757	0.0130
Pipe - (30)	CB-12	DMH-12	CONDUIT	3.6	1.0000	0.0130
Pipe - (31)	DMH-12	DH-13	CONDUIT	217.3	2.4045	0.0130
Pipe - (33)	DH-13	DP-13	CONDUIT	19.5	1.0000	0.0130
Pipe - (34)	CB-13	DMH-13	CONDUIT	5.9	0.5098	0.0130
Pipe - (35)	DMH-13	DH-13	CONDUIT	19.9	1.0989	0.0130
Pipe - (4)	DMH-4N	STU-5	CONDUIT	263.5	1.5634	0.0130
Pipe - (40)	CB-17	STU-16	CONDUIT	220.1	3.2621	0.0130
				4.1	1.0000	
Pipe - (41)	STU-16	DP-16	CONDUIT			0.0130
Pipe - (43)	CB-16	STU-16	CONDUIT	7.3	1.7930	0.0130
Pipe - (44)	CB-18	EX-18	CONDUIT	24.4	2.4990	0.0130
Pipe - (45)	EX-18	DP-18	CONDUIT	81.8	2.0000	0.0130
Pipe - (5)	STU-5	DP-5	CONDUIT	16.3	3.8608	0.0130
Pipe - (50)	CB-20	DMH-20	CONDUIT	6.5	8.1871	0.0130
Pipe - (51)	DMH-20	DH-20	CONDUIT	5.7	8.1142	0.0130
Pipe - (54)	DH-6	DP-6	CONDUIT	8.5	5.3000	0.0130
Pipe - (55)	CB-4	DMH-4N	CONDUIT	10.6	11.5699	0.0130
Pipe - (56)	DH-10	DP-10	CONDUIT	12.4	3.0000	0.0130
Pipe - (57)	DH-20	DP-20	CONDUIT	55.5	6.1646	0.0130
Pipe - (61)	CB-1	Structure -	(72)CONDUIT	79.8	2.7583	0.0130
Pipe - (62)	<u></u>					
FIDE - (07)	Structure -	(72)DP-1	CONDUIT	79.0	1.0000	0.0130
Pipe - (62) Pipe - (7)	Structure - DMH-3	(72)DP-1 DMH-4S	CONDUIT CONDUIT	79.0 124.6	1.0000 4.0212	0.0130 0.0130
Pipe - (7)	DMH-3					
	DMH-3					
Pipe - (7)  ***********************************	DMH-3 ***** ummary					
Pipe - (7)	DMH-3 ***** ummary					
Pipe - (7)  ***********************************	DMH-3 ***** ummary					
Pipe - (7)  ******************  Cross Section S ************************************	DMH-3  ***** ummary *****	DMH-4S	CONDUIT	124.6	4.0212	0.0130
Pipe - (7)  *************  Cross Section S  *************  Link	DMH-3  ***** ummary *****	DMH-4S	CONDUIT	124.6	4.0212	0.0130
Pipe - (7)  *************  Cross Section S  ***********  Link  Design	DMH-3  ***** ummary *****	DMH-4S Depth/	CONDUIT	124.6 No. of	4.0212 Cross	0.0130
Pipe - (7)  **********  Cross Section S  *********  Link  Design  ID	DMH-3  ***** ummary *****	DMH-4S Depth/	CONDUIT	124.6 No. of	4.0212 Cross	0.0130
Pipe - (7)  **********  Cross Section S  *********  Link  Design  ID	DMH-3  ***** ummary *****	DMH-4S Depth/	CONDUIT	124.6 No. of	4.0212 Cross Sectional	0.0130  Full Flow  Hydraulic
Pipe - (7)  *********  Cross Section S  *********  Link  Design  ID  Flow	DMH-3  ***** ummary *****	DMH-4S Depth/	CONDUIT	124.6 No. of	4.0212 Cross Sectional	0.0130  Full Flow  Hydraulic
Pipe - (7)  *********  Cross Section S  *********  Link  Design  ID  Flow	DMH-3  ***** ummary *****	DMH-4S  Depth/ Diameter	CONDUIT Width	124.6 No. of	4.0212  Cross Sectional Area	0.0130  Full Flow  Hydraulic  Radius
Pipe - (7)  **********  Cross Section S  *******  Link  Design  ID  Flow  Capacity	DMH-3  ***** ummary *****	DMH-4S  Depth/ Diameter	CONDUIT Width	124.6 No. of	4.0212  Cross Sectional Area	0.0130  Full Flow  Hydraulic  Radius
Pipe - (7)  ***********  Cross Section S  *******  Link  Design  ID  Flow  Capacity  cfs	DMH-3  *****  ummary  *****  Shape	DMH-4S  Depth/ Diameter	CONDUIT Width ft	No. of	4.0212  Cross Sectional  Area  ft²	0.0130  Full Flow  Hydraulic  Radius  ft
Pipe - (7)  **********  Cross Section S  *******  Link  Design  ID  Flow  Capacity  cfs	DMH-3  *****  ummary  *****  Shape	DMH-4S  Depth/ Diameter  ft	CONDUIT  Width  ft	No. of Barrels	4.0212  Cross Sectional  Area  ft²	0.0130  Full Flow  Hydraulic  Radius  ft
Pipe - (7)  ***********  Cross Section S *******  Link  Design  ID  Flow  Capacity  cfs   CB-1_Overflow	DMH-3  *****  ummary  *****  Shape	DMH-4S  Depth/ Diameter  ft	CONDUIT Width ft	No. of	4.0212  Cross Sectional  Area  ft²	0.0130  Full Flow  Hydraulic  Radius  ft
Pipe - (7)  ***********  Cross Section S *******  Link  Design ID  Flow  Capacity  cfs   CB-1_Overflow 2.70	DMH-3  ***** ummary  ***** Shape  TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28	CONDUIT  Width  ft  14.00	No. of Barrels	Cross Sectional Area ft²	0.0130  Full Flow Hydraulic Radius ft
Pipe - (7)  ***********  Cross Section S  ******  Link  Design  ID  Flow  Capacity  cfs   CB-1_Overflow  2.70  CB10-9_Gutter	DMH-3  ***** ummary  ***** Shape  TRIANGULAR	DMH-4S  Depth/ Diameter  ft	CONDUIT  Width  ft	No. of Barrels	4.0212  Cross Sectional  Area  ft²	0.0130  Full Flow  Hydraulic  Radius  ft
Pipe - (7)  ************* Cross Section S ******** Link Design ID Flow Capacity cfs CB-1_Overflow 2.70 CB10-9_Gutter 8.35	DMH-3  ***** ummary ***** Shape  TRIANGULAR TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28 0.28	CONDUIT  Width  ft  14.00  14.00	No. of Barrels	Cross Sectional Area ft²  1.96 1.96	0.0130  Full Flow Hydraulic Radius ft  0.14 0.14
Pipe - (7)  ************* Cross Section S ******** Link Design ID Flow Capacity cfs  CB-1_Overflow 2.70 CB10-9_Gutter 8.35 CB11-10_Gutter	TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28	CONDUIT  Width  ft  14.00	No. of Barrels	Cross Sectional Area ft²	0.0130  Full Flow Hydraulic Radius ft
Pipe - (7)  ************* Cross Section S ******** Link Design ID Flow Capacity cfs  CB-1_Overflow 2.70 CB10-9_Gutter 8.35 CB11-10_Gutter 7.95	DMH-3  ***** ummary ***** Shape  TRIANGULAR TRIANGULAR TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28  0.28  0.28	CONDUIT  Width  ft  14.00 14.00 14.00	No. of Barrels  1 1 1	Cross Sectional Area ft²  1.96 1.96	0.0130  Full Flow Hydraulic Radius ft  0.14 0.14 0.14
Pipe - (7)  ************  Cross Section S *******  Link  Design  ID  Flow  Capacity  cfs   CB-1_Overflow  2.70  CB10-9_Gutter  8.35  CB11-10_Gutter  7.95  CB12-13_Gutter	DMH-3  ***** ummary ***** Shape  TRIANGULAR TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28 0.28	CONDUIT  Width  ft  14.00  14.00	No. of Barrels	Cross Sectional Area ft²  1.96 1.96	0.0130  Full Flow Hydraulic Radius ft  0.14 0.14
Pipe - (7)  ***********  Cross Section S *******  Link  Design ID  Flow  Capacity  cfs   CB-1_Overflow  2.70  CB10-9_Gutter  8.35  CB11-10_Gutter  7.95  CB12-13_Gutter  9.44	*****  wmmary  ***** Shape  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28 0.28 0.28 0.28	ft  14.00 14.00 14.00 14.00	No. of Barrels  1 1 1 1	4.0212  Cross Sectional Area ft²  1.96 1.96 1.96 1.96	Full Flow Hydraulic Radius ft  0.14 0.14 0.14 0.14
Pipe - (7)  ************  Cross Section S *******  Link  Design ID Flow  Capacity  cfs   CB-1_Overflow  2.70  CB10-9_Gutter  7.95  CB12-13_Gutter  9.44  CB17-16_Gutter	DMH-3  ***** ummary ***** Shape  TRIANGULAR TRIANGULAR TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28  0.28  0.28	CONDUIT  Width  ft  14.00 14.00 14.00	No. of Barrels  1 1 1	Cross Sectional Area ft²  1.96 1.96	0.0130  Full Flow Hydraulic Radius ft  0.14 0.14 0.14
Pipe - (7)  **************  Cross Section S  ********  Link  Design  ID  Flow  Capacity  cfs   CB-1_Overflow  2.70  CB10-9_Gutter  8.35  CB11-10_Gutter  7.95  CB12-13_Gutter  9.44  CB17-16_Gutter  12.30	*****  wmmary  ***** Shape  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28 0.28 0.28 0.28 0.28	ft  14.00 14.00 14.00 14.00 14.00	No. of Barrels  1 1 1 1 1	4.0212  Cross Sectional Area ft²  1.96 1.96 1.96 1.96 1.96	0.0130  Full Flow Hydraulic Radius ft  0.14 0.14 0.14 0.14 0.14
Pipe - (7)  ************** Cross Section S ********* Link Design ID Flow  Capacity cfs  CB-1_Overflow 2.70 CB10-9_Gutter 8.35 CB11-10_Gutter 7.95 CB12-13_Gutter 9.44 CB17-16_Gutter 12.30 CB2-3_Gutter	*****  wmmary  ***** Shape  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28 0.28 0.28 0.28	ft  14.00 14.00 14.00 14.00	No. of Barrels  1 1 1 1	4.0212  Cross Sectional Area ft²  1.96 1.96 1.96 1.96	Full Flow Hydraulic Radius ft  0.14 0.14 0.14 0.14
Pipe - (7)  *************  Cross Section S  ********  Link  Design  ID  Flow  Capacity  cfs   CB-1_Overflow  2.70  CB10-9_Gutter  8.35  CB11-10_Gutter  7.95  CB12-13_Gutter  9.44  CB17-16_Gutter  12.30  CB2-3_Gutter  13.13	TRIANGULAR TRIANGULAR TRIANGULAR TRIANGULAR TRIANGULAR TRIANGULAR TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28 0.28 0.28 0.28 0.28 0.28 0.28	ft  14.00 14.00 14.00 14.00 14.00 14.00	124.6  No. of Barrels  1 1 1 1 1 1	4.0212  Cross Sectional Area ft²  1.96 1.96 1.96 1.96 1.96 1.96	0.0130  Full Flow Hydraulic Radius ft  0.14 0.14 0.14 0.14 0.14 0.14
Pipe - (7)  ************** Cross Section S ********* Link Design ID Flow  Capacity cfs  CB-1_Overflow 2.70 CB10-9_Gutter 8.35 CB11-10_Gutter 7.95 CB12-13_Gutter 9.44 CB17-16_Gutter 12.30 CB2-3_Gutter	*****  wmmary  ***** Shape  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28 0.28 0.28 0.28 0.28	ft  14.00 14.00 14.00 14.00 14.00	No. of Barrels  1 1 1 1 1	4.0212  Cross Sectional Area ft²  1.96 1.96 1.96 1.96 1.96	0.0130  Full Flow Hydraulic Radius ft  0.14 0.14 0.14 0.14 0.14

11 (4						
11.64 CB4-5_Gutter	TRIANGULAR	0.28	14.00	1	1.96	0.14
8.25 CB6-5_Gutter	TRIANGULAR	0.28	14.00	1	1.96	0.14
7.73 CB7-6_Gutter	TRIANGULAR	0.28	14.00	1	1.96	0.14
6.62 CB8-7_Gutter	TRIANGULAR	0.28	14.00	1	1.96	0.14
4.89 CB9-8_Gutter	TRIANGULAR	0.28	14.00	1	1.96	0.14
6.26 L-Pipe - (50)	IRREGULAR	0.75	6.80	1	3.82	0.50
41.01 Pipe - (12)	CIRCULAR	1.00	1.00	1	0.79	0.25
6.19 Pipe - (13)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.19 Pipe - (14)	CIRCULAR	1.00	1.00	1	0.79	0.25
5.59 Pipe - (16)	CIRCULAR	1.00	1.00	1	0.79	0.25
7.67 Pipe - (18)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.56 Pipe - (19)	CIRCULAR	1.00	1.00	1	0.79	0.25
4.29 Pipe - (2)	CIRCULAR	1.00	1.00	1	0.79	0.25
7.69 Pipe - (20)	CIRCULAR	1.00	1.00	1	0.79	0.25
2.79 Pipe - (21)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.59 Pipe - (22)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.56 Pipe - (23)	CIRCULAR	1.00	1.00	1	0.79	0.25
6.40 Pipe - (24)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.40 Pipe - (25)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.88 Pipe - (26)	CIRCULAR	1.00	1.00	1	0.79	0.25
2.52 Pipe - (27)	CIRCULAR	1.00	1.00	1	0.79	0.25
2.52 Pipe - (28)	CIRCULAR	1.00	1.00	1	0.79	0.25
8.05 Pipe - (29)	CIRCULAR	1.00	1.00	1	0.79	0.25
4.83 Pipe - (3)	CIRCULAR	1.00	1.00	1	0.79	0.25
6.35 Pipe - (30)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.56 Pipe - (31)	CIRCULAR	1.00	1.00	1	0.79	0.25
5.52 Pipe - (33)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.56 Pipe - (34)	CIRCULAR	1.00	1.00	1	0.79	0.25
2.54 Pipe - (35)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.73 Pipe - (4)	CIRCULAR	1.00	1.00	1	0.79	0.25
4.45 Pipe - (40)	CIRCULAR	1.00	1.00	1	0.79	0.25
6.43 Pipe - (41)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.56 Pipe - (43)	CIRCULAR	1.00	1.00	1	0.79	0.25

4 55								
4.77 Pipe - (44)	CIRCU	JLAR	1.00	1.00		1	0.79	0.25
5.63 Pipe - (45)	CIRCU	JLAR	1.50	1.50		1	1.77	0.38
14.86 Pipe - (5)	CIRCU	JLAR	1.00	1.00		1	0.79	0.25
7.00 Pipe - (50)	CIRCU	JLAR	1.50	1.50		1	1.77	0.38
30.06 Pipe - (51)	CIRCU	JLAR	1.00	1.00		1	0.79	0.25
10.15 Pipe - (54)	CIRCU	JLAR	1.00	1.00		1	0.79	0.25
8.20 Pipe - (55)	CIRCU	JLAR	1.00	1.00		1	0.79	0.25
12.12 Pipe - (56)	CIRCU	JLAR	1.00	1.00		1	0.79	0.25
6.17 Pipe - (57)	CIRCU	JLAR	1.50	1.50		1	1.77	0.38
26.08 Pipe - (61)	CIRCU	JLAR	1.00	1.00		1	0.79	0.25
5.92 Pipe - (62)	CIRCU	JLAR	1.00	1.00		1	0.79	0.25
3.56 Pipe - (7)	CIRCU	JLAR	1.00	1.00		1	0.79	0.25
7.14								
********								
Transect Summ								
Transect XS-I	L-Pipe - (	(13)						
Area:	0.0005	0.0019	0.0043	0.0076	0.0118			
	0.0003	0.0232	0.0305	0.0390	0.0118			
	0.0595	0.0715	0.0847	0.0990	0.1145			
	).1312 ).2323	0.1491 0.2561	0.1682 0.2810	0.1884 0.3071	0.2098 0.3338			
	).3604	0.3871	0.4137	0.4404	0.3336			
C	.4937	0.5203	0.5470	0.5736	0.6003			
	).6269 ).7602	0.6536 0.7868	0.6802 0.8135	0.7069 0.8401	0.7335 0.8668			
	0.7002	0.9201	0.9467	0.9734	1.0000			
Hrad:								
	0.0139 0.0835	0.0278 0.0963	0.0418 0.1080	0.0557 0.1202	0.0696 0.1329			
	).1459	0.1591	0.1724	0.1858	0.1994			
	2130	0.2267	0.2404	0.2542	0.2680			
	2794	0.2957	0.3095	0.3238	0.3512 0.4863			
	).3784 ).5130	0.4055 0.5396	0.4326 0.5660	0.4595 0.5924	0.4003			
C	0.6448	0.6708	0.6968	0.7226	0.7483			
	).7740 ).9005	0.7995 0.9256	0.8249 0.9505	0.8502 0.9753	0.8754 1.0000			
Width:	1.9005	0.9256	0.9505	0.9753	1.0000			
	0.0355	0.0711	0.1066	0.1422	0.1777			
	).2132 ).4283	0.2520	0.2961	0.3402 0.5605	0.3842 0.6046			
	).4283 ).6487	0.4724 0.6927	0.5164 0.7368	0.5605	0.8249			
C	.8690	0.9131	0.9572	1.0000	1.0000			
	1.0000	1.0000	1.0000	1.0000	1.0000			
	L.0000 L.0000	1.0000	1.0000	1.0000	1.0000			
1	1.0000	1.0000	1.0000	1.0000	1.0000			
1	1.0000	1.0000	1.0000	1.0000	1.0000			

Transect XS	-L-Pipe -	(16)			
Area:					
	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312 0.2323	0.1491 0.2561	0.1682 0.2810	0.1884 0.3071	0.2098
	0.2323	0.3871	0.4137	0.4404	0.3336
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868	0.8135	0.8401	0.8668
	0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:					
	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835	0.0963	0.1080	0.1202	0.1329
	0.1459 0.2130	0.1591 0.2267	0.1724 0.2404	0.1858 0.2542	0.1994 0.2680
	0.2130	0.2957	0.3095	0.2342	0.3512
	0.3784	0.4055	0.4326	0.4595	0.4863
	0.5130	0.5396	0.5660	0.5924	0.6187
	0.6448	0.6708	0.6968	0.7226	0.7483
	0.7740	0.7995	0.8249	0.8502	0.8754
	0.9005	0.9256	0.9505	0.9753	1.0000
Width:					
	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132 0.4283	0.2520 0.4724	0.2961 0.5164	0.3402 0.5605	0.3842
	0.4203	0.6927	0.7368	0.7809	0.8249
	0.8690	0.9131	0.9572	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
Transect XS	-L-Pipe -	(18)			
Area:					
	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312 0.2323	0.1491 0.2561	0.1682 0.2810	0.1884 0.3071	0.2098
	0.3604	0.3871	0.4137	0.4404	0.4670
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868	0.8135	0.8401	0.8668
	0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:	0 0120	0 0070	0 0410	0 0557	0.0606
	0.0139 0.0835	0.0278 0.0963	0.0418 0.1080	0.0557 0.1202	0.0696 0.1329
	0.1459	0.1591	0.1724	0.1202	0.1323
	0.2130	0.2267	0.2404	0.2542	0.2680
	0.2818	0.2957	0.3095	0.3238	0.3512
	0.3784	0.4055	0.4326	0.4595	0.4863
	0.5130	0.5396	0.5660	0.5924	0.6187
	0.6448	0.6708	0.6968	0.7226	0.7483
	0.7740	0.7995	0.8249	0.8502	0.8754
Width:	0.9005	0.9256	0.9505	0.9753	1.0000
Width:	0.0355	0.0711	0.1066	0.1422	0.1777
	0.0333	0.2520	0.1000	0.3402	0.3842
	0.4283	0.4724	0.5164	0.5605	0.6046
	0.6487	0.6927	0.7368	0.7809	0.8249
	0.8690	0.9131	0.9572	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000

	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	XS-L-Pipe -	- (2)			
Area:	0 0005	0 0010	0 0042	0.0056	0 0110
	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595 0.1312	0.0715 0.1491	0.0847 0.1682	0.0990 0.1884	0.1145 0.2098
	0.2323	0.2561	0.1002	0.3071	0.3338
	0.3604	0.3871	0.4137	0.4404	0.4670
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868	0.8135	0.8401	0.8668
	0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:					
	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835	0.0963	0.1080	0.1202	0.1329
	0.1459	0.1591	0.1724	0.1858	0.1994
	0.2130	0.2267	0.2404	0.2542	0.2680
	0.2818 0.3784	0.2957 0.4055	0.3095 0.4326	0.3238 0.4595	0.3512 0.4863
	0.5130	0.5396	0.5660	0.5924	0.6187
	0.6448	0.6708	0.6968	0.7226	0.7483
	0.7740	0.7995	0.8249	0.8502	0.8754
	0.9005	0.9256	0.9505	0.9753	1.0000
Width:					
	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132	0.2520	0.2961	0.3402	0.3842
	0.4283	0.4724	0.5164	0.5605	0.6046
	0.6487	0.6927	0.7368	0.7809	0.8249
	0.8690	0.9131	0.9572	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000 1.0000	1.0000 1.0000	1.0000 1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	2.0000	1.0000	1.0000	1.0000
Transect 1	XS-L-Pipe -	(24)			
Area:					
	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312	0.1491	0.1682	0.1884	0.2098
	0.2323 0.3604	0.2561 0.3871	0.2810 0.4137	0.3071 0.4404	0.3338 0.4670
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868	0.8135	0.8401	0.8668
	0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:					
	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835	0.0963	0.1080	0.1202	0.1329
	0.1459	0.1591	0.1724	0.1858	0.1994
	0.2130	0.2267	0.2404	0.2542	0.2680
	0.2818	0.2957	0.3095	0.3238	0.3512
	0.3784	0.4055	0.4326	0.4595	0.4863
	0.5130 0.6448	0.5396	0.5660 0.6968	0.5924 0.7226	0.6187 0.7483
	0.8448	0.6708 0.7995	0.8249	0.8502	0.7483
	0.7740	0.9256	0.9505	0.8302	1.0000
Width:	0.,000	0.0200	0.2505	3.2,33	
<del></del>	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132	0.2520	0.2961	0.3402	0.3842
	0.4283	0.4724	0.5164	0.5605	0.6046

	0.6487	0.6927	0.7368	0.7809	0.8249
	0.8690	0.9131	0.9572	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
Transect XS	S-L-Pipe -	(27)			
Hrad:	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312	0.1491	0.1682	0.1884	0.2098
	0.2323	0.2561	0.2810	0.3071	0.3338
	0.3604	0.3871	0.4137	0.4404	0.4670
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868	0.8135	0.8401	0.8668
	0.8934	0.9201	0.9467	0.9734	1.0000
iii au•	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835	0.0963	0.1080	0.1202	0.1329
	0.1459	0.1591	0.1724	0.1858	0.1994
	0.2130	0.2267	0.2404	0.2542	0.2680
	0.2818	0.2957	0.3095	0.3238	0.3512
	0.3784	0.4055	0.4326	0.4595	0.4863
	0.5130	0.5396	0.5660	0.5924	0.6187
	0.6448	0.6708	0.6968	0.7226	0.7483
	0.7740	0.7995	0.8249	0.8502	0.8754
	0.9005	0.9256	0.9505	0.9753	1.0000
Width:	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000	0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000 1.0000	0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000	0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000 1.0000	0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000
Transect XS	S-L-Pipe -	(28)			
	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312	0.1491	0.1682	0.1884	0.2098
	0.2323	0.2561	0.2810	0.3071	0.3338
	0.3604	0.3871	0.4137	0.4404	0.4670
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868	0.8135	0.8401	0.8668
	0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835	0.0963	0.1080	0.1202	0.1329
	0.1459	0.1591	0.1724	0.1858	0.1994
	0.2130	0.2267	0.2404	0.2542	0.2680
	0.2818	0.2957	0.3095	0.3238	0.3512
	0.3784	0.4055	0.4326	0.4595	0.4863
	0.5130	0.5396	0.5660	0.5924	0.6187
	0.6448	0.6708	0.6968	0.7226	0.7483
	0.7740	0.7995	0.8249	0.8502	0.8754
	0.9005	0.9256	0.9505	0.9753	1.0000

Width:	0.0355 0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000	0.0711 0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000	0.1066 0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000	0.1422 0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000 1.0000	0.1777 0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000
Transect XS	S-L-Pipe -	(30)			
Area:	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312	0.1491	0.1682	0.1884	0.2098
	0.2323	0.2561	0.2810	0.3071	0.3338
	0.3604	0.3871	0.4137	0.4404	0.4670
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868	0.8135	0.8401	0.8668
	0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:	0.0139	0.0278	0.0418	0.0557	0.0696
Width:	0.0835	0.0963	0.1080	0.1202	0.1329
	0.1459	0.1591	0.1724	0.1858	0.1994
	0.2130	0.2267	0.2404	0.2542	0.2680
	0.2818	0.2957	0.3095	0.3238	0.3512
	0.3784	0.4055	0.4326	0.4595	0.4863
	0.5130	0.5396	0.5660	0.5924	0.6187
	0.6448	0.6708	0.6968	0.7226	0.7483
	0.7740	0.7995	0.8249	0.8502	0.8754
	0.9005	0.9256	0.9505	0.9753	1.0000
Width:	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132	0.2520	0.2961	0.3402	0.3842
	0.4283	0.4724	0.5164	0.5605	0.6046
	0.6487	0.6927	0.7368	0.7809	0.8249
	0.8690	0.9131	0.9572	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
Transect XS	S-L-Pipe -	(37)			
Area:	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312	0.1491	0.1682	0.1884	0.2098
	0.2323	0.2561	0.2810	0.3071	0.3338
	0.3604	0.3871	0.4137	0.4404	0.4670
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868	0.8135	0.8401	0.8668
	0.8934	0.9201	0.9467	0.9734	1.0000
	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835	0.0963	0.1080	0.1202	0.1329
	0.1459	0.1591	0.1724	0.1858	0.1994
	0.2130	0.2267	0.2404	0.2542	0.2680
	0.2818	0.2957	0.3095	0.3238	0.3512
	0.3784	0.4055	0.4326	0.4595	0.4863

	0.5130	0.5396	0.5660	0.5924	0.6187
	0.6448	0.6708	0.6968	0.7226	0.7483
	0.7740	0.7995	0.8249	0.8502	0.8754
rat de la c	0.9005	0.9256	0.9505	0.9753	1.0000
Width:	0.0355	0.0711	0.1066	0.1422	0.1777
	0.0333	0.2520	0.2961	0.3402	0.3842
	0.4283	0.4724	0.5164	0.5605	0.6046
	0.6487	0.6927	0.7368	0.7809	0.8249
	0.8690	0.9131	0.9572	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	T 54	(50)			
Transect XS Area:	-r-bibe -	(50)			
ALCa.	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312	0.1491	0.1682	0.1884	0.2098
	0.2323	0.2561	0.2810	0.3071	0.3338
	0.3604	0.3871	0.4137	0.4404	0.4670
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868	0.8135	0.8401	0.8668
_	0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:	0 0120	0 0070	0 0410	0 0557	0.000
	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835 0.1459	0.0963 0.1591	0.1080 0.1724	0.1202 0.1858	0.1329 0.1994
	0.1439	0.1391	0.2404	0.2542	0.1994
	0.2818	0.2257	0.3095	0.3238	0.3512
	0.3784	0.4055	0.4326	0.4595	0.4863
	0.5130	0.5396	0.5660	0.5924	0.6187
	0.6448	0.6708	0.6968	0.7226	0.7483
	0.7740	0.7995	0.8249	0.8502	0.8754
	0.9005	0.9256	0.9505	0.9753	1.0000
Width:					
	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132	0.2520	0.2961	0.3402	0.3842
	0.4283	0.4724	0.5164	0.5605	0.6046
	0.6487	0.6927	0.7368	0.7809	0.8249
	0.8690 1.0000	0.9131 1.0000	0.9572 1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
Transect XS	-L-Pipe -	(55)			
Area:					
	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312	0.1491 0.2561	0.1682	0.1884	0.2098
	0.2323 0.3604	0.2561	0.2810 0.4137	0.3071 0.4404	0.3338 0.4670
	0.3604	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868	0.8135	0.8401	0.8668
	0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:					
	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835	0.0963	0.1080	0.1202	0.1329

Width:	0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005  0.0355 0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000	0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995 0.9256 0.0711 0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000	0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505 0.1066 0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000	0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753 0.1422 0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000	0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754 1.0000 0.1777 0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000		
******	*****	*****	Volume	Depth			
	antity Cont		acre-ft	inches			
	cipitation cy Error (%)		0.909 0.682	1.095			
******	*****	****	Volume	Volume			
	ing Continu		acre-ft	Mgallons			
External Initial S Final Sto	Inflow Outflow Stored Volume red Volume ry Error (%)	 e	0.000 0.378 0.000 0.000 -0.805	0.000 0.123 0.000 0.000			
Runoff Co	********** efficient Co	omputations	Report				
 Subbasin	Sub-CB-1						
					Area	Soil	Runoff
	ace Descrip				(acres)	Group	Coeff.
Residenti	25 years or al Lot Size Area & Wei	1 Acre, 25	years or gr f Coeff.	reater	0.17 0.19 0.36	A (6%+) A (6%+)	0.79 0.29 0.53
	Sub-CB-10	_					
Soil/Surf	ace Descrip	tion			Area (acres)	Soil Group	Runoff Coeff.
Residenti	25 years or al Lot Size Area & Wei	1 Acre, 25	years or gr f Coeff.	reater	0.12 0.01 0.13	A (6%+) A (6%+)	0.79 0.29 0.75
	Sub-CB-11	_					
		-			Area	Soil	Runoff

Soil/Surface Description	(acres)	Group	Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.11 0.09 0.20	A (6%+) A (6%+)	0.79 0.14 0.50
Subbasin Sub-CB-12			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.23 1.05 1.28	A (6%+) A (6%+)	0.79 0.14 0.26
Subbasin Sub-CB-13-14			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.25 0.09 0.34	A (6%+) A (6%+)	0.79 0.14 0.61
Subbasin Sub-CB-15-16			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Streets, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.19 0.05 0.16 0.40	A (6%+) A (6%+) B (0-2%)	0.79 0.29 0.80 0.73
Subbasin Sub-CB-17			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.15 0.13 0.29	A (6%+) A (6%+)	0.79 0.29 0.56
Subbasin Sub-CB-18-19			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.47 0.47 0.95	A (6%+) A (6%+)	0.79 0.29 0.54
Subbasin Sub-CB-2			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.17 0.23 0.40	A (6%+) A (6%+)	0.79 0.29 0.50

Subbasin Sub-CB-20			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.49 1.00 1.49	A (6%+) A (6%+)	0.79 0.14 0.35
Subbasin Sub-CB-3			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.14 2.69 2.84	A (6%+) A (6%+)	0.79 0.14 0.17
Subbasin Sub-CB-4			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.15 0.19 0.34	A (6%+) A (6%+)	0.79 0.14 0.43
Subbasin Sub-CB-5			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Soil/Surface Description	(acres)  0.32 0.01	Group  A (6%+)	Coeff. 0.79 0.14
Soil/Surface Description	(acres)  0.32 0.01	Group  A (6%+)	Coeff. 0.79 0.14
Soil/Surface Description	0.32 0.01 0.33	Group  A (6%+) A (6%+)  Soil	Coeff. 0.79 0.14 0.78
Soil/Surface Description  Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.  Subbasin Sub-CB-6  Soil/Surface Description  Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater	0.32 0.01 0.33 Area (acres)	Group  A (6%+) A (6%+)  Soil Group  A (2-6%)	Coeff.  0.79  0.14  0.78  Runoff Coeff.  0.77
Soil/Surface Description  Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.  Subbasin Sub-CB-6  Soil/Surface Description  Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.  Subbasin Sub-CB-7  Subbasin Sub-CB-7  Soil/Surface Description	0.32 0.01 0.33 Area (acres)	Group  A (6%+) A (6%+)  Soil Group  A (2-6%)	Coeff.  0.79  0.14  0.78  Runoff Coeff.  0.77
Soil/Surface Description  Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.32 0.01 0.33 Area (acres) 	Group  A (6%+) A (6%+)  Soil Group  A (2-6%) A (6%+)	Coeff.  0.79 0.14 0.78  Runoff Coeff.  0.77 0.29 0.76
Soil/Surface Description Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.  Subbasin Sub-CB-6 Soil/Surface Description Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.  Subbasin Sub-CB-7 Subbasin Sub-CB-7 Subbasin Sub-CB-7 Soil/Surface Description Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater	Area (acres)  0.32 0.01 0.33  Area (acres)  0.14 0.00 0.14  Area (acres)  0.10 0.01	Group  A (6%+)  A (6%+)  Soil Group  A (2-6%) A (6%+)  Soil Group  A (0-2%)	Coeff.  0.79 0.14 0.78  Runoff Coeff.  0.77 0.29 0.76  Runoff Coeff.  0.76 0.26

```
0.17 A (2-6%) 0.77
0.05 A (2-6%) 0.22
0.22 0.64
Streets, 25 years or greater
Meadow, 25 years or greater
Composite Area & Weighted Runoff Coeff.
                                                       0.22
Subbasin Sub-CB-9
______
                                                             Soil Runoff
Group Coeff
                                                      Area
Soil/Surface Description
                                                    (acres)
______
                                                    0.15 A (2-6%) 0.77
0.00 A (2-6%) 0.26
0.15 0.76
Streets, 25 years or greater
Residential Lot Size 1 Acre, 25 years or greater
Composite Area & Weighted Runoff Coeff.
SCS TR-55 Time of Concentration Computations Report
Sheet Flow Equation
       Tc = (0.007 * ((n * Lf)^0.8)) / ((P^0.5) * (Sf^0.4))
       Where:
       Tc = Time of Concentration (hrs)
       n = Manning's Roughness
       Lf = Flow Length (ft)
       P = 2 yr, 24 hr Rainfall (inches)
       Sf = Slope (ft/ft)
Shallow Concentrated Flow Equation
       V = 16.1345 * (Sf^0.5) (unpaved surface)

V = 20.3282 * (Sf^0.5) (paved surface)
       V = 15.0 * (Sf^0.5) (grassed waterway surface)
         = 10.0 * (Sf^0.5) (nearly bare & untilled surface)
       V = 9.0 * (Sf^0.5) (cultivated straight rows surface)
       V = 7.0 * (Sf^0.5) (short grass pasture surface)
         = 5.0 * (Sf^0.5) (woodland surface)
       V = 2.5 * (Sf^0.5) (forest w/heavy litter surface)
       Tc = (Lf / V) / (3600 sec/hr)
       Where:
       Tc = Time of Concentration (hrs)
       Lf = Flow Length (ft)
       V = Velocity (ft/sec)
       Sf = Slope (ft/ft)
Channel Flow Equation
       V = (1.49 * (R^{(2/3)}) * (Sf^{0.5})) / n
       R = Aq / Wp
       Tc = (Lf / V) / (3600 sec/hr)
       Where:
       Tc = Time of Concentration (hrs)
       Lf = Flow Length (ft)
       R = Hydraulic Radius (ft)
       Aq = Flow Area (ft<sup>2</sup>)
```

Wp = Wetted Perimeter (ft) V = Velocity (ft/sec) Sf = Slope (ft/ft)n = Manning's Roughness Subbasin Sub-CB-1 \_\_\_\_\_\_ Sheet Flow Computations Subarea A Subarea B Subarea С Manning's Roughness: 0.40 0.00 0.00 Flow Length (ft): 33.69 0.00 0.00 Slope (%): 0.00 1.60 0.00 2 yr, 24 hr Rainfall (in): 3.60 0.00 0.00 Velocity (ft/sec): 0.00 0.06 0.00 0.00 Computed Flow Time (minutes): 9.26 0.00 Shallow Concentrated Flow Computations Subarea A Subarea B Subarea С Flow Length (ft): 0.00 329.84 0.00 Slope (%): 0.77 0.00 0.00 Surface Type: Paved Paved Paved Velocity (ft/sec): 1.79 0.00 0.00 Computed Flow Time (minutes): 3.08 0.00 0.00 \_\_\_\_\_\_ Total TOC (minutes): 12.34 \_\_\_\_\_\_ Subbasin Sub-CB-10 User-Defined TOC override (minutes): 5.00 Subbasin Sub-CB-11 Sheet Flow Computations Subarea A Subarea B Subarea С Manning's Roughness: 0.40 0.00 0.00

73.91

24.40

0.00

0.00

Slope (%):

0.00

Flow Length (ft):

0 00				
0.00	2 yr, 24 hr Rainfall (in):	3.60	0.00	
0.00	Velocity (ft/sec):	0.21	0.00	
0.00	Computed Flow Time (minutes):	5.85	0.00	
0.00				
	ow Concentrated Flow Computations			
С		Subarea A	Subarea B	Subarea
0.00	Flow Length (ft):	147.74	0.00	
0.00	Slope (%):	2.17	0.00	
Paved	Surface Type:	Paved	Paved	
0.00	Velocity (ft/sec):	2.99	0.00	
0.00	Computed Flow Time (minutes):	0.82	0.00	
		:==========	=======================================	=========
	Total TOC (minutes):	6.67		
======		=======================================	=======================================	========
	Flow Computations	Cultura 3	Quibaura D	Colorado
		Subarea A	Subarea B	Subarea
	Manning's Roughness:	0.40	0.00	Subarea
C	Manning's Roughness: Flow Length (ft):	0.40	0.00	Subarea
C 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):	0.40 222.44 10.60	0.00 0.00 0.00	Subarea
C 0.00 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):	0.40 222.44 10.60 3.60	0.00 0.00 0.00 0.00	Subarea
C 0.00 0.00 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):	0.40 222.44 10.60	0.00 0.00 0.00	Subarea
C 0.00 0.00 0.00 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):	0.40 222.44 10.60 3.60	0.00 0.00 0.00 0.00	Subarea
C 0.00 0.00 0.00 0.00 0.00 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):  Velocity (ft/sec):	0.40 222.44 10.60 3.60 0.19	0.00 0.00 0.00 0.00	Subarea
C 0.00 0.00 0.00 0.00 0.00 0.00 Shallo	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):  Velocity (ft/sec):  Computed Flow Time (minutes):	0.40 222.44 10.60 3.60 0.19	0.00 0.00 0.00 0.00	Subarea
C 0.00 0.00 0.00 0.00 0.00 Shall C	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):  Velocity (ft/sec):  Computed Flow Time (minutes):  ow Concentrated Flow Computations	0.40 222.44 10.60 3.60 0.19 19.70	0.00 0.00 0.00 0.00 0.00	
C 0.00 0.00 0.00 0.00 0.00 Shall C 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):  Velocity (ft/sec):  Computed Flow Time (minutes):  ow Concentrated Flow Computations	0.40 222.44 10.60 3.60 0.19 19.70	0.00 0.00 0.00 0.00 0.00 0.00	
C 0.00 0.00 0.00 0.00 Shall C 0.00 0.00 0.00 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):  Velocity (ft/sec):  Computed Flow Time (minutes):  ow Concentrated Flow Computations  Flow Length (ft):	0.40 222.44 10.60 3.60 0.19 19.70 Subarea A 185.02	0.00 0.00 0.00 0.00 0.00 0.00 Subarea B	
C 0.00 0.00 0.00 0.00 0.00 C 0.00 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):  Velocity (ft/sec):  Computed Flow Time (minutes):  ow Concentrated Flow Computations  Flow Length (ft):  Slope (%):	0.40 222.44 10.60 3.60 0.19 19.70 Subarea A 185.02 4.77	0.00 0.00 0.00 0.00 0.00 0.00 Subarea B 0.00	
C 0.00 0.00 0.00 0.00 0.00 C 0.00 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):  Velocity (ft/sec):  Computed Flow Time (minutes):  ow Concentrated Flow Computations  Flow Length (ft):  Slope (%):  Surface Type:	0.40 222.44 10.60 3.60 0.19 19.70  Subarea A 185.02 4.77 Paved	0.00 0.00 0.00 0.00 0.00 0.00 Subarea B 0.00 0.00	
C 0.00 0.00 0.00 0.00 0.00 C 0.00 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):  Velocity (ft/sec):  Computed Flow Time (minutes):  ow Concentrated Flow Computations  Flow Length (ft):  Slope (%):  Surface Type:  Velocity (ft/sec):	0.40 222.44 10.60 3.60 0.19 19.70 Subarea A 185.02 4.77 Paved 4.44	0.00 0.00 0.00 0.00 0.00 0.00 Subarea B 0.00 0.00 Paved 0.00	

	Total TOC (minutes):	20.39		
======		=======================================	=======================================	========
	in Sub-CB-13-14			
	Flow Computations			
C		Subarea A	Subarea B	Subarea
0.00	Manning's Roughness:	0.40	0.00	
0.00	Flow Length (ft):	80.13	0.00	
0.00	Slope (%):	24.40	0.00	
0.00	2 yr, 24 hr Rainfall (in):	3.60	0.00	
0.00	Velocity (ft/sec):	0.21	0.00	
0.00	Computed Flow Time (minutes):	6.23	0.00	
	w Concentrated Flow Computations			
		Subarea A	Subarea B	Subarea
C	Flow Length (ft):	174.35	0.00	
0.00	Slope (%):	2.45	0.00	
0.00	Surface Type:	Paved	Paved	
Paved	Velocity (ft/sec):	3.18	0.00	
0.00	Computed Flow Time (minutes):	0.91	0.00	
		.=========	=======================================	:=======
	Total TOC (minutes):	7.15		
======		=======================================	===========	========
Subbas	in Sub-CB-15-16			
	User-Defined TOC override (minutes):	5.00		
Subbas	in Sub-CB-17			
	User-Defined TOC override (minutes):	5.00		
	in Sub-CB-18-19			
	User-Defined TOC override (minutes):	5.00		

## Subbasin Sub-CB-2

User-Defined TOC override (minutes): 5.00

Subbasin Sub-CB-20

Sheet Flow Computations

		Subarea A	Subarea B	Subarea
C	Manning's Roughness:	0.40	0.00	
0.00	Flow Length (ft):	227.22	0.00	
0.00	Slope (%):	7.48	0.00	
0.00	2 yr, 24 hr Rainfall (in):	3.60	0.00	
0.00	Velocity (ft/sec):	0.16	0.00	
0.00	Computed Flow Time (minutes):	23.04	0.00	
0.00				
Shallo	w Concentrated Flow Computations			
	<del>-</del>	Subarea A	Subarea B	Subarea
C	Flow Length (ft):	Subarea A	Subarea B	Subarea
C 0.00	Flow Length (ft): Slope (%):			Subarea
C 0.00 0.00	J , ,	193.35	0.00	Subarea
C 0.00 0.00 Paved	Slope (%):	193.35 2.77	0.00	Subarea
C 0.00 0.00 Paved 0.00	Slope (%): Surface Type:	193.35 2.77 Paved	0.00 0.00 Paved	Subarea
C 0.00 0.00 Paved	Slope (%): Surface Type: Velocity (ft/sec):	193.35 2.77 Paved 3.38	0.00 0.00 Paved 0.00	Subarea

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Subbasin Sub-CB-3

Sheet Flow Computations

a		Subarea A	Subarea B	Subarea
C	Manning's Roughness:	0.40	0.00	
0.00	Flow Length (ft):	492.34	0.00	
0.00	Slope (%):	3.89	0.00	
0.00	2 yr, 24 hr Rainfall (in):	3.60	0.00	
0.00	Velocity (ft/sec):	0.15	0.00	
0.00	Computed Flow Time (minutes):	55.54	0.00	

	Concentrated Flow	_			
			Subarea A		Suba
00	Flow Length (ft):		70.73	0.00	
00	Slope (%):		4.87	0.00	
ved	Surface Type:		Unpaved	Paved	
0.0	Velocity (ft/sec)	:	3.56	0.00	
00	Computed Flow Tim	e (minutes):	0.33	0.00	
				===========	
	Total TOC (minute		55.87		
Subbasin	Sub-CB-4				
	User-Defined TOC	override (minutes	): 5.00		
	 1 Sub-CB-5				
	User-Defined TOC	override (minutes	): 5.00		
Subbasin	 1 Sub-CB-6				
	User-Defined TOC	override (minutes	): 5.00		
	 n Sub-CB-7				
	User-Defined TOC	override (minutes	5.00		
Subbasin	n Sub-CB-8W				
	User-Defined TOC	override (minutes	): 5.00		
Subbasin	Sub-CB-9				
	User-Defined TOC	override (minutes	): 5.00		
Subbasin	*****************  Runoff Summary  ***************				
 Subbasin ID	a Accumulate Preci	d Rainfall	Total Pea Runoff Runof	k Weighted f Runoff Cor	Time of accentration

	in	in/hr	in	cfs	Coeff	days	hh:mm:ss
Sub-CB-1	0.91	4.45	0.48	0.86	0.530	0	00:12:20
Sub-CB-10	0.60	7.21	0.45	0.69	0.750	0	00:05:00
Sub-CB-11	0.69	6.18	0.34	0.61	0.500	0	00:06:40
Sub-CB-12	1.15	3.39	0.30	1.12	0.260	0	00:20:23
Sub-CB-13-14	0.71	5.96	0.43	1.22	0.610	0	00:07:09
Sub-CB-15-16	0.60	7.21	0.44	2.13	0.730	0	00:05:00
Sub-CB-17	0.60	7.21	0.34	1.15	0.560	0	00:05:00
Sub-CB-18-19	0.60	7.21	0.32	3.69	0.540	0	00:05:00
Sub-CB-2	0.60	7.21	0.30	1.45	0.500	0	00:05:00
Sub-CB-20	1.24	3.10	0.43	1.62	0.350	0	00:23:59
Sub-CB-3	1.70	1.82	0.29	0.88	0.170	0	00:55:52
Sub-CB-4	0.60	7.21	0.26	1.06	0.430	0	00:05:00
Sub-CB-5	0.60	7.21	0.47	1.85	0.780	0	00:05:00
Sub-CB-6	0.60	7.21	0.46	0.78	0.760	0	00:05:00
Sub-CB-7	0.60	7.21	0.43	0.56	0.720	0	00:05:00
Sub-CB-8W	0.60	7.21	0.38	1.02	0.640	0	00:05:00
Sub-CB-9	0.60	7.21	0.46	0.81	0.760	0	00:05:00

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Node Depth Summary
\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*

CB-8E 0.00 0.00 257.54 0 00:00 0 0 0:0 CIT-8 2.69 2.69 257.49 0 00:00 0 0 0:0 CIT-9 2.27 2.58 259.98 0 00:05 0 0 0:0 DH-10 0.10 0.45 265.60 0 00:05 0 0 0:0
CIT-8 2.69 2.69 257.49 0 00:00 0 0 0:00 CIT-9 2.27 2.58 259.98 0 00:05 0 0 0:00
DH-10 0.10 0.45 265.60 0.00:05 0 0.0:0
DH-13 2.76 3.15 262.95 0 00:07 0 0 0:0
DH-20 0.01 0.39 278.01 0.00:24 0 0.00
DH-6 0.05 0.29 247.24 0 00:05 0 0 0:0
DMH-10 0.10 0.45 265.77 0 00:05 0 0 0:0
DMH-11 0.10 0.28 269.03 0 00:06 0 0 0:0
DMH-12 0.34 0.71 268.41 0 00:20 0 0 0:0
DMH-13 0.10 0.59 263.36 0 00:07 0 0 0:0
DMH-20 0.44 0.82 278.47 0 00:24 0 0 0:0
DMH-3 0.11 0.38 262.62 0 00:05 0 0 0:0
DMH-4N 0.11 0.51 253.36 0 00:05 0 0 0:0
DMH-4S 0.11 0.40 257.53 0 00:05 0 0 0:0
DMH-6 4.85 5.18 252.58 0 00:05 0 0 0:0
DMH-7 1.10 1.37 255.47 0 00:05 0 0 0:0
EX-18 3.00 3.59 269.59 0 00:05 0 0 0:0
EX-7 1.20 1.44 254.24 0 00:05 0 0 0:0
Structure - (72) 0.11 0.35 276.14 0 00:12 0 0 0:0
STU-16 0.28 0.72 253.42 0 00:05 0 0 0:0
STU-5 0.12 0.60 249.23 0 00:06 0 0 0:0
DP-1 0.00 0.31 275.31 0 00:12 0 0 0:0
DP-10 0.00 0.28 265.06 0 00:05 0 0 0:0
DP-13 0.01 0.47 260.07 0 00:07 0 0 0:0
DP-16 0.00 0.72 253.38 0 00:05 0 0 0:0
DP-18 0.01 0.51 264.87 0 00:05 0 0 0:0
DP-20 0.01 0.36 274.56 0 00:24 0 0 0:00
DP-5 0.01 0.52 248.52 0 00:05 0 0 0:00
DP-6 0.00 0.20 246.70 0 00:05 0 0 0:0
DP-7 0.00 0.54 253.14 0 00:06 0 0 0:0
OFFSITE1 0.00 0.08 281.30 0 00:16 0 0 0:0
OFFSITE-1 0.01 0.19 267.87 0 00:25 0 0 0:0

Node ID	Element Type	Maximum Lateral	Peak Inflow	Time of Peak Inflow		Maximum Flooding	Time of Peak Flooding
		INIIOW	cfs	days	rrence hh:mm	cfs	days hh:mm
CB-8E	JUNCTION	0.00				0.00	
CIT-8	JUNCTION	0.00	1.51	0	00:05	0.00	
CB-0E CIT-8 CIT-9 DH-10 DH-13 DH-20 DH-6 DMH-10	JUNCTION JUNCTION	0.00	0.71 1.08	0	00:05	0.00	
DH-10	JUNCTION	0.00	1.08	0	00:05	0.00	
DH-13	JUNCTION	0.00	1.59	0	00:07	0.00	
DH-20	JUNCTION		3.24	0	00:24	0.00	
DH-6	JUNCTION	0.00	0.75	0	00:05	0.00	
DMH-10	JUNCTION	0.00	0.67	0	00:05	0.00	
DMH-11	JUNCTION		0.60	0	00:06	0.00	
DMH-12	JUNCTION	0.00	1.06	0	00:20	0.00	
DMH-13	JUNCTION	0.00	1.22	0	00:07	0.00	
DMH-20	JUNCTION	0.00	3.24	0	00:24	0.00	
DMH-3	JUNCTION		1.44	0	00:05	0.00	
DMH-4N	JUNCTION	0.00	2.30	0	00:05	0.00	
DMH-4S	JUNCTION	0.00	1.44	0	00:05	0.00	
DMH-6	JUNCTION		0.75	0	00:05		
DMH-7	JUNCTION	0.00	0.56	0	00:05	0.00	
EX-18	JUNCTION	0.00	3.67	0	00:05	0.00	
EX-7	JUNCTION		2.01	0	00:05	0.00	
Structure - (72)	JUNCTION	0.00	0.73	0	00:12	0.00	
STU-16	JUNCTION		3.10	0	00:05	0.00	
STU-5 DP-1 DP-10 DP-13	JUNCTION		3.80	0	00:05	0.00	
DP-1	OUTFALL		0.73	0	00:12		
DP-10	OUTFALL	0 00	1 08	0	00:05	0.00	
DP-13	OUTFALL OUTFALL	0.00	1.58	0	00:07	0.00	
DP-16	OUTFALL		3.10	0		0.00	
DP-18	OUTFALL		3.65	0		0.00	
DP-20	OUTFALL		3.24	0		0.00	
DP-5	OUTFALL	0.00	3.79	0		0.00	
DP-6	OUTFALL	0.00	0.75	0	00:05		
DP-7	OUTFALL	0.00	2.01	0	00:06	0.00	
OFFSITE1	OUTFALL	0.00	0.09	0	00:16	0.00	
OFFSITE-1		0.00	1.05	0		0.00	

Inlet ID	Max Gutter Spread during Peak Flow ft	Max Gutter Water Elev during Peak Flow ft	Max Gutter Water Depth during Peak Flow ft	M	Time of Maximum Depth arrence hh:mm
CB-1	5.69	281.42	0.20	0	00:12
CB-10	2.64	267.85	0.16	0	00:05
CB-11	2.51	272.25	0.15	0	00:06
CB-12	3.25	271.26	0.19	0	00:20
CB-13	4.09	265.02	0.17	0	00:07
CB-16	5.72	255.18	0.25	0	00:05
CB-17	6.62	265.71	0.22	0	00:05
CB-18	13.24	274.09	0.37	0	00:05
CB-2	3.61	277.02	0.20	0	00:05

CB-20	4.07	279.84	0.17	0	00:00
CB-3	2.93	265.56	0.17	0	00:56
CB-4	3.18	256.11	0.18	0	00:05
CB-5	5.15	251.40	0.22	0	00:05
CB-6	2.79	255.51	0.16	0	00:05
CB-7	2.43	258.56	0.15	0	00:05
CB-8W	5.59	260.28	0.20	0	00:05
CB-9	2.83	262.99	0.17	0	00:05

- Inlet Total	Peak	Peak	Peak	Peak	Inlet	Total	
ID Time	Flow	Lateral	Flow	Flow	Efficiency	Flooding	
		Flow	Intercepted				
Flooded		cfs	by Inlet	Inlet	Peak Flow %		
minutes	CIS	CIS	CIS	CIS	6	acre-III	
- CB-1	0.86	0.86	0.74	0.12	86.52	0.000	
0 CB-10	0.69	0.69	0.68	0.01	98.49	0.000	
0 CB-11	0.61	0.61	0.61	0.01	99.09	0.000	
0 CB-12 0	1.12	1.12	1.06	0.07	94.20	0.000	
CB-13	1.22	1.22	=	=	_	0.000	
CB-16	2.22	2.13	-	-	-	0.000	
CB-17	1.15	1.15	0.94	0.22	81.26	0.000	
CB-18	3.69	3.69	-	-	-	0.000	
CB-2	1.45	1.45	1.32	0.13	91.04	0.000	
CB-20	1.62	1.62	-	-	-	0.000	
CB-3	0.88	0.88	0.85	0.03	96.70	0.000	
CB-4	1.06	1.06	1.01	0.06	94.82	0.000	
CB-5	1.85	1.85	=	=	_	0.000	
CB-6	0.78	0.78	0.76	0.02	97.64	0.000	
CB-7	0.57	0.56	0.57	0.00	99.36	0.000	
CB-8W	1.02	1.02	0.88	0.15	85.72	0.000	
CB-9	0.81	0.81	0.72	0.09	89.23	0.000	

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## Outfall Loading Summary

Outfall Node ID	Flow	Average	Peak
	Frequency	Flow	Inflow
	(%)	cfs	cfs
	1 00	0.25	0.72
DP-1	1.92	0.35	0.73
DP-10	1.42	0.37	1.08
DP-13	3.30	0.67	1.58
DP-16	1.31	0.87	3.10
DP-18	0.87	1.46	3.65
DP-20	3.39	1.59	3.24
DP-5	8.53	0.57	3.79
DP-6	1.06	0.25	0.75
DP-7	2.45	0.34	2.01
OFFSITE1	2.82	0.02	0.09
OFFSITE-1	4.54	0.40	1.05
System	2.87	6.88	16.37

Link ID Ratio of To		Т	ime of	Maximum	Length	Peak Flow	Design	Ratio of
Ratio of To	tal Reported Type	Pea	k Flow	Velocity	Factor	during	Flow	Maximum
Maximum Ti	me Condition					J		
_, _ , ,		0ccu	rrence	Attained		Analysis	Capacity	/Design
Flow Surcharged		darra	hh·mm	ft/sec		cfs	cfs	Flow
Depth minutes	3	uays	1111 • 111111	IC/Sec		CIS	CIS	FIOW
CB-1_Overflow		0	00:16	1.84	1.00	0.09	2.70	0.03
0.27 0		U	00.10	1.04	1.00	0.09	2.70	0.03
CB10-9_Gutter		0	00:06	1.71	1.00	0.01	8.35	0.00
0.07 0	Calculated							
CB11-10_Gutter		0	00:08	1.14	1.00	0.01	7.95	0.00
	Calculated							
CB12-13_Gutter		0	00:22	2.15	1.00	0.06	9.44	0.01
	Calculated	0	00.06	C 01	1 00	0 17	10 20	0 01
CB17-16_Gutter 0.20 0	CHANNEL	0	00:06	6.01	1.00	0.17	12.30	0.01
	CAICUIALEG	0	00:06	4.97	1.00	0.10	13.13	0.01
0.16 0		U	00.00	4.97	1.00	0.10	13.13	0.01
	CHANNEL	0	00:57	1.52	1.00	0.03	11.64	0.00
0.11 0		ŭ	00 57	1.02	1.00	0.03	11.01	0.00
CB4-5_Gutter	CHANNEL	0	00:07	2.99	1.00	0.04	8.25	0.00
0.12 0	Calculated							
CB6-5_Gutter	CHANNEL	0	00:07	2.23	1.00	0.02	7.73	0.00
0.09 0								
CB7-6_Gutter	CHANNEL	0	00:06	1.06	1.00	0.00	6.62	0.00
0.06 0		_						
CB8-7_Gutter	CHANNEL	0	00:07	2.15	1.00	0.11	4.89	0.02
	Calculated	0	00:07	2.67	1.00	0.06	6.26	0.01
CB9-8_Gutter 0.17 0	CHANNEL Calculated	U	00.07	2.0/	1.00	0.06	0.26	0.01
L-Pipe - (50)		0	00:25	8.50	1.00	1.05	41.01	0.03
_ 11PC (30)	CILLIATION	3	50.23	0.50	1.00	1.05	11.01	0.00

0.26	0	Calculated							
Pipe - (12)	U	CONDUIT	0	00:05	5.32	1.00	0.75	6.19	0.12
0.24	0	Calculated							
Pipe - (13) 0.33	0	CONDUIT Calculated	0	00:05	3.33	1.00	0.75	3.19	0.24
0.33 Pipe - (14)	U	CONDUIT	0	00:05	6.40	1.00	1.85	5.59	0.33
0.40	0	Calculated							
Pipe - (16)	0	CONDUIT Calculated	0	00:56	6.42	1.00	0.84	7.67	0.11
0.22 Pipe - (18)	U	CONDUIT	0	00:05	3.32	1.00	0.56	3.56	0.16
0.27	0	Calculated							
Pipe - (19) 0.24	0	CONDUIT Calculated	0	00:05	3.79	1.00	0.56	4.29	0.13
0.24 Pipe - (2)	U	CONDUIT	0	00:05	12.23	1.00	1.29	7.69	0.17
0.28	0	Calculated							
Pipe - (20) 0.00	0	CONDUIT Calculated	0	00:00	0.00	1.00	0.00	2.79	0.00
Pipe - (21)	U	CONDUIT	0	00:06	4.44	1.00	1.48	3.59	0.41
0.45	0	Calculated						0 = 5	0.56
Pipe - (22) 0.54	0	CONDUIT Calculated	0	00:06	4.67	1.00	2.01	3.56	0.56
Pipe - (23)	Ü	CONDUIT	0	00:05	5.71	1.00	0.87	6.40	0.14
0.25	0	Calculated	0	00.05	2 42	1 00	0 71	2 40	0 01
Pipe - (24) 0.31	0	CONDUIT Calculated	0	00:05	3.43	1.00	0.71	3.40	0.21
Pipe - (25)		CONDUIT	0	00:05	4.83	1.00	0.68	3.88	0.18
0.28	0	Calculated	0	00:05	2.72	1.00	0 67	2.52	0.26
Pipe - (26) 0.35	0	CONDUIT Calculated	U	00.05	2.72	1.00	0.67	2.52	0.20
Pipe - (27)		CONDUIT	0	00:05	2.71	1.00	0.67	2.52	0.27
0.35 Pipe - (28)	0	Calculated CONDUIT	0	00:06	6.03	1.00	0.60	8.05	0.07
0.18	0	Calculated	U	00.00	0.03	1.00	0.00	8.05	0.07
Pipe - (29)	_	CONDUIT	0	00:07	5.92	1.00	0.59	4.83	0.12
0.23 Pipe - (3)	0	Calculated CONDUIT	0	00:06	6.58	1.00	1.43	6.35	0.23
0.32	0	Calculated	Ü	00.00	0.30	1.00	1.13	0.33	0.23
Pipe - (30)	^	CONDUIT	0	00:20	3.95	1.00	1.06	3.56	0.30
0.37 Pipe - (31)	0	Calculated CONDUIT	0	00:20	5.74	1.00	1.05	5.52	0.19
0.29	0	Calculated							
Pipe - (33) 0.47	0	CONDUIT Calculated	0	00:07	4.41	1.00	1.58	3.56	0.44
Pipe - (34)	U	CONDUIT	0	00:07	3.21	1.00	1.22	2.54	0.48
0.49	0	Calculated							
Pipe - (35) 0.39	0	CONDUIT Calculated	0	00:07	4.27	1.00	1.22	3.73	0.33
Pipe - (4)	Ü	CONDUIT	0	00:06	5.83	1.00	2.26	4.45	0.51
0.50	0	Calculated	0	00.05	10 10	1 00	0.01	C 13	0 14
Pipe - (40) 0.25	0	CONDUIT Calculated	U	00:05	10.10	1.00	0.91	6.43	0.14
Pipe - (41)		CONDUIT	0	00:05	5.11	1.00	3.10	3.56	0.87
0.72 Pipe - (43)	0	Calculated CONDUIT	0	00:05	5.97	1.00	2.22	4.77	0.47
0.48	0	Calculated	U	00.03	3.97	1.00	2.22	4.//	0.47
Pipe - (44)	_	CONDUIT	0	00:05	7.65	1.00	3.67	5.63	0.65
0.59 Pipe - (45)	0	Calculated CONDUIT	0	00:05	7.00	1.00	3.65	14.86	0.25
0.34	0	Calculated	Ü	00 00	,	1.00	3.03	11.00	0.25
Pipe - (5)	_	CONDUIT	0	00:05	9.09	1.00	3.79	7.00	0.54
0.52 Pipe - (50)	0	Calculated CONDUIT	0	00:24	11.11	1.00	3.24	30.06	0.11
0.22	0	Calculated							
Pipe - (51) 0.39	0	CONDUIT Calculated	0	00:24	11.48	1.00	3.24	10.15	0.32
Pipe - (54)	U	CONDUIT	0	00:05	6.52	1.00	0.75	8.20	0.09

0.20	0	Calculated							
Pipe - (55)		CONDUIT	0	00:05	9.35	1.00	1.01	12.12	0.08
0.19	0	Calculated							
Pipe - (56)		CONDUIT	0	00:05	5.90	1.00	1.08	6.17	0.17
0.28	0	Calculated							
Pipe - (57)		CONDUIT	0	00:24	10.06	1.00	3.24	26.08	0.12
0.24	0	Calculated							
Pipe - (61)		CONDUIT	0	00:12	5.80	1.00	0.73	5.92	0.12
0.24	0	Calculated							
Pipe - (62)		CONDUIT	0	00:12	3.57	1.00	0.73	3.56	0.21
0.31	0	Calculated							
Pipe - (7)		CONDUIT	0	00:05	7.14	1.00	1.44	7.14	0.20
0.30	0	Calculated							

All links are stable.

WARNING 108: Surcharge elevation defined for Junction EX-18 is below junction maximum elevation. Assumed surcharge elevation equal to maximum elevation.

WARNING 139 : Ponded area defined for on sag Inlet CB-18 is zero. Assumed ponded area equal to 10 ft² (0.929  $m^2$ ).

WARNING 138: Initial water surface elevation defined for Inlet CB-20 is below catchbasin invert elevation.

Assumed initial water surface elevation equal to catchbasin inlet invert

elevation.

WARNING 138: Initial water surface elevation defined for Inlet CB-4 is below catchbasin invert elevation.

Assumed initial water surface elevation equal to catchbasin inlet invert

elevation.

WARNING 138: Initial water surface elevation defined for Inlet CB-5 is below catchbasin invert elevation.

Assumed initial water surface elevation equal to catchbasin inlet invert

elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB-1\_Overflow is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB10-9\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB11-10\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB12-13\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB17-16\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB2-3\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB3-4\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB4-5\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB6-5\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB7-6\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB8-7\_Gutter is below the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB9-8\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 117 : Conduit outlet invert elevation defined for Conduit CB-1\_Overflow is below downstream node invert elevation.

Assumed conduit outlet invert elevation equal to downstream node invert

elevation.

WARNING 004 : Minimum elevation drop used for Conduit CB-1\_Overflow.

WARNING 005: Minimum slope used for Conduit CB-1\_Overflow.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB10-9\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-9.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB11-10\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-10.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB12-13\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-13.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB17-16\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-16.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB2-3\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-3.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB3-4\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-4.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB4-5\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-5.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB6-5\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-5.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB7-6\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-6.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB8-7\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-7.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB9-8\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-8W.

WARNING 116 : Conduit inlet invert elevation defined for Conduit Pipe - (14) is below upstream node invert elevation.

Assumed conduit inlet invert elevation equal to upstream node invert elevation. WARNING 116: Conduit inlet invert elevation defined for Conduit Pipe - (50) is below upstream node invert elevation.

Assumed conduit inlet invert elevation equal to upstream node invert elevation. WARNING 116: Conduit inlet invert elevation defined for Conduit Pipe - (55) is below upstream node invert elevation.

Assumed conduit inlet invert elevation equal to upstream node invert elevation.

Analysis began on: Tue Jan 31 11:10:46 2023 Analysis ended on: Tue Jan 31 11:10:49 2023

Total elapsed time: 00:00:03

```
Autodesk® Storm and Sanitary Analysis 2016 - Version 13.2.165 (Build 0)
Project Description
******
File Name ..... Grove_St_Ph2_r1-PR.SPF
******
Analysis Options
******
Flow Units ..... cfs
Subbasin Hydrograph Method. Rational
Time of Concentration..... SCS TR-55
Return Period...... 25 years
Link Routing Method ...... Kinematic Wave Storage Node Exfiltration. None
Starting Date ..... DEC-20-2022 00:00:00
Ending Date ..... DEC-21-2022 00:00:00 Report Time Step ..... 00:00:10
******
Element Count
Number of subbasins ..... 17
Number of nodes ..... 50
Number of links ..... 52
******
Subbasin Summary
******
Subbasin
                      Total
                        Area
TD
                       acres
Sub-CB-1
                    0.36
0.13
0.20
1.28
0.34
0.40
0.29
Sub-CB-10
Sub-CB-11
Sub-CB-12
Sub-CB-12
Sub-CB-13-14
Sub-CB-15-16
Sub-CB-17
Sub-CB-18-19
                       0.95
Sub-CB-2
                        0.40
                        1.49
Sub-CB-20
Sub-CB-3
                        2.84
Sub-CB-4
                        0.34
                        0.33
Sub-CB-5
Sub-CB-6
                        0.14
Sub-CB-7
                        0.11
Sub-CB-8W
                        0.22
Sub-CB-9
                        0.15
*****
Node Summary
                  Element Invert Maximum Ponded External Type Elevation Elev. Area Inflow ft ft ft
Node
TD
```

257.54 259.20 0.00

JUNCTION

CB-8E

CIT-8 CIT-9 DH-10 DH-13		JUNCTION JUNCTION JUNCTION JUNCTION		259.42 40 262.67 L5 268.15 30 265.60	0.00 0.00 0.00 0.00		
DH-20		JUNCTION		52 280.21	0.00		
DH-6		JUNCTION	246.	95 255.72	0.00		
DMH-10		JUNCTION		32 267.86	0.00		
DMH-11		JUNCTION		75 272.24	0.00		
DMH-12		JUNCTION		70 271.08	0.00		
DMH-13		JUNCTION	262.	77 265.40 55 280.22	0.00		
DMH-20		JUNCTION	277.	55 280.22	0.00		
DMH-3		JUNCTION	262.	24 265.34 35 255.95	0.00		
DMH-4N		JUNCTION			0.00		
DMH-4S		JUNCTION	257.	13 262.56	0.00		
DMH-6		JUNCTION		257.58	0.00		
DMH-7		JUNCTION		10 258.76	0.00		
EX-18		JUNCTION		273.24	0.00		
EX-7	(72)	JUNCTION		30 258.62	0.00		
Structure STU-16	- (72)	JUNCTION JUNCTION	273.	79 277.57 70 255.49	0.00		
STU-5		JUNCTION	248	53 251 88	0.00		
DP-1		OUTFALL	275	53 251.88 00 276.00	0.00		
DP-10		OUTFALL		78 265.78	0.00		
DP-13		OUTFALL		260.60	0.00		
DP-16		OUTFALL		56 253.66	0.00		
DP-18		OUTFALL			0.00		
DP-20		OUTFALL	274.	36 265.86 20 275.70	0.00		
DP-5		OUTFALL	248.	00 249.00	0.00		
DP-6		OUTFALL	246.	249.00 247.50	0.00		
DP-7		OUTFALL	252.	50 253.60	0.00		
OFFSITE1		OUTFALL	281.	22 281.50	0.00		
OFFSITE-1		OUTFALL	267.	58 268.43	0.00		
*********  Inlet Summ  *******  Inlet  Catchbasin	nary :***	Inlet	Initial	Manufacturer Grate		Inlet	Number
Inlet Summ *******  Inlet  Catchbasin	nary :***	Let Ponded		Grate			
Inlet Summ ******* Inlet	nary **** Inl	let Ponded Manufacture	<u> </u>	Grate Part		Inlet Location	Number of
Inlet Summ ******* Inlet Catchbasin ID	nary **** Inl	Let Ponded	<u> </u>	Grate Part			
Inlet Summ ******* Inlet Catchbasin ID	nary **** Inl Rim	let Ponded Manufacture: Area	<u> </u>	Grate Part Logging Number			of
Inlet Summ ******* Inlet Catchbasin ID Invert Elevation	nary *** Inl Rim Elevatio	let Ponded Manufacture Area on	Water C	Grate Part Logging Number Factor			of
Inlet Summ ******* Inlet Catchbasin ID Invert Elevation	nary **** Inl Rim	let Ponded Manufacture Area on	. Water C	Grate Part Logging Number			of
Inlet Summ ******* Inlet Catchbasin ID Invert Elevation	nary *** Inl Rim Elevatio	let Ponded Manufacture Area on	Water C	Grate Part Logging Number Factor			of
Inlet Summ  *******  Inlet Catchbasin  ID Invert  Elevation  ft	nary ***  Inl Rim Elevation	let Ponded Manufacturen Area on ft²	Water C Elevation ft	Grate Part Logging Number Factor			of
Inlet Summ  *******  Inlet Catchbasin  ID Invert  Elevation  ft	nary ***  Inl Rim Elevation	let Ponded Manufacturer Area on ft²	Water C Elevation ft	Grate Part Logging Number Factor		Location	of Inlets
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft	nary ****  Inl Rim Elevation	let Ponded Manufacturer Area on ft² FHWA HEC-22	Water C Elevation ft GENERIC	Grate Part Logging Number Factor %			of
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10	Tary  This is a second of the control of the contro	let Ponded Manufacturer Area on ft² FHWA HEC-22	Water C Elevation ft  GENERIC 278.10	Grate Part Logging Number Factor  % N/A 0.00		Location On Grade	of Inlets
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10 CB-10	Rim Elevation ft 281.22	let Ponded Manufactures Area on ft² FHWA HEC-22 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC	Grate Part logging Number Factor  % N/A 0.00 N/A		Location	of Inlets
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10	Rim Elevation ft 281.22	Let Ponded Manufactures Area on ft² FHWA HEC-22 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44	Grate Part Logging Number Factor  % N/A 0.00		Location On Grade	of Inlets
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10 CB-10 265.44	Rim Elevation ft 281.22	let Ponded Manufactures Area on ft² FHWA HEC-22 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44	Grate Part logging Number Factor  % N/A 0.00 N/A 0.00		Location  On Grade  On Grade	of Inlets  1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10 CB-10 265.44 CB-11	Inl Rim Elevation ft 281.22 267.69 272.10	Let Ponded Manufactures Area on ft² FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22	Water C. Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10	Grate Part Logging Number Factor		Location  On Grade  On Grade	of Inlets  1 1 1
Inlet Summ  ******* Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10 CB-10 265.44 CB-11 269.10	Inl Rim Elevation ft 281.22 267.69	let Ponded Manufacturer Area on ft² FHWA HEC-22 FHWA HEC-22 FHWA HEC-22	Water C. Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10	Grate Part Logging Number Factor		Location  On Grade  On Grade  On Grade	of Inlets  1 1 1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10 CB-10 265.44 CB-11 269.10 CB-12	Elevation ft 281.22 267.69 272.10 271.07	let Ponded Manufacturer Area on ft² FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 269.10 GENERIC 268.07	Grate Part Logging Number Factor  % N/A 0.00 N/A 0.00 N/A 0.00 N/A		Location  On Grade  On Grade  On Grade	of Inlets  1 1 1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft	Inl Rim Elevation ft 281.22 267.69 272.10	let Ponded Manufacturen Area on ft² FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 269.10 GENERIC 268.07	Grate Part Logging Number Factor  % N/A 0.00 N/A 0.00 N/A 0.00 N/A 0.00 N/A 0.00		On Grade On Grade On Grade On Grade	of Inlets  1 1 1
Inlet Summ ******* Inlet Catchbasin ID Invert Elevation ft	Rim Elevation ft 281.22 267.69 272.10 271.07	Let Ponded Manufactures Area  on  ft²  FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 10.00 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 268.07 GENERIC 268.07 GENERIC 262.90 GENERIC	Grate Part Logging Number Factor  % N/A 0.00 N/A		On Grade On Grade On Grade On Grade	of Inlets  1 1 1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10 CB-10 265.44 CB-11 269.10 CB-12 268.07 CB-13 262.90 CB-16 252.93	Elevation ft 281.22 267.69 272.10 271.07	Let Ponded Manufactures Area on ft² FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 10.00 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 268.07 GENERIC 262.90 GENERIC 252.93	Grate Part Logging Number Factor		On Grade On Grade On Grade On Grade On Grade On Sag On Sag	of Inlets  1 1 1 1 1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10 CB-10 265.44 CB-11 269.10 CB-12 268.07 CB-13 262.90 CB-16 252.93 CB-17	Rim Elevation ft  281.22 267.69 272.10 271.07 264.85 254.93	Let Ponded Manufactures Area on ft² FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 10.00 FHWA HEC-22 10.00 FHWA HEC-22	Water C. Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 268.07 GENERIC 262.90 GENERIC 252.93 GENERIC	Grate Part Logging Number Factor		On Grade On Grade On Grade On Grade On Grade	of Inlets  1 1 1 1 1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft	Rim Elevation ft 281.22 267.69 272.10 271.07	Let Ponded Manufactures Area  on  ft²  FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 10.00 FHWA HEC-22 10.00 FHWA HEC-22	Water C. Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 268.07 GENERIC 268.07 GENERIC 252.93 GENERIC 260.16	Grate Part Logging Number Factor  %  N/A 0.00 N/A		On Grade On Grade On Grade On Grade On Sag On Sag On Grade	of Inlets  1 1 1 1 1 1 1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft	Elevation ft 281.22 267.69 272.10 271.07 264.85 254.93 265.49	Let Ponded Manufactures Area  on  ft²  FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 10.00 FHWA HEC-22 10.00 FHWA HEC-22 10.00 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 269.10 GENERIC 262.90 GENERIC 252.93 GENERIC 260.16 GENERIC	Grate Part Logging Number Factor  % N/A 0.00 N/A		On Grade On Grade On Grade On Grade On Grade On Sag On Sag	of Inlets  1 1 1 1 1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft	Rim Elevation ft  281.22 267.69 272.10 271.07 264.85 254.93	Let Ponded Manufactures Area  on  ft²  FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 10.00 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 268.07 GENERIC 262.90 GENERIC 252.93 GENERIC 250.16 GENERIC 260.16 GENERIC 269.61	Grate Part Logging Number Factor		On Grade On Grade On Grade On Grade On Sag On Sag On Grade On Sag	of Inlets  1 1 1 1 1 1 1 1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft	Elevation ft 281.22 267.69 272.10 271.07 264.85 254.93 265.49	Let Ponded Manufactures Area  on  ft²  FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 10.00 FHWA HEC-22 10.00 FHWA HEC-22 10.00 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 268.07 GENERIC 262.90 GENERIC 252.93 GENERIC 250.16 GENERIC 260.16 GENERIC 269.61	Grate Part Logging Number Factor  % N/A 0.00 N/A		On Grade On Grade On Grade On Grade On Sag On Sag On Grade	of Inlets  1 1 1 1 1 1 1 1

CB-20		FHWA	HEC-22	GENERIC	N/A		Or	ı Sag	1	
278.18	279.	67 10.	00	278.18	0.00					
CB-3			HEC-22	GENERIC	N/A		Or	n Grade	1	
262.89	265.	39	-	262.89	0.00					
CB-4		FHWA	HEC-22	GENERIC	N/A		Or	n Grade	1	
254.18	255.	93	-	254.18	0.00					
CB-5		FHWA	HEC-22	GENERIC	N/A		Or	n Sag	1	
249.44	251.	18 10.	00	249.44	0.00					
CB-6		FHWA	HEC-22	GENERIC	N/A		Or	n Grade	1	
252.35	255.	35	-	252.35	0.00					
CB-7		FHWA	HEC-22	GENERIC	N/A		Or	ı Grade	1	
255.41	258.	41	-	255.41	0.00					
CB-8W		FHWA	HEC-22	GENERIC	N/A		Or	ı Grade	1	
257.08	260.	08	-	257.08	0.00					
CB-9		FHWA	HEC-22	GENERIC	N/A		Or	ı Grade	1	
259.82	262.	82	-	259.82	0.00					
*****	*****	*****	*							
		ter Summar								
				Doodsso	Dood	C11++0	C11++ 0	_	111++02	
Inlet ID			Roadwa: tudina		_	Gutter Cross	Gutter Width		utter ssion	
ID		rongr	Slope		_	Slope	WIGCII	рерге	SSIOII	
			ft/f		Rougilliess	ft/ft	ft		in	
			IL/I	L IL/IL					111	
CB-1			0.010	0 0.0200	0.0160	0.0620	2.00		2.00	
CB-10			0.020		0.0130	0.0620	2.00		0.00	
CB-11			0.020		0.0130	0.0620	2.00		0.00	
CB-11			0.020		0.0130	0.0620	2.00		0.00	
CB-12				- 0.0500	0.0130	0.0620	2.00		0.00	
CB-15				- 0.0500	0.0130	0.0620	2.00		0.00	
CB-17			0.010		0.0160	0.0620	2.00		2.00	
CB-17			0.010		0.0160	0.0620	2.00		2.00	
			0 020	0.0200						
CB-2			0.020		0.0130	0.0620	2.00		0.00	
CB-20			0 000	- 0.0500	0.0130	0.0620	2.00		0.00	
CB-3			0.020		0.0130	0.0620	2.00		0.00	
CB-4			0.020		0.0130	0.0620	2.00		0.00	
CB-5				- 0.0500	0.0130	0.0620	2.00		0.00	
CB-6			0.020		0.0130	0.0620	2.00		0.00	
CB-7			0.020			0.0620	2.00		0.00	
CB-8W			0.010		0.0130	0.0620	2.00		2.00	
CB-9			0.020	0.0500	0.0130	0.0620	2.00		0.00	
*****	***									
Link Sum										
Link		From Node		To Node	Element	т.	onath	Clana	Manning's	~
ID		FIOIII NOGE	:	10 Node	Element Type	L	ength ft	Slope %	Roughnes	
								·•		_
CB-1_Ove	rflow	CB-1		OFFSITE1	CHANNEL		241.8	0.2000	0.013	0
CB10-9_G		CB-10		CB-9	CHANNEL		254.5	1.9133	0.013	
CB11-10_		CB-11		CB-10	CHANNEL		254.5	1.7326	0.013	
CB12-13		CB-12		CB-13	CHANNEL		254.5	2.4437	0.013	
CB17-16_		CB-17		CB-16	CHANNEL		254.5	4.1501	0.013	
CB2-3 Gu		CB-2		CB-3	CHANNEL		241.8	4.7276	0.013	
CB2-3_Gu CB3-4 Gu		CB-3		CB-4	CHANNEL		254.5	3.7167	0.013	
CB4-5_Gu		CB-4		CB-5	CHANNEL		254.5	1.8662	0.013	
CB6-5_Gu		CB-4 CB-6		CB-5	CHANNEL		254.5	1.6383	0.013	
_									0.013	
CB7-6_Gu		CB-7		CB-6	CHANNEL		254.5	1.2022		
CB8-7_Gu		CB-8W		CB-7	CHANNEL		254.5	0.6561	0.013	
CB9-8_Gu		CB-9		CB-8W	CHANNEL		254.5	1.0765	0.013	
L-Pipe -		CB-20		OFFSITE-1	CHANNEL		546.0	2.1967	0.013	
Pipe - (		DMH-6		DH-6	CONDUIT		13.3	3.0144	0.013	
Pipe - (	13)	CB-6		DMH-6	CONDUIT		12.5	0.7995	0.013	0

Pipe - (14)	CB-5	STU-5	CONDUIT	28.8	2.4635	0.0130
Pipe - (16)	CB-3	DMH-3	CONDUIT	11.9	4.6382	0.0130
Pipe - (18)	CB-7	DMH-7	CONDUIT	20.7	1.0000	0.0130
<u> </u>						
Pipe - (19)	DMH-7	EX-7	CONDUIT	6.9	1.4505	0.0130
Pipe - (2)	CB-2	DMH-3	CONDUIT	246.6	4.6555	0.0130
Pipe - (20)	CB-8E	CIT-8	CONDUIT	7.6	0.6131	0.0130
Pipe - (21)	CIT-8	EX-7	CONDUIT	196.9	1.0156	0.0130
Pipe - (22)	EX-7	DP-7	CONDUIT	20.0	1.0000	0.0130
Pipe - (23)	CB-8W	CIT-8	CONDUIT	20.5	3.2241	0.0130
Pipe - (24)	CB-9	CIT-9	CONDUIT	16.5	0.9092	0.0130
Pipe - (25)	CIT-9	CIT-8	CONDUIT	219.0	1.1872	0.0130
Pipe - (26)	DMH-10	DH-10	CONDUIT	14.0	0.5000	0.0130
Pipe - (27)	CB-10	DMH-10	CONDUIT	4.2	0.5000	0.0130
Pipe - (28)	CB-11	DMH-11	CONDUIT	4.9	5.1092	0.0130
Pipe - (29)	DMH-11	DH-10	CONDUIT	190.5	1.8369	0.0130
Pipe - (3)	DMH-4S	DMH-4N	CONDUIT	131.6	3.1757	0.0130
Pipe - (30)	CB-12	DMH-12	CONDUIT	3.6	1.0000	0.0130
Pipe - (31)	DMH-12	DH-13	CONDUIT	217.3	2.4045	0.0130
Pipe - (33)	DH-13	DP-13	CONDUIT	19.5	1.0000	0.0130
Pipe - (34)	CB-13	DMH-13	CONDUIT	5.9	0.5098	0.0130
Pipe - (35)	DMH-13	DH-13	CONDUIT	19.9	1.0989	0.0130
Pipe - (4)	DMH-4N	STU-5	CONDUIT	263.5	1.5634	0.0130
Pipe - (40)	CB-17	STU-16	CONDUIT	220.1	3.2621	0.0130
				4.1	1.0000	
Pipe - (41)	STU-16	DP-16	CONDUIT			0.0130
Pipe - (43)	CB-16	STU-16	CONDUIT	7.3	1.7930	0.0130
Pipe - (44)	CB-18	EX-18	CONDUIT	24.4	2.4990	0.0130
Pipe - (45)	EX-18	DP-18	CONDUIT	81.8	2.0000	0.0130
Pipe - (5)	STU-5	DP-5	CONDUIT	16.3	3.8608	0.0130
Pipe - (50)	CB-20	DMH-20	CONDUIT	6.5	8.1871	0.0130
Pipe - (51)	DMH-20	DH-20	CONDUIT	5.7	8.1142	0.0130
Pipe - (54)	DH-6	DP-6	CONDUIT	8.5	5.3000	0.0130
Pipe - (55)	CB-4	DMH-4N	CONDUIT	10.6	11.5699	0.0130
Pipe - (56)	DH-10	DP-10	CONDUIT	12.4	3.0000	0.0130
Pipe - (57)	DH-20	DP-20	CONDUIT	55.5	6.1646	0.0130
Pipe - (61)	CB-1	Structure -	(72)CONDUIT	79.8	2.7583	0.0130
Pipe - (62)	<u></u>					
FIDE - (07)	Structure -	(72)DP-1	CONDUIT	79.0	1.0000	0.0130
Pipe - (62) Pipe - (7)	Structure - DMH-3	(72)DP-1 DMH-4S	CONDUIT CONDUIT	79.0 124.6	1.0000 4.0212	0.0130 0.0130
Pipe - (7)	DMH-3					
	DMH-3					
Pipe - (7)  ***********************************	DMH-3 ***** ummary					
Pipe - (7)	DMH-3 ***** ummary					
Pipe - (7)  ***********************************	DMH-3 ***** ummary					
Pipe - (7)  ******************  Cross Section S ************************************	DMH-3  ***** ummary *****	DMH-4S	CONDUIT	124.6	4.0212	0.0130
Pipe - (7)  *************  Cross Section S  *************  Link	DMH-3  ***** ummary *****	DMH-4S	CONDUIT	124.6	4.0212	0.0130
Pipe - (7)  *************  Cross Section S  ***********  Link  Design	DMH-3  ***** ummary *****	DMH-4S Depth/	CONDUIT	124.6 No. of	4.0212 Cross	0.0130
Pipe - (7)  **********  Cross Section S  *********  Link  Design  ID	DMH-3  ***** ummary *****	DMH-4S Depth/	CONDUIT	124.6 No. of	4.0212 Cross	0.0130
Pipe - (7)  **********  Cross Section S  *********  Link  Design  ID	DMH-3  ***** ummary *****	DMH-4S Depth/	CONDUIT	124.6 No. of	4.0212 Cross Sectional	0.0130  Full Flow  Hydraulic
Pipe - (7)  *********  Cross Section S  *********  Link  Design  ID  Flow	DMH-3  ***** ummary *****	DMH-4S Depth/	CONDUIT	124.6 No. of	4.0212 Cross Sectional	0.0130  Full Flow  Hydraulic
Pipe - (7)  *********  Cross Section S  *********  Link  Design  ID  Flow	DMH-3  ***** ummary *****	DMH-4S  Depth/ Diameter	CONDUIT Width	124.6 No. of	4.0212  Cross Sectional Area	0.0130  Full Flow  Hydraulic  Radius
Pipe - (7)  **********  Cross Section S  *******  Link  Design  ID  Flow  Capacity	DMH-3  ***** ummary *****	DMH-4S  Depth/ Diameter	CONDUIT Width	124.6 No. of	4.0212  Cross Sectional Area	0.0130  Full Flow  Hydraulic  Radius
Pipe - (7)  ************  Cross Section S  ********  Link  Design  ID  Flow  Capacity  cfs	DMH-3  *****  ummary  *****  Shape	DMH-4S  Depth/ Diameter	CONDUIT Width ft	No. of	4.0212  Cross Sectional  Area  ft²	0.0130  Full Flow  Hydraulic  Radius  ft
Pipe - (7)  **********  Cross Section S  *******  Link  Design  ID  Flow  Capacity  cfs	DMH-3  *****  ummary  *****  Shape	DMH-4S  Depth/ Diameter  ft	CONDUIT  Width  ft	No. of Barrels	4.0212  Cross Sectional  Area  ft²	0.0130  Full Flow  Hydraulic  Radius  ft
Pipe - (7)  ***********  Cross Section S *******  Link  Design  ID  Flow  Capacity  cfs   CB-1_Overflow	DMH-3  *****  ummary  *****  Shape	DMH-4S  Depth/ Diameter  ft	CONDUIT Width ft	No. of	4.0212  Cross Sectional  Area  ft²	0.0130  Full Flow  Hydraulic  Radius  ft
Pipe - (7)  ***********  Cross Section S *******  Link  Design ID  Flow  Capacity  cfs   CB-1_Overflow 2.70	DMH-3  ***** ummary  ***** Shape  TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28	CONDUIT  Width  ft  14.00	No. of Barrels	Cross Sectional Area ft²	0.0130  Full Flow Hydraulic Radius ft
Pipe - (7)  ***********  Cross Section S  *******  Link  Design  ID  Flow  Capacity  cfs   CB-1_Overflow  2.70  CB10-9_Gutter	DMH-3  ***** ummary  ***** Shape  TRIANGULAR	DMH-4S  Depth/ Diameter  ft	CONDUIT  Width  ft	No. of Barrels	4.0212  Cross Sectional  Area  ft²	0.0130  Full Flow  Hydraulic  Radius  ft
Pipe - (7)  ************* Cross Section S ******** Link Design ID Flow Capacity cfs CB-1_Overflow 2.70 CB10-9_Gutter 8.35	DMH-3  ***** ummary ***** Shape  TRIANGULAR TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28 0.28	CONDUIT  Width  ft  14.00  14.00	No. of Barrels	Cross Sectional Area ft²  1.96 1.96	0.0130  Full Flow Hydraulic Radius ft  0.14 0.14
Pipe - (7)  ************* Cross Section S ******** Link Design ID Flow Capacity cfs  CB-1_Overflow 2.70 CB10-9_Gutter 8.35 CB11-10_Gutter	TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28	CONDUIT  Width  ft  14.00	No. of Barrels	Cross Sectional Area ft²	0.0130  Full Flow Hydraulic Radius ft
Pipe - (7)  ************* Cross Section S ******** Link Design ID Flow Capacity cfs  CB-1_Overflow 2.70 CB10-9_Gutter 8.35 CB11-10_Gutter 7.95	DMH-3  ***** ummary ***** Shape  TRIANGULAR TRIANGULAR TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28  0.28  0.28	CONDUIT  Width  ft  14.00 14.00 14.00	No. of Barrels  1 1 1	Cross Sectional Area ft²  1.96 1.96	0.0130  Full Flow Hydraulic Radius ft  0.14 0.14 0.14
Pipe - (7)  ************  Cross Section S *******  Link  Design  ID  Flow  Capacity  cfs   CB-1_Overflow  2.70  CB10-9_Gutter  8.35  CB11-10_Gutter  7.95  CB12-13_Gutter	DMH-3  ***** ummary ***** Shape  TRIANGULAR TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28 0.28	CONDUIT  Width  ft  14.00  14.00	No. of Barrels	Cross Sectional Area ft²  1.96 1.96	0.0130  Full Flow Hydraulic Radius ft  0.14 0.14
Pipe - (7)  ***********  Cross Section S *******  Link  Design ID  Flow  Capacity  cfs   CB-1_Overflow  2.70  CB10-9_Gutter  8.35  CB11-10_Gutter  7.95  CB12-13_Gutter  9.44	*****  wmmary  ***** Shape  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28 0.28 0.28 0.28	ft  14.00 14.00 14.00 14.00	No. of Barrels  1 1 1 1	4.0212  Cross Sectional Area ft²  1.96 1.96 1.96 1.96	Full Flow Hydraulic Radius ft  0.14 0.14 0.14 0.14
Pipe - (7)  ************  Cross Section S *******  Link  Design ID Flow  Capacity  cfs   CB-1_Overflow  2.70  CB10-9_Gutter  7.95  CB12-13_Gutter  9.44  CB17-16_Gutter	DMH-3  ***** ummary ***** Shape  TRIANGULAR TRIANGULAR TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28  0.28  0.28	CONDUIT  Width  ft  14.00 14.00 14.00	No. of Barrels  1 1 1	Cross Sectional Area ft²  1.96 1.96	0.0130  Full Flow Hydraulic Radius ft  0.14 0.14 0.14
Pipe - (7)  **************  Cross Section S  ********  Link  Design  ID  Flow  Capacity  cfs   CB-1_Overflow  2.70  CB10-9_Gutter  8.35  CB11-10_Gutter  7.95  CB12-13_Gutter  9.44  CB17-16_Gutter  12.30	*****  wmmary  ***** Shape  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28 0.28 0.28 0.28 0.28	ft  14.00 14.00 14.00 14.00 14.00	No. of Barrels  1 1 1 1 1	4.0212  Cross Sectional Area ft²  1.96 1.96 1.96 1.96 1.96	0.0130  Full Flow Hydraulic Radius ft  0.14 0.14 0.14 0.14 0.14
Pipe - (7)  ************** Cross Section S ********* Link Design ID Flow  Capacity cfs  CB-1_Overflow 2.70 CB10-9_Gutter 8.35 CB11-10_Gutter 7.95 CB12-13_Gutter 9.44 CB17-16_Gutter 12.30 CB2-3_Gutter	*****  wmmary  ***** Shape  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28 0.28 0.28 0.28	ft  14.00 14.00 14.00 14.00	No. of Barrels  1 1 1 1	4.0212  Cross Sectional Area ft²  1.96 1.96 1.96 1.96	Full Flow Hydraulic Radius ft  0.14 0.14 0.14 0.14
Pipe - (7)  *************  Cross Section S  ********  Link  Design  ID  Flow  Capacity  cfs   CB-1_Overflow  2.70  CB10-9_Gutter  8.35  CB11-10_Gutter  7.95  CB12-13_Gutter  9.44  CB17-16_Gutter  12.30  CB2-3_Gutter  13.13	DMH-3  ***** ummary ***** Shape  TRIANGULAR TRIANGULAR TRIANGULAR TRIANGULAR TRIANGULAR TRIANGULAR TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28 0.28 0.28 0.28 0.28 0.28 0.28	ft  14.00 14.00 14.00 14.00 14.00 14.00	124.6  No. of Barrels  1 1 1 1 1 1	4.0212  Cross Sectional Area ft²  1.96 1.96 1.96 1.96 1.96 1.96	0.0130  Full Flow Hydraulic Radius ft  0.14 0.14 0.14 0.14 0.14 0.14
Pipe - (7)  ************** Cross Section S ********* Link Design ID Flow  Capacity cfs  CB-1_Overflow 2.70 CB10-9_Gutter 8.35 CB11-10_Gutter 7.95 CB12-13_Gutter 9.44 CB17-16_Gutter 12.30 CB2-3_Gutter	*****  wmmary  ***** Shape  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28 0.28 0.28 0.28 0.28	ft  14.00 14.00 14.00 14.00 14.00	No. of Barrels  1 1 1 1 1	4.0212  Cross Sectional Area ft²  1.96 1.96 1.96 1.96 1.96	0.0130  Full Flow Hydraulic Radius ft  0.14 0.14 0.14 0.14 0.14

11 (4						
11.64 CB4-5_Gutter	TRIANGULAR	0.28	14.00	1	1.96	0.14
8.25 CB6-5_Gutter	TRIANGULAR	0.28	14.00	1	1.96	0.14
7.73 CB7-6_Gutter	TRIANGULAR	0.28	14.00	1	1.96	0.14
6.62 CB8-7_Gutter	TRIANGULAR	0.28	14.00	1	1.96	0.14
4.89 CB9-8_Gutter	TRIANGULAR	0.28	14.00	1	1.96	0.14
6.26 L-Pipe - (50)	IRREGULAR	0.75	6.80	1	3.82	0.50
41.01 Pipe - (12)	CIRCULAR	1.00	1.00	1	0.79	0.25
6.19 Pipe - (13)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.19 Pipe - (14)	CIRCULAR	1.00	1.00	1	0.79	0.25
5.59 Pipe - (16)	CIRCULAR	1.00	1.00	1	0.79	0.25
7.67 Pipe - (18)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.56 Pipe - (19)	CIRCULAR	1.00	1.00	1	0.79	0.25
4.29 Pipe - (2)	CIRCULAR	1.00	1.00	1	0.79	0.25
7.69 Pipe - (20)	CIRCULAR	1.00	1.00	1	0.79	0.25
2.79 Pipe - (21)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.59 Pipe - (22)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.56 Pipe - (23)	CIRCULAR	1.00	1.00	1	0.79	0.25
6.40 Pipe - (24)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.40 Pipe - (25)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.88 Pipe - (26)	CIRCULAR	1.00	1.00	1	0.79	0.25
2.52 Pipe - (27)	CIRCULAR	1.00	1.00	1	0.79	0.25
2.52 Pipe - (28)	CIRCULAR	1.00	1.00	1	0.79	0.25
8.05 Pipe - (29)	CIRCULAR	1.00	1.00	1	0.79	0.25
4.83 Pipe - (3)	CIRCULAR	1.00	1.00	1	0.79	0.25
6.35 Pipe - (30)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.56 Pipe - (31)	CIRCULAR	1.00	1.00	1	0.79	0.25
5.52 Pipe - (33)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.56 Pipe - (34)	CIRCULAR	1.00	1.00	1	0.79	0.25
2.54 Pipe - (35)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.73 Pipe - (4)	CIRCULAR	1.00	1.00	1	0.79	0.25
4.45 Pipe - (40)	CIRCULAR	1.00	1.00	1	0.79	0.25
6.43 Pipe - (41)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.56 Pipe - (43)	CIRCULAR	1.00	1.00	1	0.79	0.25

4 55								
4.77 Pipe - (44)	CIRC	ULAR	1.00	1.00		1	0.79	0.25
5.63 Pipe - (45)	CIRC	ULAR	1.50	1.50		1	1.77	0.38
14.86 Pipe - (5)	CIRC	ULAR	1.00	1.00		1	0.79	0.25
7.00 Pipe - (50)	CIRC	ULAR	1.50	1.50		1	1.77	0.38
30.06 Pipe - (51)	CIRC	ULAR	1.00	1.00		1	0.79	0.25
10.15 Pipe - (54)	CIRC	ULAR	1.00	1.00		1	0.79	0.25
8.20 Pipe - (55)	CIRC	ULAR	1.00	1.00		1	0.79	0.25
12.12 Pipe - (56)	CIRC	ULAR	1.00	1.00		1	0.79	0.25
6.17 Pipe - (57)	CIRC	ULAR	1.50	1.50		1	1.77	0.38
26.08 Pipe - (61)	CIRC	ULAR	1.00	1.00		1	0.79	0.25
5.92 Pipe - (62)	CIRC	ULAR	1.00	1.00		1	0.79	0.25
3.56 Pipe - (7)	CIRC	ULAR	1.00	1.00		1	0.79	0.25
7.14								
*******								
Transect Su								
Transect XS	G-L-Pipe -	(13)						
Area:	0 0005	0 0010	0.0043	0 0076	0 0110			
	0.0005 0.0170	0.0019 0.0232	0.0043 0.0305	0.0076 0.0390	0.0118 0.0487			
	0.0595	0.0715	0.0847	0.0990	0.1145			
	0.1312	0.1491	0.1682	0.1884	0.2098			
	0.2323 0.3604	0.2561 0.3871	0.2810 0.4137	0.3071 0.4404	0.3338 0.4670			
	0.4937	0.5203	0.5470	0.5736	0.6003			
	0.6269	0.6536	0.6802	0.7069	0.7335			
	0.7602 0.8934	0.7868 0.9201	0.8135 0.9467	0.8401 0.9734	0.8668 1.0000			
Hrad:	0.0551	0.5201	0.5107	0.5751	1.0000			
	0.0139	0.0278	0.0418	0.0557	0.0696			
	0.0835 0.1459	0.0963 0.1591	0.1080 0.1724	0.1202 0.1858	0.1329 0.1994			
	0.2130	0.2267	0.2404	0.2542	0.2680			
	0.2818	0.2957	0.3095	0.3238	0.3512			
	0.3784 0.5130	0.4055 0.5396	0.4326 0.5660	0.4595 0.5924	0.4863 0.6187			
	0.6448	0.6708	0.6968	0.7226	0.7483			
	0.7740	0.7995	0.8249	0.8502	0.8754			
Width:	0.9005	0.9256	0.9505	0.9753	1.0000			
wideli.	0.0355	0.0711	0.1066	0.1422	0.1777			
	0.2132	0.2520	0.2961	0.3402	0.3842			
	0.4283 0.6487	0.4724 0.6927	0.5164 0.7368	0.5605 0.7809	0.6046 0.8249			
	0.8690	0.9131	0.9572	1.0000	1.0000			
	1.0000	1.0000	1.0000	1.0000	1.0000			
	1.0000	1.0000	1.0000	1.0000	1.0000			
	1.0000	1.0000	1.0000 1.0000	1.0000 1.0000	1.0000			
	1.0000	1.0000	1.0000	1.0000	1.0000			

Transect XS	-L-Pipe -	(16)			
Area:					
	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312 0.2323	0.1491 0.2561	0.1682 0.2810	0.1884 0.3071	0.2098
	0.2323	0.3871	0.4137	0.4404	0.3336
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868	0.8135	0.8401	0.8668
	0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:					
	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835	0.0963	0.1080	0.1202	0.1329
	0.1459 0.2130	0.1591 0.2267	0.1724 0.2404	0.1858 0.2542	0.1994 0.2680
	0.2130	0.2267	0.3095	0.3238	0.3512
	0.3784	0.4055	0.4326	0.4595	0.4863
	0.5130	0.5396	0.5660	0.5924	0.6187
	0.6448	0.6708	0.6968	0.7226	0.7483
	0.7740	0.7995	0.8249	0.8502	0.8754
	0.9005	0.9256	0.9505	0.9753	1.0000
Width:					
	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132 0.4283	0.2520 0.4724	0.2961 0.5164	0.3402 0.5605	0.3842
	0.4203	0.6927	0.7368	0.7809	0.8249
	0.8690	0.9131	0.9572	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
Transect XS	-L-Pipe -	(18)			
Area:					
	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312 0.2323	0.1491 0.2561	0.1682 0.2810	0.1884 0.3071	0.2098
	0.2323	0.2301	0.4137	0.4404	0.4670
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868	0.8135	0.8401	0.8668
	0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:	0 0120	0 0070	0 0410	0 0557	0.0606
	0.0139 0.0835	0.0278 0.0963	0.0418 0.1080	0.0557 0.1202	0.0696 0.1329
	0.1459	0.1591	0.1724	0.1202	0.1323
	0.2130	0.2267	0.2404	0.2542	0.2680
	0.2818	0.2957	0.3095	0.3238	0.3512
	0.3784	0.4055	0.4326	0.4595	0.4863
	0.5130	0.5396	0.5660	0.5924	0.6187
	0.6448	0.6708	0.6968	0.7226	0.7483
	0.7740	0.7995	0.8249	0.8502	0.8754
Width:	0.9005	0.9256	0.9505	0.9753	1.0000
Width:	0.0355	0.0711	0.1066	0.1422	0.1777
	0.0333	0.2520	0.2961	0.3402	0.3842
	0.4283	0.4724	0.5164	0.5605	0.6046
	0.6487	0.6927	0.7368	0.7809	0.8249
	0.8690	0.9131	0.9572	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000

	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	XS-L-Pipe -	(2)			
Area:	0 0005	0 0010	0.0042	0 0000	0 0110
	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595 0.1312	0.0715 0.1491	0.0847 0.1682	0.0990 0.1884	0.1145 0.2098
	0.2323	0.2561	0.2810	0.3071	0.3338
	0.3604	0.3871	0.4137	0.4404	0.4670
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868	0.8135	0.8401	0.8668
	0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:					
	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835	0.0963	0.1080	0.1202	0.1329
	0.1459	0.1591	0.1724	0.1858	0.1994
	0.2130	0.2267	0.2404	0.2542	0.2680
	0.2818 0.3784	0.2957 0.4055	0.3095 0.4326	0.3238 0.4595	0.3512 0.4863
	0.5130	0.5396	0.5660	0.5924	0.4803
	0.6448	0.6708	0.6968	0.7226	0.7483
	0.7740	0.7995	0.8249	0.8502	0.8754
	0.9005	0.9256	0.9505	0.9753	1.0000
Width:					
	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132	0.2520	0.2961	0.3402	0.3842
	0.4283	0.4724	0.5164	0.5605	0.6046
	0.6487	0.6927	0.7368	0.7809	0.8249
	0.8690	0.9131	0.9572	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000 1.0000	1.0000 1.0000	1.0000 1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	2.0000	1.0000	1.0000	1.0000
Transect :	XS-L-Pipe -	(24)			
Area:	_				
	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312	0.1491	0.1682	0.1884	0.2098
	0.2323 0.3604	0.2561 0.3871	0.2810 0.4137	0.3071 0.4404	0.3338 0.4670
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868	0.8135	0.8401	0.8668
	0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:					
	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835	0.0963	0.1080	0.1202	0.1329
	0.1459	0.1591	0.1724	0.1858	0.1994
	0.2130	0.2267	0.2404	0.2542	0.2680
	0.2818	0.2957	0.3095	0.3238	0.3512
	0.3784	0.4055	0.4326	0.4595	0.4863
	0.5130	0.5396	0.5660	0.5924 0.7226	0.6187
	0.6448 0.7740	0.6708 0.7995	0.6968 0.8249	0.7226	0.7483 0.8754
	0.7740	0.7995	0.8249	0.8502	1.0000
Width:	0.7003	0.7230	0.2503	0.7/33	1.0000
= = = = =	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132	0.2520	0.2961	0.3402	0.3842
	0.4283	0.4724	0.5164	0.5605	0.6046

	0.6487 0.8690 1.0000 1.0000 1.0000 1.0000	0.6927 0.9131 1.0000 1.0000 1.0000 1.0000	0.7368 0.9572 1.0000 1.0000 1.0000 1.0000	0.7809 1.0000 1.0000 1.0000 1.0000 1.0000	0.8249 1.0000 1.0000 1.0000 1.0000 1.0000
Transect XS	G-L-Pipe -	(27)			
Hrad:	0.0005 0.0170 0.0595 0.1312 0.2323 0.3604 0.4937 0.6269 0.7602 0.8934	0.0019 0.0232 0.0715 0.1491 0.2561 0.3871 0.5203 0.6536 0.7868 0.9201	0.0043 0.0305 0.0847 0.1682 0.2810 0.4137 0.5470 0.6802 0.8135 0.9467	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401 0.9734	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668 1.0000
iii au•	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740	0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995 0.9256	0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754 1.0000
Width:	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000	0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000 1.0000	0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000	0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000 1.0000	0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000
Transect XS	G-L-Pipe -	(28)			
	0.0005 0.0170 0.0595 0.1312 0.2323 0.3604 0.4937 0.6269 0.7602 0.8934	0.0019 0.0232 0.0715 0.1491 0.2561 0.3871 0.5203 0.6536 0.7868 0.9201	0.0043 0.0305 0.0847 0.1682 0.2810 0.4137 0.5470 0.6802 0.8135 0.9467	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401 0.9734	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668 1.0000
Hrad:	0.0139 0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005	0.0278 0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995 0.9256	0.0418 0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.0557 0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.0696 0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754 1.0000

Width:	0.0355 0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000	0.0711 0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000	0.1066 0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000	0.1422 0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000 1.0000	0.1777 0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000
Transect XX	S-L-Pipe -	(30)			
	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312	0.1491	0.1682	0.1884	0.2098
	0.2323	0.2561	0.2810	0.3071	0.3338
	0.3604	0.3871	0.4137	0.4404	0.4670
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868	0.8135	0.8401	0.8668
	0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:	0.0139	0.0278	0.0418	0.0557	0.0696
Width:	0.0835	0.0963	0.1080	0.1202	0.1329
	0.1459	0.1591	0.1724	0.1858	0.1994
	0.2130	0.2267	0.2404	0.2542	0.2680
	0.2818	0.2957	0.3095	0.3238	0.3512
	0.3784	0.4055	0.4326	0.4595	0.4863
	0.5130	0.5396	0.5660	0.5924	0.6187
	0.6448	0.6708	0.6968	0.7226	0.7483
	0.7740	0.7995	0.8249	0.8502	0.8754
	0.9005	0.9256	0.9505	0.9753	1.0000
Width:	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132	0.2520	0.2961	0.3402	0.3842
	0.4283	0.4724	0.5164	0.5605	0.6046
	0.6487	0.6927	0.7368	0.7809	0.8249
	0.8690	0.9131	0.9572	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
Transect XS	S-L-Pipe -	(37)			
Area:	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312	0.1491	0.1682	0.1884	0.2098
	0.2323	0.2561	0.2810	0.3071	0.3338
	0.3604	0.3871	0.4137	0.4404	0.4670
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868	0.8135	0.8401	0.8668
	0.8934	0.9201	0.9467	0.9734	1.0000
	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835	0.0963	0.1080	0.1202	0.1329
	0.1459	0.1591	0.1724	0.1858	0.1994
	0.2130	0.2267	0.2404	0.2542	0.2680
	0.2818	0.2957	0.3095	0.3238	0.3512
	0.3784	0.4055	0.4326	0.4595	0.4863

	0.5130	0.5396	0.5660	0.5924	0.6187
	0.6448	0.6708	0.6968	0.7226	0.7483
	0.7740	0.7995	0.8249	0.8502	0.8754
ratalele e	0.9005	0.9256	0.9505	0.9753	1.0000
Width:	0.0355	0.0711	0.1066	0.1422	0.1777
	0.0333	0.2520	0.2961	0.3402	0.3842
	0.4283	0.4724	0.5164	0.5605	0.6046
	0.6487	0.6927	0.7368	0.7809	0.8249
	0.8690	0.9131	0.9572	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
Transect XS	-L-Pipe -	(50)			
Area:	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0003	0.0019	0.0305	0.0390	0.0118
	0.0595	0.0232	0.0847	0.0990	0.1145
	0.1312	0.1491	0.1682	0.1884	0.2098
	0.2323	0.2561	0.2810	0.3071	0.3338
	0.3604	0.3871	0.4137	0.4404	0.4670
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868	0.8135	0.8401	0.8668
	0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:					
	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835	0.0963	0.1080	0.1202	0.1329
	0.1459	0.1591	0.1724	0.1858	0.1994
	0.2130	0.2267	0.2404	0.2542	0.2680
	0.2818	0.2957	0.3095	0.3238	0.3512
	0.3784 0.5130	0.4055 0.5396	0.4326 0.5660	0.4595 0.5924	0.4863 0.6187
	0.6448	0.5390	0.6968	0.7226	0.7483
	0.7740	0.0708	0.8249	0.8502	0.8754
	0.9005	0.7555	0.9505	0.9753	1.0000
Width:	0.5005	0.5250	0.,,,,	0.7733	1.0000
	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132	0.2520	0.2961	0.3402	0.3842
	0.4283	0.4724	0.5164	0.5605	0.6046
	0.6487	0.6927	0.7368	0.7809	0.8249
	0.8690	0.9131	0.9572	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000 1.0000	1.0000	1.0000 1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
Transect XS	-L-Pipe -	(55)			
Area:	-	•			
	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312	0.1491	0.1682	0.1884	0.2098
	0.2323	0.2561	0.2810	0.3071	0.3338
	0.3604	0.3871	0.4137	0.4404	0.4670
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269 0.7602	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868 0.9201	0.8135 0.9467	0.8401 0.9734	0.8668 1.0000
Hrad:	0.0751	0.7201	0.7107	0.7/34	1.0000
	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835	0.0963	0.1080	0.1202	0.1329

Width:	0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005 0.0355 0.2132 0.4283 0.6487	0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995 0.9256 0.0711 0.2520 0.4724 0.6927	0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505 0.1066 0.2961 0.5164 0.7368	0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753 0.1422 0.3402 0.5605 0.7809	0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754 1.0000 0.1777 0.3842 0.6046 0.8249		
	0.8690 1.0000 1.0000 1.0000 1.0000	0.9131 1.0000 1.0000 1.0000 1.0000	0.9572 1.0000 1.0000 1.0000 1.0000	1.0000 1.0000 1.0000 1.0000 1.0000	1.0000 1.0000 1.0000 1.0000 1.0000		
Runoff Qu	antity Cont	inuity	Volume acre-ft	Depth inches			
Total Pre	ecipitation cy Error (%)		1.103	1.328			
Flow Rout	************ ing Continu	ity	Volume acre-ft	Volume Mgallons			
External External Initial S Final Sto	Inflow Outflow Stored Volume ored Volume ty Error (%)	  e	0.000 0.458 0.000 0.000 -0.802	0.000 0.149 0.000 0.000			
Runoff Co	************ efficient Co	omputations	Report				
Subbasin	Sub-CB-1						
Soil/Surf	ace Descrip	tion			Area (acres)	Soil Group	Runoff Coeff.
Residenti	25 years or al Lot Size Area & Weig	1 Acre, 25	years or gr	reater	0.17 0.19 0.36	A (6%+) A (6%+)	0.79 0.29 0.53
Subbasin	Sub-CB-10	-					
Soil/Surf	ace Descrip	tion			Area (acres)	Soil Group	Runoff Coeff.
Residenti	25 years or al Lot Size Area & Wei	1 Acre, 25	years or g	reater	0.12 0.01 0.13	A (6%+) A (6%+)	0.79 0.29 0.75
Subbasin	Sub-CB-11	_					
					Area	Soil	Runoff

Soil/Surface Description	(acres)	Group	Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.11 0.09 0.20	A (6%+) A (6%+)	0.79 0.14 0.50
Subbasin Sub-CB-12			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.23 1.05 1.28	A (6%+) A (6%+)	0.79 0.14 0.26
Subbasin Sub-CB-13-14			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.25 0.09 0.34	A (6%+) A (6%+)	0.79 0.14 0.61
Subbasin Sub-CB-15-16			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Streets, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.19 0.05 0.16 0.40	A (6%+) A (6%+) B (0-2%)	0.79 0.29 0.80 0.73
Subbasin Sub-CB-17			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.15 0.13 0.29	A (6%+) A (6%+)	0.79 0.29 0.56
Subbasin Sub-CB-18-19			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.47 0.47 0.95	A (6%+) A (6%+)	0.79 0.29 0.54
Subbasin Sub-CB-2			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.17 0.23 0.40	A (6%+) A (6%+)	0.79 0.29 0.50

Subbasin Sub-CB-20			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.49 1.00 1.49	A (6%+) A (6%+)	0.79 0.14 0.35
Subbasin Sub-CB-3			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.14 2.69 2.84	A (6%+) A (6%+)	0.79 0.14 0.17
Subbasin Sub-CB-4			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.15 0.19 0.34	A (6%+) A (6%+)	0.79 0.14 0.43
Subbasin Sub-CB-5			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Soil/Surface Description	(acres)  0.32 0.01	Group  A (6%+)	Coeff. 0.79 0.14
Soil/Surface Description	(acres)  0.32 0.01	Group  A (6%+)	Coeff. 0.79 0.14
Soil/Surface Description	0.32 0.01 0.33	Group  A (6%+) A (6%+)  Soil	Coeff. 0.79 0.14 0.78
Soil/Surface Description  Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.  Subbasin Sub-CB-6  Soil/Surface Description  Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater	0.32 0.01 0.33 Area (acres)	Group  A (6%+) A (6%+)  Soil Group  A (2-6%)	Coeff.  0.79  0.14  0.78  Runoff Coeff.  0.77
Soil/Surface Description  Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.  Subbasin Sub-CB-6  Soil/Surface Description  Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.  Subbasin Sub-CB-7  Subbasin Sub-CB-7  Soil/Surface Description	0.32 0.01 0.33 Area (acres)	Group  A (6%+) A (6%+)  Soil Group  A (2-6%)	Coeff.  0.79  0.14  0.78  Runoff Coeff.  0.77
Soil/Surface Description  Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.32 0.01 0.33 Area (acres) 	Group  A (6%+) A (6%+)  Soil Group  A (2-6%) A (6%+)	Coeff.  0.79 0.14 0.78  Runoff Coeff.  0.77 0.29 0.76
Soil/Surface Description Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.  Subbasin Sub-CB-6 Soil/Surface Description Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.  Subbasin Sub-CB-7 Subbasin Sub-CB-7 Subbasin Sub-CB-7 Soil/Surface Description Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater	Area (acres)  0.32 0.01 0.33  Area (acres)  0.14 0.00 0.14  Area (acres)  0.10 0.01	Group  A (6%+)  A (6%+)  Soil Group  A (2-6%)  A (6%+)  Soil Group  A (6%+)	Coeff.  0.79 0.14 0.78  Runoff Coeff.  0.77 0.29 0.76  Runoff Coeff.  0.76 0.26

```
0.17 A (2-6%) 0.77
0.05 A (2-6%) 0.22
0.22 0.64
Streets, 25 years or greater
Meadow, 25 years or greater
Composite Area & Weighted Runoff Coeff.
                                                       0.22
Subbasin Sub-CB-9
______
                                                             Soil Runoff
Group Coeff
                                                      Area
Soil/Surface Description
                                                    (acres)
______
                                                    0.15 A (2-6%) 0.77
0.00 A (2-6%) 0.26
0.15 0.76
Streets, 25 years or greater
Residential Lot Size 1 Acre, 25 years or greater
Composite Area & Weighted Runoff Coeff.
SCS TR-55 Time of Concentration Computations Report
Sheet Flow Equation
       Tc = (0.007 * ((n * Lf)^0.8)) / ((P^0.5) * (Sf^0.4))
       Where:
       Tc = Time of Concentration (hrs)
       n = Manning's Roughness
       Lf = Flow Length (ft)
       P = 2 yr, 24 hr Rainfall (inches)
       Sf = Slope (ft/ft)
Shallow Concentrated Flow Equation
       V = 16.1345 * (Sf^0.5) (unpaved surface)

V = 20.3282 * (Sf^0.5) (paved surface)
       V = 15.0 * (Sf^0.5) (grassed waterway surface)
         = 10.0 * (Sf^0.5) (nearly bare & untilled surface)
       V = 9.0 * (Sf^0.5) (cultivated straight rows surface)
       V = 7.0 * (Sf^0.5) (short grass pasture surface)
         = 5.0 * (Sf^0.5) (woodland surface)
       V = 2.5 * (Sf^0.5) (forest w/heavy litter surface)
       Tc = (Lf / V) / (3600 sec/hr)
       Where:
       Tc = Time of Concentration (hrs)
       Lf = Flow Length (ft)
       V = Velocity (ft/sec)
       Sf = Slope (ft/ft)
Channel Flow Equation
       V = (1.49 * (R^{(2/3)}) * (Sf^{0.5})) / n
       R = Aq / Wp
       Tc = (Lf / V) / (3600 sec/hr)
       Where:
       Tc = Time of Concentration (hrs)
       Lf = Flow Length (ft)
       R = Hydraulic Radius (ft)
       Aq = Flow Area (ft<sup>2</sup>)
```

Wp = Wetted Perimeter (ft) V = Velocity (ft/sec) Sf = Slope (ft/ft)n = Manning's Roughness Subbasin Sub-CB-1 \_\_\_\_\_\_ Sheet Flow Computations Subarea A Subarea B Subarea С Manning's Roughness: 0.40 0.00 0.00 Flow Length (ft): 33.69 0.00 0.00 Slope (%): 0.00 1.60 0.00 2 yr, 24 hr Rainfall (in): 3.60 0.00 0.00 Velocity (ft/sec): 0.00 0.06 0.00 0.00 Computed Flow Time (minutes): 9.26 0.00 Shallow Concentrated Flow Computations Subarea A Subarea B Subarea С Flow Length (ft): 0.00 329.84 0.00 Slope (%): 0.77 0.00 0.00 Surface Type: Paved Paved Paved Velocity (ft/sec): 1.79 0.00 0.00 Computed Flow Time (minutes): 3.08 0.00 0.00 \_\_\_\_\_\_ Total TOC (minutes): 12.34 \_\_\_\_\_\_ Subbasin Sub-CB-10 User-Defined TOC override (minutes): 5.00 Subbasin Sub-CB-11 Sheet Flow Computations Subarea A Subarea B Subarea С Manning's Roughness: 0.40 0.00 0.00

73.91

24.40

0.00

0.00

Slope (%):

0.00

Flow Length (ft):

0 00				
0.00	2 yr, 24 hr Rainfall (in):	3.60	0.00	
0.00	Velocity (ft/sec):	0.21	0.00	
0.00	Computed Flow Time (minutes):	5.85	0.00	
0.00				
	ow Concentrated Flow Computations			
С		Subarea A	Subarea B	Subarea
0.00	Flow Length (ft):	147.74	0.00	
0.00	Slope (%):	2.17	0.00	
Paved	Surface Type:	Paved	Paved	
0.00	Velocity (ft/sec):	2.99	0.00	
0.00	Computed Flow Time (minutes):	0.82	0.00	
		:==========	=======================================	=========
	Total TOC (minutes):	6.67		
======		=======================================	=======================================	========
	Flow Computations	Cultura 3	Quibaura D	Colorado
		Subarea A	Subarea B	Subarea
	Manning's Roughness:	0.40	0.00	Subarea
C	Manning's Roughness: Flow Length (ft):	0.40	0.00	Subarea
C 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):	0.40 222.44 10.60	0.00 0.00 0.00	Subarea
C 0.00 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):	0.40 222.44 10.60 3.60	0.00 0.00 0.00 0.00	Subarea
C 0.00 0.00 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):	0.40 222.44 10.60	0.00 0.00 0.00	Subarea
C 0.00 0.00 0.00 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):	0.40 222.44 10.60 3.60	0.00 0.00 0.00 0.00	Subarea
C 0.00 0.00 0.00 0.00 0.00 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):  Velocity (ft/sec):	0.40 222.44 10.60 3.60 0.19	0.00 0.00 0.00 0.00	Subarea
C 0.00 0.00 0.00 0.00 0.00 0.00 Shallo	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):  Velocity (ft/sec):  Computed Flow Time (minutes):	0.40 222.44 10.60 3.60 0.19	0.00 0.00 0.00 0.00	Subarea
C 0.00 0.00 0.00 0.00 0.00 Shall C	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):  Velocity (ft/sec):  Computed Flow Time (minutes):  ow Concentrated Flow Computations	0.40 222.44 10.60 3.60 0.19 19.70	0.00 0.00 0.00 0.00 0.00	
C 0.00 0.00 0.00 0.00 0.00 Shall C 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):  Velocity (ft/sec):  Computed Flow Time (minutes):  ow Concentrated Flow Computations	0.40 222.44 10.60 3.60 0.19 19.70	0.00 0.00 0.00 0.00 0.00 0.00	
C 0.00 0.00 0.00 0.00 Shall C 0.00 0.00 0.00 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):  Velocity (ft/sec):  Computed Flow Time (minutes):  ow Concentrated Flow Computations  Flow Length (ft):	0.40 222.44 10.60 3.60 0.19 19.70 Subarea A 185.02	0.00 0.00 0.00 0.00 0.00 0.00 Subarea B	
C 0.00 0.00 0.00 0.00 0.00 C 0.00 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):  Velocity (ft/sec):  Computed Flow Time (minutes):  ow Concentrated Flow Computations  Flow Length (ft):  Slope (%):	0.40 222.44 10.60 3.60 0.19 19.70 Subarea A 185.02 4.77	0.00 0.00 0.00 0.00 0.00 0.00 Subarea B 0.00	
C 0.00 0.00 0.00 0.00 0.00 C 0.00 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):  Velocity (ft/sec):  Computed Flow Time (minutes):  ow Concentrated Flow Computations  Flow Length (ft):  Slope (%):  Surface Type:	0.40 222.44 10.60 3.60 0.19 19.70  Subarea A 185.02 4.77 Paved	0.00 0.00 0.00 0.00 0.00 0.00 Subarea B 0.00 0.00	
C 0.00 0.00 0.00 0.00 0.00 C 0.00 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):  Velocity (ft/sec):  Computed Flow Time (minutes):  ow Concentrated Flow Computations  Flow Length (ft):  Slope (%):  Surface Type:  Velocity (ft/sec):	0.40 222.44 10.60 3.60 0.19 19.70 Subarea A 185.02 4.77 Paved 4.44	0.00 0.00 0.00 0.00 0.00 0.00 Subarea B 0.00 0.00 Paved 0.00	

	Total TOC (minutes):	20.39		
======		=======================================	=======================================	========
	in Sub-CB-13-14			
	Flow Computations			
C		Subarea A	Subarea B	Subarea
0.00	Manning's Roughness:	0.40	0.00	
0.00	Flow Length (ft):	80.13	0.00	
0.00	Slope (%):	24.40	0.00	
0.00	2 yr, 24 hr Rainfall (in):	3.60	0.00	
0.00	Velocity (ft/sec):	0.21	0.00	
0.00	Computed Flow Time (minutes):	6.23	0.00	
	w Concentrated Flow Computations			
		Subarea A	Subarea B	Subarea
C	Flow Length (ft):	174.35	0.00	
0.00	Slope (%):	2.45	0.00	
0.00	Surface Type:	Paved	Paved	
Paved	Velocity (ft/sec):	3.18	0.00	
0.00	Computed Flow Time (minutes):	0.91	0.00	
		.=========	=======================================	:=======
	Total TOC (minutes):	7.15		
======		=======================================	===========	========
Subbas	in Sub-CB-15-16			
	User-Defined TOC override (minutes):	5.00		
Subbas	in Sub-CB-17			
	User-Defined TOC override (minutes):	5.00		
	in Sub-CB-18-19			
	User-Defined TOC override (minutes):	5.00		

## Subbasin Sub-CB-2

User-Defined TOC override (minutes): 5.00

Subbasin Sub-CB-20

Sheet Flow Computations

		Subarea A	Subarea B	Subarea
C	Manning's Roughness:	0.40	0.00	
0.00	Flow Length (ft):	227.22	0.00	
0.00	Slope (%):	7.48	0.00	
0.00	2 yr, 24 hr Rainfall (in):	3.60	0.00	
0.00	Velocity (ft/sec):	0.16	0.00	
0.00	Computed Flow Time (minutes):	23.04	0.00	
0.00				
Shallo	w Concentrated Flow Computations			
	<del>-</del>	Subarea A	Subarea B	Subarea
C	Flow Length (ft):	Subarea A	Subarea B	Subarea
C 0.00	Flow Length (ft): Slope (%):			Subarea
C 0.00 0.00	J , ,	193.35	0.00	Subarea
C 0.00 0.00 Paved	Slope (%):	193.35 2.77	0.00	Subarea
C 0.00 0.00 Paved 0.00	Slope (%): Surface Type:	193.35 2.77 Paved	0.00 0.00 Paved	Subarea
C 0.00 0.00 Paved	Slope (%): Surface Type: Velocity (ft/sec):	193.35 2.77 Paved 3.38	0.00 0.00 Paved 0.00	Subarea

\_\_\_\_\_\_

Subbasin Sub-CB-3

Sheet Flow Computations

a		Subarea A	Subarea B	Subarea
C	Manning's Roughness:	0.40	0.00	
0.00	Flow Length (ft):	492.34	0.00	
0.00	Slope (%):	3.89	0.00	
0.00	2 yr, 24 hr Rainfall (in):	3.60	0.00	
0.00	Velocity (ft/sec):	0.15	0.00	
0.00	Computed Flow Time (minutes):	55.54	0.00	

	Concentrated Flow	_			
			Subarea A		Suba
00	Flow Length (ft):		70.73	0.00	
00	Slope (%):		4.87	0.00	
ved	Surface Type:		Unpaved	Paved	
0.0	Velocity (ft/sec)	:	3.56	0.00	
00	Computed Flow Tim	e (minutes):	0.33	0.00	
				===========	
	Total TOC (minute		55.87		
Subbasin	Sub-CB-4				
	User-Defined TOC	override (minutes	): 5.00		
	 1 Sub-CB-5				
	User-Defined TOC	override (minutes	): 5.00		
Subbasin	 1 Sub-CB-6				
	User-Defined TOC	override (minutes	): 5.00		
	 n Sub-CB-7				
	User-Defined TOC	override (minutes	5.00		
Subbasin	n Sub-CB-8W				
	User-Defined TOC	override (minutes	): 5.00		
Subbasin	Sub-CB-9				
	User-Defined TOC	override (minutes	): 5.00		
Subbasin	*****************  Runoff Summary  ***************				
 Subbasin ID	a Accumulate Preci	d Rainfall	Total Pea Runoff Runof	k Weighted f Runoff Cor	Time of accentration

	in	in/hr	in	cfs	Coeff	days	hh:mm:ss
Sub-CB-1	1.11	5.40	0.59	1.04	0.530	0	00:12:20
Sub-CB-10	0.73	8.75	0.55	0.84	0.750	0	00:05:00
Sub-CB-11	0.83	7.50	0.42	0.74	0.500	0	00:06:40
Sub-CB-12	1.39	4.11	0.36	1.36	0.260	0	00:20:23
Sub-CB-13-14	0.86	7.23	0.53	1.48	0.610	0	00:07:09
Sub-CB-15-16	0.73	8.75	0.53	2.58	0.730	0	00:05:00
Sub-CB-17	0.73	8.75	0.41	1.40	0.560	0	00:05:00
Sub-CB-18-19	0.73	8.75	0.39	4.48	0.540	0	00:05:00
Sub-CB-2	0.73	8.75	0.36	1.76	0.500	0	00:05:00
Sub-CB-20	1.50	3.75	0.53	1.96	0.350	0	00:23:59
Sub-CB-3	2.06	2.21	0.35	1.07	0.170	0	00:55:52
Sub-CB-4	0.73	8.75	0.31	1.29	0.430	0	00:05:00
Sub-CB-5	0.73	8.75	0.57	2.24	0.780	0	00:05:00
Sub-CB-6	0.73	8.75	0.55	0.95	0.760	0	00:05:00
Sub-CB-7	0.73	8.75	0.52	0.68	0.720	0	00:05:00
Sub-CB-8W	0.73	8.75	0.47	1.23	0.640	0	00:05:00
Sub-CB-9	0.73	8.75	0.55	0.98	0.760	0	00:05:00

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Node Depth Summary
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Node ID	Average Depth Attained ft	Maximum Depth Attained ft	Maximum HGL Attained ft		of Max urrence	Total Flooded Volume acre-in	Total Time Flooded minutes	Retention Time hh:mm:ss
CB-8E	0.00	0.00	257.54	0	00:00	0	0	0:00:00
CIT-8	2.69	2.69	257.49	0	00:00	0	0	0:00:00
CIT-9	2.27	2.61	260.01	0	00:05	0	0	0:00:00
DH-10	0.10	0.49	265.64	0	00:05	0	0	0:00:00
DH-13	2.76	3.19	262.99	0	00:07	0	0	0:00:00
DH-20	0.01	0.43	278.05	0	00:24	0	0	0:00:00
DH-6	0.05	0.31	247.26	0	00:05	0	0	0:00:00
DMH-10	0.10	0.49	265.81	0	00:05	0	0	0:00:00
DMH-11	0.10	0.30	269.05	0	00:06	0	0	0:00:00
DMH-12	0.34	0.74	268.44	0	00:20	0	0	0:00:00
DMH-13	0.11	0.65	263.42	0	00:07	0	0	0:00:00
DMH-20	0.44	0.86	278.51	0	00:24	0	0	0:00:00
DMH-3	0.11	0.40	262.64	0	00:05	0	0	0:00:00
DMH-4N	0.12	0.57	253.42	0	00:05	0	0	0:00:00
DMH-4S	0.11	0.44	257.57	0	00:05	0	0	0:00:00
DMH-6	4.85	5.21	252.61	0	00:05	0	0	0:00:00
DMH-7	1.11	1.40	255.50	0	00:05	0	0	0:00:00
EX-18	3.00	3.67	269.67	0	00:05	0	0	0:00:00
EX-7	1.20	1.47	254.27	0	00:05	0	0	0:00:00
Structure - (72	0.11	0.37	276.16	0	00:12	0	0	0:00:00
STU-16	0.28	2.79	255.49	0	00:04	0.00	1	0:00:00
STU-5	0.12	0.67	249.30	0	00:06	0	0	0:00:00
DP-1	0.00	0.33	275.33	0	00:12	0	0	0:00:00
DP-10	0.00	0.31	265.09	0	00:05	0	0	0:00:00
DP-13	0.01	0.52	260.12	0	00:07	0	0	0:00:00
DP-16	0.00	0.86	253.52	0	00:05	0	0	0:00:00
DP-18	0.01	0.57	264.93	0	00:05	0	0	0:00:00
DP-20	0.01	0.39	274.59	0	00:24	0	0	0:00:00
DP-5	0.02	0.59	248.59	0	00:05	0	0	0:00:00
DP-6	0.00	0.22	246.72	0	00:05	0	0	0:00:00
DP-7	0.00	0.60	253.20	0	00:06	0	0	0:00:00
OFFSITE1	0.00	0.09	281.31	0	00:16	0	0	0:00:00
OFFSITE-1	0.01	0.21	267.89	0	00:25	0	0	0:00:00

Node	Element	Maximum	Peak	T	ime of	Maximum	Time of Peak
ID	Type	Lateral	Inflow	Peak	Inflow	Flooding	Flooding
		Inflow		Occu	rrence	Overflow	Occurrence
		cfs	cfs	days	hh:mm	cfs	days hh:mm
CB-8E	JUNCTION	0.00	0.00	0	00:00	0.00	
CIT-8	JUNCTION	0.00	1.78	0	00:05	0.00	
CIT-9	JUNCTION	0.00	0.84	0	00:05	0.00	
DH-10	JUNCTION	0.00	1.30	0	00:05	0.00	
DH-13	JUNCTION	0.00	1.92	0	00:07	0.00	
DH-20	JUNCTION	0.00	3.92	0	00:24	0.00	
DH-6	JUNCTION	0.00	0.90	0	00:05	0.00	
DMH-10	JUNCTION	0.00	0.80	0	00:05	0.00	
DMH-11	JUNCTION	0.00	0.72	0	00:06	0.00	
DMH-12	JUNCTION	0.00	1.25	0	00:20	0.00	
DMH-13	JUNCTION	0.00	1.48	0	00:07	0.00	
DMH-20	JUNCTION	0.00	3.92	0	00:24	0.00	
DMH-3	JUNCTION	0.00	1.75	0	00:05	0.00	
DMH-4N	JUNCTION	0.00	2.76	0	00:05	0.00	
DMH-4S	JUNCTION	0.00	1.74	0	00:05	0.00	
DMH-6	JUNCTION	0.00	0.90	0	00:05	0.00	
DMH-7	JUNCTION	0.00	0.68	0	00:05	0.00	
EX-18	JUNCTION	0.00	4.46	0	00:05	0.00	
EX-7	JUNCTION	0.00	2.40	0	00:06	0.00	
Structure - (72)	JUNCTION	0.00	0.86	0	00:12	0.00	
STU-16	JUNCTION	0.00	3.76	0	00:05	0.20	0 00:05
STU-5	JUNCTION	0.00	4.64	0	00:05	0.00	
DP-1	OUTFALL	0.00	0.86	0	00:12	0.00	
DP-10	OUTFALL	0.00	1.30	0	00:05	0.00	
DP-13	OUTFALL	0.00	1.92	0	00:07	0.00	
DP-16	OUTFALL	0.00	3.70	0	00:05	0.00	
DP-18	OUTFALL	0.00	4.43	0	00:05	0.00	
DP-20	OUTFALL	0.00	3.92	0	00:24	0.00	
DP-5	OUTFALL	0.00	4.63	0	00:05	0.00	
DP-6	OUTFALL	0.00	0.90	0	00:05	0.00	
DP-7	OUTFALL	0.00	2.40	0	00:06	0.00	
OFFSITE1	OUTFALL	0.00	0.13	0	00:16	0.00	
OFFSITE-1	OUTFALL	0.00	1.27	0	00:25	0.00	
	00111111	0.00	/	Ü	30 23	3.00	

Inlet ID	Max Gutter Spread during Peak Flow ft	Max Gutter Water Elev during Peak Flow ft	Max Gutter Water Depth during Peak Flow ft	M	Time of Maximum Depth arrence hh:mm
CB-1	6.29	281.43	0.21	0	00:12
CB-10	2.87	267.86	0.17	0	00:05
CB-11	2.73	272.26	0.16	0	00:06
CB-12	3.52	271.27	0.20	0	00:20
CB-13	4.54	265.04	0.19	0	00:07
CB-16	6.46	255.22	0.29	0	00:05
CB-17	7.30	265.72	0.23	0	00:05
CB-18	15.22	274.13	0.41	0	00:05
CB-2	3.91	277.04	0.22	0	00:05

CB-20	4.52	279.86	0.19	0	00:00
CB-3	3.18	265.57	0.18	0	00:56
CB-4	3.44	256.13	0.20	0	00:05
CB-5	5.76	251.43	0.25	0	00:05
CB-6	3.03	255.53	0.18	0	00:05
CB-7	2.66	258.57	0.16	0	00:05
CB-8W	6.22	260.29	0.21	0	00:05
CB-9	3.07	263.00	0.18	0	00:05

- Inlet Total	Peak	Peak	Peak	Peak	Inlet	Total
ID Time	Flow	Lateral	Flow	Flow	Efficiency	Flooding
Flooded		Flow	Intercepted	Bypassing	during	
riooded	afa	cfs		Inlet cfs		acre-in
minutes	CIB	CIB	CIS	CIB	•	acic in
CB-1	1.04	1.04	0.86	0.18	83.12	0.000
CB-10	0.84	0.84	0.81	0.02	97.13	0.000
CB-11	0.74	0.74	0.73	0.01	98.00	0.000
CB-12	1.36	1.36	1.25	0.11	91.85	0.000
CB-13	1.48	1.48	-	_	-	0.000
CB-16	2.74	2.58	-	-	-	0.000
CB-17	1.40	1.40	1.09	0.31	77.60	0.000
0 CB-18	4.48	4.48	-	-	-	0.000
0 CB-2	1.76	1.76	1.55	0.21	88.28	0.000
0 CB-20	1.96	1.96	-	-	-	0.000
0 CB-3	1.07	1.07	1.01	0.06	94.80	0.000
0 CB-4	1.29	1.29	1.20	0.10	92.54	0.000
0 CB-5	2.25	2.24	-	_	-	0.000
0 CB-6	0.95	0.95	0.91	0.04	95.99	0.000
0 CB-7	0.71	0.68	0.69	0.01	98.34	0.000
0 CB-8W	1.25	1.23	1.03	0.23	81.85	0.000
0 CB-9	0.98	0.98	0.85	0.14	86.12	0.000
0						

\*\*\*\*\*\*\*

## Outfall Loading Summary

Outfall Node ID	Flow Frequency (%)	Average Flow cfs	Peak Inflow cfs
DP-1 DP-10 DP-13 DP-16 DP-18 DP-20 DP-5 DP-6 DP-7 OFFSITE1 OFFSITE-1	1.92 1.48 3.32 1.33 0.88 3.39 8.54 1.31 2.53 2.80 4.57	0.41 0.43 0.80 1.04 1.76 1.93 0.70 0.25 0.40 0.04	0.86 1.30 1.92 3.70 4.43 3.92 4.63 0.90 2.40 0.13 1.27
System	2.91	8.22	19.80

Link ID	Element	Т	ime of	Maximum	Length	Peak Flow	Design	Ratio of
Ratio of To	tal Reported	D		77-7		a	<b>7</b> 1.	36 - 3
Maximum Ti	Type me Condition	Pea.	K LTOM	velocity	Factor	during	F.TOM.	Maximum
raximam 11	me condicion	0ccu:	rrence	Attained		Analysis	Capacity	/Design
Flow Surcharged						-		
		days	hh:mm	ft/sec		cfs	cfs	Flow
Depth minutes	1							
CB-1_Overflow		0	00:16	1.96	1.00	0.13	2.70	0.05
0.31 0								
CB10-9_Gutter		0	00:07	2.31	1.00	0.02	8.35	0.00
0.09 0		0	00.00	1 70	1 00	0.00	7.05	0.00
CB11-10_Gutter 0.08 0	Calculated	0	00:09	1.78	1.00	0.02	7.95	0.00
CB12-13_Gutter		0	00:22	2.30	1.00	0.11	9.44	0.01
	Calculated	O	00.22	2.50	1.00	0.11	J. 11	0.01
CB17-16_Gutter		0	00:06	6.40	1.00	0.26	12.30	0.02
	Calculated							
CB2-3_Gutter	CHANNEL	0	00:06	5.43	1.00	0.17	13.13	0.01
0.19 0	Calculated							
CB3-4_Gutter		0	00:57	1.63	1.00	0.06	11.64	0.00
0.13 0								
CB4-5_Gutter		0	00:06	3.40	1.00	0.06	8.25	0.01
0.15 0 CB6-5 Gutter	Calculated CHANNEL	0	00:07	2.53	1.00	0.03	7.73	0.00
0.11 0		U	00.07	2.53	1.00	0.03	1.13	0.00
	CHANNEL	0	00:07	1.56	1.00	0.01	6.62	0.00
0.09 0		Ü	00.07	1.50	1.00	0.01	0.02	0.00
CB8-7_Gutter		0	00:08	2.40	1.00	0.16	4.89	0.03
0.26 0								
CB9-8_Gutter		0	00:07	2.84	1.00	0.10	6.26	0.02
0.20 0								
L-Pipe - (50)	CHANNEL	0	00:25	8.77	1.00	1.27	41.01	0.03

0.28	0	Calculated							
Pipe - (12)		CONDUIT	0	00:05	5.63	1.00	0.90	6.19	0.15
0.26	0	Calculated	0	00.05	2 50	1 00	0.00	2 10	0.00
Pipe - (13) 0.36	0	CONDUIT Calculated	0	00:05	3.50	1.00	0.90	3.19	0.28
Pipe - (14)		CONDUIT	0	00:05	6.74	1.00	2.24	5.59	0.40
0.44	0	Calculated	0	00.56	6 88	1 00	1 01		0 10
Pipe - (16) 0.24	0	CONDUIT Calculated	0	00:56	6.77	1.00	1.01	7.67	0.13
Pipe - (18)	Ū	CONDUIT	0	00:05	3.50	1.00	0.68	3.56	0.19
0.30	0	Calculated	0	00.05	4 00	1 00	0.60	4 00	0.16
Pipe - (19) 0.27	0	CONDUIT Calculated	0	00:05	4.00	1.00	0.68	4.29	0.16
Pipe - (2)		CONDUIT	0	00:05	12.72	1.00	1.51	7.69	0.20
0.30	0	Calculated	0	00:00	0.00	1 00	0.00	2.79	0.00
Pipe - (20) 0.00	0	CONDUIT Calculated	0	00.00	0.00	1.00	0.00	2.79	0.00
Pipe - (21)		CONDUIT	0	00:06	4.63	1.00	1.75	3.59	0.49
0.49 Pipe - (22)	0	Calculated CONDUIT	0	00:06	4.87	1.00	2.40	3.56	0.67
0.60	0	Calculated	U	00.00	4.07	1.00	2.40	3.50	0.07
Pipe - (23)		CONDUIT	0	00:05	5.96	1.00	1.02	6.40	0.16
0.27 Pipe - (24)	0	Calculated CONDUIT	0	00:05	3.59	1.00	0.84	3.40	0.25
0.34	0	Calculated	O	00.03	3.35	1.00	0.01	3.10	0.23
Pipe - (25)		CONDUIT	0	00:05	4.89	1.00	0.81	3.88	0.21
0.31 Pipe - (26)	0	Calculated CONDUIT	0	00:05	2.85	1.00	0.80	2.52	0.32
0.39	0	Calculated	ŭ	00 00	2.00	2.00	0.00	2.32	0.52
Pipe - (27)	0	CONDUIT Calculated	0	00:05	2.85	1.00	0.80	2.52	0.32
0.39 Pipe - (28)	0	Calculated	0	00:06	6.36	1.00	0.72	8.05	0.09
0.20	0	Calculated							
Pipe - (29) 0.26	0	CONDUIT Calculated	0	00:07	6.22	1.00	0.70	4.83	0.15
Pipe - (3)	U	CONDUIT	0	00:06	6.92	1.00	1.73	6.35	0.27
0.36	0	Calculated	_						
Pipe - (30) 0.41	0	CONDUIT Calculated	0	00:20	4.13	1.00	1.25	3.56	0.35
Pipe - (31)	O	CONDUIT	0	00:20	5.99	1.00	1.24	5.52	0.22
0.32	0	Calculated	0	00.05	4 63	1 00	1 00	2.56	0.54
Pipe - (33) 0.52	0	CONDUIT Calculated	0	00:07	4.63	1.00	1.92	3.56	0.54
Pipe - (34)		CONDUIT	0	00:07	3.36	1.00	1.48	2.54	0.58
0.55 Pipe - (35)	0	Calculated CONDUIT	0	00:07	4.49	1.00	1.48	3.73	0.40
0.44	0	Calculated	U	00.07	4.49	1.00	1.40	3.73	0.40
Pipe - (4)		CONDUIT	0	00:06	6.12	1.00	2.73	4.45	0.61
0.56 Pipe - (40)	0	Calculated CONDUIT	0	00:05	10.58	1.00	1.06	6.43	0.16
0.27	0	Calculated							
Pipe - (41)	0	CONDUIT	0	00:05	5.27	1.00	3.70	3.56	1.04
0.93 Pipe - (43)	0	> CAPACITY CONDUIT	0	00:05	6.28	1.00	2.74	4.77	0.57
0.54	0	Calculated							
Pipe - (44) 0.67	0	CONDUIT Calculated	0	00:05	7.97	1.00	4.46	5.63	0.79
Pipe - (45)	0	CONDUIT	0	00:05	7.38	1.00	4.43	14.86	0.30
0.37	0	Calculated	_						
Pipe - (5) 0.59	0	CONDUIT Calculated	0	00:05	9.53	1.00	4.63	7.00	0.66
Pipe - (50)	J	CONDUIT	0	00:24	11.76	1.00	3.92	30.06	0.13
0.24	0	Calculated	0	00.04	10.00	1 00	2.00	10 15	0.20
Pipe - (51) 0.43	0	CONDUIT Calculated	0	00:24	12.09	1.00	3.92	10.15	0.39
Pipe - (54)		CONDUIT	0	00:05	6.87	1.00	0.90	8.20	0.11

0.22	0	Calculated							
Pipe - (55)		CONDUIT	0	00:05	9.83	1.00	1.19	12.12	0.10
0.21	0	Calculated							
Pipe - (56)		CONDUIT	0	00:05	6.22	1.00	1.30	6.17	0.21
0.31	0	Calculated							
Pipe - (57)		CONDUIT	0	00:24	10.63	1.00	3.92	26.08	0.15
0.26	0	Calculated							
Pipe - (61)		CONDUIT	0	00:12	6.07	1.00	0.86	5.92	0.15
0.26	0	Calculated							
Pipe - (62)		CONDUIT	0	00:12	3.74	1.00	0.86	3.56	0.24
0.33	0	Calculated							
Pipe - (7)		CONDUIT	0	00:05	7.53	1.00	1.74	7.14	0.24
0.34	0	Calculated							

All links are stable.

WARNING 108: Surcharge elevation defined for Junction EX-18 is below junction maximum elevation. Assumed surcharge elevation equal to maximum elevation.

WARNING 139 : Ponded area defined for on sag Inlet CB-18 is zero. Assumed ponded area equal to 10 ft $^2$  (0.929 m $^2$ ).

WARNING 138: Initial water surface elevation defined for Inlet CB-20 is below catchbasin invert elevation.

Assumed initial water surface elevation equal to catchbasin inlet invert

elevation.

WARNING 138: Initial water surface elevation defined for Inlet CB-4 is below catchbasin invert elevation.

Assumed initial water surface elevation equal to catchbasin inlet invert

elevation.

WARNING 138: Initial water surface elevation defined for Inlet CB-5 is below catchbasin invert elevation.

Assumed initial water surface elevation equal to catchbasin inlet invert

elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB-1\_Overflow is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB10-9\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB11-10\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB12-13\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB17-16\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB2-3\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB3-4\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB4-5\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB6-5\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB7-6\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB8-7\_Gutter is below the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB9-8\_Gutter is below the storm drain inlet rim elevation.

WARNING 117 : Conduit outlet invert elevation defined for Conduit CB-1\_Overflow is below downstream node invert elevation.

Assumed conduit outlet invert elevation equal to downstream node invert

elevation.

WARNING 004 : Minimum elevation drop used for Conduit CB-1\_Overflow.

WARNING 005: Minimum slope used for Conduit CB-1\_Overflow.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB10-9\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-9.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB11-10\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-10.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB12-13\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-13.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB17-16\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-16.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB2-3\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-3.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB3-4\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-4.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB4-5\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-5.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB6-5\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-5.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB7-6\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-6.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB8-7\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-7.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB9-8\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-8W.

WARNING 116 : Conduit inlet invert elevation defined for Conduit Pipe - (14) is below upstream node invert elevation.

Assumed conduit inlet invert elevation equal to upstream node invert elevation. WARNING 116: Conduit inlet invert elevation defined for Conduit Pipe - (50) is below upstream node invert elevation.

Assumed conduit inlet invert elevation equal to upstream node invert elevation. WARNING 116: Conduit inlet invert elevation defined for Conduit Pipe - (55) is below upstream node invert elevation.

Assumed conduit inlet invert elevation equal to upstream node invert elevation.

Analysis began on: Tue Jan 31 11:11:19 2023 Analysis ended on: Tue Jan 31 11:11:22 2023

Total elapsed time: 00:00:03

```
Autodesk® Storm and Sanitary Analysis 2016 - Version 13.2.165 (Build 0)
Project Description
******
File Name ..... Grove_St_Ph2_r1-PR.SPF
******
Analysis Options
******
Flow Units ..... cfs
Subbasin Hydrograph Method. Rational
Time of Concentration..... SCS TR-55
Return Period..... 100 years
Link Routing Method ...... Kinematic Wave Storage Node Exfiltration. None
Starting Date ..... DEC-20-2022 00:00:00
Ending Date ..... DEC-21-2022 00:00:00 Report Time Step ..... 00:00:10
******
Element Count
Number of subbasins ..... 17
Number of nodes ..... 50
Number of links ..... 52
******
Subbasin Summary
******
Subbasin
                      Total
                        Area
TD
                       acres
Sub-CB-1
                    0.36
0.13
0.20
1.28
0.34
0.40
0.29
Sub-CB-10
Sub-CB-11
Sub-CB-12
Sub-CB-12
Sub-CB-13-14
Sub-CB-15-16
Sub-CB-17
Sub-CB-18-19
                       0.95
Sub-CB-2
                        0.40
                        1.49
Sub-CB-20
Sub-CB-3
                        2.84
Sub-CB-4
                        0.34
                        0.33
Sub-CB-5
Sub-CB-6
                        0.14
Sub-CB-7
                        0.11
Sub-CB-8W
                        0.22
Sub-CB-9
                        0.15
*****
Node Summary
                  Element Invert Maximum Ponded External Type Elevation Elev. Area Inflow ft ft ft
Node
TD
```

257.54 259.20 0.00

JUNCTION

CB-8E

CIT-8 CIT-9 DH-10 DH-13		JUNCTION JUNCTION JUNCTION JUNCTION		259.42 40 262.67 L5 268.15 30 265.60	0.00 0.00 0.00 0.00		
DH-20		JUNCTION		52 280.21	0.00		
DH-6		JUNCTION	246.	95 255.72	0.00		
DMH-10		JUNCTION		32 267.86	0.00		
DMH-11		JUNCTION		75 272.24	0.00		
DMH-12		JUNCTION		70 271.08	0.00		
DMH-13		JUNCTION	262.	77 265.40 55 280.22	0.00		
DMH-20		JUNCTION	277.	55 280.22	0.00		
DMH-3		JUNCTION	262.	24 265.34 35 255.95	0.00		
DMH-4N		JUNCTION			0.00		
DMH-4S		JUNCTION	257.	13 262.56	0.00		
DMH-6		JUNCTION		257.58	0.00		
DMH-7		JUNCTION		10 258.76	0.00		
EX-18		JUNCTION		273.24	0.00		
EX-7	(72)	JUNCTION		30 258.62	0.00		
Structure STU-16	- (72)	JUNCTION JUNCTION	273.	79 277.57 70 255.49	0.00		
STU-5		JUNCTION	248	53 251 88	0.00		
DP-1		OUTFALL	275	53 251.88 00 276.00	0.00		
DP-10		OUTFALL		78 265.78	0.00		
DP-13		OUTFALL		260.60	0.00		
DP-16		OUTFALL		56 253.66	0.00		
DP-18		OUTFALL			0.00		
DP-20		OUTFALL	274.	36 265.86 20 275.70	0.00		
DP-5		OUTFALL	248.	00 249.00	0.00		
DP-6		OUTFALL	246.	249.00 247.50	0.00		
DP-7		OUTFALL	252.	50 253.60	0.00		
OFFSITE1		OUTFALL	281.	22 281.50	0.00		
OFFSITE-1		OUTFALL	267.	58 268.43	0.00		
*********  Inlet Summ  *******  Inlet  Catchbasin	nary :***	Inlet	Initial	Manufacturer Grate		Inlet	Number
Inlet Summ *******  Inlet  Catchbasin	nary :***	Let Ponded		Grate			
Inlet Summ ******* Inlet	nary **** Inl	let Ponded Manufacture	<u> </u>	Grate Part		Inlet Location	Number of
Inlet Summ ******* Inlet Catchbasin ID	nary **** Inl	Let Ponded	<u> </u>	Grate Part			
Inlet Summ ******* Inlet Catchbasin ID	nary **** Inl Rim	let Ponded Manufacture: Area	<u> </u>	Grate Part Logging Number			of
Inlet Summ ******* Inlet Catchbasin ID Invert Elevation	nary *** Inl Rim Elevatio	let Ponded Manufacture Area on	Water C	Grate Part Logging Number Factor			of
Inlet Summ ******* Inlet Catchbasin ID Invert Elevation	nary **** Inl Rim	let Ponded Manufacture Area on	. Water C	Grate Part Logging Number			of
Inlet Summ ******* Inlet Catchbasin ID Invert Elevation	nary *** Inl Rim Elevatio	let Ponded Manufacture Area on	Water C	Grate Part Logging Number Factor			of
Inlet Summ  *******  Inlet Catchbasin  ID Invert  Elevation  ft	nary ***  Inl Rim Elevation	let Ponded Manufacturen Area on ft²	Water C Elevation ft	Grate Part Logging Number Factor			of
Inlet Summ  *******  Inlet Catchbasin  ID Invert  Elevation  ft	nary ***  Inl Rim Elevation	let Ponded Manufacturer Area on ft²	Water C Elevation ft	Grate Part Logging Number Factor		Location	of Inlets
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft	Rim Elevation	let Ponded Manufacturer Area on ft² FHWA HEC-22	Water C Elevation ft GENERIC	Grate Part Logging Number Factor %			of
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10	Tary  This is a second of the control of the contro	let Ponded Manufacturer Area on ft² FHWA HEC-22	Water C Elevation ft  GENERIC 278.10	Grate Part Logging Number Factor  % N/A 0.00		Location On Grade	of Inlets
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10 CB-10	Rim Elevation ft 281.22	let Ponded Manufactures Area on ft² FHWA HEC-22 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC	Grate Part logging Number Factor  % N/A 0.00 N/A		Location	of Inlets
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10	Rim Elevation ft 281.22	Let Ponded Manufactures Area on ft² FHWA HEC-22 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44	Grate Part Logging Number Factor  % N/A 0.00		Location On Grade	of Inlets
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft	Rim Elevation ft 281.22	let Ponded Manufactures Area on ft² FHWA HEC-22 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44	Grate Part logging Number Factor  % N/A 0.00 N/A 0.00		Location  On Grade  On Grade	of Inlets  1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10 CB-10 265.44 CB-11	Inl Rim Elevation ft 281.22 267.69 272.10	Let Ponded Manufactures Area on ft² FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22	Water C. Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10	Grate Part Logging Number Factor		Location  On Grade  On Grade	of Inlets  1 1 1
Inlet Summ  ******* Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10 CB-10 265.44 CB-11 269.10	Inl Rim Elevation ft 281.22 267.69	let Ponded Manufacturer Area on ft² FHWA HEC-22 FHWA HEC-22 FHWA HEC-22	Water C. Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10	Grate Part Logging Number Factor		Location  On Grade  On Grade  On Grade	of Inlets  1 1 1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10 CB-10 265.44 CB-11 269.10 CB-12	Elevation ft 281.22 267.69 272.10 271.07	let Ponded Manufacturer Area on ft² FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 269.10 GENERIC 268.07	Grate Part Logging Number Factor  % N/A 0.00 N/A 0.00 N/A 0.00 N/A		Location  On Grade  On Grade  On Grade	of Inlets  1 1 1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft	Inl Rim Elevation ft 281.22 267.69 272.10	let Ponded Manufacturen Area on ft² FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 269.10 GENERIC 268.07	Grate Part Logging Number Factor  % N/A 0.00 N/A 0.00 N/A 0.00 N/A 0.00 N/A 0.00		On Grade On Grade On Grade On Grade	of Inlets  1 1 1
Inlet Summ ******* Inlet Catchbasin ID Invert Elevation ft	Rim Elevation ft 281.22 267.69 272.10 271.07	Let Ponded Manufactures Area  on  ft²  FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 10.00 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 268.07 GENERIC 268.07 GENERIC 262.90 GENERIC	Grate Part Logging Number Factor  % N/A 0.00 N/A		On Grade On Grade On Grade On Grade	of Inlets  1 1 1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10 CB-10 265.44 CB-11 269.10 CB-12 268.07 CB-13 262.90 CB-16 252.93	Elevation ft 281.22 267.69 272.10 271.07	Let Ponded Manufactures Area on ft² FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 10.00 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 268.07 GENERIC 262.90 GENERIC 252.93	Grate Part Logging Number Factor		On Grade On Grade On Grade On Grade On Grade On Sag On Sag	of Inlets  1 1 1 1 1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft  CB-1 278.10 CB-10 265.44 CB-11 269.10 CB-12 268.07 CB-13 262.90 CB-16 252.93 CB-17	Rim Elevation ft  281.22 267.69 272.10 271.07 264.85 254.93	Let Ponded Manufactures Area on ft² FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 10.00 FHWA HEC-22 10.00 FHWA HEC-22	Water C. Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 268.07 GENERIC 262.90 GENERIC 252.93 GENERIC	Grate Part Logging Number Factor		On Grade On Grade On Grade On Grade On Grade	of Inlets  1 1 1 1 1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft	Rim Elevation ft 281.22 267.69 272.10 271.07	Let Ponded Manufactures Area  on  ft²  FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 10.00 FHWA HEC-22 10.00 FHWA HEC-22	Water C. Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 268.07 GENERIC 268.07 GENERIC 252.93 GENERIC 260.16	Grate Part Logging Number Factor  % N/A 0.00 N/A		On Grade On Grade On Grade On Grade On Sag On Sag On Grade	of Inlets  1 1 1 1 1 1 1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft	Elevation ft 281.22 267.69 272.10 271.07 264.85 254.93 265.49	Let Ponded Manufactures Area  on  ft²  FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 10.00 FHWA HEC-22 10.00 FHWA HEC-22 10.00 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 269.10 GENERIC 262.90 GENERIC 252.93 GENERIC 260.16 GENERIC	Grate Part Logging Number Factor  % N/A 0.00 N/A		On Grade On Grade On Grade On Grade On Grade On Sag On Sag	of Inlets  1 1 1 1 1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft	Rim Elevation ft  281.22 267.69 272.10 271.07 264.85 254.93	Let Ponded Manufactures Area  on  ft²  FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 10.00 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 268.07 GENERIC 262.90 GENERIC 252.93 GENERIC 250.16 GENERIC 260.16 GENERIC 269.61	Grate Part Logging Number Factor		On Grade On Grade On Grade On Grade On Sag On Sag On Grade On Sag	of Inlets  1 1 1 1 1 1 1 1
Inlet Summ ******** Inlet Catchbasin ID Invert Elevation ft	Elevation ft 281.22 267.69 272.10 271.07 264.85 254.93 265.49	Let Ponded Manufactures Area  on  ft²  FHWA HEC-22 FHWA HEC-22 FHWA HEC-22 10.00 FHWA HEC-22 10.00 FHWA HEC-22 10.00 FHWA HEC-22 FHWA HEC-22 FHWA HEC-22	Water C Elevation ft  GENERIC 278.10 GENERIC 265.44 GENERIC 269.10 GENERIC 268.07 GENERIC 262.90 GENERIC 252.93 GENERIC 250.16 GENERIC 260.16 GENERIC 269.61	Grate Part Logging Number Factor  % N/A 0.00 N/A		On Grade On Grade On Grade On Grade On Sag On Sag On Grade	of Inlets  1 1 1 1 1 1 1 1

CB-20		FHWA	HEC-22	GENERIC	N/A		Or	ı Sag	1	
278.18	279.	67 10.	00	278.18	0.00					
CB-3			HEC-22	GENERIC	N/A		Or	n Grade	1	
262.89	265.	39	-	262.89	0.00					
CB-4		FHWA	HEC-22	GENERIC	N/A		Or	n Grade	1	
254.18	255.	93	-	254.18	0.00					
CB-5		FHWA	HEC-22	GENERIC	N/A		Or	n Sag	1	
249.44	251.	18 10.	00	249.44	0.00					
CB-6		FHWA	HEC-22	GENERIC	N/A		Or	n Grade	1	
252.35	255.	35	-	252.35	0.00					
CB-7		FHWA	HEC-22	GENERIC	N/A		Or	ı Grade	1	
255.41	258.	41	-	255.41	0.00					
CB-8W		FHWA	HEC-22	GENERIC	N/A		Or	ı Grade	1	
257.08	260.	08	-	257.08	0.00					
CB-9		FHWA	HEC-22	GENERIC	N/A		Or	ı Grade	1	
259.82	262.	82	-	259.82	0.00					
*****	*****	*****	*							
		ter Summar								
				Doodsso	Dood	C11++0	C11++ 0	_	111++02	
Inlet ID			Roadwa: tudina		_	Gutter Cross	Gutter Width		utter ssion	
ID		rongr	Slope		_	Slope	WIGCII	рерге	SSIOII	
			ft/f		Rougilliess	ft/ft	ft		in	
			IL/I	L IL/IL					111	
CB-1			0.010	0 0.0200	0.0160	0.0620	2.00		2.00	
CB-10			0.020		0.0130	0.0620	2.00		0.00	
CB-11			0.020		0.0130	0.0620	2.00		0.00	
CB-11			0.020		0.0130	0.0620	2.00		0.00	
CB-12				- 0.0500	0.0130	0.0620	2.00		0.00	
CB-15				- 0.0500	0.0130	0.0620	2.00		0.00	
CB-17			0.010		0.0160	0.0620	2.00		2.00	
CB-17			0.010		0.0160	0.0620	2.00		2.00	
			0 020	- 0.0200						
CB-2			0.020		0.0130	0.0620	2.00		0.00	
CB-20			0 000	- 0.0500	0.0130	0.0620	2.00		0.00	
CB-3			0.020		0.0130	0.0620	2.00		0.00	
CB-4			0.020		0.0130	0.0620	2.00		0.00	
CB-5				- 0.0500	0.0130	0.0620	2.00		0.00	
CB-6			0.020		0.0130	0.0620	2.00		0.00	
CB-7			0.020			0.0620	2.00		0.00	
CB-8W			0.010		0.0130	0.0620	2.00		2.00	
CB-9			0.020	0.0500	0.0130	0.0620	2.00		0.00	
*****	***									
Link Sum										
Link		From Node		To Node	Element	т	ona+h	Clana	Manning's	~
ID		FIOIII NOGE	:	10 Node	Element Type	ь	ength ft	Slope %	Roughnes	
								·•		_
CB-1_Ove	rflow	CB-1		OFFSITE1	CHANNEL		241.8	0.2000	0.013	0
CB10-9_G		CB-10		CB-9	CHANNEL		254.5	1.9133	0.013	
CB11-10_		CB-11		CB-10	CHANNEL		254.5	1.7326	0.013	
CB12-13		CB-12		CB-13	CHANNEL		254.5	2.4437	0.013	
CB17-16_		CB-17		CB-16	CHANNEL		254.5	4.1501	0.013	
CB2-3 Gu		CB-2		CB-3	CHANNEL		241.8	4.7276	0.013	
CB2-3_Gu CB3-4 Gu		CB-3		CB-4	CHANNEL		254.5	3.7167	0.013	
CB4-5_Gu		CB-4		CB-5	CHANNEL		254.5	1.8662	0.013	
CB6-5_Gu		CB-4 CB-6		CB-5	CHANNEL		254.5	1.6383	0.013	
_									0.013	
CB7-6_Gu		CB-7		CB-6	CHANNEL		254.5	1.2022		
CB8-7_Gu		CB-8W		CB-7	CHANNEL		254.5	0.6561	0.013	
CB9-8_Gu		CB-9		CB-8W	CHANNEL		254.5	1.0765	0.013	
L-Pipe -		CB-20		OFFSITE-1	CHANNEL		546.0	2.1967	0.013	
Pipe - (		DMH-6		DH-6	CONDUIT		13.3	3.0144	0.013	
Pipe - (	13)	CB-6		DMH-6	CONDUIT		12.5	0.7995	0.013	0

Pipe - (14)	CB-5	STU-5	CONDUIT	28.8	2.4635	0.0130
Pipe - (16)	CB-3	DMH-3	CONDUIT	11.9	4.6382	0.0130
Pipe - (18)	CB-7	DMH-7	CONDUIT	20.7	1.0000	0.0130
<u> </u>						
Pipe - (19)	DMH-7	EX-7	CONDUIT	6.9	1.4505	0.0130
Pipe - (2)	CB-2	DMH-3	CONDUIT	246.6	4.6555	0.0130
Pipe - (20)	CB-8E	CIT-8	CONDUIT	7.6	0.6131	0.0130
Pipe - (21)	CIT-8	EX-7	CONDUIT	196.9	1.0156	0.0130
Pipe - (22)	EX-7	DP-7	CONDUIT	20.0	1.0000	0.0130
Pipe - (23)	CB-8W	CIT-8	CONDUIT	20.5	3.2241	0.0130
Pipe - (24)	CB-9	CIT-9	CONDUIT	16.5	0.9092	0.0130
Pipe - (25)	CIT-9	CIT-8	CONDUIT	219.0	1.1872	0.0130
Pipe - (26)	DMH-10	DH-10	CONDUIT	14.0	0.5000	0.0130
Pipe - (27)	CB-10	DMH-10	CONDUIT	4.2	0.5000	0.0130
Pipe - (28)	CB-11	DMH-11	CONDUIT	4.9	5.1092	0.0130
Pipe - (29)	DMH-11	DH-10	CONDUIT	190.5	1.8369	0.0130
Pipe - (3)	DMH-4S	DMH-4N	CONDUIT	131.6	3.1757	0.0130
Pipe - (30)	CB-12	DMH-12	CONDUIT	3.6	1.0000	0.0130
Pipe - (31)	DMH-12	DH-13	CONDUIT	217.3	2.4045	0.0130
Pipe - (33)	DH-13	DP-13	CONDUIT	19.5	1.0000	0.0130
Pipe - (34)	CB-13	DMH-13	CONDUIT	5.9	0.5098	0.0130
Pipe - (35)	DMH-13	DH-13	CONDUIT	19.9	1.0989	0.0130
Pipe - (4)	DMH-4N	STU-5	CONDUIT	263.5	1.5634	0.0130
Pipe - (40)	CB-17	STU-16	CONDUIT	220.1	3.2621	0.0130
				4.1	1.0000	
Pipe - (41)	STU-16	DP-16	CONDUIT			0.0130
Pipe - (43)	CB-16	STU-16	CONDUIT	7.3	1.7930	0.0130
Pipe - (44)	CB-18	EX-18	CONDUIT	24.4	2.4990	0.0130
Pipe - (45)	EX-18	DP-18	CONDUIT	81.8	2.0000	0.0130
Pipe - (5)	STU-5	DP-5	CONDUIT	16.3	3.8608	0.0130
Pipe - (50)	CB-20	DMH-20	CONDUIT	6.5	8.1871	0.0130
Pipe - (51)	DMH-20	DH-20	CONDUIT	5.7	8.1142	0.0130
Pipe - (54)	DH-6	DP-6	CONDUIT	8.5	5.3000	0.0130
Pipe - (55)	CB-4	DMH-4N	CONDUIT	10.6	11.5699	0.0130
Pipe - (56)	DH-10	DP-10	CONDUIT	12.4	3.0000	0.0130
Pipe - (57)	DH-20	DP-20	CONDUIT	55.5	6.1646	0.0130
Pipe - (61)	CB-1	Structure -	(72)CONDUIT	79.8	2.7583	0.0130
Pipe - (62)	<u></u>					
FIDE - (07)	Structure -	(72)DP-1	CONDUIT	79.0	1.0000	0.0130
Pipe - (62) Pipe - (7)	Structure - DMH-3	(72)DP-1 DMH-4S	CONDUIT CONDUIT	79.0 124.6	1.0000 4.0212	0.0130 0.0130
Pipe - (7)	DMH-3					
	DMH-3					
Pipe - (7)  ***********************************	DMH-3 ***** ummary					
Pipe - (7)	DMH-3 ***** ummary					
Pipe - (7)  ***********************************	DMH-3 ***** ummary					
Pipe - (7)  ******************  Cross Section S ************************************	DMH-3  ***** ummary *****	DMH-4S	CONDUIT	124.6	4.0212	0.0130
Pipe - (7)  *************  Cross Section S  *************  Link	DMH-3  ***** ummary *****	DMH-4S	CONDUIT	124.6	4.0212	0.0130
Pipe - (7)  *************  Cross Section S  ***********  Link  Design	DMH-3  ***** ummary *****	DMH-4S Depth/	CONDUIT	124.6 No. of	4.0212 Cross	0.0130
Pipe - (7)  *********  Cross Section S  ********  Link  Design  ID	DMH-3  ***** ummary *****	DMH-4S Depth/	CONDUIT	124.6 No. of	4.0212 Cross	0.0130
Pipe - (7)  *********  Cross Section S  ********  Link  Design  ID	DMH-3  ***** ummary *****	DMH-4S Depth/	CONDUIT	124.6 No. of	4.0212 Cross Sectional	0.0130  Full Flow  Hydraulic
Pipe - (7)  *********  Cross Section S  *********  Link  Design  ID  Flow	DMH-3  ***** ummary *****	DMH-4S Depth/	CONDUIT	124.6 No. of	4.0212 Cross Sectional	0.0130  Full Flow  Hydraulic
Pipe - (7)  *********  Cross Section S  *********  Link  Design  ID  Flow	DMH-3  ***** ummary *****	DMH-4S  Depth/ Diameter	CONDUIT Width	124.6 No. of	4.0212  Cross Sectional Area	0.0130  Full Flow  Hydraulic  Radius
Pipe - (7)  **********  Cross Section S  *******  Link  Design  ID  Flow  Capacity	DMH-3  ***** ummary *****	DMH-4S  Depth/ Diameter	CONDUIT Width	124.6 No. of	4.0212  Cross Sectional Area	0.0130  Full Flow  Hydraulic  Radius
Pipe - (7)  ***********  Cross Section S  *******  Link  Design  ID  Flow  Capacity  cfs	DMH-3  *****  ummary  *****  Shape	DMH-4S  Depth/ Diameter	CONDUIT Width ft	No. of	4.0212  Cross Sectional  Area  ft²	0.0130  Full Flow  Hydraulic  Radius  ft
Pipe - (7)  **********  Cross Section S  *******  Link  Design  ID  Flow  Capacity  cfs	DMH-3  *****  ummary  *****  Shape	DMH-4S  Depth/ Diameter  ft	CONDUIT  Width  ft	No. of Barrels	4.0212  Cross Sectional  Area  ft²	0.0130  Full Flow  Hydraulic  Radius  ft
Pipe - (7)  ***********  Cross Section S *******  Link  Design  ID  Flow  Capacity  cfs   CB-1_Overflow	DMH-3  *****  ummary  *****  Shape	DMH-4S  Depth/ Diameter  ft	CONDUIT Width ft	No. of	4.0212  Cross Sectional  Area  ft²	0.0130  Full Flow  Hydraulic  Radius  ft
Pipe - (7)  ***********  Cross Section S *******  Link  Design ID  Flow  Capacity  cfs   CB-1_Overflow 2.70	DMH-3  ***** ummary  ***** Shape  TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28	CONDUIT  Width  ft  14.00	No. of Barrels	Cross Sectional Area ft²	0.0130  Full Flow Hydraulic Radius ft
Pipe - (7)  ***********  Cross Section S  *******  Link  Design  ID  Flow  Capacity  cfs   CB-1_Overflow  2.70  CB10-9_Gutter	DMH-3  ***** ummary  ***** Shape  TRIANGULAR	DMH-4S  Depth/ Diameter  ft	CONDUIT  Width  ft	No. of Barrels	4.0212  Cross Sectional  Area  ft²	0.0130  Full Flow  Hydraulic  Radius  ft
Pipe - (7)  ************* Cross Section S ******** Link Design ID Flow Capacity cfs CB-1_Overflow 2.70 CB10-9_Gutter 8.35	DMH-3  ***** ummary ***** Shape  TRIANGULAR TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28 0.28	CONDUIT  Width  ft  14.00  14.00	No. of Barrels	Cross Sectional Area ft²  1.96 1.96	0.0130  Full Flow Hydraulic Radius ft  0.14 0.14
Pipe - (7)  ************* Cross Section S ******** Link Design ID Flow Capacity cfs  CB-1_Overflow 2.70 CB10-9_Gutter 8.35 CB11-10_Gutter	TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28	CONDUIT  Width  ft  14.00	No. of Barrels	Cross Sectional Area ft²	0.0130  Full Flow Hydraulic Radius ft
Pipe - (7)  ************* Cross Section S ******** Link Design ID Flow Capacity cfs  CB-1_Overflow 2.70 CB10-9_Gutter 8.35 CB11-10_Gutter 7.95	DMH-3  ***** ummary ***** Shape  TRIANGULAR TRIANGULAR TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28  0.28  0.28	CONDUIT  Width  ft  14.00 14.00 14.00	No. of Barrels  1 1 1	Cross Sectional Area ft²  1.96 1.96	0.0130  Full Flow Hydraulic Radius ft  0.14 0.14 0.14
Pipe - (7)  ************  Cross Section S *******  Link  Design  ID  Flow  Capacity  cfs   CB-1_Overflow  2.70  CB10-9_Gutter  8.35  CB11-10_Gutter  7.95  CB12-13_Gutter	DMH-3  ***** ummary ***** Shape  TRIANGULAR TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28 0.28	CONDUIT  Width  ft  14.00  14.00	No. of Barrels	Cross Sectional Area ft²  1.96 1.96	0.0130  Full Flow Hydraulic Radius ft  0.14 0.14
Pipe - (7)  ***********  Cross Section S *******  Link  Design ID  Flow  Capacity  cfs   CB-1_Overflow  2.70  CB10-9_Gutter  8.35  CB11-10_Gutter  7.95  CB12-13_Gutter  9.44	*****  wmmary  ***** Shape  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28 0.28 0.28 0.28	ft  14.00 14.00 14.00 14.00	No. of Barrels  1 1 1 1	4.0212  Cross Sectional Area ft²  1.96 1.96 1.96 1.96	Full Flow Hydraulic Radius ft  0.14 0.14 0.14 0.14
Pipe - (7)  ************  Cross Section S *******  Link  Design ID Flow  Capacity  cfs   CB-1_Overflow  2.70  CB10-9_Gutter  7.95  CB12-13_Gutter  9.44  CB17-16_Gutter	DMH-3  ***** ummary ***** Shape  TRIANGULAR TRIANGULAR TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28  0.28  0.28	CONDUIT  Width  ft  14.00 14.00 14.00	No. of Barrels  1 1 1	Cross Sectional Area ft²  1.96 1.96	0.0130  Full Flow Hydraulic Radius ft  0.14 0.14 0.14
Pipe - (7)  **************  Cross Section S  ********  Link  Design  ID  Flow  Capacity  cfs   CB-1_Overflow  2.70  CB10-9_Gutter  8.35  CB11-10_Gutter  7.95  CB12-13_Gutter  9.44  CB17-16_Gutter  12.30	*****  wmmary  ***** Shape  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28 0.28 0.28 0.28 0.28	ft  14.00 14.00 14.00 14.00 14.00	No. of Barrels  1 1 1 1 1	4.0212  Cross Sectional Area ft²  1.96 1.96 1.96 1.96 1.96	0.0130  Full Flow Hydraulic Radius ft  0.14 0.14 0.14 0.14 0.14
Pipe - (7)  ************** Cross Section S ********* Link Design ID Flow  Capacity cfs  CB-1_Overflow 2.70 CB10-9_Gutter 8.35 CB11-10_Gutter 7.95 CB12-13_Gutter 9.44 CB17-16_Gutter 12.30 CB2-3_Gutter	*****  wmmary  ***** Shape  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28 0.28 0.28 0.28	ft  14.00 14.00 14.00 14.00	No. of Barrels  1 1 1 1	4.0212  Cross Sectional Area ft²  1.96 1.96 1.96 1.96	Full Flow Hydraulic Radius ft  0.14 0.14 0.14 0.14
Pipe - (7)  *************  Cross Section S  ********  Link  Design  ID  Flow  Capacity  cfs   CB-1_Overflow  2.70  CB10-9_Gutter  8.35  CB11-10_Gutter  7.95  CB12-13_Gutter  9.44  CB17-16_Gutter  12.30  CB2-3_Gutter  13.13	DMH-3  ***** ummary ***** Shape  TRIANGULAR TRIANGULAR TRIANGULAR TRIANGULAR TRIANGULAR TRIANGULAR TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28 0.28 0.28 0.28 0.28 0.28 0.28	ft  14.00 14.00 14.00 14.00 14.00 14.00	124.6  No. of Barrels  1 1 1 1 1 1	4.0212  Cross Sectional Area ft²  1.96 1.96 1.96 1.96 1.96 1.96	0.0130  Full Flow Hydraulic Radius ft  0.14 0.14 0.14 0.14 0.14 0.14
Pipe - (7)  ************** Cross Section S ********* Link Design ID Flow  Capacity cfs  CB-1_Overflow 2.70 CB10-9_Gutter 8.35 CB11-10_Gutter 7.95 CB12-13_Gutter 9.44 CB17-16_Gutter 12.30 CB2-3_Gutter	*****  wmmary  ***** Shape  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR  TRIANGULAR	DMH-4S  Depth/ Diameter  ft  0.28 0.28 0.28 0.28 0.28	ft  14.00 14.00 14.00 14.00 14.00	No. of Barrels  1 1 1 1 1	4.0212  Cross Sectional Area ft²  1.96 1.96 1.96 1.96 1.96	0.0130  Full Flow Hydraulic Radius ft  0.14 0.14 0.14 0.14 0.14

11 64						
11.64 CB4-5_Gutter	TRIANGULAR	0.28	14.00	1	1.96	0.14
8.25 CB6-5_Gutter	TRIANGULAR	0.28	14.00	1	1.96	0.14
7.73 CB7-6_Gutter	TRIANGULAR	0.28	14.00	1	1.96	0.14
6.62 CB8-7_Gutter	TRIANGULAR	0.28	14.00	1	1.96	0.14
4.89 CB9-8_Gutter	TRIANGULAR	0.28	14.00	1	1.96	0.14
6.26 L-Pipe - (50)	IRREGULAR	0.75	6.80	1	3.82	0.50
41.01 Pipe - (12)	CIRCULAR	1.00	1.00	1	0.79	0.25
6.19 Pipe - (13)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.19 Pipe - (14)	CIRCULAR	1.00	1.00	1	0.79	0.25
5.59 Pipe - (16)	CIRCULAR	1.00	1.00	1	0.79	0.25
7.67 Pipe - (18)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.56 Pipe - (19)	CIRCULAR	1.00	1.00	1	0.79	0.25
4.29 Pipe - (2)	CIRCULAR	1.00	1.00	1	0.79	0.25
7.69 Pipe - (20)	CIRCULAR	1.00	1.00	1	0.79	0.25
2.79 Pipe - (21)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.59 Pipe - (22)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.56 Pipe - (23)	CIRCULAR	1.00	1.00	1	0.79	0.25
6.40 Pipe - (24)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.40 Pipe - (25)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.88 Pipe - (26)	CIRCULAR	1.00	1.00	1	0.79	0.25
2.52 Pipe - (27)	CIRCULAR	1.00	1.00	1	0.79	0.25
2.52 Pipe - (28)	CIRCULAR	1.00	1.00	1	0.79	0.25
8.05 Pipe - (29)	CIRCULAR	1.00	1.00	1	0.79	0.25
4.83 Pipe - (3)	CIRCULAR	1.00	1.00	1	0.79	0.25
6.35 Pipe - (30)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.56 Pipe - (31)	CIRCULAR	1.00	1.00	1	0.79	0.25
5.52 Pipe - (33)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.56 Pipe - (34)	CIRCULAR	1.00	1.00	1	0.79	0.25
2.54 Pipe - (35)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.73 Pipe - (4)	CIRCULAR	1.00	1.00	1	0.79	0.25
4.45 Pipe - (40)	CIRCULAR	1.00	1.00	1	0.79	0.25
6.43 Pipe - (41)	CIRCULAR	1.00	1.00	1	0.79	0.25
3.56 Pipe - (43)	CIRCULAR	1.00	1.00	1	0.79	0.25

4 55								
4.77 Pipe - (44)	CIRC	ULAR	1.00	1.00		1	0.79	0.25
5.63 Pipe - (45)	CIRC	ULAR	1.50	1.50		1	1.77	0.38
14.86 Pipe - (5)	CIRC	ULAR	1.00	1.00		1	0.79	0.25
7.00 Pipe - (50)	CIRC	ULAR	1.50	1.50		1	1.77	0.38
30.06 Pipe - (51)	CIRC	ULAR	1.00	1.00		1	0.79	0.25
10.15 Pipe - (54)	CIRC	ULAR	1.00	1.00		1	0.79	0.25
8.20 Pipe - (55)	CIRC	ULAR	1.00	1.00		1	0.79	0.25
12.12 Pipe - (56)	CIRC	ULAR	1.00	1.00		1	0.79	0.25
6.17 Pipe - (57)	CIRC	ULAR	1.50	1.50		1	1.77	0.38
26.08 Pipe - (61)	CIRC	ULAR	1.00	1.00		1	0.79	0.25
5.92 Pipe - (62)	CIRC	ULAR	1.00	1.00		1	0.79	0.25
3.56 Pipe - (7)	CIRC	ULAR	1.00	1.00		1	0.79	0.25
7.14								
*******								
Transect Su								
Transect XS	G-L-Pipe -	(13)						
Area:	0 0005	0 0010	0.0043	0 0076	0 0110			
	0.0005 0.0170	0.0019 0.0232	0.0043 0.0305	0.0076 0.0390	0.0118 0.0487			
	0.0595	0.0715	0.0847	0.0990	0.1145			
	0.1312	0.1491	0.1682	0.1884	0.2098			
	0.2323 0.3604	0.2561 0.3871	0.2810 0.4137	0.3071 0.4404	0.3338 0.4670			
	0.4937	0.5203	0.5470	0.5736	0.6003			
	0.6269	0.6536	0.6802	0.7069	0.7335			
	0.7602 0.8934	0.7868 0.9201	0.8135 0.9467	0.8401 0.9734	0.8668 1.0000			
Hrad:	0.0551	0.5201	0.5107	0.5751	1.0000			
	0.0139	0.0278	0.0418	0.0557	0.0696			
	0.0835 0.1459	0.0963 0.1591	0.1080 0.1724	0.1202 0.1858	0.1329 0.1994			
	0.2130	0.2267	0.2404	0.2542	0.2680			
	0.2818	0.2957	0.3095	0.3238	0.3512			
	0.3784 0.5130	0.4055 0.5396	0.4326 0.5660	0.4595 0.5924	0.4863 0.6187			
	0.6448	0.6708	0.6968	0.7226	0.7483			
	0.7740	0.7995	0.8249	0.8502	0.8754			
Width:	0.9005	0.9256	0.9505	0.9753	1.0000			
wideli.	0.0355	0.0711	0.1066	0.1422	0.1777			
	0.2132	0.2520	0.2961	0.3402	0.3842			
	0.4283 0.6487	0.4724 0.6927	0.5164 0.7368	0.5605 0.7809	0.6046 0.8249			
	0.8690	0.9131	0.9572	1.0000	1.0000			
	1.0000	1.0000	1.0000	1.0000	1.0000			
	1.0000	1.0000	1.0000	1.0000	1.0000			
	1.0000	1.0000	1.0000 1.0000	1.0000 1.0000	1.0000			
	1.0000	1.0000	1.0000	1.0000	1.0000			

Transect XS	-L-Pipe -	(16)			
Area:					
	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312 0.2323	0.1491 0.2561	0.1682 0.2810	0.1884 0.3071	0.2098
	0.2323	0.3871	0.4137	0.4404	0.3336
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868	0.8135	0.8401	0.8668
	0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:					
	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835	0.0963	0.1080	0.1202	0.1329
	0.1459 0.2130	0.1591 0.2267	0.1724 0.2404	0.1858 0.2542	0.1994 0.2680
	0.2130	0.2267	0.3095	0.3238	0.3512
	0.3784	0.4055	0.4326	0.4595	0.4863
	0.5130	0.5396	0.5660	0.5924	0.6187
	0.6448	0.6708	0.6968	0.7226	0.7483
	0.7740	0.7995	0.8249	0.8502	0.8754
	0.9005	0.9256	0.9505	0.9753	1.0000
Width:					
	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132 0.4283	0.2520 0.4724	0.2961 0.5164	0.3402 0.5605	0.3842
	0.4203	0.6927	0.7368	0.7809	0.8249
	0.8690	0.9131	0.9572	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
Transect XS	-L-Pipe -	(18)			
Area:					
	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312 0.2323	0.1491 0.2561	0.1682 0.2810	0.1884 0.3071	0.2098
	0.2323	0.2301	0.4137	0.4404	0.4670
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868	0.8135	0.8401	0.8668
	0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:	0 0120	0 0070	0 0410	0 0557	0.0606
	0.0139 0.0835	0.0278 0.0963	0.0418 0.1080	0.0557 0.1202	0.0696 0.1329
	0.1459	0.1591	0.1724	0.1202	0.1323
	0.2130	0.2267	0.2404	0.2542	0.2680
	0.2818	0.2957	0.3095	0.3238	0.3512
	0.3784	0.4055	0.4326	0.4595	0.4863
	0.5130	0.5396	0.5660	0.5924	0.6187
	0.6448	0.6708	0.6968	0.7226	0.7483
	0.7740	0.7995	0.8249	0.8502	0.8754
Width:	0.9005	0.9256	0.9505	0.9753	1.0000
Width:	0.0355	0.0711	0.1066	0.1422	0.1777
	0.0333	0.2520	0.2961	0.3402	0.3842
	0.4283	0.4724	0.5164	0.5605	0.6046
	0.6487	0.6927	0.7368	0.7809	0.8249
	0.8690	0.9131	0.9572	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000

	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
Transect X Area:	S-L-Pipe -	(2)			
	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312	0.1491	0.1682	0.1884	0.2098
	0.2323	0.2561	0.2810	0.3071	0.3338
	0.3604	0.3871	0.4137	0.4404	0.4670
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868	0.8135	0.8401	0.8668
	0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:					
	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835	0.0963	0.1080	0.1202	0.1329
	0.1459	0.1591	0.1724	0.1858	0.1994
	0.2130	0.2267	0.2404	0.2542	0.2680
	0.2818	0.2957	0.3095	0.3238	0.3512
	0.3784	0.4055	0.4326	0.4595	0.4863
	0.5130	0.5396	0.5660	0.5924	0.6187
	0.6448	0.6708	0.6968	0.7226	0.7483
	0.7740	0.7995	0.8249	0.8502	0.8754
*** 1.1.	0.9005	0.9256	0.9505	0.9753	1.0000
Width:	0 0255	0 0711	0 1000	0 1400	0 1777
	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132	0.2520	0.2961	0.3402	0.3842
	0.4283 0.6487	0.4724	0.5164	0.5605	0.6046
	0.8690	0.6927 0.9131	0.7368 0.9572	0.7809 1.0000	0.8249 1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
Transect X Area:	S-L-Pipe -	(24)			
	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312	0.1491	0.1682	0.1884	0.2098
	0.2323	0.2561	0.2810	0.3071	0.3338
	0.3604	0.3871	0.4137	0.4404	0.4670
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868	0.8135	0.8401	0.8668
1.	0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:	0 0120	0 0070	0 0410	0 0557	0 0000
	0.0139 0.0835	0.0278	0.0418	0.0557	0.0696
		0.0963	0.1080	0.1202	0.1329
	0.1459	0.1591 0.2267	0.1724	0.1858	0.1994
	0.2130 0.2818	0.2267	0.2404 0.3095	0.2542 0.3238	0.2680 0.3512
	0.2818	0.4055	0.4326	0.3238	0.3512
	0.5130	0.4055	0.5660	0.5924	0.4003
	0.5130	0.5396	0.6968	0.7226	0.7483
	0.8448	0.8708	0.8249	0.8502	0.7463
	0.9005	0.7995	0.9505	0.8302	1.0000
Width:	0.,000	0.7230	0.,,,,,	0.2733	1.0000
	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132	0.2520	0.2961	0.3402	0.3842
	0.4283	0.4724	0.5164	0.5605	0.6046
	0.1200	V. 1/21	0.0101	0.5005	0.0010

	0.6487 0.8690 1.0000 1.0000 1.0000 1.0000	0.6927 0.9131 1.0000 1.0000 1.0000 1.0000	0.7368 0.9572 1.0000 1.0000 1.0000 1.0000	0.7809 1.0000 1.0000 1.0000 1.0000 1.0000	0.8249 1.0000 1.0000 1.0000 1.0000 1.0000
Transect XS	G-L-Pipe -	(27)			
Hrad:	0.0005 0.0170 0.0595 0.1312 0.2323 0.3604 0.4937 0.6269 0.7602 0.8934	0.0019 0.0232 0.0715 0.1491 0.2561 0.3871 0.5203 0.6536 0.7868 0.9201	0.0043 0.0305 0.0847 0.1682 0.2810 0.4137 0.5470 0.6802 0.8135 0.9467	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401 0.9734	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668 1.0000
iii au•	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740	0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995 0.9256	0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754 1.0000
Width:	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000	0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000 1.0000	0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000	0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000 1.0000	0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000
Transect XS	G-L-Pipe -	(28)			
	0.0005 0.0170 0.0595 0.1312 0.2323 0.3604 0.4937 0.6269 0.7602 0.8934	0.0019 0.0232 0.0715 0.1491 0.2561 0.3871 0.5203 0.6536 0.7868 0.9201	0.0043 0.0305 0.0847 0.1682 0.2810 0.4137 0.5470 0.6802 0.8135 0.9467	0.0076 0.0390 0.0990 0.1884 0.3071 0.4404 0.5736 0.7069 0.8401 0.9734	0.0118 0.0487 0.1145 0.2098 0.3338 0.4670 0.6003 0.7335 0.8668 1.0000
Hrad:	0.0139 0.0835 0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005	0.0278 0.0963 0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995 0.9256	0.0418 0.1080 0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505	0.0557 0.1202 0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753	0.0696 0.1329 0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754 1.0000

Width:	0.0355 0.2132 0.4283 0.6487 0.8690 1.0000 1.0000 1.0000	0.0711 0.2520 0.4724 0.6927 0.9131 1.0000 1.0000 1.0000	0.1066 0.2961 0.5164 0.7368 0.9572 1.0000 1.0000 1.0000	0.1422 0.3402 0.5605 0.7809 1.0000 1.0000 1.0000 1.0000 1.0000	0.1777 0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000
Transect XX	S-L-Pipe -	(30)			
	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312	0.1491	0.1682	0.1884	0.2098
	0.2323	0.2561	0.2810	0.3071	0.3338
	0.3604	0.3871	0.4137	0.4404	0.4670
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868	0.8135	0.8401	0.8668
	0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:	0.0139	0.0278	0.0418	0.0557	0.0696
Width:	0.0835	0.0963	0.1080	0.1202	0.1329
	0.1459	0.1591	0.1724	0.1858	0.1994
	0.2130	0.2267	0.2404	0.2542	0.2680
	0.2818	0.2957	0.3095	0.3238	0.3512
	0.3784	0.4055	0.4326	0.4595	0.4863
	0.5130	0.5396	0.5660	0.5924	0.6187
	0.6448	0.6708	0.6968	0.7226	0.7483
	0.7740	0.7995	0.8249	0.8502	0.8754
	0.9005	0.9256	0.9505	0.9753	1.0000
Width:	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132	0.2520	0.2961	0.3402	0.3842
	0.4283	0.4724	0.5164	0.5605	0.6046
	0.6487	0.6927	0.7368	0.7809	0.8249
	0.8690	0.9131	0.9572	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
Transect XS	S-L-Pipe -	(37)			
Area:	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312	0.1491	0.1682	0.1884	0.2098
	0.2323	0.2561	0.2810	0.3071	0.3338
	0.3604	0.3871	0.4137	0.4404	0.4670
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868	0.8135	0.8401	0.8668
	0.8934	0.9201	0.9467	0.9734	1.0000
	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835	0.0963	0.1080	0.1202	0.1329
	0.1459	0.1591	0.1724	0.1858	0.1994
	0.2130	0.2267	0.2404	0.2542	0.2680
	0.2818	0.2957	0.3095	0.3238	0.3512
	0.3784	0.4055	0.4326	0.4595	0.4863

	0.5130	0.5396	0.5660	0.5924	0.6187
	0.6448	0.6708	0.6968	0.7226	0.7483
	0.7740	0.7995	0.8249	0.8502	0.8754
ratalele e	0.9005	0.9256	0.9505	0.9753	1.0000
Width:	0.0355	0.0711	0.1066	0.1422	0.1777
	0.0333	0.2520	0.2961	0.3402	0.3842
	0.4283	0.4724	0.5164	0.5605	0.6046
	0.6487	0.6927	0.7368	0.7809	0.8249
	0.8690	0.9131	0.9572	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
Transect XS	-L-Pipe -	(50)			
Area:	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0003	0.0019	0.0305	0.0390	0.0118
	0.0595	0.0232	0.0847	0.0990	0.1145
	0.1312	0.1491	0.1682	0.1884	0.2098
	0.2323	0.2561	0.2810	0.3071	0.3338
	0.3604	0.3871	0.4137	0.4404	0.4670
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868	0.8135	0.8401	0.8668
	0.8934	0.9201	0.9467	0.9734	1.0000
Hrad:					
	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835	0.0963	0.1080	0.1202	0.1329
	0.1459	0.1591	0.1724	0.1858	0.1994
	0.2130	0.2267	0.2404	0.2542	0.2680
	0.2818	0.2957	0.3095	0.3238	0.3512
	0.3784 0.5130	0.4055 0.5396	0.4326 0.5660	0.4595 0.5924	0.4863 0.6187
	0.6448	0.5390	0.6968	0.7226	0.7483
	0.7740	0.0708	0.8249	0.8502	0.8754
	0.9005	0.7555	0.9505	0.9753	1.0000
Width:	0.5005	0.5250	0.,,,,	0.7733	1.0000
	0.0355	0.0711	0.1066	0.1422	0.1777
	0.2132	0.2520	0.2961	0.3402	0.3842
	0.4283	0.4724	0.5164	0.5605	0.6046
	0.6487	0.6927	0.7368	0.7809	0.8249
	0.8690	0.9131	0.9572	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
	1.0000	1.0000 1.0000	1.0000	1.0000 1.0000	1.0000
	1.0000	1.0000	1.0000	1.0000	1.0000
Transect XS	-L-Pipe -	(55)			
Area:	-	•			
	0.0005	0.0019	0.0043	0.0076	0.0118
	0.0170	0.0232	0.0305	0.0390	0.0487
	0.0595	0.0715	0.0847	0.0990	0.1145
	0.1312	0.1491	0.1682	0.1884	0.2098
	0.2323	0.2561	0.2810	0.3071	0.3338
	0.3604	0.3871	0.4137	0.4404	0.4670
	0.4937	0.5203	0.5470	0.5736	0.6003
	0.6269 0.7602	0.6536	0.6802	0.7069	0.7335
	0.7602	0.7868 0.9201	0.8135 0.9467	0.8401 0.9734	0.8668 1.0000
Hrad:	0.0751	0.7201	0.7107	0.7/34	1.0000
	0.0139	0.0278	0.0418	0.0557	0.0696
	0.0835	0.0963	0.1080	0.1202	0.1329

Width:	0.1459 0.2130 0.2818 0.3784 0.5130 0.6448 0.7740 0.9005 0.0355 0.2132 0.4283 0.6487 0.8690 1.0000 1.0000	0.1591 0.2267 0.2957 0.4055 0.5396 0.6708 0.7995 0.9256 0.0711 0.2520 0.4724 0.6927 0.9131 1.0000 1.0000	0.1724 0.2404 0.3095 0.4326 0.5660 0.6968 0.8249 0.9505 0.1066 0.2961 0.5164 0.7368 0.9572 1.0000 1.0000	0.1858 0.2542 0.3238 0.4595 0.5924 0.7226 0.8502 0.9753 0.1422 0.3402 0.5605 0.7809 1.0000 1.0000 1.0000	0.1994 0.2680 0.3512 0.4863 0.6187 0.7483 0.8754 1.0000 0.1777 0.3842 0.6046 0.8249 1.0000 1.0000 1.0000 1.0000		
	1.0000 1.0000	1.0000	1.0000 1.0000	1.0000 1.0000	1.0000		
Runoff Qua ****** Total Prec	********* ntity Cont: ******** ipitation Error (%)	inuity *****	Volume acre-ft  1.402 0.682	Depth inches			
******	*****	* * * * *	Volume	Volume			
	ng Continu:		acre-ft	Mgallons			
External O Initial St Final Stor	nflow utflow ored Volume ed Volume Error (%)	 e	0.000 0.580 0.000 0.000 -0.797	0.000 0.189 0.000 0.000			
Runoff Coe	fficient Co	********** omputations ******	Report				
Subbasin S	 ub-CB-1						
Soil/Surfa	ce Descript	tion			Area (acres)	Soil Group	Runoff Coeff.
Residentia			years or g	reater	0.17 0.19 0.36	A (6%+) A (6%+)	0.79 0.29 0.53
Subbasin S	ub-CB-10	_					
Soil/Surfa	ce Descript	tion			Area (acres)	Soil Group	Runoff Coeff.
Residentia			years or g	reater	0.12 0.01 0.13	A (6%+) A (6%+)	0.79 0.29 0.75
Subbasin S		=					
		_			Area	Soil	Runoff

Soil/Surface Description	(acres)	Group	Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.11 0.09 0.20	A (6%+) A (6%+)	0.79 0.14 0.50
Subbasin Sub-CB-12			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.23 1.05 1.28	A (6%+) A (6%+)	0.79 0.14 0.26
Subbasin Sub-CB-13-14			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.25 0.09 0.34	A (6%+) A (6%+)	0.79 0.14 0.61
Subbasin Sub-CB-15-16			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Streets, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.19 0.05 0.16 0.40	A (6%+) A (6%+) B (0-2%)	0.79 0.29 0.80 0.73
Subbasin Sub-CB-17			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.15 0.13 0.29	A (6%+) A (6%+)	0.79 0.29 0.56
Subbasin Sub-CB-18-19			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.47 0.47 0.95	A (6%+) A (6%+)	0.79 0.29 0.54
Subbasin Sub-CB-2			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.17 0.23 0.40	A (6%+) A (6%+)	0.79 0.29 0.50

Subbasin Sub-CB-20			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.49 1.00 1.49	A (6%+) A (6%+)	0.79 0.14 0.35
Subbasin Sub-CB-3			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.14 2.69 2.84	A (6%+) A (6%+)	0.79 0.14 0.17
Subbasin Sub-CB-4			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.15 0.19 0.34	A (6%+) A (6%+)	0.79 0.14 0.43
Subbasin Sub-CB-5			
Soil/Surface Description	Area (acres)	Soil Group	Runoff Coeff.
Soil/Surface Description	(acres)  0.32 0.01	Group  A (6%+)	Coeff. 0.79 0.14
Soil/Surface Description	(acres)  0.32 0.01	Group  A (6%+)	Coeff. 0.79 0.14
Soil/Surface Description	0.32 0.01 0.33	Group  A (6%+) A (6%+)  Soil	Coeff. 0.79 0.14 0.78
Soil/Surface Description  Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.  Subbasin Sub-CB-6  Soil/Surface Description  Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater	0.32 0.01 0.33 Area (acres)	Group  A (6%+) A (6%+)  Soil Group  A (2-6%)	Coeff.  0.79  0.14  0.78  Runoff Coeff.  0.77
Soil/Surface Description  Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.  Subbasin Sub-CB-6  Soil/Surface Description  Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.  Subbasin Sub-CB-7  Subbasin Sub-CB-7  Soil/Surface Description	0.32 0.01 0.33 Area (acres)	Group  A (6%+) A (6%+)  Soil Group  A (2-6%)	Coeff.  0.79  0.14  0.78  Runoff Coeff.  0.77
Soil/Surface Description  Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.	0.32 0.01 0.33 Area (acres) 	Group  A (6%+) A (6%+)  Soil Group  A (2-6%) A (6%+)	Coeff.  0.79 0.14 0.78  Runoff Coeff.  0.77 0.29 0.76
Soil/Surface Description Streets, 25 years or greater Forest, 25 years or greater Composite Area & Weighted Runoff Coeff.  Subbasin Sub-CB-6 Soil/Surface Description Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater Composite Area & Weighted Runoff Coeff.  Subbasin Sub-CB-7 Subbasin Sub-CB-7 Subbasin Sub-CB-7 Soil/Surface Description Streets, 25 years or greater Residential Lot Size 1 Acre, 25 years or greater	Area (acres)  0.32 0.01 0.33  Area (acres)  0.14 0.00 0.14  Area (acres)  0.10 0.01	Group  A (6%+) A (6%+)  Soil Group  A (2-6%) A (6%+)  Soil Group	Coeff.  0.79 0.14 0.78  Runoff Coeff.  0.77 0.29 0.76  Runoff Coeff.  0.76 0.26

```
0.17 A (2-6%) 0.77
0.05 A (2-6%) 0.22
0.22 0.64
Streets, 25 years or greater
Meadow, 25 years or greater
Composite Area & Weighted Runoff Coeff.
                                                       0.22
Subbasin Sub-CB-9
______
                                                             Soil Runoff
Group Coeff
                                                      Area
Soil/Surface Description
                                                    (acres)
______
                                                    0.15 A (2-6%) 0.77
0.00 A (2-6%) 0.26
0.15 0.76
Streets, 25 years or greater
Residential Lot Size 1 Acre, 25 years or greater
Composite Area & Weighted Runoff Coeff.
SCS TR-55 Time of Concentration Computations Report
Sheet Flow Equation
       Tc = (0.007 * ((n * Lf)^0.8)) / ((P^0.5) * (Sf^0.4))
       Where:
       Tc = Time of Concentration (hrs)
       n = Manning's Roughness
       Lf = Flow Length (ft)
       P = 2 yr, 24 hr Rainfall (inches)
       Sf = Slope (ft/ft)
Shallow Concentrated Flow Equation
       V = 16.1345 * (Sf^0.5) (unpaved surface)

V = 20.3282 * (Sf^0.5) (paved surface)
       V = 15.0 * (Sf^0.5) (grassed waterway surface)
         = 10.0 * (Sf^0.5) (nearly bare & untilled surface)
       V = 9.0 * (Sf^0.5) (cultivated straight rows surface)
       V = 7.0 * (Sf^0.5) (short grass pasture surface)
         = 5.0 * (Sf^0.5) (woodland surface)
       V = 2.5 * (Sf^0.5) (forest w/heavy litter surface)
       Tc = (Lf / V) / (3600 sec/hr)
       Where:
       Tc = Time of Concentration (hrs)
       Lf = Flow Length (ft)
       V = Velocity (ft/sec)
       Sf = Slope (ft/ft)
Channel Flow Equation
       V = (1.49 * (R^{(2/3)}) * (Sf^{0.5})) / n
       R = Aq / Wp
       Tc = (Lf / V) / (3600 sec/hr)
       Where:
       Tc = Time of Concentration (hrs)
       Lf = Flow Length (ft)
       R = Hydraulic Radius (ft)
       Aq = Flow Area (ft<sup>2</sup>)
```

Wp = Wetted Perimeter (ft) V = Velocity (ft/sec) Sf = Slope (ft/ft)n = Manning's Roughness Subbasin Sub-CB-1 \_\_\_\_\_\_ Sheet Flow Computations Subarea A Subarea B Subarea С Manning's Roughness: 0.40 0.00 0.00 Flow Length (ft): 33.69 0.00 0.00 Slope (%): 0.00 1.60 0.00 2 yr, 24 hr Rainfall (in): 3.60 0.00 0.00 Velocity (ft/sec): 0.00 0.06 0.00 0.00 Computed Flow Time (minutes): 9.26 0.00 Shallow Concentrated Flow Computations Subarea A Subarea B Subarea С Flow Length (ft): 0.00 329.84 0.00 Slope (%): 0.77 0.00 0.00 Surface Type: Paved Paved Paved Velocity (ft/sec): 1.79 0.00 0.00 Computed Flow Time (minutes): 3.08 0.00 0.00 \_\_\_\_\_\_ Total TOC (minutes): 12.34 \_\_\_\_\_\_ Subbasin Sub-CB-10 User-Defined TOC override (minutes): 5.00 Subbasin Sub-CB-11 Sheet Flow Computations Subarea A Subarea B Subarea С Manning's Roughness: 0.40 0.00 0.00

73.91

24.40

0.00

0.00

Slope (%):

0.00

Flow Length (ft):

0 00				
0.00	2 yr, 24 hr Rainfall (in):	3.60	0.00	
0.00	Velocity (ft/sec):	0.21	0.00	
0.00	Computed Flow Time (minutes):	5.85	0.00	
0.00				
	ow Concentrated Flow Computations			
С		Subarea A	Subarea B	Subarea
0.00	Flow Length (ft):	147.74	0.00	
0.00	Slope (%):	2.17	0.00	
Paved	Surface Type:	Paved	Paved	
0.00	Velocity (ft/sec):	2.99	0.00	
0.00	Computed Flow Time (minutes):	0.82	0.00	
		:==========	=======================================	========
	Total TOC (minutes):	6.67		
======		=======================================	=======================================	========
	Flow Computations	Qulbarra 3	Quibaura D	Colores
		Subarea A	Subarea B	Subarea
	Manning's Roughness:	0.40	0.00	Subarea
C	Manning's Roughness: Flow Length (ft):	0.40	0.00	Subarea
C 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):	0.40 222.44 10.60	0.00 0.00 0.00	Subarea
C 0.00 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):	0.40 222.44 10.60 3.60	0.00 0.00 0.00 0.00	Subarea
C 0.00 0.00 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):	0.40 222.44 10.60	0.00 0.00 0.00	Subarea
C 0.00 0.00 0.00 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):	0.40 222.44 10.60 3.60	0.00 0.00 0.00 0.00	Subarea
C 0.00 0.00 0.00 0.00 0.00 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):  Velocity (ft/sec):	0.40 222.44 10.60 3.60 0.19	0.00 0.00 0.00 0.00	Subarea
C 0.00 0.00 0.00 0.00 0.00 0.00 Shallo	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):  Velocity (ft/sec):  Computed Flow Time (minutes):	0.40 222.44 10.60 3.60 0.19	0.00 0.00 0.00 0.00	Subarea
C 0.00 0.00 0.00 0.00 0.00 Shall C	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):  Velocity (ft/sec):  Computed Flow Time (minutes):  ow Concentrated Flow Computations	0.40 222.44 10.60 3.60 0.19 19.70	0.00 0.00 0.00 0.00 0.00	
C 0.00 0.00 0.00 0.00 0.00 Shall C 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):  Velocity (ft/sec):  Computed Flow Time (minutes):  ow Concentrated Flow Computations	0.40 222.44 10.60 3.60 0.19 19.70	0.00 0.00 0.00 0.00 0.00 0.00	
C 0.00 0.00 0.00 0.00 Shall C 0.00 0.00 0.00 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):  Velocity (ft/sec):  Computed Flow Time (minutes):  ow Concentrated Flow Computations  Flow Length (ft):	0.40 222.44 10.60 3.60 0.19 19.70 Subarea A 185.02	0.00 0.00 0.00 0.00 0.00 0.00 Subarea B	
C 0.00 0.00 0.00 0.00 0.00 C 0.00 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):  Velocity (ft/sec):  Computed Flow Time (minutes):  ow Concentrated Flow Computations  Flow Length (ft):  Slope (%):	0.40 222.44 10.60 3.60 0.19 19.70 Subarea A 185.02 4.77	0.00 0.00 0.00 0.00 0.00 0.00 Subarea B 0.00	
C 0.00 0.00 0.00 0.00 0.00 C 0.00 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):  Velocity (ft/sec):  Computed Flow Time (minutes):  ow Concentrated Flow Computations  Flow Length (ft):  Slope (%):  Surface Type:	0.40 222.44 10.60 3.60 0.19 19.70  Subarea A 185.02 4.77 Paved	0.00 0.00 0.00 0.00 0.00 0.00 Subarea B 0.00 0.00	
C 0.00 0.00 0.00 0.00 0.00 C 0.00 0.00	Manning's Roughness:  Flow Length (ft):  Slope (%):  2 yr, 24 hr Rainfall (in):  Velocity (ft/sec):  Computed Flow Time (minutes):  ow Concentrated Flow Computations  Flow Length (ft):  Slope (%):  Surface Type:  Velocity (ft/sec):	0.40 222.44 10.60 3.60 0.19 19.70  Subarea A 185.02 4.77 Paved 4.44	0.00 0.00 0.00 0.00 0.00 0.00 Subarea B 0.00 0.00 Paved 0.00	

	Total TOC (minutes):	20.39		
======		=======================================	============	========
	in Sub-CB-13-14			
	Flow Computations			
C		Subarea A	Subarea B	Subarea
0.00	Manning's Roughness:	0.40	0.00	
0.00	Flow Length (ft):	80.13	0.00	
0.00	Slope (%):	24.40	0.00	
0.00	2 yr, 24 hr Rainfall (in):	3.60	0.00	
0.00	Velocity (ft/sec):	0.21	0.00	
0.00	Computed Flow Time (minutes):	6.23	0.00	
	w Concentrated Flow Computations			
		Subarea A	Subarea B	Subarea
C	Flow Length (ft):	174.35	0.00	
0.00	Slope (%):	2.45	0.00	
0.00	Surface Type:	Paved	Paved	
Paved	Velocity (ft/sec):	3.18	0.00	
0.00	Computed Flow Time (minutes):	0.91	0.00	
		.========	=======================================	:=======
	Total TOC (minutes):	7.15		
======		=======================================	===========	
Subbas	in Sub-CB-15-16			
	User-Defined TOC override (minutes):	5.00		
Subbas	in Sub-CB-17			
	User-Defined TOC override (minutes):	5.00		
	in Sub-CB-18-19			
	User-Defined TOC override (minutes):	5.00		

## Subbasin Sub-CB-2

User-Defined TOC override (minutes): 5.00

Subbasin Sub-CB-20

Sheet Flow Computations

		Subarea A	Subarea B	Subarea
C	Manning's Roughness:	0.40	0.00	
0.00	Flow Length (ft):	227.22	0.00	
0.00	Slope (%):	7.48	0.00	
0.00	2 yr, 24 hr Rainfall (in):	3.60	0.00	
0.00	Velocity (ft/sec):	0.16	0.00	
0.00	Computed Flow Time (minutes):	23.04	0.00	
0.00				
Shallo	w Concentrated Flow Computations			
	<del>-</del>	Subarea A	Subarea B	Subarea
C	Flow Length (ft):	Subarea A	Subarea B	Subarea
C 0.00	Flow Length (ft): Slope (%):			Subarea
C 0.00 0.00	J , ,	193.35	0.00	Subarea
C 0.00 0.00 Paved	Slope (%):	193.35 2.77	0.00	Subarea
C 0.00 0.00 Paved 0.00	Slope (%): Surface Type:	193.35 2.77 Paved	0.00 0.00 Paved	Subarea
C 0.00 0.00 Paved	Slope (%): Surface Type: Velocity (ft/sec):	193.35 2.77 Paved 3.38	0.00 0.00 Paved 0.00	Subarea

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Subbasin Sub-CB-3

Sheet Flow Computations

a		Subarea A	Subarea B	Subarea
C	Manning's Roughness:	0.40	0.00	
0.00	Flow Length (ft):	492.34	0.00	
0.00	Slope (%):	3.89	0.00	
0.00	2 yr, 24 hr Rainfall (in):	3.60	0.00	
0.00	Velocity (ft/sec):	0.15	0.00	
0.00	Computed Flow Time (minutes):	55.54	0.00	

	Concentrated							
!				Suk	oarea A	Subare	a B Su	ubarea
.00	Flow Length	(ft):			70.73	0	.00	
.00	Slope (%):				4.87	0	.00	
aved	Surface Type	:		τ	Inpaved	Pa	ved	
.00	Velocity (ft	/sec):			3.56	0	.00	
.00	Computed Flor	w Time (mi	inutes):		0.33	0	.00	
	=========	=======	========	:======	:=======	:========	===========	====:
	Total TOC (m.	inutes):			55.87			
======	========	======	========	:======	=======	========	===========	=====
	n Sub-CB-4							
	User-Defined	TOC over	ride (minutes	;):	5.00			
	n Sub-CB-5							
	User-Defined	TOC over	ride (minutes	;):	5.00			
	n Sub-CB-6 							
	User-Defined	TOC over	ride (minutes	;):	5.00			
	 n Sub-CB-7							
	User-Defined	TOC over	ride (minutes	;):	5.00			
	n Sub-CB-8W	_						
		_						
	User-Defined	TOC over	ride (minutes	;):	5.00			
	n Sub-CB-9							
	User-Defined		ride (minutes	;):	5.00			
Subbasir	************* n Runoff Summa ******	ary						
	n Accum	ulated		Total	Peak	Weighted Runoff	Time of Concentration	

	in	in/hr	in	cfs	Coeff	days	hh:mm:ss
Sub-CB-1	1.41	6.86	0.75	1.32	0.530	0	00:12:20
Sub-CB-10	0.93	11.10	0.69	1.06	0.750	0	00:05:00
Sub-CB-11	1.06	9.52	0.53	0.94	0.500	0	00:06:40
Sub-CB-12	1.77	5.22	0.46	1.73	0.260	0	00:20:23
Sub-CB-13-14	1.10	9.17	0.67	1.88	0.610	0	00:07:09
Sub-CB-15-16	0.93	11.10	0.68	3.28	0.730	0	00:05:00
Sub-CB-17	0.93	11.10	0.52	1.77	0.560	0	00:05:00
Sub-CB-18-19	0.93	11.10	0.50	5.68	0.540	0	00:05:00
Sub-CB-2	0.93	11.10	0.46	2.23	0.500	0	00:05:00
Sub-CB-20	1.91	4.78	0.67	2.50	0.350	0	00:23:59
Sub-CB-3	2.61	2.81	0.44	1.35	0.170	0	00:55:52
Sub-CB-4	0.93	11.10	0.40	1.64	0.430	0	00:05:00
Sub-CB-5	0.93	11.10	0.72	2.85	0.780	0	00:05:00
Sub-CB-6	0.93	11.10	0.70	1.20	0.760	0	00:05:00
Sub-CB-7	0.93	11.10	0.67	0.87	0.720	0	00:05:00
Sub-CB-8W	0.93	11.10	0.59	1.56	0.640	0	00:05:00
Sub-CB-9	0.93	11.10	0.70	1.25	0.760	0	00:05:00

CB-8E	Node ID	Average Depth Attained ft	Maximum Depth Attained ft	Maximum HGL Attained ft		of Max urrence	Total Flooded Volume acre-in	Total Time Flooded minutes	Retention Time
CIT-8									
CIT-9	CB-8E	0.00	0.00	257.54	0	00:00	0	0	0:00:00
DH-10	CIT-8	2.69	2.69	257.49	0	00:00	0	0	0:00:00
DH-13	CIT-9	2.27	2.64	260.04	0	00:05	0	0	0:00:00
DH-20	DH-10	0.10	0.54	265.69	0	00:05	0	0	0:00:00
DH-6	DH-13	2.76	3.26	263.05	0	00:07	0	0	0:00:00
DMH-10	DH-20				0		•	0	0:00:00
DMH-11	DH-6	0.05	0.34		0	00:05	0	0	0:00:00
DMH-12					0		0	0	0:00:00
DMH-13					0		0	0	0:00:00
DMH-20         0.44         0.93         278.58         0 00:24         0 0 0:00:0           DMH-3         0.12         0.43         262.67         0 00:05         0 0 0:00:0           DMH-4N         0.12         0.66         253.51         0 00:05         0 0 0:00:0           DMH-4S         0.12         0.48         257.61         0 00:05         0 0 0:00:0           DMH-6         4.85         5.26         252.66         0 00:05         0 0 0:00:0           DMH-7         1.11         1.44         255.54         0 00:05         0 0 0:00:0           EX-18         3.00         3.89         269.89         0 00:05         0 0 0:00:0           EX-7         1.20         1.51         254.31         0 00:05         0 0 0:00:0           Structure - (72)         0.11         0.39         276.18         0 00:12         0 0 0:00:0           STU-5         0.12         0.76         249.39         0 00:04         0.03         3 0:00:0           DP-1         0.00         0.37         275.37         0 00:06         0 0 0:00:0           DP-13         0.01         0.61         265.13         0 00:05         0 0 0:00:0           DP-16         0.00	DMH-12	0.34			0	00:20	0	0	0:00:00
DMH-3	DMH-13				0		0	0	0:00:00
DMH-4N         0.12         0.66         253.51         0 00:05         0         0 0:00:0           DMH-4S         0.12         0.48         257.61         0 00:05         0         0 0:00:0           DMH-6         4.85         5.26         252.66         0 00:05         0         0 0:00:0           DMH-7         1.11         1.44         255.54         0 00:05         0         0 0:00:0           EX-18         3.00         3.89         269.89         0 00:05         0         0 0:00:0           EX-7         1.20         1.51         254.31         0 00:05         0         0 0:00:0           Structure - (72)         0.11         0.39         276.18         0 00:12         0         0 0:00:0           STU-5         0.12         0.76         249.39         0 00:04         0.03         3 0:00:0           DP-1         0.00         0.37         275.37         0 00:12         0         0 0:00:0           DP-10         0.00         0.35         265.13         0 00:05         0         0 0:00:0           DP-13         0.01         0.61         260.21         0 00:07         0         0 0:00:0           DP-18         0.01 </td <td></td> <td></td> <td></td> <td></td> <td>0</td> <td></td> <td>-</td> <td></td> <td>0:00:00</td>					0		-		0:00:00
DMH-4S         0.12         0.48         257.61         0 00:05         0 00:00:0           DMH-6         4.85         5.26         252.66         0 00:05         0 00:00:0           DMH-7         1.11         1.44         255.54         0 00:05         0 0 0:00:0           EX-18         3.00         3.89         269.89         0 00:05         0 0 0:00:0           EX-7         1.20         1.51         254.31         0 00:05         0 0 0:00:0           Structure - (72)         0.11         0.39         276.18         0 00:12         0 0 0:00:0           STU-16         0.29         2.79         255.49         0 00:04         0.03         3 0:00:0           STU-5         0.12         0.76         249.39         0 00:06         0 0 0:00:0           DP-1         0.00         0.37         275.37         0 00:12         0 0 0:00:0           DP-10         0.00         0.35         265.13         0 00:05         0 0 0:00:0           DP-13         0.01         0.61         260.21         0 00:07         0 0 0:00:0           DP-18         0.01         0.65         265.01         0 00:05         0 0 0:00:0           DP-5         0.02	DMH-3				0		0	0	0:00:00
DMH-6         4.85         5.26         252.66         0 00:05         0 0 0:00:0           DMH-7         1.11         1.44         255.54         0 00:05         0 0 0:00:0           EX-18         3.00         3.89         269.89         0 00:05         0 0 0:00:0           EX-7         1.20         1.51         254.31         0 00:05         0 0 0:00:0           Structure - (72)         0.11         0.39         276.18         0 00:12         0 0 0:00:0           STU-16         0.29         2.79         255.49         0 00:04         0.03         3 0:00:0           STU-5         0.12         0.76         249.39         0 00:06         0 0 0:00:0           DP-1         0.00         0.37         275.37         0 00:12         0 0 0:00:0           DP-10         0.00         0.35         265.13         0 00:05         0 0 0:00:0           DP-13         0.01         0.61         260.21         0 00:07         0 0 0:00:0           DP-16         0.00         1.00         253.66         0 00:04         0 0 0:00:0           DP-20         0.01         0.44         274.64         0 00:24         0 0 0:00:0           DP-5         0.02					-		-	-	0:00:00
DMH-7         1.11         1.44         255.54         0 00:05         0 0 0:00:0           EX-18         3.00         3.89         269.89         0 00:05         0 0 0:00:0           EX-7         1.20         1.51         254.31         0 00:05         0 0 0:00:0           Structure - (72)         0.11         0.39         276.18         0 00:12         0 0 0:00:0           STU-16         0.29         2.79         255.49         0 00:04         0.03         3 0:00:0           STU-5         0.12         0.76         249.39         0 00:06         0 0 0:00:0           DP-1         0.00         0.37         275.37         0 00:12         0 0 0:00:0           DP-10         0.00         0.35         265.13         0 00:05         0 0 0:00:0           DP-13         0.01         0.61         260.21         0 00:07         0 0 0:00:0           DP-16         0.00         1.00         253.66         0 00:04         0 0 0:00:0           DP-20         0.01         0.44         274.64         0 00:24         0 0 0:00:0           DP-5         0.02         0.70         248.70         0 00:05         0 0 0:00:0           DP-6         0.00					0		ū	-	0:00:00
EX-18 3.00 3.89 269.89 0 00:05 0 0 0:00:0  EX-7 1.20 1.51 254.31 0 00:05 0 0 0:00:0  Structure - (72) 0.11 0.39 276.18 0 00:12 0 0 0:00:0  STU-16 0.29 2.79 255.49 0 00:04 0.03 3 0:00:0  STU-5 0.12 0.76 249.39 0 00:06 0 0 0:00:0  DP-1 0.00 0.37 275.37 0 00:12 0 0 0 0:00:0  DP-10 0.00 0.35 265.13 0 00:05 0 0 0:00:0  DP-13 0.01 0.61 260.21 0 00:07 0 0 0:00:0  DP-16 0.00 1.00 253.66 0 00:04 0 0 0:00:0  DP-18 0.01 0.65 265.01 0 00:05 0 0 0:00:0  DP-20 0.01 0.44 274.64 0 00:24 0 0 0:00:0  DP-5 0.02 0.70 248.70 0 00:05 0 0 0:00:0  DP-6 0.00 0.25 246.75 0 00:05 0 0 0:00:0  DP-6 0.00 0.70 253.30 0 00:06 0 0 0:00:0	DMH-6				0		0		0:00:00
EX-7					-		-		0:00:00
Structure - (72)         0.11         0.39         276.18         0 00:12         0 00:03         3 0:00:0           STU-16         0.29         2.79         255.49         0 00:04         0.03         3 0:00:0           STU-5         0.12         0.76         249.39         0 00:06         0 0 0         0 0:00:0           DP-1         0.00         0.37         275.37         0 00:12         0 0 0         0 0:00:0           DP-10         0.00         0.35         265.13         0 00:05         0 0 0         0 0:00:0           DP-13         0.01         0.61         260.21         0 00:07         0 0 0 0:00:0           DP-16         0.00         1.00         253.66         0 00:04         0 0 0 0:00:0           DP-18         0.01         0.65         265.01         0 00:05         0 0 0:00:0           DP-20         0.01         0.44         274.64         0 00:24         0 0 0 0:00:0           DP-5         0.02         0.70         248.70         0 00:05         0 0 0:00:0           DP-6         0.00         0.25         246.75         0 00:05         0 0 0:00:0           DP-7         0.00         0.70         253.30         0 00:06	EX-18				0		-	-	0:00:00
STU-16         0.29         2.79         255.49         0 00:04         0.03         3 0:00:0           STU-5         0.12         0.76         249.39         0 00:06         0 0 0:00:0           DP-1         0.00         0.37         275.37         0 00:12         0 0 0:00:0           DP-10         0.00         0.35         265.13         0 00:05         0 0 0:00:0           DP-13         0.01         0.61         260.21         0 00:07         0 0 0:00:0           DP-16         0.00         1.00         253.66         0 00:04         0 0 0:00:0           DP-18         0.01         0.65         265.01         0 00:05         0 0 0:00:0           DP-20         0.01         0.44         274.64         0 00:24         0 0 0:00:0           DP-5         0.02         0.70         248.70         0 00:05         0 0 0:00:0           DP-6         0.00         0.25         246.75         0 00:05         0 0 0:00:0           DP-7         0.00         0.70         253.30         0 00:06         0 0 0:00:0	EX-7				0		0	-	0:00:00
STU-5       0.12       0.76       249.39       0 00:06       0 0 0:00:0         DP-1       0.00       0.37       275.37       0 00:12       0 0 0:00:0         DP-10       0.00       0.35       265.13       0 00:05       0 0 0:00:0         DP-13       0.01       0.61       260.21       0 00:07       0 0 0:00:0         DP-16       0.00       1.00       253.66       0 00:04       0 0 0:00:0         DP-18       0.01       0.65       265.01       0 00:05       0 0 0:00:0         DP-20       0.01       0.44       274.64       0 00:24       0 0 0:00:0         DP-5       0.02       0.70       248.70       0 00:05       0 0 0:00:0         DP-6       0.00       0.25       246.75       0 00:05       0 0 0:00:0         DP-7       0.00       0.70       253.30       0 00:06       0 0 0:00:0	Structure - (72	,			0	00:12	-		0:00:00
DP-1         0.00         0.37         275.37         0 00:12         0 0 0:00:0           DP-10         0.00         0.35         265.13         0 00:05         0 0 0:00:0           DP-13         0.01         0.61         260.21         0 00:07         0 0 0:00:0           DP-16         0.00         1.00         253.66         0 00:04         0 0 0:00:0           DP-18         0.01         0.65         265.01         0 00:05         0 0 0:00:0           DP-20         0.01         0.44         274.64         0 00:24         0 0 0:00:0           DP-5         0.02         0.70         248.70         0 00:05         0 0 0:00:0           DP-6         0.00         0.25         246.75         0 00:05         0 0 0:00:0           DP-7         0.00         0.70         253.30         0 00:06         0 0 0:00:0	STU-16			255.49	0	00:04	0.03	3	0:00:00
DP-10         0.00         0.35         265.13         0 00:05         0 0 0:00:0           DP-13         0.01         0.61         260.21         0 00:07         0 0 0:00:0           DP-16         0.00         1.00         253.66         0 00:04         0 0 0:00:0           DP-18         0.01         0.65         265.01         0 00:05         0 0 0:00:0           DP-20         0.01         0.44         274.64         0 00:24         0 0 0:00:0           DP-5         0.02         0.70         248.70         0 00:05         0 0 0:00:0           DP-6         0.00         0.25         246.75         0 00:05         0 0 0:00:0           DP-7         0.00         0.70         253.30         0 00:06         0 0 0:00:0	STU-5	0.12	0.76	249.39	0	00:06	0	0	0:00:00
DP-13         0.01         0.61         260.21         0 00:07         0 0 0:00:0           DP-16         0.00         1.00         253.66         0 00:04         0 0 0:00:0           DP-18         0.01         0.65         265.01         0 00:05         0 0 0:00:0           DP-20         0.01         0.44         274.64         0 00:24         0 0 0:00:0           DP-5         0.02         0.70         248.70         0 00:05         0 0 0:00:0           DP-6         0.00         0.25         246.75         0 00:05         0 0 0:00:0           DP-7         0.00         0.70         253.30         0 00:06         0 0 0:00:0	DP-1				0		0	0	0:00:00
DP-16         0.00         1.00         253.66         0 00:04         0 0 0:00:0           DP-18         0.01         0.65         265.01         0 00:05         0 0 0:00:0           DP-20         0.01         0.44         274.64         0 00:24         0 0 0:00:0           DP-5         0.02         0.70         248.70         0 00:05         0 0 0:00:0           DP-6         0.00         0.25         246.75         0 00:05         0 0 0:00:0           DP-7         0.00         0.70         253.30         0 00:06         0 0 0:00:0	DP-10	0.00	0.35	265.13	0	00:05	0	0	0:00:00
DP-18         0.01         0.65         265.01         0 00:05         0 0 0:00:0           DP-20         0.01         0.44         274.64         0 00:24         0 0 0:00:0           DP-5         0.02         0.70         248.70         0 00:05         0 0 0:00:0           DP-6         0.00         0.25         246.75         0 00:05         0 0 0:00:0           DP-7         0.00         0.70         253.30         0 00:06         0 0 0:00:0	DP-13	0.01	0.61	260.21	0	00:07	0	0	0:00:00
DP-20     0.01     0.44     274.64     0 00:24     0 0:00:0       DP-5     0.02     0.70     248.70     0 00:05     0 0 0:00:0       DP-6     0.00     0.25     246.75     0 00:05     0 0 0:00:0       DP-7     0.00     0.70     253.30     0 00:06     0 0 0:00:0	DP-16	0.00	1.00	253.66	0	00:04	0	0	0:00:00
DP-5     0.02     0.70     248.70     0 00:05     0 0 0:00:0       DP-6     0.00     0.25     246.75     0 00:05     0 0 0:00:0       DP-7     0.00     0.70     253.30     0 00:06     0 0 0:00:0	DP-18	0.01	0.65	265.01	0	00:05	0	0	0:00:00
DP-6 0.00 0.25 246.75 0 00:05 0 0 0:00:0 DP-7 0.00 0.70 253.30 0 00:06 0 0 0:00:0	DP-20	0.01	0.44	274.64	0	00:24	0	0	0:00:00
DP-7 0.00 0.70 253.30 0 00:06 0 0:00:0	DP-5	0.02	0.70	248.70	0	00:05	0	0	0:00:00
	DP-6	0.00		246.75	0	00:05	0	0	0:00:00
	DP-7	0.00	0.70	253.30	0	00:06	0	0	0:00:00
OFFSITE1 0.00 0.11 281.33 0 00:15 0 0 0:00:0	OFFSITE1	0.00	0.11	281.33	0	00:15	0	0	0:00:00
OFFSITE-1 0.01 0.23 267.91 0 00:24 0 0 0:00:0	OFFSITE-1	0.01	0.23	267.91	0	00:24	0	0	0:00:00

Node	Element	Maximum	Peak	T	ime of	Maximum	Time of Peak
ID	Type	Lateral	Inflow	Peak	Inflow	Flooding	Flooding
		Inflow		Occu	rrence	Overflow	Occurrence
		cfs	cfs	days	hh:mm	cfs	days hh:mm
CB-8E	JUNCTION	0.00	0.00	0	00:00	0.00	
CIT-8	JUNCTION	0.00	2.17	0	00:05	0.00	
CIT-9	JUNCTION	0.00	1.02	0	00:05	0.00	
DH-10	JUNCTION	0.00	1.63	0	00:05	0.00	
DH-13	JUNCTION	0.00	2.44	0	00:07	0.00	
DH-20	JUNCTION	0.00	5.00	0	00:24	0.00	
DH-6	JUNCTION	0.00	1.11	0	00:05	0.00	
DMH-10	JUNCTION	0.00	1.00	0	00:05	0.00	
DMH-11	JUNCTION	0.00	0.90	0	00:06	0.00	
DMH-12	JUNCTION	0.00	1.53	0	00:20	0.00	
DMH-13	JUNCTION	0.00	1.88	0	00:07	0.00	
DMH-20	JUNCTION	0.00	5.00	0	00:24	0.00	
DMH-3	JUNCTION	0.00	2.22	0	00:05	0.00	
DMH-4N	JUNCTION	0.00	3.45	0	00:05	0.00	
DMH-4S	JUNCTION	0.00	2.21	0	00:05	0.00	
DMH-6	JUNCTION	0.00	1.12	0	00:05	0.00	
DMH-7	JUNCTION	0.00	0.89	0	00:05	0.00	
EX-18	JUNCTION	0.00	5.97	0	00:05	0.00	
EX-7	JUNCTION	0.00	3.00	0	00:06	0.00	
Structure - (72)	JUNCTION	0.00	1.03	0	00:12	0.00	
STU-16	JUNCTION	0.00	4.78	0	00:05	1.22	0 00:05
STU-5	JUNCTION	0.00	5.86	0	00:05	0.00	
DP-1	OUTFALL	0.00	1.03	0	00:12	0.00	
DP-10	OUTFALL	0.00	1.63	0	00:05	0.00	
DP-13	OUTFALL	0.00	2.43	0	00:07	0.00	
DP-16	OUTFALL	0.00	3.82	0	00:06	0.00	
DP-18	OUTFALL	0.00	5.66	0	00:05	0.00	
DP-20	OUTFALL	0.00	4.99	0	00:24	0.00	
DP-5	OUTFALL	0.00	5.86	0	00:05	0.00	
DP-6	OUTFALL	0.00	1.11	0	00:05	0.00	
DP-7	OUTFALL	0.00	3.00	0	00:06	0.00	
OFFSITE1	OUTFALL	0.00	0.23	0	00:15	0.00	
OFFSITE-1	OUTFALL	0.00	1.62	0	00:25	0.00	
	00111111	0.00	1.02	O	30 23	5.00	

Inlet ID	Max Gutter Spread during Peak Flow ft	Max Gutter Water Elev during Peak Flow ft	Max Gutter Water Depth during Peak Flow ft	M	Time of Maximum Depth arrence hh:mm
CB-1	7.11	281.45	0.23	0	00:12
CB-10	3.17	267.87	0.18	0	00:05
CB-11	3.02	272.27	0.17	0	00:06
CB-12	3.89	271.29	0.22	0	00:20
CB-13	5.20	265.07	0.22	0	00:07
CB-16	7.54	255.27	0.34	0	00:05
CB-17	8.14	265.74	0.25	0	00:05
CB-18	18.03	274.19	0.47	0	00:05
CB-2	4.30	277.06	0.24	0	00:05

CB-20	5.18	279.89	0.22	0	00:00
CB-3	3.51	265.59	0.20	0	00:56
CB-4	3.80	256.14	0.21	0	00:05
CB-5	6.65	251.47	0.29	0	00:05
CB-6	3.35	255.54	0.19	0	00:05
CB-7	2.99	258.58	0.17	0	00:05
CB-8W	7.07	260.31	0.23	0	00:05
CB-9	3.40	263.01	0.19	0	00:05

- Inlet Total	Peak	Peak	Peak	Peak	Inlet	Total	
ID Time	Flow	Lateral	Flow	Flow	Efficiency	Flooding	
Flooded		Flow	Intercepted	Bypassing	during		
riodaca	cfs	cfs	by Inlet cfs	Inlet cfs	Peak Flow %	acre-in	
minutes	015	015	012	010	v	4010 111	
CB-1 0	1.32	1.32	1.04	0.28	78.64	0.000	
CB-10	1.06	1.06	1.01	0.05	94.86	0.000	
CB-11	0.94	0.94	0.91	0.04	96.04	0.000	
CB-12	1.73	1.73	1.53	0.20	88.48	0.000	
CB-13	1.88	1.88	-	-	-	0.000	
CB-16	3.55	3.28	=	=	=	0.000	
CB-17	1.77	1.77	1.30	0.48	73.16	0.000	
CB-18	5.68	5.68	-	-	-	0.000	
CB-2 0	2.23	2.23	1.89	0.34	84.58	0.000	
CB-20	2.50	2.50	-	-	-	0.000	
CB-3	1.35	1.35	1.24	0.11	91.94	0.000	
CB-4	1.64	1.64	1.46	0.18	89.31	0.000	
CB-5	2.88	2.85	-	_	-	0.000	
CB-6	1.20	1.20	1.12	0.08	93.41	0.000	
CB-7	0.92	0.87	0.89	0.03	96.24	0.000	
CB-8W	1.61	1.56	1.24	0.37	76.84	0.000	
CB-9	1.25	1.25	1.02	0.22	82.02	0.000	
U							

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## Outfall Loading Summary

Outfall Node ID	Flow Frequency (%)	Average Flow cfs	Peak Inflow cfs
DP-1 DP-10 DP-13 DP-16 DP-18 DP-20 DP-5 DP-6 DP-7 OFFSITE1 OFFSITE-1	1.93 1.55 3.35 1.35 0.88 3.40 8.55 1.49 2.60 2.93 4.61	0.50 0.51 1.01 1.20 2.23 2.45 0.88 0.28 0.49 0.06 0.60	1.03 1.63 2.43 3.82 5.66 4.99 5.86 1.11 3.00 0.23 1.62
System	2.97	10.21	23.93

Link ID	Element	Т	ime of	Maximum	Length	Peak Flow	Design	Ratio of
Ratio of To	tal Reported	D		***		a	<b>7</b> 1.	36 - 3
Maximum Ti	Type me Condition	Pea.	K LTOM	velocity	Factor	during	F.TOM	Maximum
raximam 11	me condicion	0ccu:	rrence	Attained		Analysis	Capacity	/Design
Flow Surcharged						-		. 3
		days	hh:mm	ft/sec		cfs	cfs	Flow
Depth minutes	1							
CB-1_Overflow		0	00:15	2.12	1.00	0.23	2.70	0.08
0.39 0		_						
CB10-9_Gutter		0	00:07	2.67	1.00	0.04	8.35	0.00
0.12 0		0	00:09	2.86	1.00	0.03	7.95	0.00
CB11-10_Gutter 0.11 0	CHANNEL	U	00.09	2.80	1.00	0.03	7.95	0.00
CB12-13_Gutter		0	00:21	2.50	1.00	0.19	9.44	0.02
	Calculated	O	00.21	2.50	1.00	0.10	5.11	0.02
CB17-16_Gutter		0	00:06	6.91	1.00	0.41	12.30	0.03
	Calculated							
CB2-3_Gutter	CHANNEL	0	00:06	6.02	1.00	0.29	13.13	0.02
0.23 0	Calculated							
CB3-4_Gutter		0	00:57	1.89	1.00	0.11	11.64	0.01
0.17 0								
CB4-5_Gutter		0	00:06	3.91	1.00	0.12	8.25	0.02
0.20 0		0	00.07	0.00	1 00	0.05	7 72	0 01
CB6-5_Gutter 0.14 0	CHANNEL	0	00:07	2.89	1.00	0.05	7.73	0.01
	CAICUIALEG	0	00:08	2.18	1.00	0.03	6.62	0.01
0.12 0		U	00.00	2.10	1.00	0.03	0.02	0.01
CB8-7_Gutter		0	00:07	2.74	1.00	0.27	4.89	0.06
0.32 0								
CB9-8_Gutter	CHANNEL	0	00:07	3.07	1.00	0.16	6.26	0.03
0.24 0								
L-Pipe - (50)	CHANNEL	0	00:25	9.25	1.00	1.62	41.01	0.04

0.30	0	Calculated							
Pipe - (12)		CONDUIT	0	00:05	5.96	1.00	1.11	6.19	0.18
0.29 Pipe - (13)	0	Calculated CONDUIT	0	00:05	3.70	1.00	1.12	3.19	0.35
0.41	0	Calculated	U	00.05	3.70	1.00	1.12	3.19	0.35
Pipe - (14)		CONDUIT	0	00:05	7.17	1.00	2.86	5.59	0.51
0.51	0	Calculated CONDUIT	0	00:56	7.17	1.00	1.24	7.67	0.16
Pipe - (16) 0.27	0	Calculated	U	00.50	7.17	1.00	1.24	7.67	0.10
Pipe - (18)		CONDUIT	0	00:05	3.76	1.00	0.89	3.56	0.25
0.34 Pipe - (19)	0	Calculated CONDUIT	0	00:05	4.30	1.00	0.89	4.29	0.21
0.31	0	Calculated	U	00.05	4.30	1.00	0.69	4.29	0.21
Pipe - (2)		CONDUIT	0	00:05	13.26	1.00	1.84	7.69	0.24
0.33 Pipe - (20)	0	Calculated CONDUIT	0	00:00	0.00	1.00	0.00	2.79	0.00
0.00	0	Calculated	U	00.00	0.00	1.00	0.00	2.79	0.00
Pipe - (21)		CONDUIT	0	00:06	4.85	1.00	2.13	3.59	0.59
0.55 Pipe - (22)	0	Calculated CONDUIT	0	00:06	5.08	1.00	3.00	3.56	0.84
0.70	0	Calculated	Ü	00.00	3.00	1.00	3.00	3.30	0.01
Pipe - (23)	0	CONDUIT	0	00:05	6.29	1.00	1.23	6.40	0.19
0.30 Pipe - (24)	0	Calculated CONDUIT	0	00:05	3.78	1.00	1.02	3.40	0.30
0.37	0	Calculated							
Pipe - (25) 0.34	0	CONDUIT Calculated	0	00:05	5.00	1.00	0.98	3.88	0.25
Pipe - (26)	U	CONDUIT	0	00:05	3.03	1.00	1.00	2.52	0.40
0.44	0	Calculated	_						
Pipe - (27) 0.44	0	CONDUIT Calculated	0	00:05	3.03	1.00	1.00	2.52	0.40
Pipe - (28)	Ü	CONDUIT	0	00:06	6.78	1.00	0.90	8.05	0.11
0.23	0	Calculated	0	00.05	c 11	1 00	0.00	4 02	0 10
Pipe - (29) 0.29	0	CONDUIT Calculated	0	00:07	6.44	1.00	0.88	4.83	0.18
Pipe - (3)	ŭ	CONDUIT	0	00:06	7.38	1.00	2.20	6.35	0.35
0.41	0	Calculated	0	00:20	4.36	1.00	1 52	2 56	0.42
Pipe - (30) 0.46	0	CONDUIT Calculated	U	00.20	4.30	1.00	1.53	3.56	0.43
Pipe - (31)		CONDUIT	0	00:20	6.27	1.00	1.52	5.52	0.28
0.36 Pipe - (33)	0	Calculated CONDUIT	0	00:07	4.88	1.00	2.43	3.56	0.68
0.61	0	Calculated	O	00.07	1.00	1.00	2.15	3.30	0.00
Pipe - (34)	0	CONDUIT	0	00:07	3.55	1.00	1.88	2.54	0.74
0.64 Pipe - (35)	0	Calculated CONDUIT	0	00:07	4.77	1.00	1.88	3.73	0.50
0.50	0	Calculated							
Pipe - (4) 0.65	0	CONDUIT Calculated	0	00:06	6.42	1.00	3.42	4.45	0.77
Pipe - (40)	U	CONDUIT	0	00:05	11.06	1.00	1.27	6.43	0.20
0.30	0	Calculated	0	00.06	5 05	1 00	2 00	2.56	1 00
Pipe - (41) 1.00	2	CONDUIT SURCHARGED	0	00:06	5.27	1.00	3.82	3.56	1.07
Pipe - (43)	_	CONDUIT	0	00:05	6.66	1.00	3.55	4.77	0.74
0.64	0	Calculated	0	00.05	0 27	1 00	F 0.7	F 63	1 00
Pipe - (44) 0.91	0	CONDUIT > CAPACITY	0	00:05	8.37	1.00	5.97	5.63	1.06
Pipe - (45)		CONDUIT	0	00:05	8.03	1.00	5.66	14.86	0.38
0.43	0	Calculated CONDUIT	0	00:05	9.98	1.00	5.86	7.00	0.84
Pipe - (5) 0.70	0	Calculated	U	00.05	2.20	1.00	3.00	7.00	0.04
Pipe - (50)		CONDUIT	0	00:24	12.59	1.00	5.00	30.06	0.17
0.28 Pipe - (51)	0	Calculated CONDUIT	0	00:24	12.87	1.00	5.00	10.15	0.49
0.50	0	Calculated	J						
Pipe - (54)		CONDUIT	0	00:05	7.30	1.00	1.11	8.20	0.14

0.25 Pipe - (55)	0	Calculated CONDUIT	0	00:05	10.40	1.00	1.46	12.12	0.12
0.23	0	Calculated	· ·	00 05	10.10	1.00	1.10		0.11
Pipe - (56)		CONDUIT	0	00:05	6.63	1.00	1.63	6.17	0.26
0.35	0	Calculated							
Pipe - (57)		CONDUIT	0	00:24	11.39	1.00	4.99	26.08	0.19
0.30	0	Calculated							
Pipe - (61)		CONDUIT	0	00:12	6.41	1.00	1.03	5.92	0.17
0.28	0	Calculated							
Pipe - (62)		CONDUIT	0	00:12	3.94	1.00	1.03	3.56	0.29
0.37	0	Calculated							
Pipe - (7)		CONDUIT	0	00:05	8.05	1.00	2.21	7.14	0.31
0.38	0	Calculated							

All links are stable.

WARNING 108: Surcharge elevation defined for Junction EX-18 is below junction maximum elevation. Assumed surcharge elevation equal to maximum elevation.

WARNING 139 : Ponded area defined for on sag Inlet CB-18 is zero. Assumed ponded area equal to 10 ft $^2$  (0.929 m $^2$ ).

WARNING 138: Initial water surface elevation defined for Inlet CB-20 is below catchbasin invert elevation.

Assumed initial water surface elevation equal to catchbasin inlet invert

elevation.

WARNING 138: Initial water surface elevation defined for Inlet CB-4 is below catchbasin invert elevation.

Assumed initial water surface elevation equal to catchbasin inlet invert

elevation.

WARNING 138: Initial water surface elevation defined for Inlet CB-5 is below catchbasin invert elevation.

Assumed initial water surface elevation equal to catchbasin inlet invert

elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB-1\_Overflow is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB10-9\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB11-10\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB12-13\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB17-16\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB2-3\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB3-4\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB4-5\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB6-5\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB7-6\_Gutter is below the storm drain inlet rim elevation.

Assumed the downstream bypass roadway link inlet invert elevation equal to the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB8-7\_Gutter is below the storm drain inlet rim elevation.

WARNING 141: Inlet invert elevation defined for downstream Bypass Roadway Link CB9-8\_Gutter is below the storm drain inlet rim elevation.

WARNING 117 : Conduit outlet invert elevation defined for Conduit CB-1\_Overflow is below downstream node invert elevation.

Assumed conduit outlet invert elevation equal to downstream node invert

elevation.

WARNING 004 : Minimum elevation drop used for Conduit CB-1\_Overflow.

WARNING 005: Minimum slope used for Conduit CB-1\_Overflow.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB10-9\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-9.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB11-10\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-10.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB12-13\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-13.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB17-16\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-16.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB2-3\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-3.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB3-4\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-4.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB4-5\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-5.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB6-5\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-5.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB7-6\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-6.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB8-7\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-7.

WARNING 142: Outlet invert elevation defined for Upstream Roadway Link CB9-8\_Gutter is below the storm drain inlet rim elevation.

Assumed the upstream roadway link outlet invert elevation equal to the storm drain inlet rim elevation. Please verify the "Upstream roadway links" defined for storm drain inlet CB-8W.

WARNING 116 : Conduit inlet invert elevation defined for Conduit Pipe - (14) is below upstream node invert elevation.

Assumed conduit inlet invert elevation equal to upstream node invert elevation. WARNING 116: Conduit inlet invert elevation defined for Conduit Pipe - (50) is below upstream node invert elevation.

Assumed conduit inlet invert elevation equal to upstream node invert elevation. WARNING 116: Conduit inlet invert elevation defined for Conduit Pipe - (55) is below upstream node invert elevation.

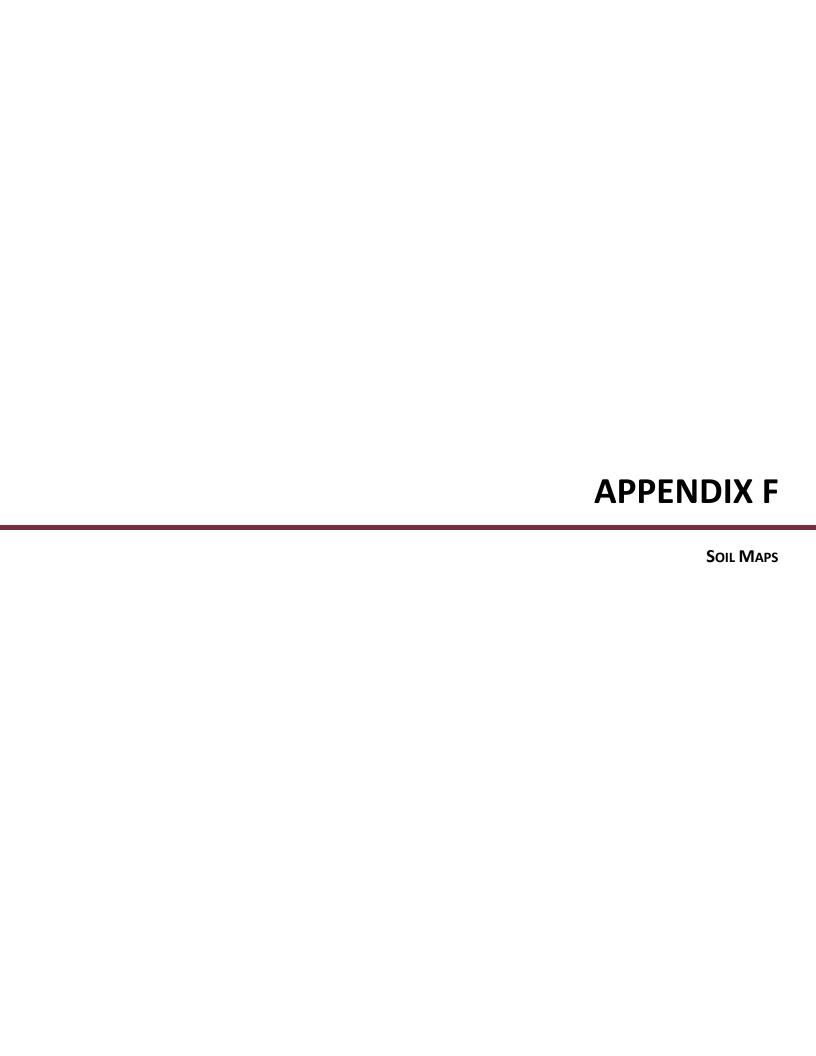
Assumed conduit inlet invert elevation equal to upstream node invert elevation.

Analysis began on: Tue Jan 31 11:11:57 2023 Analysis ended on: Tue Jan 31 11:11:59 2023

Total elapsed time: 00:00:02



Description of Section 1997   Sectio	Test Hole ID:		(See map for location)		Percolati	ion Test:		Groundwater Data		Standing Water Depth, in.	Not observed	Sc
Duste Duste All Description #2 (2011)   Start Physics   Start Physics   Phys	Weather	Cloudy; 45°		Depth of Perc				Sh = Sc - [(Sr/Owr)*(	Owc-Owmax)]	or, Depth Weeping from Pit Face	Not observed	Sc
And Cannesed III 7 A Brough Note - Masses Annual State Product Coron Stead Research and State Product Coron Stead Research and State Product Coron Stead Research and State Product Product Coron Stead Research and State Product Pro	Date:	December 29, 2021		Start Pre-Soak	requirea			 	•	USGS Index Well(s) Number/ID		per USGS
Advanced to Library 1996   Time 49 12   Time	Soil Evaluator		Group, Inc.						•			-
Fine Service of Normal Total Service Street Disneys, Freedrish MAX Time 49 in 1			•					7		9		Owmax
Find the El - 280 Servi Read of an assumed dulump or Plani) Relation (Inter- 4 and 19 Page 1 Mark Rays for wall 18ge in levels for similar lappoprasity (Sie secretaring (Igna 11) 974UE) Sr Productor Adjusted Opph (Fingrore), fit 974UE) Sr Product	Project:	Grove Street Drainage	e, Franklin, MA	Time @ 9-in.				7		Index Well Level		
The file of the	Project / Number	7548		Time @ 6-in.						Max Range for well		Owr
Depth   Soil Flortring daying   Soil Flortring daying   Soil Flortring (ISSIA)   Course Florgring (I				Time 9 - 6in.				Rage in leve	ls for Similar Topo	ography (5% exceedance, Figure 11)		Sr
Soli Horizon (Luyer)   Soli Horizon (Luyer)   Soli Texture (USDA)   Course Fragment % Dry   Structure   Consistence   Redoxmorphic restures (motives)   Other	Top Hole El. = 280.5+/-	(Based on assumed d	atum per Plan)	Rate (min./inch)					Pred	dicted Adjusted Depth (Frimpter), ft	#VALUE!	Sh
Depth Soil Horizon (Layer) (Mansell) Soil Teature (USDA) Volume Structure (MSDA) (USDA) Graved Scotches of Sonoses (MSDA) Graved Graved Sonoses (MSDA) Graved							Test Hole Log					
(inches)  B4* Loam  4-1207 G 2.598 871 Send O 0 G R I Mone observed  Coolbule Stiffing and Topourapity  Landform  Landscape Position Parent Material  Coores Sand  Corres Sand	5 11			C 'I T   (IICDA)		•				5		OII
Ormalia Sumit (SU) Derve Compact Gladial Till Sand Corres Sand Cor	Depth	Soil Horizon (Layer)	(IVIunseII)	Soil Texture (USDA)	V		Structure	Consistence		Redoximorphic Features (mottles)		Other
4-120" C 2-578 8/1 Sand 0 0 0 GR I None abserved    Cooling String and Topography   Position   Parent Molerial   Texture (USDA)   Coarse Fragments   Structure   Common Structure   Comm	(inches)			(USDA)	Gravel				Depth	Color	Percent	
Codogle Setting and Topography  Landform Landscape Position Parent Material Texture (USDA) Coarse Fragments Structure Corbole Zomin to 3' 3' to 10' Angular Blacky (ABC)		Loam										
Landform Landscape Position Parent Material Texture (USDA) Coarse Fragments Structure Consistence Redox %  Drumlin Summit (SU) Dense Compact Glacial Till Coarse Sand Cravel = Cobble = 7mm to 3" 3" to 10" or 25" (ARC)  Till Ridge Shoulder (SH) Loose Ablation Till Sand Sand Sold Screen Shoulder (SH) Loose Ablation Till Sand Sold Sold Screen Shoulder (SH) Loose Ablation Till Sand Sold Sold Screen Shoulder (SH) Loose Ablation Till Sand Sold Sold Sold Sold Sold Sold Sold Sol	4-120"	С	2.5YR 8/1	Sand	0	0	GR	L		None observed		
Landform Landscape Position Parent Material Texture (USDA) Coarse Fragments Structure Consistence Redox %  Drumlin Summit (SU) Dense Compact Glacial Till Coarse Sand Cravel = Cobble = 7mm to 3" 3" to 10" or 25" (ARC)  Till Ridge Shoulder (SH) Loose Ablation Till Sand Sand Sold Screen Shoulder (SH) Loose Ablation Till Sand Sold Sold Screen Shoulder (SH) Loose Ablation Till Sand Sold Sold Screen Shoulder (SH) Loose Ablation Till Sand Sold Sold Sold Sold Sold Sold Sold Sol												
Landform Landscape Position Parent Material Texture (USDA) Coarse Fragments Structure Consistence Redox %  Drumlin Summit (SU) Dense Compact Glacial Till Coarse Sand Cravel = Cobble = 7mm to 3" 3" to 10" or 25" (ARC)  Till Ridge Shoulder (SH) Loose Ablation Till Sand Sand Sold Screen Shoulder (SH) Loose Ablation Till Sand Sold Sold Screen Shoulder (SH) Loose Ablation Till Sand Sold Sold Screen Shoulder (SH) Loose Ablation Till Sand Sold Sold Sold Sold Sold Sold Sold Sol												
Landform Landscape Position Parent Material Texture (USDA) Coarse Fragments Structure Consistence Redox %  Drumlin Summit (SU) Dense Compact Glacial Till Coarse Sand Cravel = Cobble = 7mm to 3" 3" to 10" or 25" (ARC)  Till Ridge Shoulder (SH) Loose Ablation Till Sand Sand Sold Screen Shoulder (SH) Loose Ablation Till Sand Sold Sold Screen Shoulder (SH) Loose Ablation Till Sand Sold Sold Screen Shoulder (SH) Loose Ablation Till Sand Sold Sold Sold Sold Sold Sold Sold Sol												
Landform Landscape Position Parent Material Texture (USDA) Coarse Fragments Structure Consistence Redox %  Drumlin Summit (SU) Dense Compact Glacial Till Coarse Sand Cravel = Cobble = 7mm to 3" 3" to 10" or 25" (ARC)  Till Ridge Shoulder (SH) Loose Ablation Till Sand Sand Sold Screen Shoulder (SH) Loose Ablation Till Sand Sold Sold Screen Shoulder (SH) Loose Ablation Till Sand Sold Sold Screen Shoulder (SH) Loose Ablation Till Sand Sold Sold Sold Sold Sold Sold Sold Sol												
Landform Landscape Position Parent Material Texture (USDA) Coarse Fragments Structure Consistence Redox %  Drumlin Summit (SU) Dense Compact Glacial Till Coarse Sand Cravel = Cobble = 7mm to 3" 3" to 10" or 25" (ARC)  Till Ridge Shoulder (SH) Loose Ablation Till Sand Sand Sold Screen Shoulder (SH) Loose Ablation Till Sand Sold Sold Screen Shoulder (SH) Loose Ablation Till Sand Sold Sold Screen Shoulder (SH) Loose Ablation Till Sand Sold Sold Sold Sold Sold Sold Sold Sol	Geolo	gic Setting and Topogr	aphy			Textura	al and Structure				Photo(s)	
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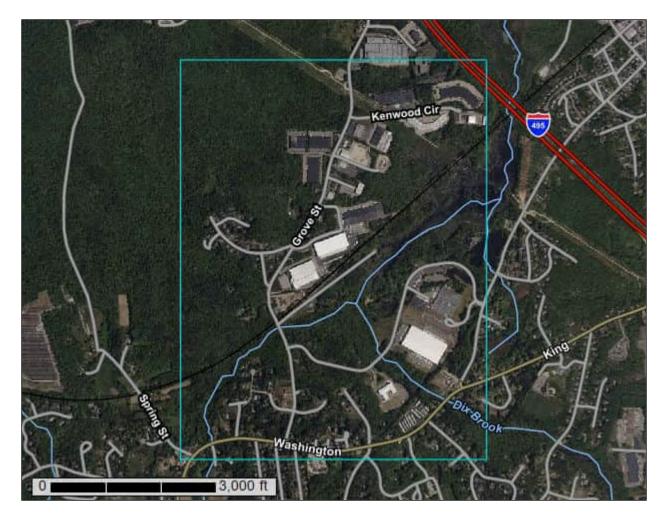




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Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

## Custom Soil Resource Report for Norfolk and Suffolk Counties, Massachusetts



## **Preface**

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2 053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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## **How Soil Surveys Are Made**

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

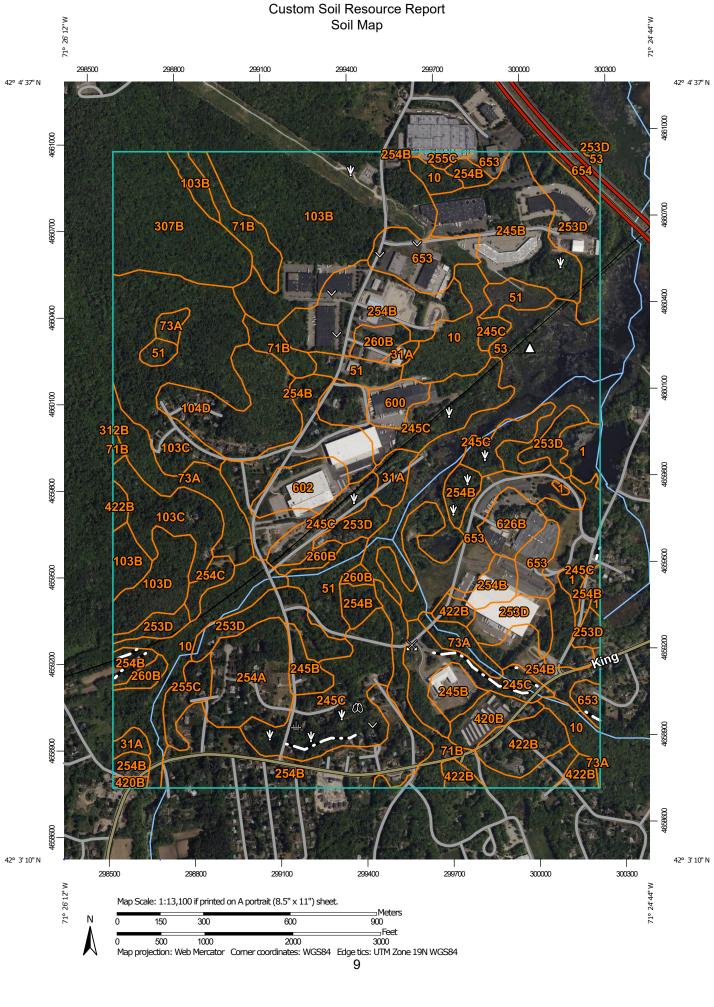
Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

## Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



#### MAP LEGEND

#### Area of Interest (AOI)

Area of Interest (AOI)

#### Soils

Soil Map Unit Polygons

Soil Map Unit Lines

Soil Map Unit Points

#### **Special Point Features**

 $\odot$ 

Blowout

Borrow Pit

Clay Spot

**Closed Depression** 

Gravel Pit

Gravelly Spot

Landfill Lava Flow

Marsh or swamp

Mine or Quarry

Miscellaneous Water Perennial Water

Rock Outcrop

Saline Spot

Sandy Spot

Severely Eroded Spot

Sinkhole

Slide or Slip

Sodic Spot

Spoil Area Stony Spot



Very Stony Spot



Wet Spot Other



Special Line Features

#### **Water Features**

Streams and Canals

#### Transportation

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Rails

Interstate Highways

**US Routes** 

Major Roads

 $\sim$ 

Local Roads

#### Background

Aerial Photography

#### MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:25.000.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Norfolk and Suffolk Counties, Massachusetts Survey Area Data: Version 18, Sep 9, 2022

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: May 22, 2022—Jun 5, 2022

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

## **Map Unit Legend**

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
1	Water	8.7	0.9%
10	Scarboro and Birdsall soils, 0 to 3 percent slopes	48.0	5.2%
31A	Walpole sandy loam, 0 to 3 percent slopes	8.6	0.9%
51	Swansea muck, 0 to 1 percent slopes	24.2	2.6%
53	Freetown muck, ponded, 0 to 1 percent slopes	57.0	6.2%
71B	Ridgebury fine sandy loam, 3 to 8 percent slopes, extremely stony	35.0	3.8%
73A	Whitman fine sandy loam, 0 to 3 percent slopes, extremely stony	24.5	2.6%
103B	Charlton-Hollis-Rock outcrop complex, 3 to 8 percent slopes	76.6	8.3%
103C	Charlton-Hollis-Rock outcrop complex, 8 to 15 percent slopes	67.9	7.3%
103D	Charlton-Hollis-Rock outcrop complex, 15 to 25 percent slopes	13.8	1.5%
104D	Hollis-Rock outcrop-Charlton complex, 15 to 35 percent slopes	27.0	2.9%
245B	Hinckley loamy sand, 3 to 8 percent slopes	45.4	4.9%
245C	Hinckley loamy sand, 8 to 15 percent slopes	107.2	11.6%
253D	Hinckley loamy sand, 15 to 35 percent slopes	55.7	6.0%
254A	Merrimac fine sandy loam, 0 to 3 percent slopes	22.8	2.5%
254B	Merrimac fine sandy loam, 3 to 8 percent slopes	128.4	13.9%
254C	Merrimac fine sandy loam, 8 to 15 percent slopes	3.9	0.4%
255C	Windsor loamy sand, 8 to 15 percent slopes	8.4	0.9%
260B	Sudbury fine sandy loam, 2 to 8 percent slopes	11.3	1.2%
307B	Paxton fine sandy loam, 0 to 8 percent slopes, extremely stony	37.6	4.1%

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI		
312B	Woodbridge fine sandy loam, 0 to 8 percent slopes, extremely stony	0.0	0.0%		
420B	Canton fine sandy loam, 3 to 8 percent slopes	9.3	1.0%		
422B	Canton fine sandy loam, 0 to 8 percent slopes, extremely stony	21.5	2.3%		
600	Pits, sand and gravel	6.2	0.7%		
602	Urban land, 0 to 15 percent slopes	11.3	1.2%		
626B	Merrimac-Urban land complex, 0 to 8 percent slopes	8.8	1.0%		
653	Udorthents, sandy	53.8	5.8%		
654	Udorthents, loamy	3.6	0.4%		
Totals for Area of Interest		926.9	100.0%		

## **Map Unit Descriptions**

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it

was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

## Norfolk and Suffolk Counties, Massachusetts

## 1—Water

## **Map Unit Setting**

National map unit symbol: vkyp

Mean annual precipitation: 32 to 50 inches Mean annual air temperature: 45 to 50 degrees F

Frost-free period: 120 to 200 days

Farmland classification: Not prime farmland

## **Map Unit Composition**

Water: 100 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

## 10—Scarboro and Birdsall soils, 0 to 3 percent slopes

## **Map Unit Setting**

National map unit symbol: vkxw

Elevation: 0 to 2,100 feet

Mean annual precipitation: 45 to 54 inches Mean annual air temperature: 43 to 54 degrees F

Frost-free period: 145 to 240 days

Farmland classification: Not prime farmland

## **Map Unit Composition**

Scarboro and similar soils: 65 percent Birdsall and similar soils: 25 percent Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

## **Description of Scarboro**

## Setting

Landform: Terraces

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Loose sandy glaciofluvial deposits

#### Typical profile

H1 - 0 to 9 inches: mucky fine sandy loam

H2 - 9 to 60 inches: stratified loamy fine sand to gravelly coarse sand

## Properties and qualities

Slope: 0 to 3 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Very poorly drained

Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat): High to very high (6.00

to 20.00 in/hr)

Depth to water table: About 0 inches

Frequency of flooding: None Frequency of ponding: Frequent

Available water supply, 0 to 60 inches: Low (about 5.1 inches)

## Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 5w

Hydrologic Soil Group: A/D

Ecological site: F144AY031MA - Very Wet Outwash

Hydric soil rating: Yes

## **Description of Birdsall**

## Setting

Landform: Terraces

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Soft coarse-silty glaciolacustrine deposits

## **Typical profile**

H1 - 0 to 8 inches: very fine sandy loam H2 - 8 to 16 inches: very fine sandy loam

H3 - 16 to 60 inches: silt loam

## **Properties and qualities**

Slope: 0 to 3 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Very poorly drained

Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to

moderately high (0.06 to 0.20 in/hr) Depth to water table: About 0 inches

Frequency of flooding: None Frequency of ponding: Frequent

Available water supply, 0 to 60 inches: Very high (about 12.8 inches)

## Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 5w

Hvdrologic Soil Group: C/D

Ecological site: F144AY031MA - Very Wet Outwash

Hydric soil rating: Yes

## **Minor Components**

## **Swansea**

Percent of map unit: 5 percent

Landform: Bogs Hydric soil rating: Yes

## Raynham

Percent of map unit: 3 percent Landform: Depressions Hydric soil rating: Yes

## Walpole

Percent of map unit: 2 percent

Landform: Terraces
Hydric soil rating: Yes

## 31A—Walpole sandy loam, 0 to 3 percent slopes

## **Map Unit Setting**

National map unit symbol: 2svkl

Elevation: 0 to 1,020 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 250 days

Farmland classification: Not prime farmland

## **Map Unit Composition**

Walpole and similar soils: 80 percent Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

## **Description of Walpole**

## Setting

Landform: Depressions, outwash plains, outwash terraces, depressions, deltas

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread, dip, talf

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Sandy glaciofluvial deposits derived from igneous, metamorphic

and sedimentary rock

#### Typical profile

Oe - 0 to 1 inches: mucky peat
A - 1 to 7 inches: sandy loam
Bg - 7 to 21 inches: sandy loam

BC - 21 to 25 inches: gravelly sandy loam C - 25 to 65 inches: very gravelly sand

#### **Properties and qualities**

Slope: 0 to 3 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: About 0 to 4 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Moderate (about 6.4 inches)

## Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4w

Hydrologic Soil Group: B/D

Ecological site: F144AY028MA - Wet Outwash

Hydric soil rating: Yes

## **Minor Components**

#### Scarboro

Percent of map unit: 10 percent

Landform: Outwash plains, deltas, outwash terraces Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread, dip

Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

## Sudbury

Percent of map unit: 10 percent

Landform: Outwash plains, deltas, terraces Landform position (two-dimensional): Footslope Landform position (three-dimensional): Tread, dip

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

## 51—Swansea muck, 0 to 1 percent slopes

## **Map Unit Setting**

National map unit symbol: 2trl2 Elevation: 0 to 1,140 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

## **Map Unit Composition**

Swansea and similar soils: 80 percent

Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

## **Description of Swansea**

#### Setting

Landform: Bogs, swamps

Landform position (three-dimensional): Dip

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Highly decomposed organic material over loose sandy and gravelly glaciofluvial deposits

## **Typical profile**

Oa1 - 0 to 24 inches: muck
Oa2 - 24 to 34 inches: muck
Cg - 34 to 79 inches: coarse sand

## **Properties and qualities**

Slope: 0 to 1 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Very poorly drained

Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: About 0 to 6 inches

Frequency of flooding: Rare Frequency of ponding: Frequent

Available water supply, 0 to 60 inches: Very high (about 16.5 inches)

## Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8w

Hydrologic Soil Group: B/D

Ecological site: F144AY043MA - Acidic Organic Wetlands

Hydric soil rating: Yes

## **Minor Components**

## Freetown

Percent of map unit: 10 percent

Landform: Bogs, swamps

Landform position (three-dimensional): Dip

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

## Whitman

Percent of map unit: 5 percent

Landform: Drainageways, depressions

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

## Scarboro

Percent of map unit: 5 percent

Landform: Drainageways, depressions

Landform position (two-dimensional): Toeslope

Landform position (three-dimensional): Base slope, tread, dip

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

## 53—Freetown muck, ponded, 0 to 1 percent slopes

## **Map Unit Setting**

National map unit symbol: 2t2qc

Elevation: 0 to 1,140 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

## **Map Unit Composition**

Freetown, ponded, and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

## **Description of Freetown, Ponded**

## Setting

Landform: Kettles, marshes, depressions, depressions, bogs, swamps

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread, dip

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Highly decomposed organic material

## Typical profile

Oe - 0 to 2 inches: mucky peat Oa - 2 to 79 inches: muck

## Properties and qualities

Slope: 0 to 1 percent

Surface area covered with cobbles, stones or boulders: 0.0 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Very poorly drained

Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: About 0 to 6 inches

Frequency of flooding: Rare Frequency of ponding: Frequent

Available water supply, 0 to 60 inches: Very high (about 19.2 inches)

## Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 5w

Hydrologic Soil Group: B/D

Ecological site: F144AY043MA - Acidic Organic Wetlands

Hydric soil rating: Yes

## **Minor Components**

#### Scarboro

Percent of map unit: 5 percent

Landform: Drainageways, depressions

Landform position (two-dimensional): Toeslope

Landform position (three-dimensional): Base slope, tread, dip

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

## Whitman, ponded

Percent of map unit: 5 percent

Landform: Depressions on ground moraines
Landform position (two-dimensional): Toeslope
Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

## Swansea, ponded

Percent of map unit: 5 percent

Landform: Bogs, swamps, marshes, depressions, depressions, kettles

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread, dip

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

## 71B—Ridgebury fine sandy loam, 3 to 8 percent slopes, extremely stony

## Map Unit Setting

National map unit symbol: 2w69c

Elevation: 0 to 1,290 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

## **Map Unit Composition**

Ridgebury, extremely stony, and similar soils: 80 percent

Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

## **Description of Ridgebury, Extremely Stony**

## Setting

 $\textit{Landform:} \ \mathsf{Drumlins}, \ \mathsf{depressions}, \ \mathsf{ground} \ \mathsf{moraines}, \ \mathsf{hills}, \ \mathsf{drainageways}$ 

Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Head slope, base slope

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Coarse-loamy lodgment till derived from gneiss, granite, and/or

schist

## Typical profile

Oe - 0 to 1 inches: moderately decomposed plant material

A - 1 to 6 inches: fine sandy loam Bw - 6 to 10 inches: sandy loam

Bg - 10 to 19 inches: gravelly sandy loam Cd - 19 to 66 inches: gravelly sandy loam

## Properties and qualities

Slope: 3 to 8 percent

Surface area covered with cobbles, stones or boulders: 9.0 percent Depth to restrictive feature: 15 to 35 inches to densic material

Drainage class: Poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.14 in/hr)

Depth to water table: About 0 to 6 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 3.0 inches)

## Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: D

Ecological site: F144AY009CT - Wet Till Depressions

Hydric soil rating: Yes

## **Minor Components**

## Woodbridge, extremely stony

Percent of map unit: 10 percent

Landform: Ground moraines, hills, drumlins

Landform position (two-dimensional): Summit, backslope, footslope

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

#### Whitman, extremely stony

Percent of map unit: 8 percent Landform: Depressions Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

## Paxton, extremely stony

Percent of map unit: 2 percent

Landform: Ground moraines, hills, drumlins

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Convex, linear

Across-slope shape: Linear, convex

Hydric soil rating: No

## 73A—Whitman fine sandy loam, 0 to 3 percent slopes, extremely stony

## **Map Unit Setting**

National map unit symbol: 2w695

Elevation: 0 to 1,580 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

## **Map Unit Composition**

Whitman, extremely stony, and similar soils: 81 percent

Minor components: 19 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

## **Description of Whitman, Extremely Stony**

## Setting

Landform: Drumlins, ground moraines, hills, drainageways, depressions

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave Across-slope shape: Concave

Parent material: Coarse-loamy lodgment till derived from gneiss, granite, and/or

schist

## Typical profile

Oi - 0 to 1 inches: peat

A - 1 to 10 inches: fine sandy loam

*Bg - 10 to 17 inches:* gravelly fine sandy loam *Cdg - 17 to 61 inches:* fine sandy loam

## Properties and qualities

Slope: 0 to 3 percent

Surface area covered with cobbles, stones or boulders: 9.0 percent Depth to restrictive feature: 7 to 38 inches to densic material

Drainage class: Very poorly drained

Runoff class: Negligible

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.14 in/hr)

Depth to water table: About 0 to 6 inches

Frequency of flooding: None Frequency of ponding: Frequent

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 3.0 inches)

## Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hvdrologic Soil Group: D

Ecological site: F144AY041MA - Very Wet Till Depressions

Hydric soil rating: Yes

## **Minor Components**

## Ridgebury, extremely stony

Percent of map unit: 10 percent

Landform: Drumlins, depressions, ground moraines, hills, drainageways

Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Head slope, base slope

Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

## Scarboro

Percent of map unit: 5 percent

Landform: Drainageways, depressions, outwash terraces, outwash deltas

Landform position (three-dimensional): Tread

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

#### **Swansea**

Percent of map unit: 3 percent Landform: Marshes, bogs, swamps Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

## Woodbridge, extremely stony

Percent of map unit: 1 percent

Landform: Ground moraines, hills, drumlins

Landform position (two-dimensional): Summit, backslope, footslope

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

## 103B—Charlton-Hollis-Rock outcrop complex, 3 to 8 percent slopes

## Map Unit Setting

National map unit symbol: vktd Elevation: 0 to 480 feet

Mean annual precipitation: 32 to 54 inches Mean annual air temperature: 43 to 54 degrees F

Frost-free period: 120 to 240 days

Farmland classification: Not prime farmland

## **Map Unit Composition**

Charlton and similar soils: 40 percent Hollis and similar soils: 25 percent

Rock outcrop: 20 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

## **Description of Charlton**

## Setting

Landform: Hills

Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Friable coarse-loamy ablation till derived from granite

## **Typical profile**

H1 - 0 to 6 inches: fine sandy loam H2 - 6 to 36 inches: fine sandy loam H3 - 36 to 60 inches: fine sandy loam

## Properties and qualities

Slope: 3 to 8 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.60 to 6.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 7.8 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: A

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

## **Description of Hollis**

#### Setting

Landform: Hills

Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Shallow, friable loamy ablation till derived from igneous rock

#### Typical profile

H1 - 0 to 3 inches: fine sandy loam

H2 - 3 to 14 inches: gravelly fine sandy loam H3 - 14 to 18 inches: unweathered bedrock

## **Properties and qualities**

Slope: 3 to 8 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: 10 to 20 inches to lithic bedrock

Drainage class: Well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.14 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Very low (about 1.8 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: D

Ecological site: F144AY033MA - Shallow Dry Till Uplands

Hydric soil rating: No

## **Description of Rock Outcrop**

## Setting

Parent material: Igneous and metamorphic rock

## **Properties and qualities**

Slope: 3 to 8 percent

Depth to restrictive feature: 0 inches to lithic bedrock

## Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8s

Hydric soil rating: Unranked

## **Minor Components**

## Canton

Percent of map unit: 7 percent

Hydric soil rating: No

#### Chatfield

Percent of map unit: 5 percent

Hydric soil rating: No

#### **Scituate**

Percent of map unit: 2 percent

Hydric soil rating: No

## Whitman

Percent of map unit: 1 percent

Landform: Depressions Hydric soil rating: Yes

## 103C—Charlton-Hollis-Rock outcrop complex, 8 to 15 percent slopes

## Map Unit Setting

National map unit symbol: 2wzp1

Elevation: 0 to 1,390 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

## **Map Unit Composition**

Charlton, extremely stony, and similar soils: 50 percent Hollis, extremely stony, and similar soils: 20 percent

Rock outcrop: 10 percent Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

## **Description of Charlton, Extremely Stony**

## Setting

Landform: Ridges, hills

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Convex, linear Across-slope shape: Convex

Parent material: Coarse-loamy melt-out till derived from granite, gneiss, and/or

schist

## Typical profile

Oe - 0 to 2 inches: moderately decomposed plant material

A - 2 to 4 inches: fine sandy loam

Bw - 4 to 27 inches: gravelly fine sandy loam C - 27 to 65 inches: gravelly fine sandy loam

## **Properties and qualities**

Slope: 8 to 15 percent

Surface area covered with cobbles, stones or boulders: 9.0 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Moderate (about 8.7 inches)

## Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

## **Description of Hollis, Extremely Stony**

## Setting

Landform: Ridges, hills

Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Nose slope, side slope, crest

Down-slope shape: Convex

Across-slope shape: Linear, convex

Parent material: Coarse-loamy melt-out till derived from granite, gneiss, and/or

schist

## **Typical profile**

Oi - 0 to 2 inches: slightly decomposed plant material

A - 2 to 7 inches: gravelly fine sandy loam Bw - 7 to 16 inches: gravelly fine sandy loam

2R - 16 to 26 inches: bedrock

## **Properties and qualities**

Slope: 8 to 15 percent

Surface area covered with cobbles, stones or boulders: 9.0 percent

Depth to restrictive feature: 8 to 23 inches to lithic bedrock

Drainage class: Somewhat excessively drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Very low (0.00 to 0.00

in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Very low (about 2.7 inches)

## Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: D

Ecological site: F144AY033MA - Shallow Dry Till Uplands

Hydric soil rating: No

## **Description of Rock Outcrop**

## Setting

Landform: Ridges, hills

Parent material: Igneous and metamorphic rock

## Typical profile

R - 0 to 79 inches: bedrock

## Properties and qualities

Slope: 8 to 15 percent

Depth to restrictive feature: 0 inches to lithic bedrock

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Very low (0.00 to 0.00

in/hr)

Available water supply, 0 to 60 inches: Very low (about 0.0 inches)

## Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8

Hydrologic Soil Group: D Hydric soil rating: No

## **Minor Components**

## Woodbridge, extremely stony

Percent of map unit: 8 percent

Landform: Ground moraines, hills, drumlins

Landform position (two-dimensional): Backslope, footslope

Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Linear Hydric soil rating: No

## Chatfield, extremely stony

Percent of map unit: 5 percent

Landform: Ridges, hills

Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Nose slope, side slope, crest

Down-slope shape: Convex

Across-slope shape: Linear, convex

Hydric soil rating: No

## Canton, extremely stony

Percent of map unit: 5 percent Landform: Moraines, hills, ridges

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Convex, linear Across-slope shape: Convex

Hydric soil rating: No

## Ridgebury, extremely stony

Percent of map unit: 2 percent

Landform: Hills, drainageways, drumlins, depressions, ground moraines

Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Head slope, base slope

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

## 103D—Charlton-Hollis-Rock outcrop complex, 15 to 25 percent slopes

## **Map Unit Setting**

National map unit symbol: vktk

Elevation: 0 to 490 feet

Mean annual precipitation: 32 to 54 inches Mean annual air temperature: 43 to 54 degrees F

Frost-free period: 120 to 240 days

Farmland classification: Not prime farmland

## **Map Unit Composition**

Charlton and similar soils: 35 percent Hollis and similar soils: 25 percent

Rock outcrop: 20 percent Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

## **Description of Charlton**

## Setting

Landform: Hills

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Linear Across-slope shape: Convex

Parent material: Friable coarse-loamy ablation till derived from granite

## Typical profile

H1 - 0 to 6 inches: fine sandy loam H2 - 6 to 36 inches: fine sandy loam H3 - 36 to 60 inches: fine sandy loam

## Properties and qualities

Slope: 15 to 25 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.60 to 6.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 7.8 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: A

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

## **Description of Hollis**

#### Settina

Landform: Hills

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Linear Across-slope shape: Convex

Parent material: Shallow, friable loamy ablation till derived from igneous rock

## **Typical profile**

H1 - 0 to 3 inches: fine sandy loam

H2 - 3 to 14 inches: gravelly fine sandy loam H3 - 14 to 18 inches: unweathered bedrock

## **Properties and qualities**

Slope: 15 to 25 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: 10 to 20 inches to lithic bedrock

Drainage class: Well drained Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.14 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Very low (about 1.8 inches)

## Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: D

Ecological site: F144AY033MA - Shallow Dry Till Uplands

Hydric soil rating: No

## **Description of Rock Outcrop**

#### Settina

Parent material: Igneous and metamorphic rock

#### **Properties and qualities**

Slope: 15 to 25 percent

Depth to restrictive feature: 0 inches to lithic bedrock

## Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8s

Hydric soil rating: Unranked

## **Minor Components**

## Chatfield

Percent of map unit: 8 percent

Hydric soil rating: No

#### Canton

Percent of map unit: 8 percent

Hydric soil rating: No

## **Montauk**

Percent of map unit: 4 percent

Hydric soil rating: No

## 104D—Hollis-Rock outcrop-Charlton complex, 15 to 35 percent slopes

## **Map Unit Setting**

National map unit symbol: vkvh

Elevation: 20 to 610 feet

Mean annual precipitation: 32 to 54 inches
Mean annual air temperature: 43 to 54 degrees F

Frost-free period: 120 to 240 days

Farmland classification: Not prime farmland

## **Map Unit Composition**

Hollis and similar soils: 35 percent

Rock outcrop: 30 percent

Charlton and similar soils: 25 percent Minor components: 10 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

## **Description of Hollis**

#### Setting

Landform: Hills

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Linear Across-slope shape: Convex

Parent material: Shallow, friable loamy ablation till derived from igneous and

metamorphic rock

## Typical profile

H1 - 0 to 3 inches: fine sandy loam

H2 - 3 to 14 inches: gravelly fine sandy loam H3 - 14 to 18 inches: unweathered bedrock

## Properties and qualities

Slope: 15 to 35 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: 10 to 20 inches to lithic bedrock

Drainage class: Well drained Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.14 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Very low (about 1.8 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: D

Ecological site: F144AY033MA - Shallow Dry Till Uplands

Hydric soil rating: No

## **Description of Rock Outcrop**

## Setting

Parent material: Igneous and metamorphic rock

## **Properties and qualities**

Slope: 15 to 35 percent

Depth to restrictive feature: 0 inches to lithic bedrock

## Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8s

Hydric soil rating: Unranked

## **Description of Charlton**

## Setting

Landform: Hills

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Linear Across-slope shape: Convex

Parent material: Friable coarse-loamy ablation till derived from granite

## Typical profile

H1 - 0 to 6 inches: fine sandy loam H2 - 6 to 36 inches: fine sandy loam H3 - 36 to 60 inches: fine sandy loam

#### Properties and qualities

Slope: 15 to 35 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Well drained Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.60 to 6.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Moderate (about 7.8 inches)

## Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: A

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

## **Minor Components**

#### Chatfield

Percent of map unit: 5 percent Hydric soil rating: No

#### Canton

Percent of map unit: 5 percent

Hydric soil rating: No

## 245B—Hinckley loamy sand, 3 to 8 percent slopes

## **Map Unit Setting**

National map unit symbol: 2svm8

Elevation: 0 to 1,430 feet

Mean annual precipitation: 36 to 53 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 250 days

Farmland classification: Farmland of statewide importance

## **Map Unit Composition**

Hinckley and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

## **Description of Hinckley**

## Setting

Landform: Outwash deltas, outwash terraces, kames, kame terraces, moraines, eskers, outwash plains

Landform position (two-dimensional): Summit, shoulder, backslope, footslope Landform position (three-dimensional): Nose slope, side slope, base slope, crest, riser, tread

Down-slope shape: Concave, convex, linear Across-slope shape: Convex, linear, concave

Parent material: Sandy and gravelly glaciofluvial deposits derived from gneiss

and/or granite and/or schist

## **Typical profile**

Oe - 0 to 1 inches: moderately decomposed plant material

A - 1 to 8 inches: loamy sand

Bw1 - 8 to 11 inches: gravelly loamy sand Bw2 - 11 to 16 inches: gravelly loamy sand

BC - 16 to 19 inches: very gravelly loamy sand C - 19 to 65 inches: very gravelly sand

## **Properties and qualities**

Slope: 3 to 8 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Excessively drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very

high (1.42 to 99.90 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Very low (about 3.0 inches)

## Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3s

Hydrologic Soil Group: A

Ecological site: F144AY022MA - Dry Outwash

Hydric soil rating: No

## **Minor Components**

#### Windsor

Percent of map unit: 8 percent

Landform: Outwash deltas, outwash terraces, moraines, eskers, kames, outwash plains, kame terraces

Landform position (two-dimensional): Summit, shoulder, backslope, footslope
Landform position (three-dimensional): Nose slope, side slope, base slope, crest.

riser, tread

Down-slope shape: Concave, convex, linear Across-slope shape: Convex, linear, concave

Hydric soil rating: No

#### Sudbury

Percent of map unit: 5 percent

Landform: Outwash deltas, outwash terraces, moraines, outwash plains, kame terraces

Landform position (two-dimensional): Backslope, footslope

Landform position (three-dimensional): Head slope, side slope, base slope, tread

Down-slope shape: Concave, linear Across-slope shape: Concave, linear

Hydric soil rating: No

## **Agawam**

Percent of map unit: 2 percent

Landform: Outwash deltas, outwash terraces, moraines, eskers, kames, outwash

plains, kame terraces

Landform position (two-dimensional): Summit, shoulder, backslope, footslope Landform position (three-dimensional): Nose slope, side slope, base slope, crest, riser, tread

Down-slope shape: Concave, convex, linear Across-slope shape: Convex, linear, concave

Hydric soil rating: No

## 245C—Hinckley loamy sand, 8 to 15 percent slopes

## **Map Unit Setting**

National map unit symbol: 2svm9

Elevation: 0 to 1,480 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Farmland of statewide importance

## **Map Unit Composition**

Hinckley and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

## **Description of Hinckley**

## Setting

Landform: Outwash deltas, outwash terraces, moraines, eskers, kames, outwash plains, kame terraces

Landform position (two-dimensional): Shoulder, backslope, footslope, toeslope Landform position (three-dimensional): Head slope, nose slope, side slope, crest, riser

Down-slope shape: Concave, convex, linear Across-slope shape: Convex, linear, concave

Parent material: Sandy and gravelly glaciofluvial deposits derived from gneiss and/or granite and/or schist

## **Typical profile**

Oe - 0 to 1 inches: moderately decomposed plant material

A - 1 to 8 inches: loamy sand

Bw1 - 8 to 11 inches: gravelly loamy sand Bw2 - 11 to 16 inches: gravelly loamy sand BC - 16 to 19 inches: very gravelly loamy sand

C - 19 to 65 inches: very gravelly sand

## Properties and qualities

Slope: 8 to 15 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Excessively drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very

high (1.42 to 99.90 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 3.1 inches)

## Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: A

Ecological site: F144AY022MA - Dry Outwash

Hydric soil rating: No

## **Minor Components**

#### Windsor

Percent of map unit: 5 percent

Landform: Moraines, eskers, kames, outwash deltas, outwash terraces, outwash plains. kame terraces

plains, kame terraces

Landform position (two-dimensional): Shoulder, backslope, footslope, toeslope Landform position (three-dimensional): Head slope, nose slope, side slope, crest,

riser

Down-slope shape: Concave, convex, linear Across-slope shape: Convex, linear, concave

Hydric soil rating: No

## Sudbury

Percent of map unit: 5 percent

Landform: Outwash deltas, moraines, outwash plains, kame terraces, outwash

terraces

Landform position (two-dimensional): Backslope, footslope Landform position (three-dimensional): Base slope, tread

Down-slope shape: Concave, linear Across-slope shape: Concave, linear

Hydric soil rating: No

#### Merrimac

Percent of map unit: 5 percent

Landform: Kames, outwash plains, outwash terraces, moraines, eskers

Landform position (two-dimensional): Shoulder, backslope, footslope, toeslope

Landform position (three-dimensional): Head slope, nose slope, side slope, crest,
riser

Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

## 253D—Hinckley loamy sand, 15 to 35 percent slopes

## **Map Unit Setting**

National map unit symbol: 2svmd

Elevation: 0 to 860 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

## **Map Unit Composition**

Hinckley and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

## **Description of Hinckley**

## Setting

Landform: Outwash deltas, outwash terraces, moraines, eskers, kames, outwash plains, kame terraces

Landform position (two-dimensional): Backslope

Landform position (three-dimensional): Head slope, nose slope, side slope, crest, riser

Down-slope shape: Concave, convex, linear Across-slope shape: Convex, linear, concave

Parent material: Sandy and gravelly glaciofluvial deposits derived from gneiss and/or granite and/or schist

## Typical profile

Oe - 0 to 1 inches: moderately decomposed plant material

A - 1 to 8 inches: loamy sand

Bw1 - 8 to 11 inches: gravelly loamy sand Bw2 - 11 to 16 inches: gravelly loamy sand BC - 16 to 19 inches: very gravelly loamy sand C - 19 to 65 inches: very gravelly sand

## Properties and qualities

Slope: 15 to 35 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Excessively drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very

high (1.42 to 99.90 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 3.1 inches)

## Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6e

Hydrologic Soil Group: A

Ecological site: F144AY022MA - Dry Outwash

Hydric soil rating: No

## **Minor Components**

#### Windsor

Percent of map unit: 10 percent

Landform: Moraines, eskers, kames, outwash deltas, outwash terraces, outwash plains, kame terraces

Landform position (two-dimensional): Backslope

Landform position (three-dimensional): Head slope, nose slope, side slope, crest,

rise

Down-slope shape: Concave, convex, linear

Across-slope shape: Convex, linear, concave

Hydric soil rating: No

#### Merrimac

Percent of map unit: 3 percent

Landform: Kame terraces, outwash plains, outwash terraces, moraines, eskers,

Landform position (two-dimensional): Backslope

Landform position (three-dimensional): Head slope, nose slope, side slope, crest,

riser

Down-slope shape: Concave, convex, linear Across-slope shape: Convex, linear, concave

Hydric soil rating: No

#### Sudbury

Percent of map unit: 2 percent

 ${\it Land form:} \ {\it Outwash \ deltas}, \ {\it outwash \ plains}, \ {\it kame \ terraces}, \ {\it outwash \ terraces},$ 

moraines

Landform position (two-dimensional): Backslope, footslope, toeslope

Landform position (three-dimensional): Base slope, tread

Down-slope shape: Concave, linear Across-slope shape: Concave, linear

Hydric soil rating: No

#### 254A—Merrimac fine sandy loam, 0 to 3 percent slopes

#### **Map Unit Setting**

National map unit symbol: 2tygr

Elevation: 0 to 1,100 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: All areas are prime farmland

#### **Map Unit Composition**

Merrimac and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Merrimac**

#### Setting

Landform: Outwash plains, outwash terraces, moraines, eskers, kames Landform position (two-dimensional): Summit, shoulder, backslope, footslope

Landform position (three-dimensional): Side slope, crest, riser, tread

Davis alare along Course

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Loamy glaciofluvial deposits derived from granite, schist, and gneiss over sandy and gravelly glaciofluvial deposits derived from granite, schist, and gneiss

#### Typical profile

Ap - 0 to 10 inches: fine sandy loam Bw1 - 10 to 22 inches: fine sandy loam

Bw2 - 22 to 26 inches: stratified gravel to gravelly loamy sand 2C - 26 to 65 inches: stratified gravel to very gravelly sand

#### **Properties and qualities**

Slope: 0 to 3 percent

Depth to restrictive feature: More than 80 inches Drainage class: Somewhat excessively drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very

high (1.42 to 99.90 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum content: 2 percent Maximum salinity: Nonsaline (0.0 to 1.4 mmhos/cm)

Sodium adsorption ratio, maximum: 1.0

Available water supply, 0 to 60 inches: Low (about 4.6 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2s

Hydrologic Soil Group: A

Ecological site: F145XY008MA - Dry Outwash

Hydric soil rating: No

#### **Minor Components**

#### Sudbury

Percent of map unit: 5 percent

Landform: Deltas, terraces, outwash plains
Landform position (two-dimensional): Footslope
Landform position (three-dimensional): Tread, dip

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

#### Hinckley

Percent of map unit: 5 percent

Landform: Deltas, kames, eskers, outwash plains

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Head slope, nose slope, side slope, crest,

rise

Down-slope shape: Convex

Across-slope shape: Convex, linear

Hydric soil rating: No

#### **Agawam**

Percent of map unit: 3 percent

Landform: Stream terraces, outwash terraces, outwash plains, moraines, eskers,

kames

Landform position (three-dimensional): Rise

Down-slope shape: Convex Across-slope shape: Convex

Hydric soil rating: No

#### Windsor

Percent of map unit: 2 percent

Landform: Dunes, deltas, outwash terraces, outwash plains

Landform position (two-dimensional): Summit Landform position (three-dimensional): Tread, riser

Down-slope shape: Convex, linear Across-slope shape: Convex, linear

Hydric soil rating: No

#### 254B—Merrimac fine sandy loam, 3 to 8 percent slopes

#### **Map Unit Setting**

National map unit symbol: 2tyqs

Elevation: 0 to 1,290 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: All areas are prime farmland

#### **Map Unit Composition**

Merrimac and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Merrimac**

#### Setting

Landform: Outwash plains, outwash terraces, moraines, eskers, kames Landform position (two-dimensional): Summit, shoulder, backslope, footslope

Landform position (three-dimensional): Side slope, crest, riser, tread

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Loamy glaciofluvial deposits derived from granite, schist, and gneiss over sandy and gravelly glaciofluvial deposits derived from granite,

schist, and gneiss

#### **Typical profile**

Ap - 0 to 10 inches: fine sandy loam Bw1 - 10 to 22 inches: fine sandy loam

Bw2 - 22 to 26 inches: stratified gravel to gravelly loamy sand 2C - 26 to 65 inches: stratified gravel to very gravelly sand

#### Properties and qualities

Slope: 3 to 8 percent

Depth to restrictive feature: More than 80 inches Drainage class: Somewhat excessively drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very

high (1.42 to 99.90 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum content: 2 percent Maximum salinity: Nonsaline (0.0 to 1.4 mmhos/cm)

Sodium adsorption ratio, maximum: 1.0

Available water supply, 0 to 60 inches: Low (about 4.6 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2s

Hydrologic Soil Group: A

Ecological site: F145XY008MA - Dry Outwash

Hydric soil rating: No

#### **Minor Components**

#### **Sudbury**

Percent of map unit: 5 percent

Landform: Deltas, terraces, outwash plains
Landform position (two-dimensional): Footslope
Landform position (three-dimensional): Tread, dip

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

#### Hinckley

Percent of map unit: 5 percent

Landform: Deltas, kames, eskers, outwash plains

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Head slope, nose slope, side slope, crest,

rise

Down-slope shape: Convex Across-slope shape: Convex, linear

Hydric soil rating: No

#### Windsor

Percent of map unit: 3 percent

Landform: Outwash plains, outwash terraces, dunes, deltas

Landform position (two-dimensional): Shoulder Landform position (three-dimensional): Tread, riser

Down-slope shape: Linear, convex Across-slope shape: Linear, convex

Hydric soil rating: No

#### Agawam

Percent of map unit: 2 percent

Landform: Outwash plains, outwash terraces, moraines, stream terraces, eskers,

kames

Landform position (three-dimensional): Rise

Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

#### 254C—Merrimac fine sandy loam, 8 to 15 percent slopes

#### **Map Unit Setting**

National map unit symbol: 2tyqt Elevation: 0 to 1,030 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Farmland of statewide importance

#### Map Unit Composition

Merrimac and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Merrimac**

#### Setting

Landform: Eskers, outwash plains, moraines, kames, outwash terraces Landform position (two-dimensional): Backslope, footslope, summit, shoulder

Landform position (three-dimensional): Side slope, crest, riser, tread

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Loamy glaciofluvial deposits derived from granite, schist, and gneiss over sandy and gravelly glaciofluvial deposits derived from granite,

schist, and gneiss

#### Typical profile

Ap - 0 to 10 inches: fine sandy loam Bw1 - 10 to 22 inches: fine sandy loam

Bw2 - 22 to 26 inches: stratified gravel to gravelly loamy sand 2C - 26 to 65 inches: stratified gravel to very gravelly sand

#### Properties and qualities

Slope: 8 to 15 percent

Depth to restrictive feature: More than 80 inches Drainage class: Somewhat excessively drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very

high (1.42 to 99.90 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum content: 2 percent Maximum salinity: Nonsaline (0.0 to 1.4 mmhos/cm)

Sodium adsorption ratio, maximum: 1.0

Available water supply, 0 to 60 inches: Low (about 4.6 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2s

Hydrologic Soil Group: A

Ecological site: F145XY008MA - Dry Outwash

Hydric soil rating: No

#### **Minor Components**

#### Hinckley

Percent of map unit: 5 percent

Landform: Deltas, kames, eskers, outwash plains

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Head slope, nose slope, side slope, crest,

rise

Down-slope shape: Convex

Across-slope shape: Convex, linear

Hydric soil rating: No

#### Sudbury

Percent of map unit: 5 percent

Landform: Deltas, terraces, outwash plains
Landform position (two-dimensional): Footslope
Landform position (three-dimensional): Tread, dip

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

#### Windsor

Percent of map unit: 5 percent

Landform: Outwash plains, dunes, deltas, outwash terraces

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Tread, riser

Down-slope shape: Linear, convex Across-slope shape: Linear, convex

Hydric soil rating: No

#### 255C—Windsor loamy sand, 8 to 15 percent slopes

#### **Map Unit Setting**

National map unit symbol: 2svkq

Elevation: 0 to 1,260 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Farmland of statewide importance

#### **Map Unit Composition**

Windsor and similar soils: 85 percent Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Windsor**

#### Setting

Landform: — error in exists on —

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Side slope, riser

Down-slope shape: Convex

Across-slope shape: Convex, linear

Parent material: Loose sandy glaciofluvial deposits derived from granite and/or loose sandy glaciofluvial deposits derived from schist and/or loose sandy

glaciofluvial deposits derived from gneiss

#### **Typical profile**

Oe - 0 to 1 inches: moderately decomposed plant material

Ap - 1 to 11 inches: loamy sand Bw - 11 to 31 inches: loamy sand

C - 31 to 65 inches: sand

#### Properties and qualities

Slope: 8 to 15 percent

Depth to restrictive feature: More than 80 inches

Drainage class: Excessively drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very

high (1.42 to 99.90 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 4.2 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: A

Ecological site: F144AY022MA - Dry Outwash

Hydric soil rating: No

#### **Minor Components**

#### Hinckley

Percent of map unit: 10 percent

Landform: Deltas, kames, eskers, outwash plains

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Head slope, nose slope, crest, side slope,

rise

Down-slope shape: Convex

Across-slope shape: Convex, linear

Hydric soil rating: No

#### Deerfield

Percent of map unit: 5 percent

Landform: Deltas, terraces, outwash plains
Landform position (two-dimensional): Footslope
Landform position (three-dimensional): Tread, talf

Down-slope shape: Linear

Across-slope shape: Linear Hydric soil rating: No

#### 260B—Sudbury fine sandy loam, 2 to 8 percent slopes

#### **Map Unit Setting**

National map unit symbol: vky4 Elevation: 0 to 2,100 feet

Mean annual precipitation: 45 to 54 inches Mean annual air temperature: 43 to 54 degrees F

Frost-free period: 145 to 240 days

Farmland classification: All areas are prime farmland

#### **Map Unit Composition**

Sudbury and similar soils: 85 percent *Minor components*: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Sudbury**

#### Setting

Landform: Outwash plains

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Riser

Down-slope shape: Linear Across-slope shape: Concave

Parent material: Friable coarse-loamy eolian deposits over loose sandy

glaciofluvial deposits

#### **Typical profile**

H1 - 0 to 11 inches: sandy loam H2 - 11 to 22 inches: sandy loam

H3 - 22 to 60 inches: gravelly coarse sand

#### Properties and qualities

Slope: 2 to 8 percent

Depth to restrictive feature: 18 to 36 inches to strongly contrasting textural

stratification

Drainage class: Moderately well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): High (2.00 to 6.00

in/hr)

Depth to water table: About 18 to 36 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Low (about 4.0 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: B

Ecological site: F144AY027MA - Moist Sandy Outwash

Hydric soil rating: No

#### **Minor Components**

#### Walpole

Percent of map unit: 5 percent

Landform: Terraces
Hydric soil rating: Yes

#### Merrimac

Percent of map unit: 5 percent

Hydric soil rating: No

#### Deerfield

Percent of map unit: 5 percent Landform: Outwash plains

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Tread

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: No

#### 307B—Paxton fine sandy loam, 0 to 8 percent slopes, extremely stony

#### Map Unit Setting

National map unit symbol: 2w675

Elevation: 0 to 1,580 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Paxton, extremely stony, and similar soils: 80 percent

Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Paxton, Extremely Stony**

#### Setting

Landform: Ground moraines, hills, drumlins

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Convex, linear Across-slope shape: Linear, convex

Parent material: Coarse-loamy lodgment till derived from gneiss, granite, and/or

schist

#### **Typical profile**

Oe - 0 to 2 inches: moderately decomposed plant material

A - 2 to 10 inches: fine sandy loam

Bw1 - 10 to 17 inches: fine sandy loam

Bw2 - 17 to 28 inches: fine sandy loam

Cd - 28 to 67 inches: gravelly fine sandy loam

#### **Properties and qualities**

Slope: 0 to 8 percent

Surface area covered with cobbles, stones or boulders: 9.0 percent Depth to restrictive feature: 20 to 43 inches to densic material

Drainage class: Well drained Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.14 in/hr)

Depth to water table: About 18 to 37 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 4.7 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: C

Ecological site: F144AY007CT - Well Drained Dense Till Uplands

Hydric soil rating: No

#### **Minor Components**

#### Woodbridge, extremely stony

Percent of map unit: 10 percent

Landform: Hills, drumlins, ground moraines

Landform position (two-dimensional): Summit, backslope, footslope

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

#### Charlton, extremely stony

Percent of map unit: 5 percent

Landform: Hills

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

#### Ridgebury, extremely stony

Percent of map unit: 4 percent

Landform: Drumlins, drainageways, depressions, ground moraines, hills

Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Head slope, base slope

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

#### Whitman, extremely stony

Percent of map unit: 1 percent

Landform: Depressions
Down-slope shape: Concave
Across-slope shape: Concave
Hydric soil rating: Yes

# 312B—Woodbridge fine sandy loam, 0 to 8 percent slopes, extremely stony

#### **Map Unit Setting**

National map unit symbol: 2t2qs

Elevation: 0 to 1,580 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Woodbridge, extremely stony, and similar soils: 82 percent

Minor components: 18 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Woodbridge, Extremely Stony**

#### Setting

Landform: Ground moraines, hills, drumlins

Landform position (two-dimensional): Summit, backslope, footslope

Landform position (three-dimensional): Side slope

Down-slope shape: Concave Across-slope shape: Linear

Parent material: Coarse-loamy lodgment till derived from gneiss, granite, and/or

schist

#### Typical profile

Oe - 0 to 2 inches: moderately decomposed plant material

A - 2 to 9 inches: fine sandy loam

Bw1 - 9 to 20 inches: fine sandy loam

Bw2 - 20 to 32 inches: fine sandy loam

Cd - 32 to 67 inches: gravelly fine sandy loam

#### Properties and qualities

Slope: 0 to 8 percent

Surface area covered with cobbles, stones or boulders: 9.0 percent Depth to restrictive feature: 20 to 43 inches to densic material

Drainage class: Moderately well drained

Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately

low (0.00 to 0.14 in/hr)

Depth to water table: About 19 to 27 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 4.0 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: C/D

Ecological site: F144AY037MA - Moist Dense Till Uplands

Hydric soil rating: No

#### **Minor Components**

#### Paxton, extremely stony

Percent of map unit: 10 percent

Landform: Ground moraines, hills, drumlins

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Convex, linear Across-slope shape: Linear, convex

Hydric soil rating: No

#### Ridgebury, extremely stony

Percent of map unit: 8 percent

Landform: Hills, drainageways, drumlins, depressions, ground moraines

Landform position (two-dimensional): Toeslope

Landform position (three-dimensional): Head slope, base slope

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

#### 420B—Canton fine sandy loam, 3 to 8 percent slopes

#### Map Unit Setting

National map unit symbol: 2w81b

Elevation: 0 to 1,180 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 240 days

Farmland classification: All areas are prime farmland

#### **Map Unit Composition**

Canton and similar soils: 80 percent Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Canton**

#### Setting

Landform: Moraines, ridges, hills

Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Nose slope, side slope, crest

Down-slope shape: Convex, linear Across-slope shape: Convex

Parent material: Coarse-loamy over sandy melt-out till derived from gneiss,

granite, and/or schist

#### **Typical profile**

Ap - 0 to 7 inches: fine sandy loam Bw1 - 7 to 15 inches: fine sandy loam

Bw2 - 15 to 26 inches: gravelly fine sandy loam 2C - 26 to 65 inches: gravelly loamy sand

#### Properties and qualities

Slope: 3 to 8 percent

Depth to restrictive feature: 19 to 39 inches to strongly contrasting textural

stratification

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water supply, 0 to 60 inches: Very low (about 2.7 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2s

Hydrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

#### **Minor Components**

#### **Scituate**

Percent of map unit: 10 percent

Landform: Hills, drumlins, ground moraines

Landform position (two-dimensional): Summit, backslope, footslope

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Convex, linear Across-slope shape: Convex Hydric soil rating: No

#### Montauk

Percent of map unit: 5 percent

Landform: Moraines, ground moraines, hills, drumlins

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Convex, linear Across-slope shape: Convex Hydric soil rating: No

#### Charlton

Percent of map unit: 4 percent

Landform: Ridges, ground moraines, hills

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Convex, linear

Across-slope shape: Convex Hydric soil rating: No

#### Swansea

Percent of map unit: 1 percent

Landform: Marshes, depressions, bogs, swamps, kettles

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

#### 422B—Canton fine sandy loam, 0 to 8 percent slopes, extremely stony

#### **Map Unit Setting**

National map unit symbol: 2w818

Elevation: 0 to 1,180 feet

Mean annual precipitation: 36 to 71 inches
Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 145 to 240 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Canton, extremely stony, and similar soils: 80 percent

Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Canton, Extremely Stony**

#### Setting

Landform: Moraines, hills, ridges

Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Nose slope, side slope, crest

Down-slope shape: Convex, linear Across-slope shape: Convex

Parent material: Coarse-loamy over sandy melt-out till derived from gneiss, granite, and/or schist

#### Typical profile

Oi - 0 to 2 inches: slightly decomposed plant material

A - 2 to 5 inches: fine sandy loam Bw1 - 5 to 16 inches: fine sandy loam

Bw2 - 16 to 22 inches: gravelly fine sandy loam 2C - 22 to 67 inches: gravelly loamy sand

#### Properties and qualities

Slope: 0 to 8 percent

Surface area covered with cobbles, stones or boulders: 9.0 percent Depth to restrictive feature: 19 to 39 inches to strongly contrasting textural

stratification

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high

(0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 3.4 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

#### **Minor Components**

#### Scituate, extremely stony

Percent of map unit: 6 percent

Landform: Hills, ground moraines, drumlins

Landform position (two-dimensional): Summit, backslope, footslope

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Convex, linear Across-slope shape: Convex

Hydric soil rating: No

#### Charlton, extremely stony

Percent of map unit: 6 percent

Landform: Ridges, ground moraines, hills

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Convex, linear Across-slope shape: Convex

Hydric soil rating: No

#### Montauk, extremely stony

Percent of map unit: 4 percent

Landform: Recessionial moraines, ground moraines, hills, drumlins Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Side slope, crest

Down-slope shape: Convex, linear Across-slope shape: Convex

Hydric soil rating: No

#### Swansea

Percent of map unit: 4 percent

Landform: Marshes, depressions, bogs, swamps, kettles

Down-slope shape: Concave Across-slope shape: Concave

Hydric soil rating: Yes

#### 600—Pits, sand and gravel

#### **Map Unit Setting**

National map unit symbol: vkxc

Mean annual precipitation: 32 to 50 inches Mean annual air temperature: 45 to 50 degrees F

Frost-free period: 120 to 200 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Pits: 100 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Pits**

#### Setting

Parent material: Loose, excavated sandy and gravelly glaciofluvial deposits

#### 602—Urban land, 0 to 15 percent slopes

#### **Map Unit Setting**

National map unit symbol: vkyj

Mean annual precipitation: 32 to 50 inches
Mean annual air temperature: 45 to 50 degrees F

Frost-free period: 120 to 200 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Urban land: 99 percent Minor components: 1 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Urban Land**

#### Setting

Parent material: Excavated and filled land

#### **Minor Components**

#### **Rock outcrops**

Percent of map unit: 1 percent Hydric soil rating: Unranked

#### 626B—Merrimac-Urban land complex, 0 to 8 percent slopes

#### **Map Unit Setting**

National map unit symbol: 2tyr9

Elevation: 0 to 820 feet

Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 140 to 250 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Merrimac and similar soils: 45 percent

Urban land: 40 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Merrimac**

#### Setting

Landform: Outwash plains, outwash terraces, moraines, eskers, kames Landform position (two-dimensional): Summit, shoulder, backslope, footslope

Landform position (three-dimensional): Side slope, crest, riser, tread

Down-slope shape: Convex Across-slope shape: Convex

Parent material: Loamy glaciofluvial deposits derived from granite, schist, and gneiss over sandy and gravelly glaciofluvial deposits derived from granite,

schist, and gneiss

#### **Typical profile**

Ap - 0 to 10 inches: fine sandy loam Bw1 - 10 to 22 inches: fine sandy loam

Bw2 - 22 to 26 inches: stratified gravel to gravelly loamy sand 2C - 26 to 65 inches: stratified gravel to very gravelly sand

#### **Properties and qualities**

Slope: 0 to 8 percent

Depth to restrictive feature: More than 80 inches Drainage class: Somewhat excessively drained

Runoff class: Very low

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very

high (1.42 to 99.90 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Calcium carbonate, maximum content: 2 percent Maximum salinity: Nonsaline (0.0 to 1.4 mmhos/cm)

Sodium adsorption ratio, maximum: 1.0

Available water supply, 0 to 60 inches: Low (about 4.6 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 2e

Hydrologic Soil Group: A

Ecological site: F144AY022MA - Dry Outwash

Hydric soil rating: No

#### **Description of Urban Land**

#### Typical profile

M - 0 to 10 inches: cemented material

#### **Properties and qualities**

Slope: 0 to 8 percent

Depth to restrictive feature: 0 inches to manufactured layer

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Very low (0.00 to 0.00

in/hr

Available water supply, 0 to 60 inches: Very low (about 0.0 inches)

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8

Hydrologic Soil Group: D Hydric soil rating: Unranked

#### **Minor Components**

#### Windsor

Percent of map unit: 5 percent

Landform: Outwash terraces, dunes, outwash plains, deltas

Landform position (three-dimensional): Tread, riser

Down-slope shape: Linear, convex Across-slope shape: Linear, convex

Hydric soil rating: No

#### Sudbury

Percent of map unit: 5 percent

Landform: Deltas, terraces, outwash plains
Landform position (two-dimensional): Footslope
Landform position (three-dimensional): Tread, dip

Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: No

#### Hinckley

Percent of map unit: 5 percent

Landform: Deltas, kames, eskers, outwash plains

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Head slope, nose slope, side slope, crest,

rise

Down-slope shape: Convex

Across-slope shape: Convex, linear

Hydric soil rating: No

#### 653—Udorthents, sandy

#### Map Unit Setting

National map unit symbol: vky8 Elevation: 0 to 3.000 feet

Mean annual precipitation: 45 to 54 inches
Mean annual air temperature: 43 to 54 degrees F

Frost-free period: 145 to 240 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Udorthents and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Udorthents**

#### Setting

Landform position (two-dimensional): Shoulder, summit Landform position (three-dimensional): Riser, tread

Down-slope shape: Convex, linear Across-slope shape: Convex, linear

Parent material: Excavated and filled sandy glaciofluvial deposits

#### **Typical profile**

H1 - 0 to 6 inches: variable H2 - 6 to 60 inches: variable

#### Properties and qualities

Slope: 0 to 25 percent

Depth to restrictive feature: More than 80 inches

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to very

high (0.06 to 20.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: A Hydric soil rating: Unranked

#### **Minor Components**

#### **Udorthents**

Percent of map unit: 8 percent Hydric soil rating: Unranked

#### **Urban land**

Percent of map unit: 5 percent Hydric soil rating: Unranked

#### **Swansea**

Percent of map unit: 2 percent

Landform: Bogs Hydric soil rating: Yes

#### 654—Udorthents, loamy

#### **Map Unit Setting**

National map unit symbol: vkyb Elevation: 0 to 3.000 feet

Mean annual precipitation: 45 to 54 inches
Mean annual air temperature: 43 to 54 degrees F

Frost-free period: 145 to 240 days

Farmland classification: Not prime farmland

#### **Map Unit Composition**

Udorthents and similar soils: 80 percent

Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

#### **Description of Udorthents**

#### Setting

Landform position (two-dimensional): Shoulder, summit Landform position (three-dimensional): Riser, tread

Down-slope shape: Convex, linear Across-slope shape: Convex, linear

Parent material: Excavated and filled coarse-loamy human transported material

#### Typical profile

H1 - 0 to 6 inches: variable H2 - 6 to 60 inches: variable

#### Properties and qualities

Slope: 0 to 25 percent

Depth to restrictive feature: More than 80 inches

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to very

high (0.06 to 20.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

#### Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: A

Hydric soil rating: Unranked

#### **Minor Components**

#### **Udorthents, sandy**

Percent of map unit: 8 percent Hydric soil rating: Unranked

#### Udorthents,wet substr.

Percent of map unit: 8 percent Hydric soil rating: Unranked

#### **Urban land**

Percent of map unit: 4 percent Hydric soil rating: Unranked

# Soil Information for All Uses

## **Soil Properties and Qualities**

The Soil Properties and Qualities section includes various soil properties and qualities displayed as thematic maps with a summary table for the soil map units in the selected area of interest. A single value or rating for each map unit is generated by aggregating the interpretive ratings of individual map unit components. This aggregation process is defined for each property or quality.

#### Soil Qualities and Features

Soil qualities are behavior and performance attributes that are not directly measured, but are inferred from observations of dynamic conditions and from soil properties. Example soil qualities include natural drainage, and frost action. Soil features are attributes that are not directly part of the soil. Example soil features include slope and depth to restrictive layer. These features can greatly impact the use and management of the soil.

## **Hydrologic Soil Group**

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

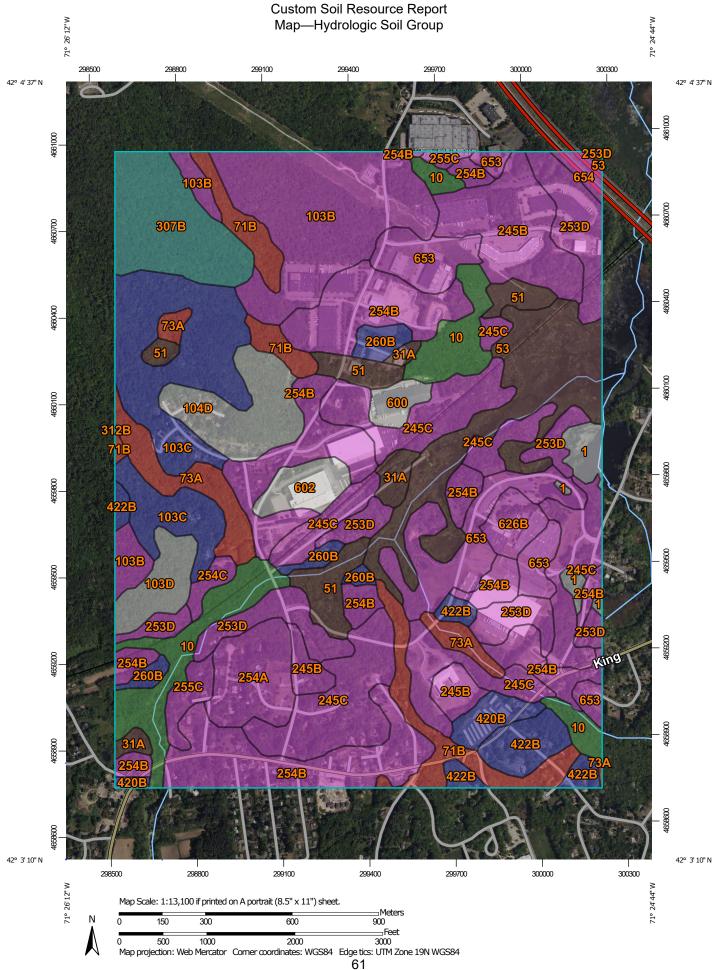
Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.



#### MAP LEGEND MAP INFORMATION Area of Interest (AOI) The soil surveys that comprise your AOI were mapped at С 1:25.000. Area of Interest (AOI) C/D Soils Please rely on the bar scale on each map sheet for map D Soil Rating Polygons measurements. Not rated or not available Α Source of Map: Natural Resources Conservation Service **Water Features** A/D Web Soil Survey URL: Streams and Canals В Coordinate System: Web Mercator (EPSG:3857) Transportation B/D Rails ---Maps from the Web Soil Survey are based on the Web Mercator С projection, which preserves direction and shape but distorts Interstate Highways distance and area. A projection that preserves area, such as the C/D **US Routes** Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. D Major Roads ~ Not rated or not available Local Roads -This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. Soil Rating Lines Background Aerial Photography Soil Survey Area: Norfolk and Suffolk Counties, Massachusetts Survey Area Data: Version 18, Sep 9, 2022 Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. Date(s) aerial images were photographed: May 22, 2022—Jun C/D 5, 2022 The orthophoto or other base map on which the soil lines were Not rated or not available compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor **Soil Rating Points** shifting of map unit boundaries may be evident. Α A/D B/D

## Table—Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
1	Water		8.7	0.9%
10	Scarboro and Birdsall soils, 0 to 3 percent slopes	A/D	48.0	5.2%
31A	Walpole sandy loam, 0 to 3 percent slopes	B/D	8.6	0.9%
51	Swansea muck, 0 to 1 percent slopes	B/D	24.2	2.6%
53	Freetown muck, ponded, 0 to 1 percent slopes	B/D	57.0	6.2%
71B	Ridgebury fine sandy loam, 3 to 8 percent slopes, extremely stony	D	35.0	3.8%
73A	Whitman fine sandy loam, 0 to 3 percent slopes, extremely stony	D	24.5	2.6%
103B	Charlton-Hollis-Rock outcrop complex, 3 to 8 percent slopes	А	76.6	8.3%
103C	Charlton-Hollis-Rock outcrop complex, 8 to 15 percent slopes	В	67.9	7.3%
103D	Charlton-Hollis-Rock outcrop complex, 15 to 25 percent slopes		13.8	1.5%
104D	Hollis-Rock outcrop- Charlton complex, 15 to 35 percent slopes		27.0	2.9%
245B	Hinckley loamy sand, 3 to 8 percent slopes	A	45.4	4.9%
245C	Hinckley loamy sand, 8 to 15 percent slopes	А	107.2	11.6%
253D	Hinckley loamy sand, 15 to 35 percent slopes	А	55.7	6.0%
254A	Merrimac fine sandy loam, 0 to 3 percent slopes	А	22.8	2.5%
254B	Merrimac fine sandy loam, 3 to 8 percent slopes	A	128.4	13.9%
254C	Merrimac fine sandy loam, 8 to 15 percent slopes	A	3.9	0.4%
255C	Windsor loamy sand, 8 to 15 percent slopes	A	8.4	0.9%

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
260B	Sudbury fine sandy loam, 2 to 8 percent slopes	В	11.3	1.2%
307B	Paxton fine sandy loam, 0 to 8 percent slopes, extremely stony	С	37.6	4.1%
312B	Woodbridge fine sandy loam, 0 to 8 percent slopes, extremely stony	C/D	0.0	0.0%
420B	Canton fine sandy loam, 3 to 8 percent slopes	В	9.3	1.0%
422B	Canton fine sandy loam, 0 to 8 percent slopes, extremely stony	В	21.5	2.3%
600	Pits, sand and gravel		6.2	0.7%
602	Urban land, 0 to 15 percent slopes		11.3	1.2%
626B	Merrimac-Urban land complex, 0 to 8 percent slopes	A	8.8	1.0%
653	Udorthents, sandy	Α	53.8	5.8%
654	Udorthents, loamy	Α	3.6	0.4%
Totals for Area of Interest			926.9	100.0%

64

## Rating Options—Hydrologic Soil Group

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified

Tie-break Rule: Higher

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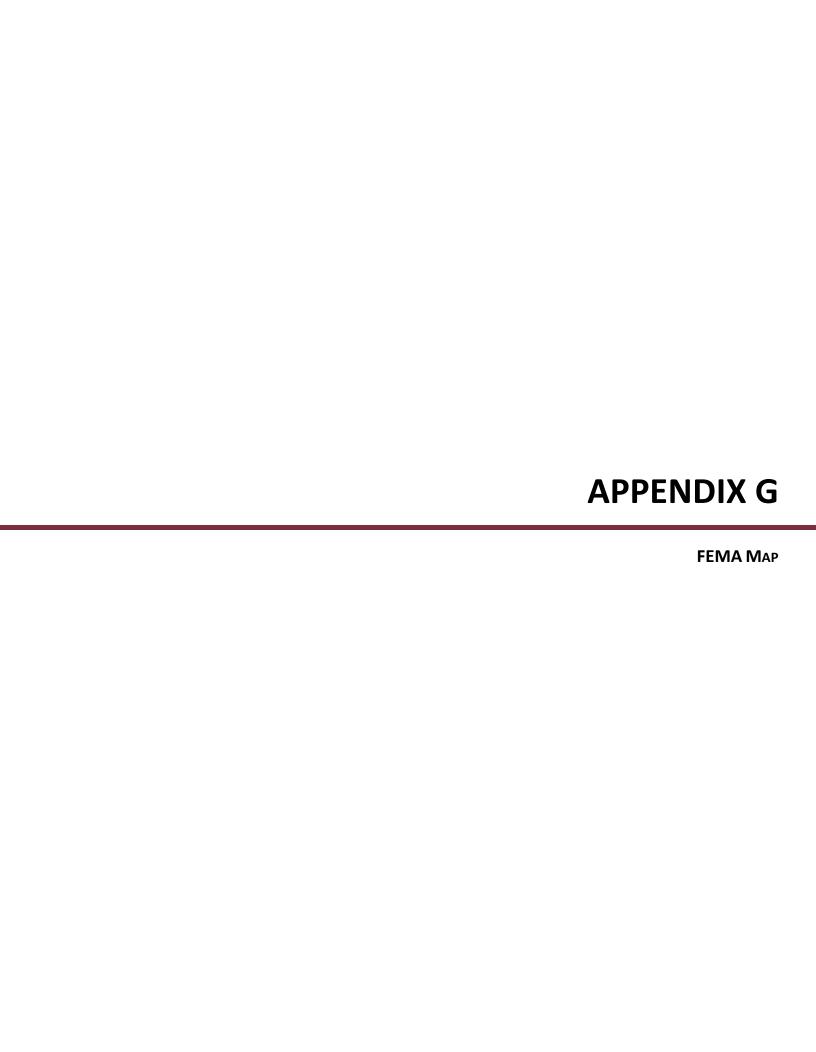
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# National Flood Hazard Layer FIRMette

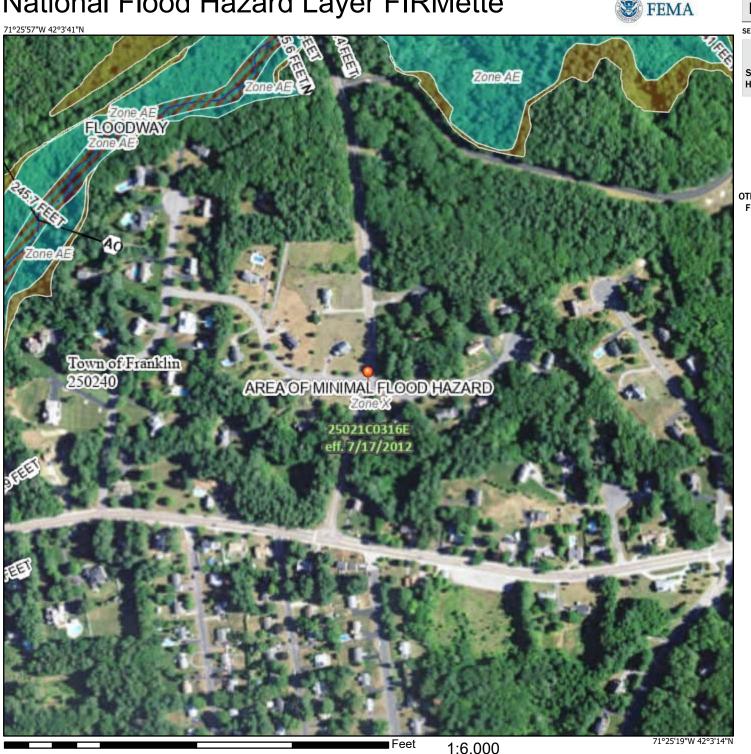
250

500

1,000

1,500



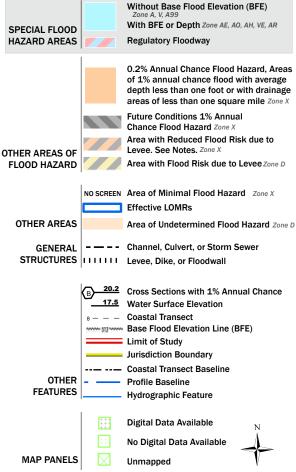


2.000

Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020

#### Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT



This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap

an authoritative property location.

The pin displayed on the map is an approximate point selected by the user and does not represent

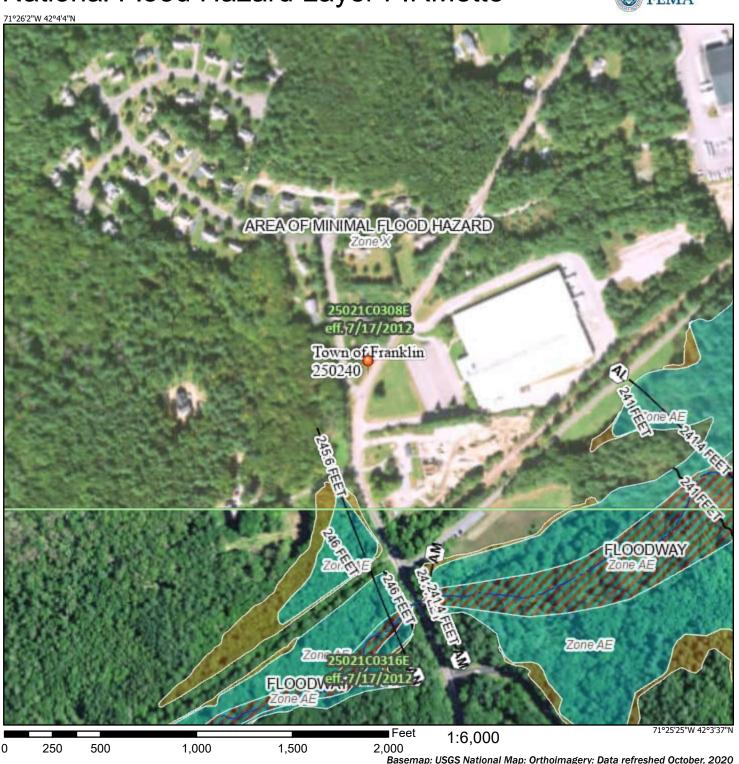
accuracy standards The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 12/29/2022 at 10:35 AM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or

become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

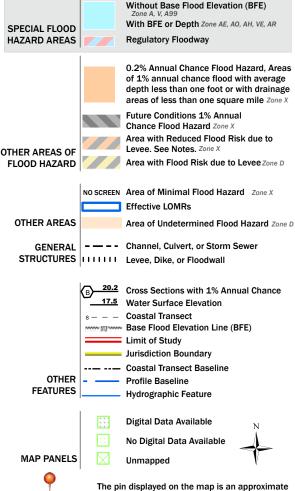
# National Flood Hazard Layer FIRMette





#### Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT



This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap

accuracy standards

point selected by the user and does not represent

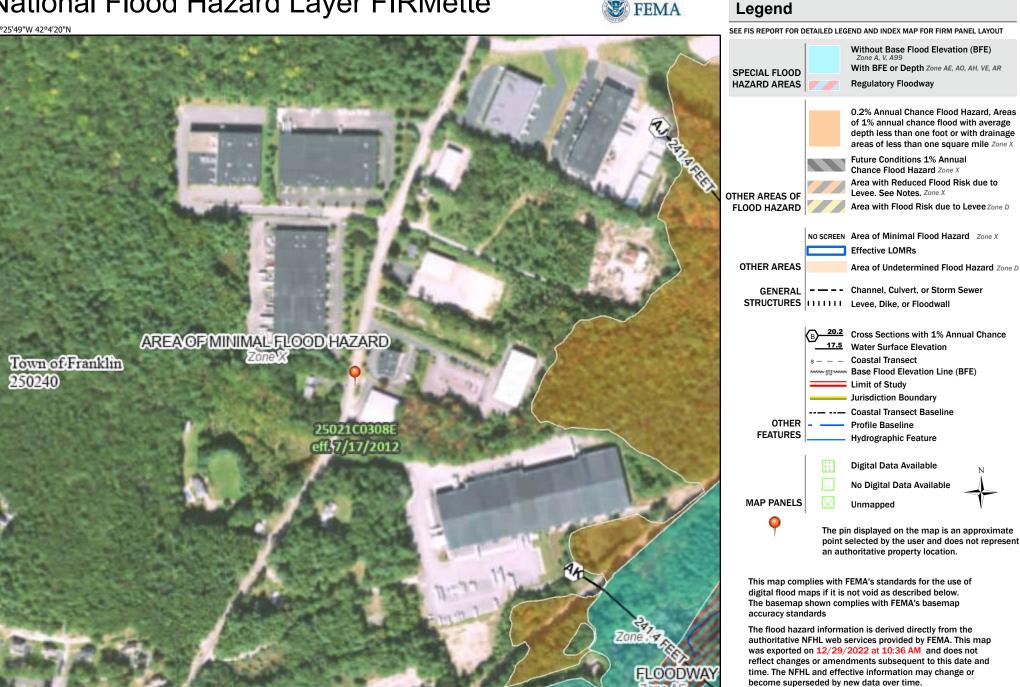
an authoritative property location.

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 12/29/2022 at 10:38 AM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

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# National Flood Hazard Layer FIRMette





Feet

2.000

250

500

1,000

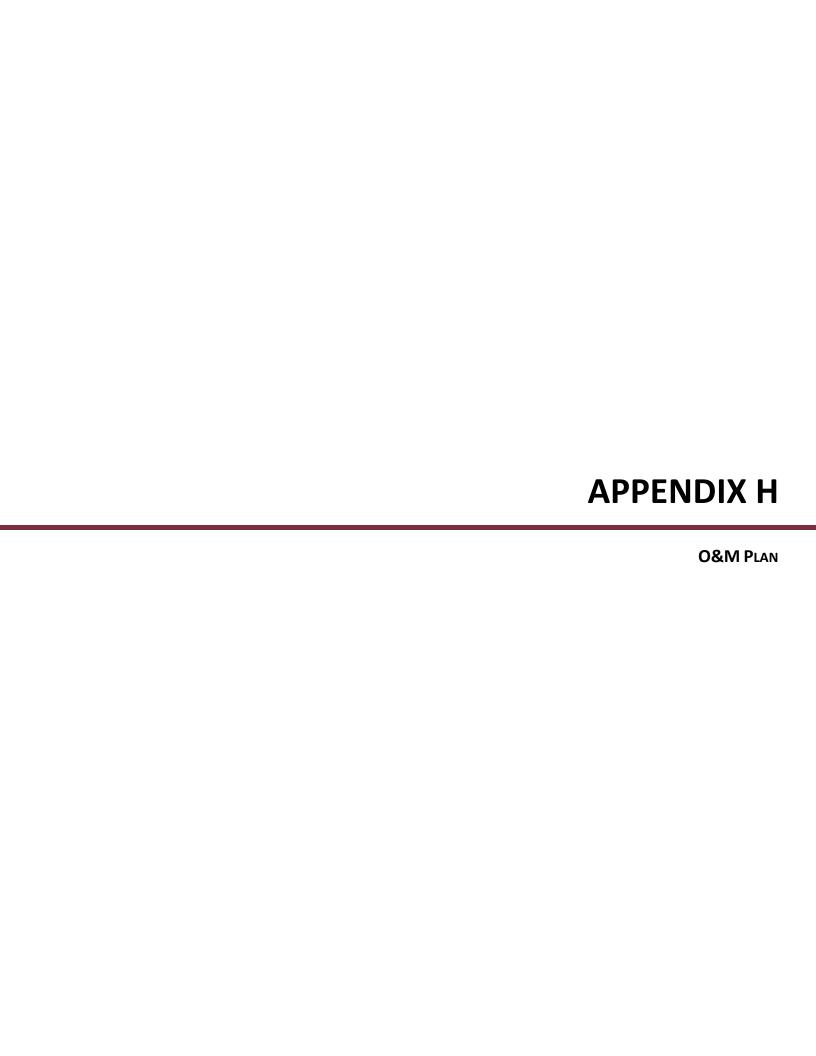
1,500

1:6.000

legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

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Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020



## TOWN OF FRANKLIN LONG TERM POLLUTION PREVENTION PLAN

#### GROVE STREET IMPROVEMTNS PHASE 2

FRANKLIN, MA February 2023

The following provides protocols for the management and prevention of pollution related to the construction and long-term maintenance of improvements along Grove Street.

#### **Good Housekeeping Best Management Practices (BMPS):**

<u>Waste Materials</u>: Debris and trash will be collected in a metal dumpster. The dumpster will meet all Municipal requirements. Surplus soil material will be removed from the site and legally disposed of. Handling, sampling, manifesting, transportation, and disposal of waste material will be documented.

<u>Hazardous Waste:</u> Hazardous waste will be disposed of as required under local, state, and federal regulations. Site personnel will be instructed regarding proper management of hazardous waste. The individual in charge of this activity will be properly trained in hazardous waste management in accordance with OSHA regulations and MassDEP regulation 310 CMR 30 and 310 CMR 40.

<u>Sanitary Waste:</u> Temporary sanitary waste facilities will be provided onsite. Waste will be collected as required, and in any event as required by local regulation, by a sanitary waste management contractor.

<u>Hazardous Products:</u> The following practices will be used to reduce the risks associated with hazardous materials onsite:

- a. All shipments will be promptly inspected to assure that products comply with requirements and items are undamaged.
- b. Products will be stored and protected in accordance with the manufacturer's instructions with seals and labels intact and legible.
- c. Products will be stored in a secure location and access to the materials will be provided to authorize personnel only.

#### **Establish Proper Building Material Staging Areas:**

- a. Material deliveries will be coordinated with installation to ensure minimum holding time for items that are hazardous, flammable, easily damaged or sensitive to deterioration.
- b. Delivers will be scheduled to reduce long-term onsite storage prior to installation unless written authorization is provided by the engineer.
- c. Materials stored onsite will be stored in manufacturer's original sealed containers or other packing systems complete with instruction for handling, storing, unpacking, protecting and installing.
- d. Adequate equipment and personnel will be provided to ensure materials can be safely handled.
- e. Cement and lime will be stored under a roof and off the ground to be kept completely dry at all times.
- f. Petroleum products will be stored in a secure location under control of the site superintendent.
- g. Mechanical and electrical equipment will be stored in a weatherproof structure.

#### **Designated Washout Areas:**

- a. Concrete contractors should be encouraged where possible to use the washout facilities at their own plants.
- b. Concrete washouts areas shall be established onsite with signs noting the locations. The washout area is to be inspected daily during concrete operations.
- c. Provide adequate containment for the amount of wash water that will be used.
- d. Dispose of materials properly. Concrete wash water can be highly polluted. It is not to be discharged to any surface water or storm drain system.

#### **Establish Proper Vehicle / Equipment Maintenance Practices:**

- a. Train employees and subcontractor in proper fueling procedures (stay with vehicles during fueling, proper use of pumps, emergency shutoff valves, and such).
- b. Inspect onsite vehicles and equipment daily for leaks, equipment damage and other service problems.
- c. Clearly designate vehicle / equipment service areas away from drainage facilities and water course to prevent stormwater run-on and runoff.
- d. Use drip pans, drip cloths, or absorbent pads when replacing spent fluids.
- e. Collect all spent fluids, store in appropriate labeled containers in the proper storage areas and recycle fluids whenever possible.

#### Allowance for Non-Stormwater Discharges and Control Equipment/Vehicle Washing:

There will not be non-permitted non-stormwater discharges associated with this project. Specifically prohibited are the discharges of process water, non-contact cooling water, vehicle wash water and sanitary wastewater via stormwater drainage systems. Allowable non-stormwater discharges include discharges from fire-fighting activities, fire hydrant flushing, water used to control dust and uncontaminated air condition condensation.

#### **Spill Prevention and Control Plan:**

In addition to the good housekeeping and material management practices discussed in the previous sections of this plan, the following practices will be followed for spill prevention and clean up:

- a. Manufacturer's recommended methods for spill cleanup will be clearly posted and site personnel will be made aware of the procedures and the location of the information and cleanup supplies.
- b. The contractor shall provide a 55-gallon spill containment kit and maintain it onsite throughout the construction period.
- c. All spills will be cleaned up immediately after discovery.
- d. The spill area will be kept well ventilated, and personnel will wear appropriate protective clothing to prevent injury from contact with a hazardous substance.
- e. Spills of toxic or hazardous materials, at or greater than reportable quantities, will be reported to the appropriate state or local government agency.
- f. The spill prevention plan will be adjusted to include measures to prevent this type of spill from reoccurring and how to clean up the spill if there is another one. A description of the spill, what caused it, and the cleanup measures will also be included.
- g. The Site Superintendent is the designated responsible party for day-to-day operations and spill cleanup procedures.

#### **Allowable Non-Stormwater Discharge Management**:

The allowable non-stormwater discharges may include the following:

- a. Discharges from fire-fighting activities.
- b. Fire hydrant flushings.
- c. Waters used to wash vehicles where detergents are not used.
- d. Water used to control dust in accordance with EPA's CGP Part 3, Subpart 3.4 G.
- e. Potable water including uncontaminated water line flushings.
- f. Pavement wash where spills or leaks of toxic or hazardous materials have not occurred (unless all spilled material has been removed) and where detergents are not used.
- g. Uncontaminated air conditioning or compressor condensate.
- h. Uncontaminated ground water or spring water.
- i. Foundation or footing drains where flows are not contaminated with process materials such as solvents.
- j. Uncontaminated excavation dewatering.
- k. Landscape irrigation.

Non-stormwater discharges should be eliminated or reduced to the extent feasible.

#### a. Water used to control dust:

Dust control will be implemented as needed once site grading has begun and during windy conditions (forecasted or actual wind conditions of 20 mph or greater) while site grading is occurring. Spraying of potable water at a rate of 300 gallons per acre or less will be performed by a mobile pressure-type distributor truck no more than three times a day during the months of May through September or whenever the dryness of the soil warrants it.

#### b. Uncontaminated Excavation Dewatering:

Dewatering activities are not anticipated for this project due to the depth of the groundwater. If dewatering does occur, the LTPPP will be revised to address the need for appropriate BMPs.

#### c. Landscape Irrigation:

Irrigation waters will not be sprayed onto impermeable surfaces such as paved driveways and roads. Waters will be directed onto soil and lawns by using hoses and correctly sized sprinklers with adjustable spray patterns. To avoid discharges or irrigation waters, the sprinkler will have low-flow rates and increased watering time. The irrigated area will be inspected for excess watering and to adjust watering times and schedules.

#### **Inspection Personnel**:

Inspections must be conducted by qualified personnel. "Qualified Personnel" means a person knowledgeable in the principals and practice of erosion and sediment controls who possesses the skills to assess conditions at the construction site that could impact stormwater quality and to assess the effectiveness of any sediment and erosion control measure selected to control the quality of stormwater discharges for the construction activity. Prior to construction the contractor shall submit the names of the personnel who will be responsible for the inspections.

#### **Inspection Schedule and Procedures:**

Inspections of the site will be performed once every 7 days and within 24 hours of the end of a storm event of <u>one-half inch</u> or greater. The inspections will verify that all BMPs are implemented,

Long Term Pollution Prevention Plan

Grove Steet Phase 2

maintained, and effectively minimizing erosion and preventing stormwater contamination from construction materials.

February 2023

Page 4

Inspections must include all areas of the site disturbed by construction activity and areas used for storage of materials that are exposed to precipitation. Inspectors must look for evidence of, or the potential for, pollutants entering the stormwater conveyance system. Sedimentation and erosion control measures identified in the LTPPP must be observed to ensure proper operation. Discharge locations must be inspected to ascertain whether erosion control measures are effective. Where discharge locations are inaccessible, nearby downstream locations must be inspected to the extent that such inspections are practicable. Locations where vehicles enter or exit the site must be inspected for evidence of offsite sediment tracking.

If corrective actions are identified during the inspections, the construction managers will be notified, and a copy of the inspection report will be submitted to them. Corrective action is to be initiated within 24 hours of the report and the maintenance completed as soon as possible or before the next storm event. In addition, the LTPPP shall be modified as necessary to include the additional or modified BMPs designed to correct the problems identified. Revisions to the LTPPP must be completed within seven (7) calendar days following the inspection.

# TOWN OF FRANKLIN OPERATION & MAINTENANCE PLAN GROVE STREET IMPROVEMENTS PHASE 2 FRANKLIN, MA

#### February 2023

The following provides protocols for the prevention and management of erosion and sedimentation during construction of the proposed improvements, as well as, for long term maintenance of those improvements.

#### **SILTATION CONTROLS**

The first phase of construction will consist of the placement of siltation controls in accordance with the detail and at the location indicated on the plans. No further construction activity will take place until the siltation controls are inspected and approved. No encroachment or alteration shall occur beyond the erosion control barriers. Erosion control barriers shall be maintained and replaced, if necessary, throughout the course of construction.

#### SITE CONSTRUCTION

All unvegetated areas, including stockpiles, that will remain unvegetated for greater than 21 days should be mulched or seeded within 7 days of their grading. The perimeter sedimentation controls at the stockpiles should be in place at the end of each day and before rain events.

During the construction of the drainage system, care must be taken to prevent siltation from entering the system or flowing into the river. Drainage pipes in open excavations shall not remain open overnight. Hay bales shall be staked around the catch basins and/or a woven geotextile material shall be placed in the catch basins until the binder course has been placed. The silt and sand, which may accumulate around the drain inlets, shall be removed after every rainstorm.

Work shall commence as soon as practical on the perimeter disturbed areas not to be paved. Four inches (4") of topsoil is to be placed in these areas and the areas hydroseeded. All areas shall be stabilized within sixty (60) days of disturbance. When weather conditions do not permit stabilization by seeding, hay mulch, straw mats, jute netting or other approved means shall be used for temporary stabilization.

#### INSPECTION AND MAINTENANCE

Prior to construction, the Contractor shall formulate a schedule for inspection and maintenance of the erosion control measures. This schedule shall establish, at a minimum, the weekly inspections of the sedimentation controls, stockpiles, catch basins, water quality structures, unstabilized areas within the site and a report of any required maintenance. The schedule will also appoint an individual who will be responsible for performing the weekly inspections.

During the weekly inspection, and at any time during the course of construction, the Engineer, the Conservation Commission Agent, the Owner or the individual responsible for the erosion control measures may direct the Contractor to take immediate action to correct a deficiency or to increase the erosion control measures.

#### **ADDITIONAL REQUIREMENTS**

The contractor shall employ measures to control dust during construction. All debris shall be properly contained and disposed of.

Grove Street shall be swept clean of any soils tracked onto the pavement from vehicles exiting the site.

A supply of compost-filled silt sock and/or straw wattles shall be kept on site to provide for additional siltation control, as may be required. Any construction equipment observed leaking or dripping oil shall be removed from the site. No construction equipment shall be refueled within 100 feet of the resource area(s).

The above requirements are intended to be a minimum set of guidelines. The contractor shall be responsible for their implementation. Should additional controls be required, the contractor shall take whatever steps are necessary.

Temporary grass stabilization shall be applied at rate of 4-pounds/1,000 sf. and conform to the specifications outlined in Table 1.

#### <u>Table 1</u> – <u>Seed Mixture</u>

Winter Rye	80%	Min.
Red Fescue (Creeping)	4%	Min.
Perennial Rye Grass	3%	Min.
Red Clover	3%	Min.
Other Crop Grass	0.5%	Min.
Noxious Weed Seed	0.5%	MAX.
Inert Matter	1%	MAX.

#### BMP MAINTENANCE SCHEDULE FOR CONSTRUCTED SITE

This maintenance schedule is intended for the entire project following completion of proposed improvements, including work previously completed at this project site.

- 1. Inspect catch basins, hydrodynamic separator, and water quality infiltration basin quarterly if all tributary areas are stabilized with vegetation or monthly if not. Clean out if more than 1/4 full of sediment (1 foot deep in a 4-foot sump). Inspect and clean as necessary after intense rainfall and as soon as practical after winter sanding.
- 2. Inspect drainage system discharge points (flared end sections) on a quarterly basis and remove any trash/debris. Verify flared end sections are structurally intact and no erosion is occurring after the aprons.
- 3. Keep all pervious site areas always stabilized. Keep any stockpiled earth covered. Leaves and trimmings shall be removed from the site and not discarded within the onsite wetland area.
- 4. Remove any visible trash or debris from within the onsite wetland resource area on an annual basis.
- 5. Sweep parking areas and site access roadways with vacuum sweeper on an annual basis, typically after the winter sanding season.

6. <u>Hydrodynamic Separator Recommended Maintenance Procedure</u> (CDS 2015)

Follow manufacturer recommendations.

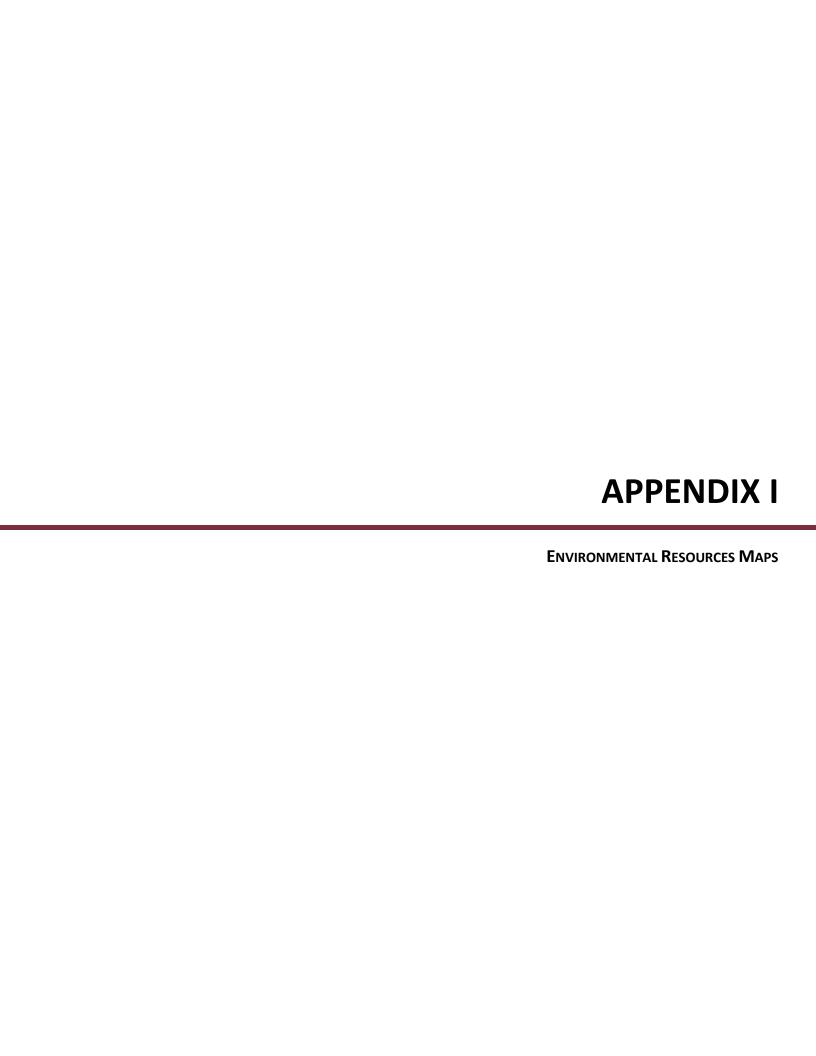
At a minimum, inspections should be performed twice per year (e.g., spring and fall) however more frequent inspections may be necessary in climates where winter sanding operations may lead to rapid accumulations, or in equipment washdown areas. The visual inspection should ascertain that the system components are in working order and that there are no blockages or obstructions in the inlet and separation screen. The inspection should also quantify the accumulation of hydrocarbons, trash, and sediment in the system. Measuring pollutant accumulation can be done with a calibrated dipstick, tape measure or other measuring instrument.

The CDS system should be cleaned when the level of sediment has reached 75% of capacity in the isolated sump or when an appreciable level of hydrocarbons and trash has accumulated.

- 7. Snow from plowing operations shall not be stockpiled adjacent to or within any delineated wetland areas. Stockpiled snow shall be removed from the site and transported to an approved dumping area as needed following storm events.
- 8. The Town of Franklin is the Owner and solely responsible for the operation and maintenance of the onsite stormwater management system.

Their address is:

Town of Franklin 355 E Central Street Franklin, MA 02038 Tel. 508-528-7900



# **Environmental Resources Map**

